

Entsorgungsforschung

1st Chinese-German Workshop on Radioactive Waste Disposal

**Sino-German Science Centre
Beijing, CHINA
May 28 – 31, 2007**

A joint workshop organized by

Beijing Research Institute of Uranium Geology,
(BRIUG), China
China National Nuclear Corporation (CNNC)
Project Management Agency Karlsruhe (PTKA) -
Karlsruhe Institute of Technology, Germany
DBE Technology GmbH, Germany

Ed. W. Steininger

**Projektträger Karlsruhe
Wassertechnologie und Entsorgung (PTKA-WTE)**

Projekträger für das



Bundesministerium
für Wirtschaft
und Energie

Herausgeber:
Projekträger Karlsruhe
Wassertechnologie und Entsorgung (PTKA-WTE)
Karlsruher Institut für Technologie (KIT)
Hermann-von-Helmholtz-Platz 1
76344 Eggenstein-Leopoldshafen
Internet: www.ptka.kit.edu

neu zusammengestellt Juli 2017



PTKA
Projekträger Karlsruhe

Karlsruher Institut für Technologie

Der vorliegende Materialienband dient der aktuellen Unterrichtung der auf dem Gebiet der Entsorgung radioaktiver Abfälle arbeitenden Institutionen und der zuständigen Behörden.

Verantwortlich für den Inhalt sind die Autoren. Das Karlsruher Institut für Technologie (KIT) übernimmt keine Gewähr insbesondere für die Richtigkeit, Genauigkeit und Vollständigkeit der Angaben sowie die Beachtung privater Rechte Dritter. Eine auszugsweise oder vollständige Vervielfältigung ist erlaubt, wenn die Zustimmung der betroffenen Autoren vorliegt.

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Projektstatusgesprächen, Kolloquien und Fachgesprächen
sind über die Internetseite**

www.ptka.kit.edu/wte/171.php

des PTKA zu finden.



中德放射性废物处置研讨会

CHINESE-GERMAN WORKSHOP ON RADIOACTIVE WASTE DISPOSAL

CHINESE-GERMAN SCIENCE CENTRE, BEIJING, CHINA

MAY28-31, 2007

Jointly organized by the

BEIJING RESEARCH INSTITUTE OF URANIUM GEOLOGY,

CHINA NATIONAL NUCLEAR CORPORATION, CHINA

PROJECT MANAGEMENT AGENCY FORSCHUNGSZENTRUM KARLSRUHE &

DBE TECHNOLOGY GmbH, GERMANY

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DBE TECHNOLOGY GmbH, GERMANY

Monday, May 28

09 00 Arrival at the Sino-German Science Center and workshop registration

Opening Ceremony

Chairs: WANG Ju, Walter.Steininger

10 00 Welcome address by Mr. LIN Sen, (China Atomic Energy Authority)
Welcome address by Mr. MA Fei, (BRIUG, China National Nuclear Corporation)
Welcome address by Dr. Walter.Steininger (PTKA-WTE, Germany)
Break: Taking Group Photo

Invited lectures/ National Programs and Activities

Chairs: FAN Zhong, E. Biurrun

10 40 Prof. D. Fuhrmann (PTKA-WTE), Prof. Yun Guichun (INET, Tsinghua University)
Water research – an example of 20 years successful Chinese-German cooperation

11 10 LI Jingying, Director General, Department of Planning, China National Nuclear Corporation
Radioactive Waste Management in the P.R. China

11 40 E. Biurrun, DBE Technology
Development of repository technologies in Germany

12 10 Lunch

Technical Sessions

National Program /Decommissioning /Siting / Host rock characterization

Chairs: YANG Chunhe, V. Bräuer

13 30 WANG Ju, BRIUG, CNNC
Geological Disposal of High Level Radioactive Waste in China: latest progress

14 00 Dr. Weigl, FZK:
"Decommissioning of Nuclear Facilities - German R&D"
V. Bräuer, BGR
Clay formations - a possible alternative as host rocks for radioactive waste disposal in Germany ?

15 00 K.-H.Lux, TU Clausthal
Radioactive waste disposal in various host rock formations – Geomechanical aspects (fundamentals)

15 30 Break

16 00 YANG Chunhe, Chinese Academy of Science
Rock Mechanical Research on Granite from Beishan site, Gansu, NW China

H. Shao, BGR

A presentation on German's research on granite讲花岗岩

18 00 Move to Peking Duck Restaurant (close to the Olympic Game Centre)

19 00 Welcome Banquet hosted by BRIUG, CNNC

Tuesday, May 27

Siting / Host rock characterization

Chairs: LIU Xiaodong, K.-H.Lux

09 00 H. Shao, BGR, Germany

In situ hydro-mechanical characterization of rock formation and coupled HM modeling

CHEN Weiming, BRIUG, CNNC

Geological characterization of Beishan Potential Site for China's High Level Radioactive Waste Repository

10 00 Guo Yonghai, BRIUG, CNNC

Hydrogeological Characterization of Beishan Potential Site for China's High Level Radioactive Waste Repository

SU Rui, BRIUG, CNNC

Hydraulic tests at bore holes at Beishan site, NW China

11 00 Break

11 15 O. Czaikowski, TU Clausthal, Germany

Radioactive waste disposal in various host rock formations – Geomechanical aspects (Selected applications)

LIU Yuemiao, BRIUG, CNNC

Physical-mechanical property and time- temperature effect of Beishan deep intact granite

12 15 LUNCH

Waste forms

Chairs: ZHANG Shendong, R. Odoj

13 30 M. Sailer, Öko-Institut e.V.

Handling of nuclear waste in Germany in the light of final disposal

14 00 B. Kienzler, Forschungszentrum Karlsruhe, Institute for Nuclear Waste Management

Experiences with the performance/behavior of HLW-forms in different host rock media

ZHANG Zhengtao, China Institute of Atomic Energy, CNNC

TMD

15 00 R. Odoj, Forschungszentrum Jülich, Institute for Safety Research and Reactor Technology

Quality control of radioactive waste in Germany

15 30 Break

Repository Technology, Engineering and Design

Chairs: YE Weiming, W. Bollingerfehr

16 00 W. Bollingerfehr, DBE Technology

Technical aspects of direct disposal of HLW

LI Tingjun, ZHANG Wei, Beijing Institute of Nuclear Engineering, CNNC

Waste Management Strategy and Design Concept for Geological Disposal of Radioactive Waste in China

WEN Zhijian, BRIUG, CNNC

Characteristic of Gaomiaozi Bentonite as potential backfill material for China's HLW repository YE Weiming, Tongji University, China

- 17 00 **Some achievements in study of Gaomiaozi bentonite used as backfill materials**
- 18 00 **Adjourn**
- 19 00 **Conference Dinner at Xijiao Hotel**

Wednesday, May 30

Repository Technology / Modelling and Safety Assessment

Chairs: SU Rui, W. Brewitz

- 09 00 B. Haverkamp, DBE Technology
Development of a new Closure Concept for the Richard Repository, Czech Republic – an example for successful international cooperation
 W. Brewitz, Gesellschaft für Anlagen-und Reaktorsicherheit (GRS) mbH, Department Final Repository Safety Research
Monitoring and modeling of groundwater parameters as a basis for radionuclide transport modelling
 PAN Wei, China Institute for Radiation Protection, CNNC
The experiment research of radionuclide migration in aquifer
- 10 30 **Break**
- 10 45 **Discussion on potential cooperation**

Chairs: WANG Ju, W.Steiningger
- 11 30 **Summary of the Workshop**
 Outlook, future perspectives for cooperation from the viewpoint of the P.R. China
 Outlook, future perspectives for cooperation from the viewpoint of Germany
- 12 00 **LUNCH**
- 13 00 **visit to the Great Wall at Mutianyu, Huairou County, Beijing**

Thursday, May 31

- 09 00 **Technical visit (Nuclear Research Centre, INET, Tsinghua University)**
- **End of workshop**

Chinese-German Workshop on Radioactive Waste Disposal

Sino-German Science Centre

May 28 - 31, 2007

Water Research - an example of 20 years successful Chinese-German co-operation

Dieter Fuhrmann

Project Management Agency Forschungszentrum Karlsruhe
for Water Technology and Waste Management
acting on behalf of BMBF and BMWi

BMBF: German Federal Ministry for Education and Research
BMWi: German Federal Ministry of Economics and Technology

BMBF Program „FONA“ - Research for Sustainability

Framework Program of the German
Federal Ministry of Education
and Research (BMBF) for a sustainable,
innovative society (launched 2004)

fields of action:

- Concepts for sustainability in industry and business
- Sustainable use concepts for regions
- Concepts for sustainable use of natural resources
- Social action geared to sustainability

www.fona.de

www.fona.de/engl/



Research for Sustainability

Framework programme of the German Federal Ministry of
Education and Research (BMBF) for a sustainable, innovative society

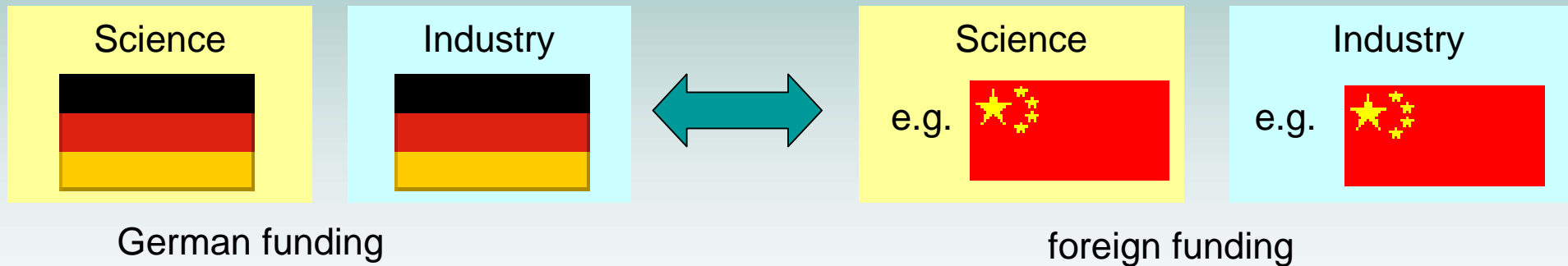


PTKA Annual Budget (2006)

- **PTKA's project funding in the field of water technology:**
 - ~ 40 million EUR
 - ~ 450 projects
 - **PTKA's international projects:**
 - ~ 18 million EUR
 - ~ 130 projects
- funding only for German research institutes, German industry
funding of foreign research institutes is not possible
(in exceptional cases: grants, consumable materials,
equipment)**

Preferred Structure of International Co-operations

so-called “2+2 Project”



Superordinated Targets of BMBF's Water Research

- World Summits of Rio and Johannesburg
- The EU Water Framework Directive (“good status of water bodies”)
- Conflicts resulting from the (over-)use of transboundary watersheds
- Sustainability of water supply and sanitation
- Security of the drinking water supply
- Water for agriculture (food production and energy crops)
- Influence of the climate change on water supply
- Germany as a location of high-technology
- Export of German water technology
- Amendment of the German legislation

Overview on Current Activities in the Field of Water Technology

- **Decentralized (alternative) water systems**
- **Adaptation of available water technology to other climate zones, levels of education, and culture**
- **Integrated water resources management (IWRM)**
- **Retention and degradation processes to reduce contaminations in groundwater and soil**
- **Permeable reactive barriers for groundwater remediation**
- **Prognosis of the entry of noxious substances in ground-water**
- **Risk-management of extreme flood events**
- **Phosphorous recovery from sewage sludge**

BMBF/PTKA - Bilateral Co-operations in the Field of Water:



EU



Algeria



Brazil



China



Chile



Ghana



Indonesia



Iran



Israel



Japan



Jordan



Palestine



Russia



South Africa



Thailand



Turkey



Vietnam

Contract for the Scientific Technological Co-operation
between

The Peoples Republic of China

and

The Federal Republic of Germany

signed on

October 9th, 1978

by

State Commission for Science and Technology (SCST)

Federal Ministry of Research and Technology (BMFT)

30th Anniversary of Co-operation in 2008

Fields of Co-operation

- Cultural Heritage
- Production Techniques
- Optical Technologies / Laser Technologies
- Material Research / Nano Technologies
- Marine Research / Geo Sciences
- Biological Research and Technology
- Environmental Technologies and Ecology
- Health Research
- Information and Communication Technologies

Meeting of the Joint Commission for Scientific Technological Cooperation

19th Meeting in April, 2006, Bonn

Meeting of the Steering Committee “Environmental Technology and Ecology”

5th Meeting in February, 2004, Sanya

6th Meeting in March, 2007, Bonn

Bilateral Cooperation with China in the Field of Water

On-going projects: since 1988
Number of projects: 43 in total; 23 on-going projects
budget: 17 million EUR (6,1 million EUR on-going projects)

Current fields of cooperation:

- **New technologies for industrial waste water treatment**
- **Disinfection of municipal waste water for reuse purposes**
- **Enrichment of groundwater**
- **Management of storm water, utilization of rainwater – Olympic Park 2008**
- **Concepts for the remediation of lake Chao**
- **Decentralized water systems**
- **Drinking water: simultaneous elimination of nitrate and pesticides**

BMBF Program „Decentralized (Alternative) Water Systems“ - Rapidly growing urban areas, China -

New technical solutions (“semi-central approach”) to enable a sustainable supply and disposal of rapidly growing urban areas

partners:

TU Darmstadt and German private companies

Tongji-University Shanghai

Qingdao Tech University

Topics of investigation are:

- comparison of different ways of gray water treatment**
- application of ultrasound to clean membranes**
- production of lactic acid from biomass**

Concepts for the Remediation of Lake Chao

partners:

**Technical University of
Braunschweig,
Leibnitz Institute for the Ecology
of Closed Water Bodies,
University of Göttingen**

**Anhui Environmental
Protection Bureau,
University of Hefei**

**Lake Chao/Anhui Province
China**



Lake Chao Project (concepts for remediation)

Problem:

- eutrophication of lake Chao (760km²)
- seasonal occurrence of blue algae
- breakdown of the drinking water supply from the lake water



Visit to Hefei in June, 2006

Lake Chao: Concepts for drinking water treatment



Processes close to nature (green liver)



technical solution

Sustainable Water Concept and its Application for the 2008 Olympic Games in Beijing

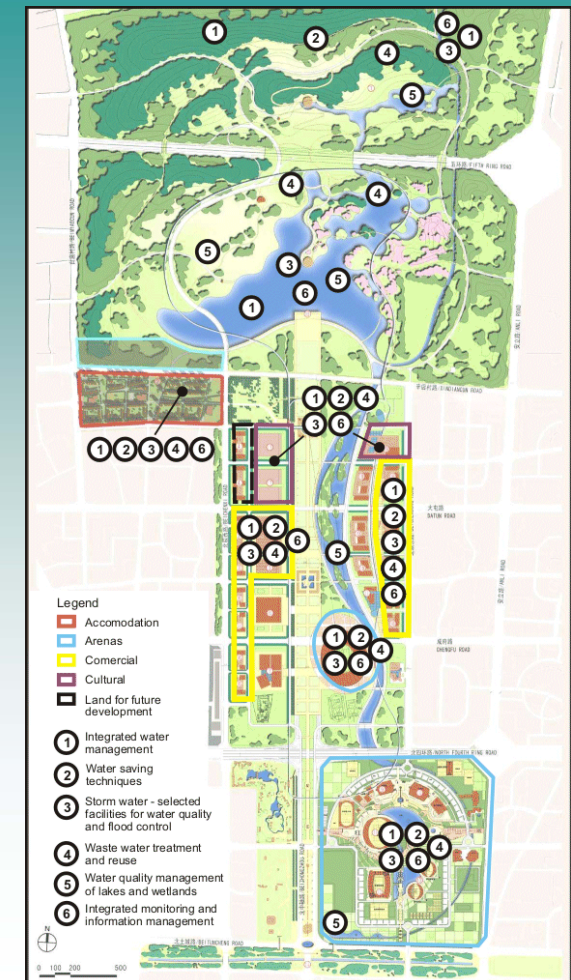
WASY Limited, TU Berlin, Geoterra
Obermeyer, TU Essen, Institut für
Gewässerökologie

Tsinghua University
Beijing Water Authority

Fields of activities:

- integrated water management
- water saving
- rain water resources and flood control
- waste water treatment and reuse
- water quality management of lakes and wetlands
- integrated monitoring and information management

All activities are carried out on the Olympic Park

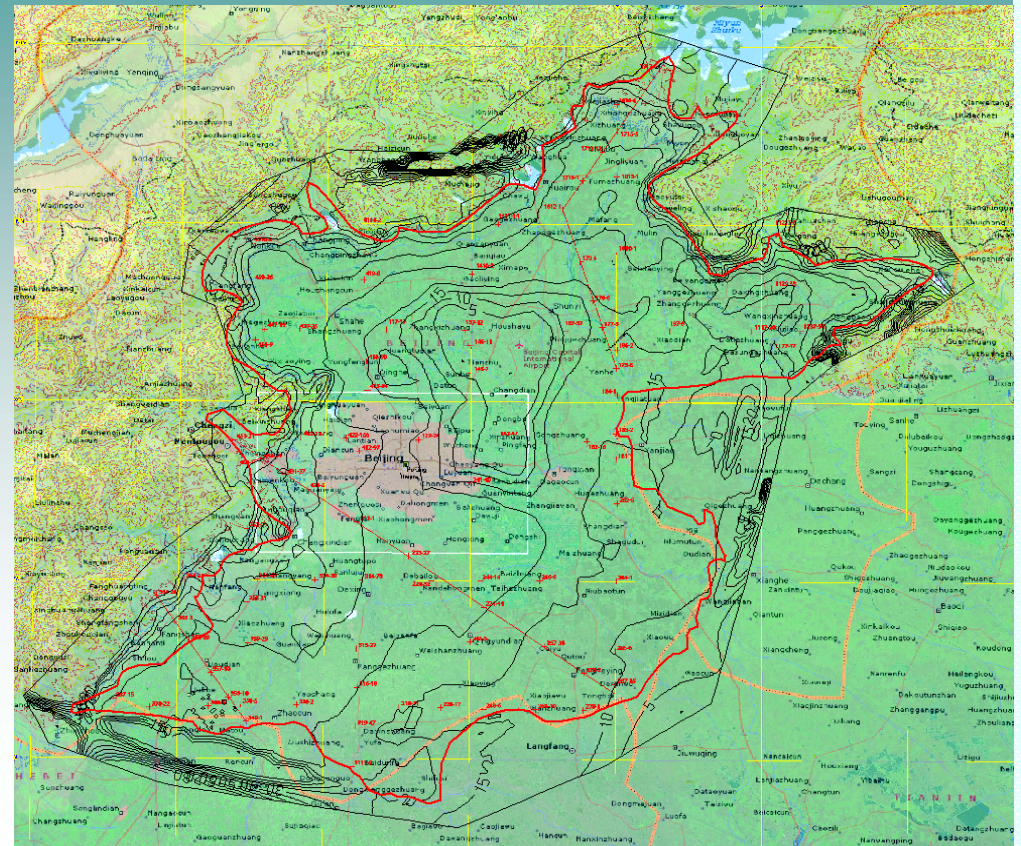


Water Management in Beijing Area

partner:
Fraunhofer Institute
Beijing Water Authority

Development of a decision support
system for the water supply of
megacities under consideration of

- the resources
(reservoirs, groundwater)
- transport (channels, rivers)
- water works
- consumer



Establishment of Courses in Environmental Sciences

**University
of Aachen**

**Tsinghua University
(Beijing)
and
Sichuan University
(Chengdu)**



Recently started projects:

- **“Simultaneous elimination of nitrate and pesticides during drinking water treatment in rural areas”**
partners:
Forschungszentrum Karlsruhe, Universität of Karlsruhe
University of Halle
Tsinghua University Beijing
and private companies
- **“Different methods of disinfection of waste water for reuse purposes”**
partners:
Technical University of Darmstadt
Tongji-University Shanghai
private companies

Yangtze River - Three Gorges Dam



Three Gorges Area



Three Gorges Dam Project - Proposed Fields of Co-operation

➤ Joint Research Projects

➤ Scientist Exchange Program

➤ PhD - Students Exchange

➤ Capacity Building

Proposed Topics for Joint Research Projects

- **Exchange of pollutants between water, suspended matter, and sediment**
 - impact on water quality management
- **Erosion**
 - impact on the stability of banks and slopes
- **Vegetation**
 - impact on plants in the flooded area
- **Climate**
 - impact on the deposition of air pollutants
- **Socio-economic aspects**

Thanks a lot for your attention !!!

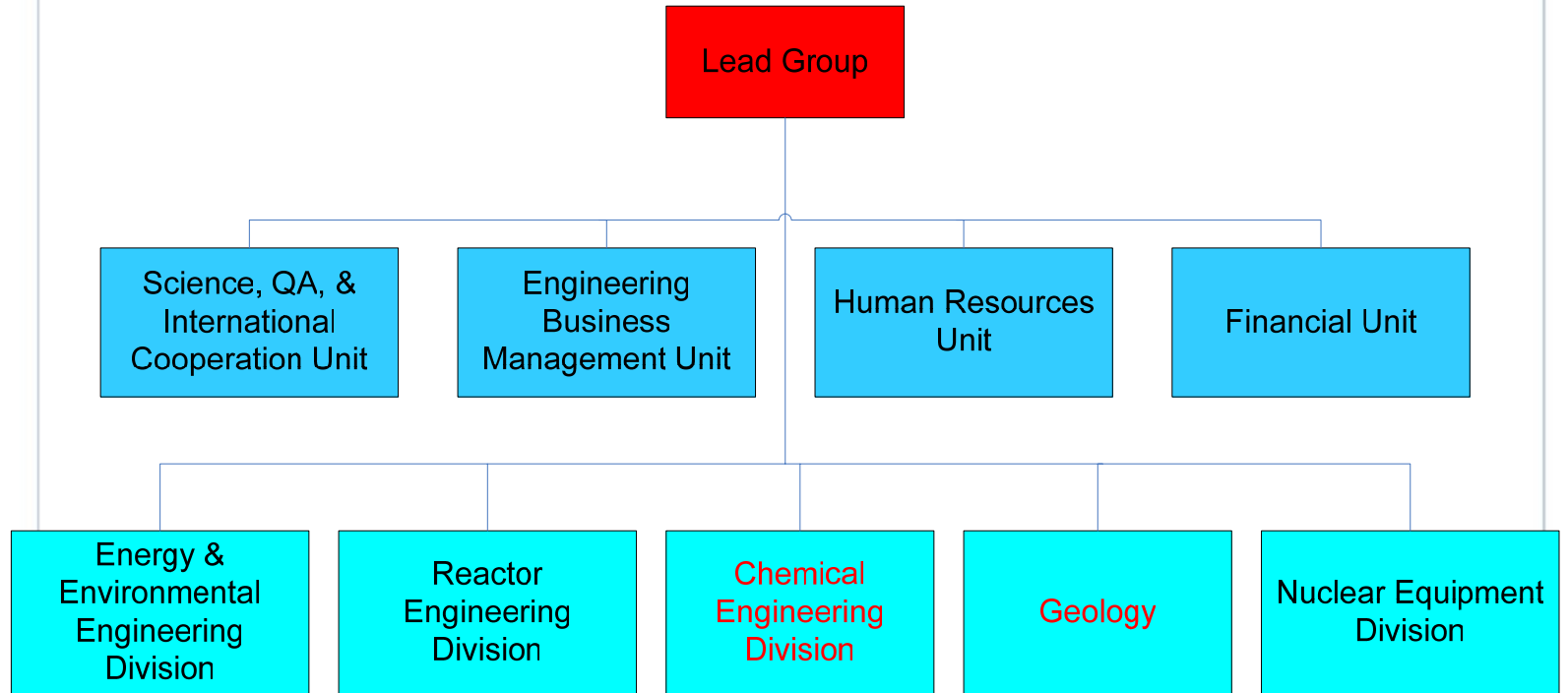
Forschungszentrum Karlsruhe - Research Center Karlsruhe



Founded on January, 1958.

The first and largest comprehensive institute for nuclear engineering research and design in China.

951 technicians of various specialties , 45 professoriate senior engineers, 301 senior engineers.

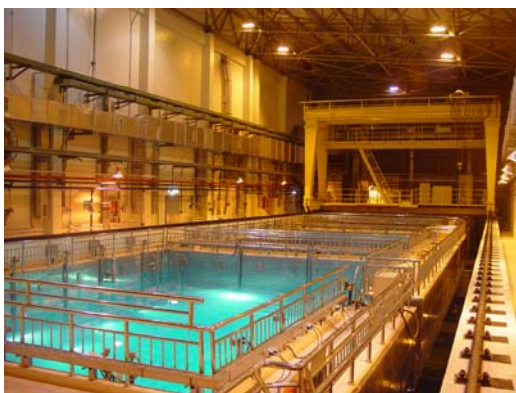




Nuclear Reactor Design and Engineering

- Qin Shan-II PWR NPP
- DaYa Wan PWR NPP
- Ling Ao-I&II PWR NPP
- Tian Wan VVER NPP (Consultancy)
- New NPP (Viability)
- Experimental Faster Breeder Reactor
- Small scale reactor





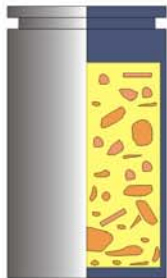
Spent Fuel Reprocessing Design and Engineering

- Spent fuel reprocessing pilot plant with the processing capacity of 300 kgU/d
- Storage pool of the plant with the capacity of 550 tU
- Spent fuel large scale reprocessing plant (Planning)



Decommissioning and Radioactive Waste Management

- Decontamination and decommissioning
- Low and intermediate liquid waste solidification
- Low and intermediate waste conditioning
- Low and intermediate waste near surface disposal
- High level liquid waste evaporation and storage
- Spent source storage
- Organic waste pyrolysis incineration
- Very low level waste disposal
- Alpha bearing waste conditioning
- High level liquid waste vitrification
- High level waste geological disposal





- Nuclear Power Development
- Spent Fuel Management
- Waste Study
- Design Concept of the Repository

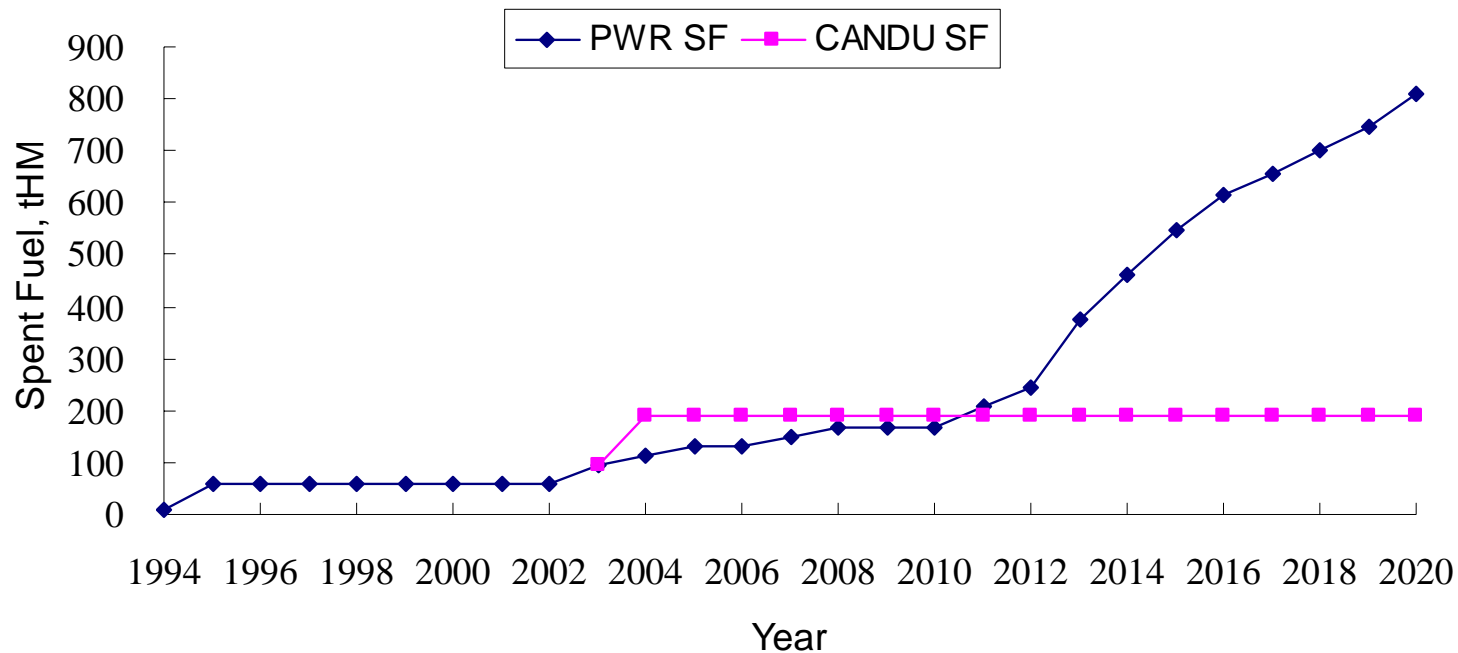


Ten commercial nuclear power reactors totaling 7,700 MWe are producing electricity.

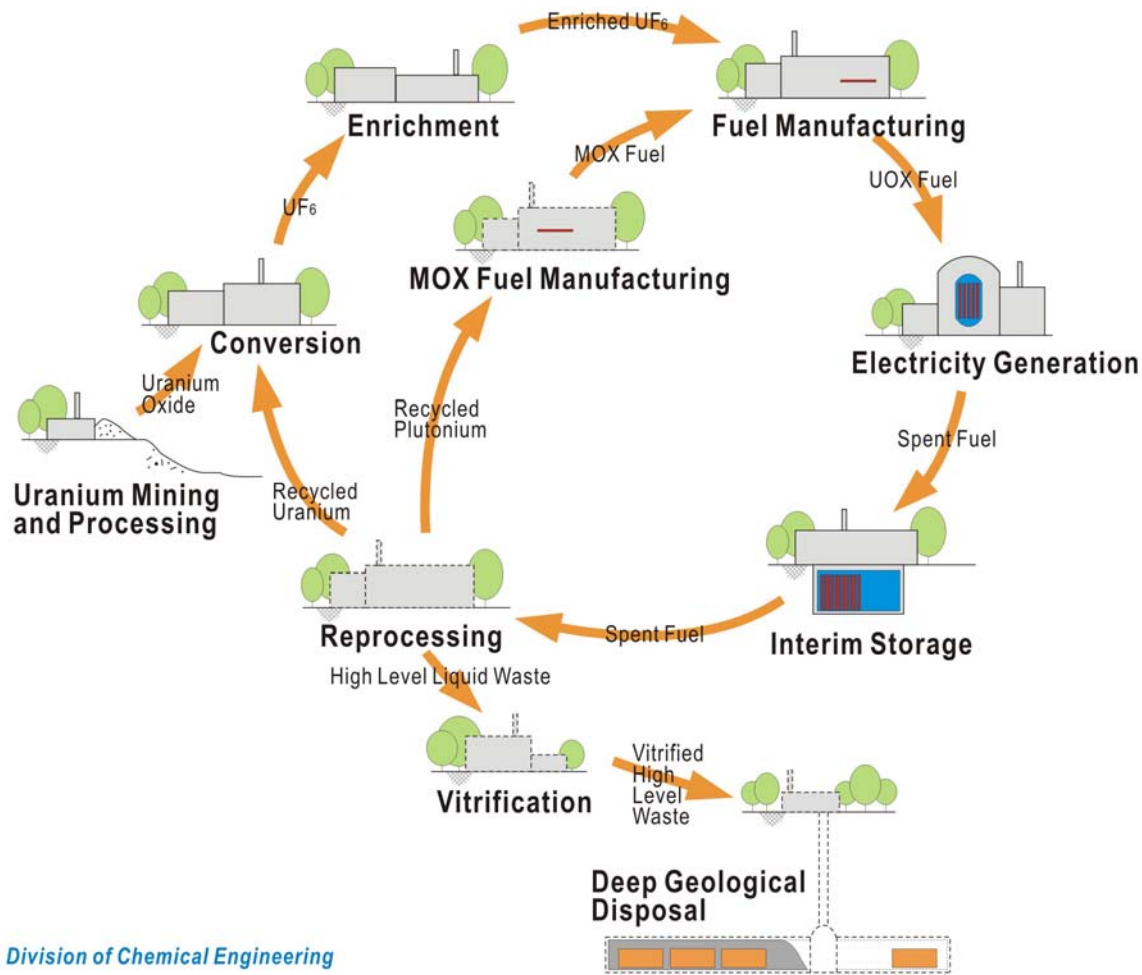


It is scheduled that installed nuclear capacity will be 40 GWe by 2020.

NPPs in mainland of China



Spent Fuel unloaded annually
(estimated by BINE)



Division of Chemical Engineering



Currently, Chinese nuclear fuel management is based on a closed fuel cycle strategy.

Spent fuel from nuclear power plants will be reprocessed to recover usable elements which will be recycled into new fuel assembly.

China chooses reprocessing to save amounts of natural resources and minimize radioactive waste.

A pilot reprocessing plant is under commissioning and has accepted PWR spent fuel.



According to “Radioactive Pollution Prevent Law of 2003”, high level radioactive solid waste and alpha bearing solid waste will be disposed in deep geological repositories.

The objective of Chinese HLW geological disposal R&D program is to construct a national HLW repository in the middle of the 21st century.

The waste studied for geological disposal contains vitrified high level glass, other type high level waste, and alpha bearing waste.



Vitrified high level waste

High level liquid waste is immobilized into a stable glass matrix in stainless steel canisters which is called as vitrified high level waste (VHLW).

This waste will be stored in interim storage facilities for several decades until it is suitable for final disposal and the repository is available.



Other type high level waste

Other type high level waste includes fuel structural materials, special devices dismantled from reprocessing line. This waste also give rise to significant heat generation, although to a lesser degree and of shorter duration.

The conditioning technology to convert other type high level waste into suitable waste form to be disposed of in the repository has not been developed.



Alpha bearing waste

Alpha bearing waste in China is defined as single waste package contains more than 4×10^6 Bq/kg of alpha emitting radionuclides with half-lives greater than 30 years.

Alpha bearing waste originates mainly from reprocessing of spent fuel and includes plutonium contaminated equipments, tools and cloth.

The conditioning technology to convert alpha bearing waste into suitable waste form to be disposed of in the repository has not been developed.



In view of waste origin, waste to be disposed of in the geological repository is classified into commercial waste and legacy waste.



- Commercial waste

Most volume, decay heat and radioactivity of the waste to be disposed in the repository will be contributed by commercial waste.

Commercial waste originates from future re-processing of NPP spent fuel. It is foreseen that 10,000-15,000 canisters each containing 150 liters of vitrified waste could be accumulated up to 2050.

- Legacy waste

Legacy waste is stored in the former nuclear facilities and will be generated throughout the decommissioning activities.



With cooperation with BRIUG, CIAE, CIRP and other organizations, BINE carries out her work in respect of radioactive waste geological disposal.

- Characterization for the waste stream of the repository.
- Conceptual design for the underground research laboratory (URL), including surface facility and underground facility.
- Concept making for the HLW geological repository, including surface facility and underground facility.

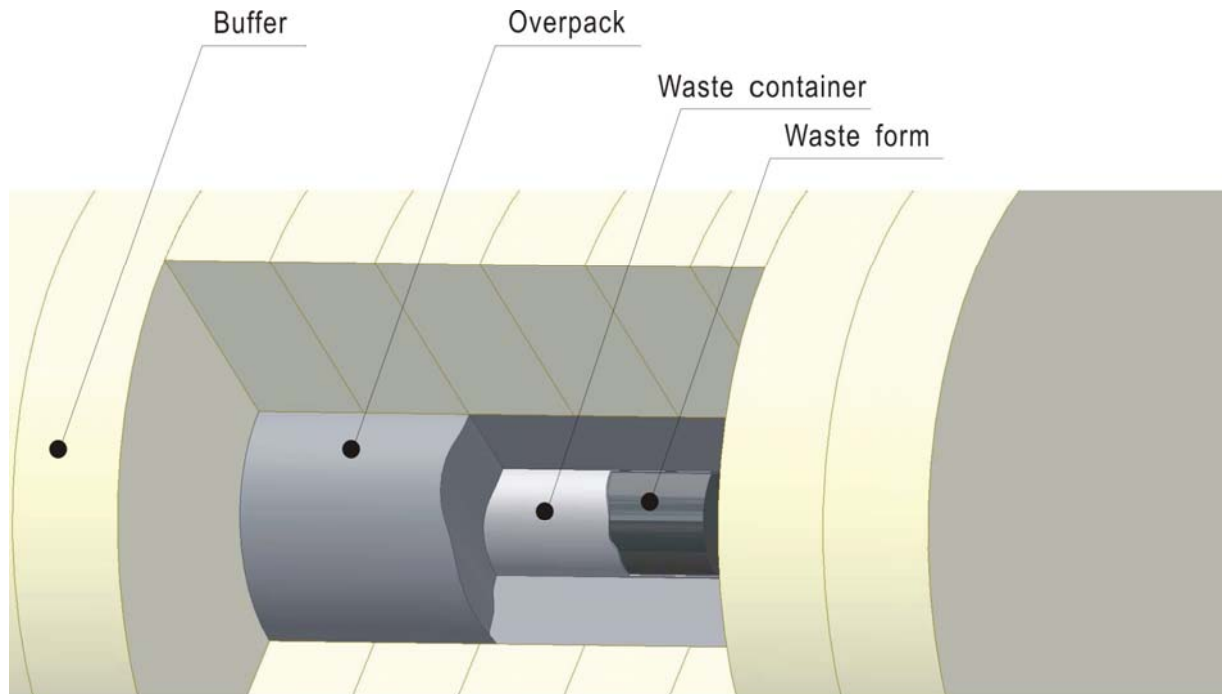


Disposal of radioactive waste in a facility located underground in a stable geological formation is intended to provide long term isolation of the radionuclides in the waste from the biosphere.

The geological disposal system can be defined as a combination of engineered and geological barrier which is generally known as a “multi-barrier” system.



The engineered barrier system (EBS) comprises a variety of sub-systems or components.



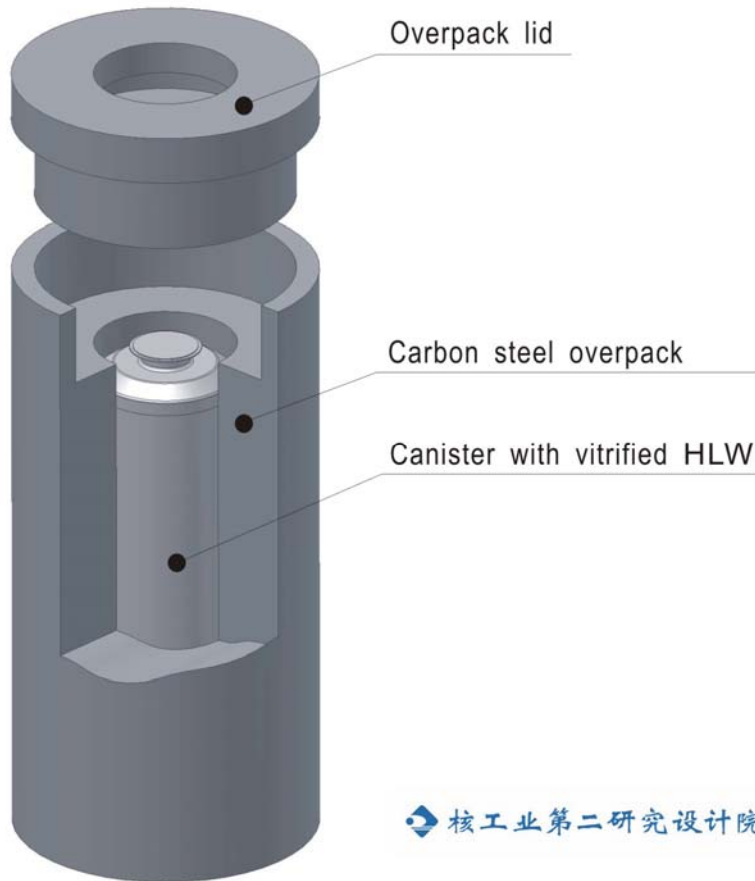


Waste package

The waste package is the combination of the waste form and its surrounding container.

Standardization of waste containers for high level waste and alpha bearing waste is under research. Stainless steel containers are preferred to contain high level waste and alpha bearing waste.

The draft of industrial standard of the container for alpha bearing waste and high level solid waste has just been completed by BINE. It will be issued by the end of this year.



Overpack

Overpacks are designed to contribute to the containment function of the EBS. Current study is focused on the overpack for VHLW. Description on the overpack is only narrowed on what is for the VHLW.



Buffer

The purpose of the buffer is to limit and delay any release of radionuclides into the underground environment when the overpack fails.

Bentonite is the main material of the buffer and its properties are investigated.

Compacted bentonite rings could be placed around the overpack or be inserted with the overpack into a large container to form a so called “supper container”.



Thank you!

DEVELOPMENT OF REPOSITORY TECHNOLOGIES IN GERMANY

==== Nuclear Industry in Germany =====

- Introduction of Nuclear Power Research in the fifties and sixties
- Commercial Nuclear Power Use since the late sixties
 - 1968 (Obrigheim)
 - 1974 Biblis A
- 17 Power Plants in Operation
- 20,200 MW installed Power (second to France)
- 28% of the Electricity Delivered to the Public Grid is Nuclear

Milestones in Waste Disposal

- 60's: All Waste to go to Deep Geological Repositories
- Asse Experimental Repository
1967 - 1978

Worldwide First Deep Geological Repository



- 1979 Federal Council Decision on Waste Management:
“Entsorgungsnachweis” a Requirement for NPP Operation

Waste Management Concept

- Interim Storage in NPP Pools (limited capacity)
- Spent Fuel Reprocessing
- Pu Recycling as MOx in LWR
- AFR HLW/SF Interim Storage
- Deep Geological Disposal



Concept Implementation

- Gorleben Site Characterization Starts in 1979
- Exploration Mine Starts in 1985
- Konrad Licensing Starts in 1982
- Centralized Interim Storage
- Development of Direct Disposal



Repository Technologies

- Morsleben: Operational Waste (discontinued October 1998)
- Konrad: Non-heat Generating Waste
- Gorleben: Spent Fuel and HLW
- Encapsulation Plant
- AFR Interim Storage: Gorleben / Ahaus



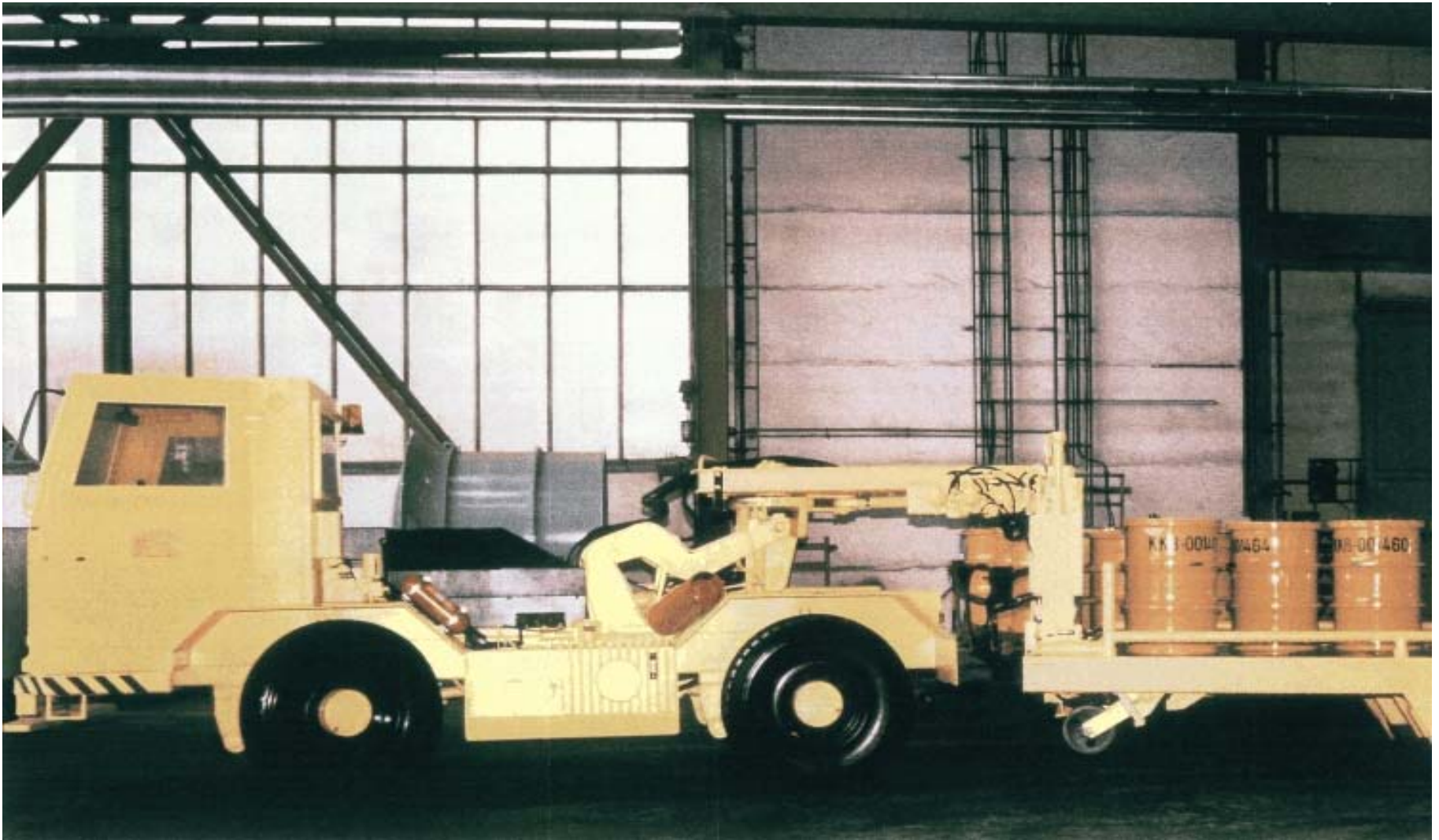
Morsleben Repository



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DBE 

Morsleben Repository



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Morsleben Repository



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Morsleben Repository



DBE-TEC

DBE 

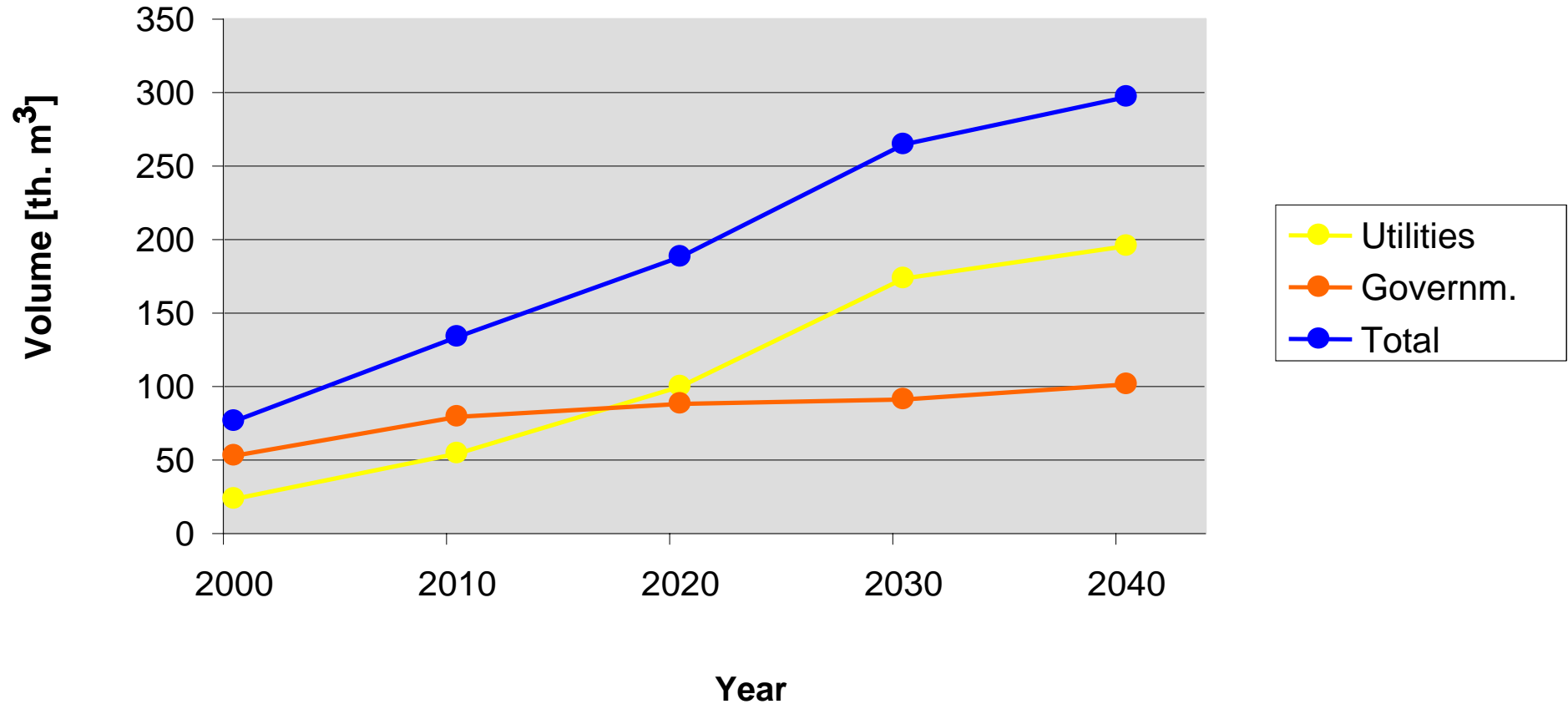
Morsleben Repository



Konrad Repository



Waste with Negligible Decay Heat



KONRAD REPOSITORY MILESTONES

- 1933 Konrad iron deposit discovered
- 1957-09 / 1960-01 shaft Konrad 1 sunk to 1232 m
- 1960 start of iron ore production
- 1976 ore production abandoned



KONRAD REPOSITORY MILESTONES

- 1972 – 1982 site suitability study
- August 31, 1982
license application submitted
- 1983 – 1990 comprehensive site survey
plan development



KONRAD REPOSITORY MILESTONES

- May 22 – July 15, 1991 Konrad plan presented to the public
- 289,387 objections raised
- 1992 – 25 – 09 / 1993 – 03- 06 Konrad hearing (longest ever)
- 1994 – 1996 License Procedure completed...



KONRAD REPOSITORY MILESTONES

- June 14, 2000 Consensus Agreement
 - *Finishing license procedure*
 - *Withdrawal immediate validity*
- July 2000 Immediate Validity cancelled
- **May 22, 2002 NMU grant license**
- 6 Plaintiffs file suit against NMU



KONRAD REPOSITORY MILESTONES

- March 8, 2006 Higher Administrative Court Verdict
 - *Salzgitter, Lengede, Vechelde suits invalid*
 - *Traube family suit unfounded*
 - *Verdict Revision excluded*
- April 2007 final court verdict
- May 21, 2007 construction kick-off by the BMU

KONRAD REPOSITORY MILESTONES

Nr.	ACTIVITY	2007	2008	2009	2010	2011	2012	2013
1	Staff and Organizational Requirements	█						
2	Mining Licenses	█						
3	Construction Prerequisites according to License Documents	█	█					
4	Preparation of Construction Documents incl. Tendering & Awarding	█	█	█				
5	Adjustment of existing Contracts for Construction Work	█						
6	Adjustment of planned Rehabilitation Measures incl. Supplementary Technical Equipment for the Conversion	█	█	█				
7	Construction of the Infrastructure for Konrad 1 und Konrad 2		█	█				
8	Conversion into a Repository including Operation Start up			█	█	█	█	
9	Start of Waste Disposal							█

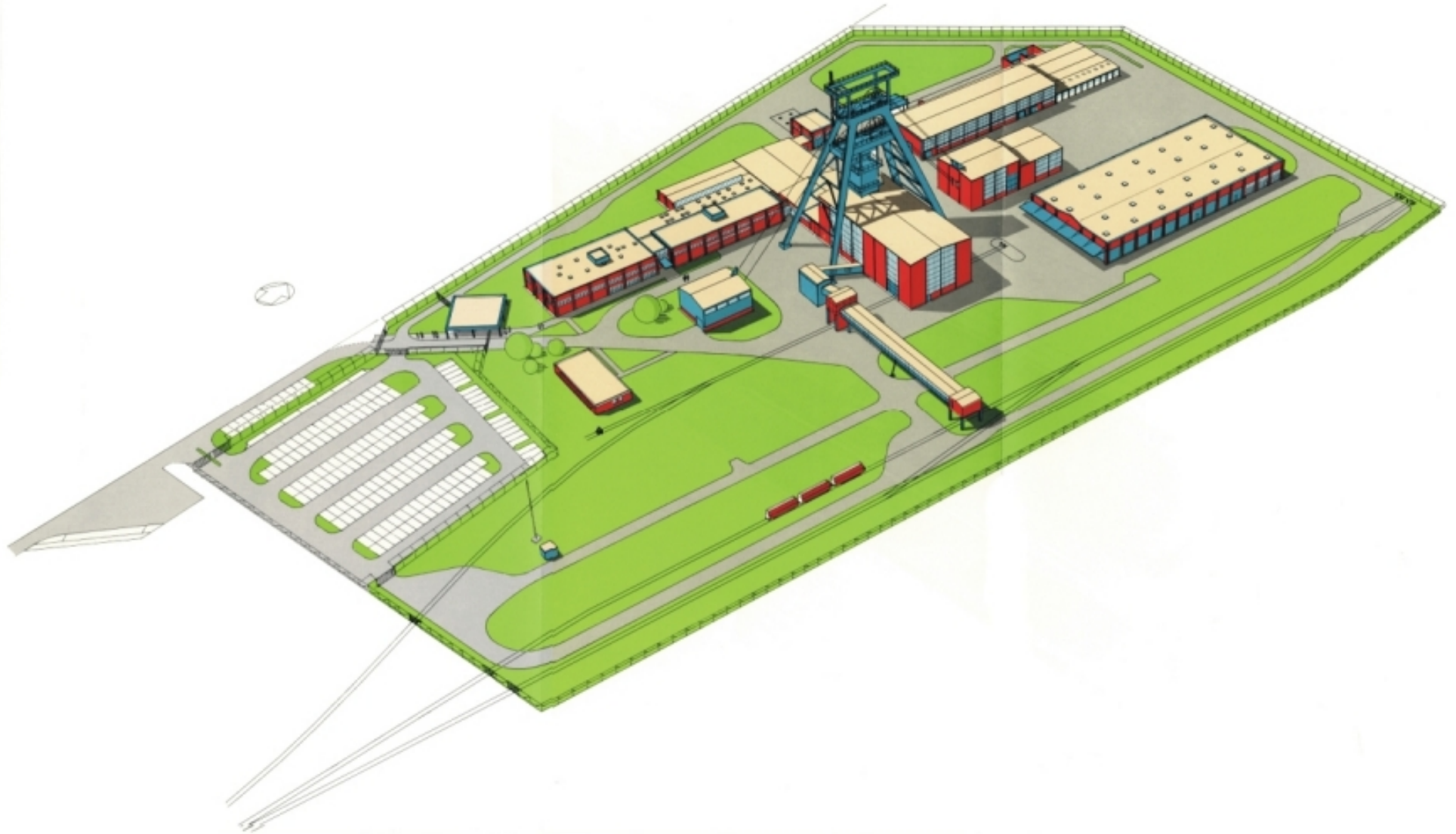
Konrad Shaft 1



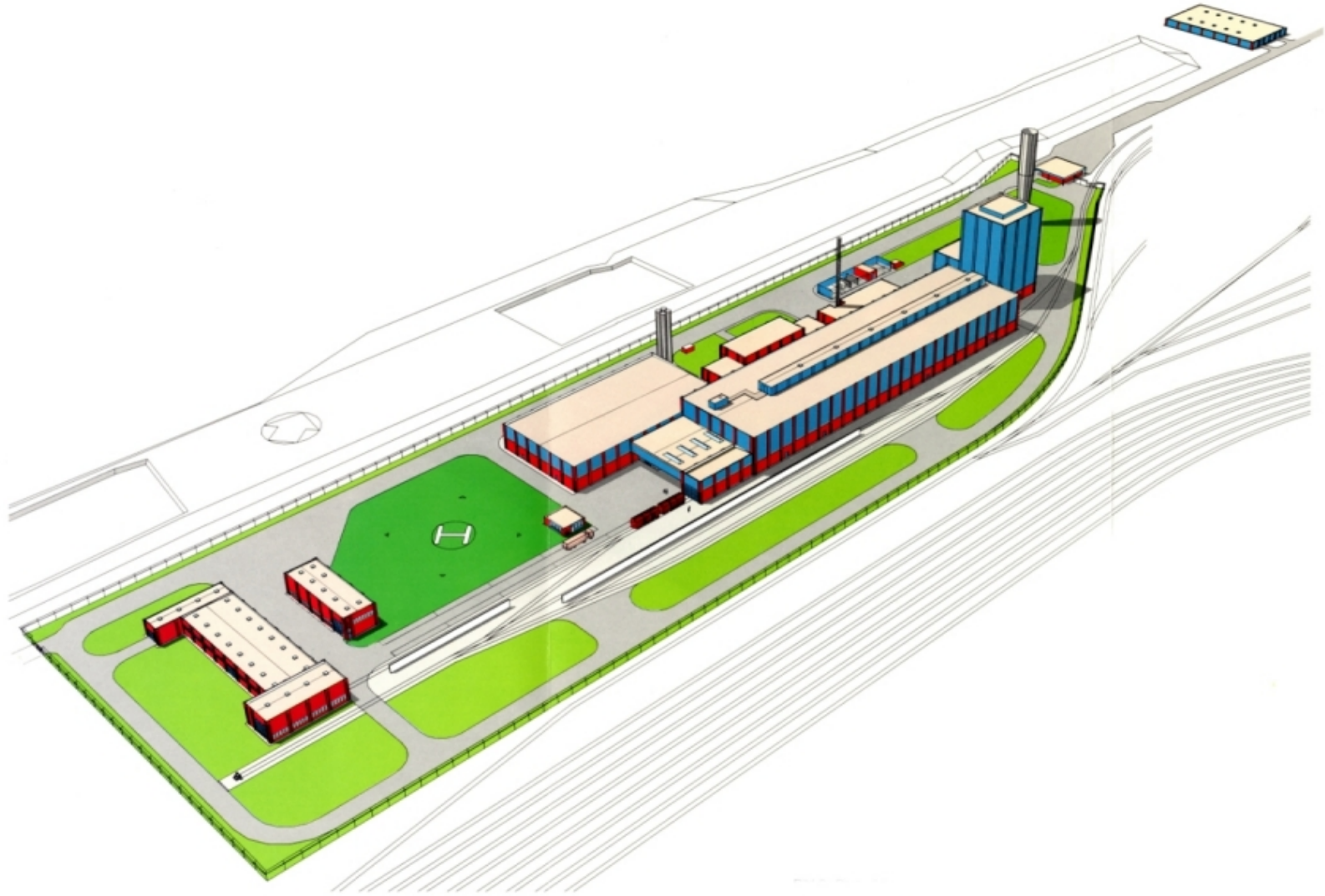
DBE-TEC

DBE 

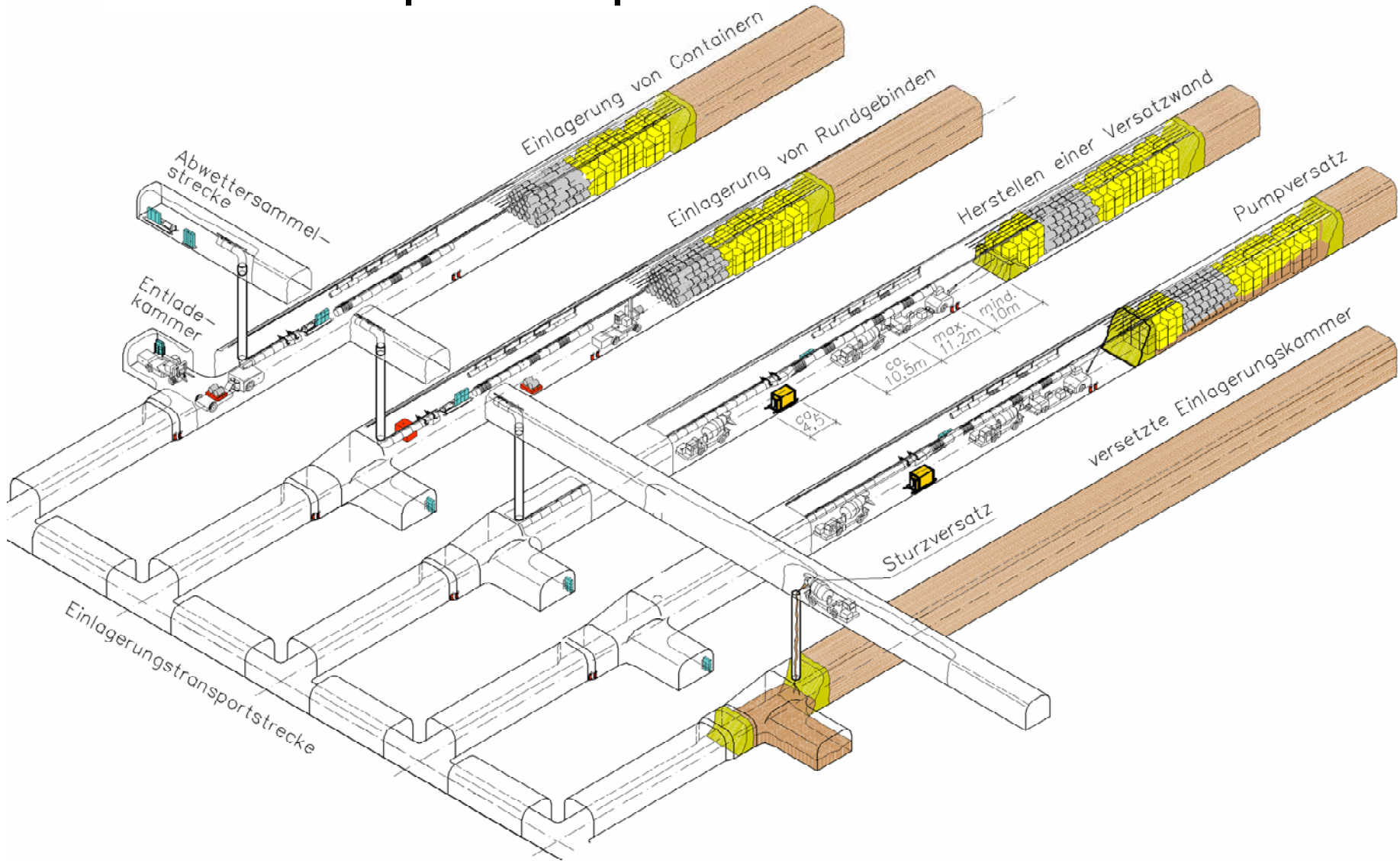
Konrad – Shaft 1 Facilities



Konrad – Shaft 2 Facilities



Konrad – Disposal Sequence



Waste disposal at Konrad



Konrad Equipment



DBETEC

DBE 

Konrad Equipment



Konrad Equipment



DBETEC

DBE 

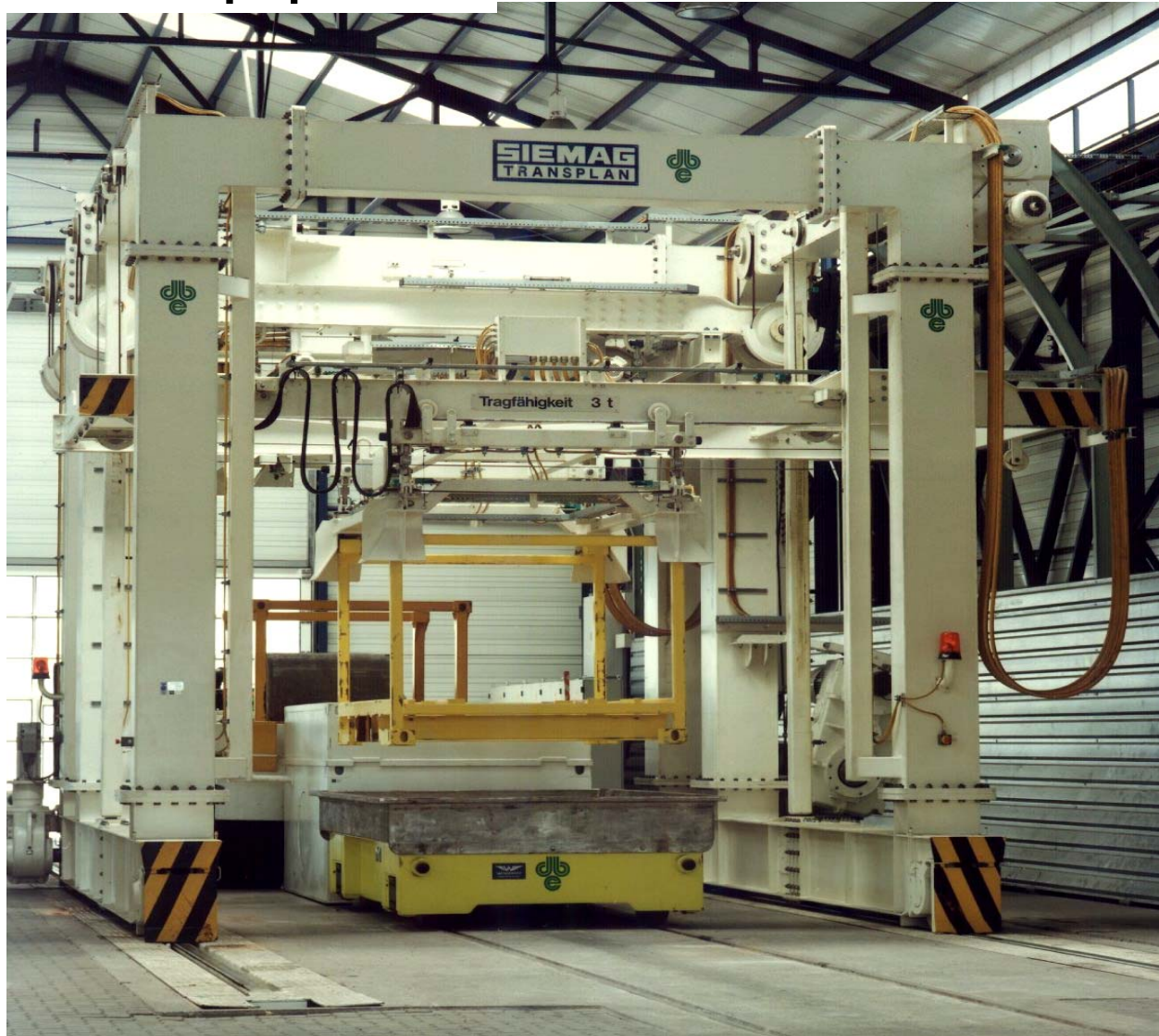
Konrad Equipment



DBETEC

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Konrad Equipment



Konrad Equipment



DBETEC

DBE 

Konrad Equipment



DBETEC

DBE 

Konrad Repository



Konrad Repository



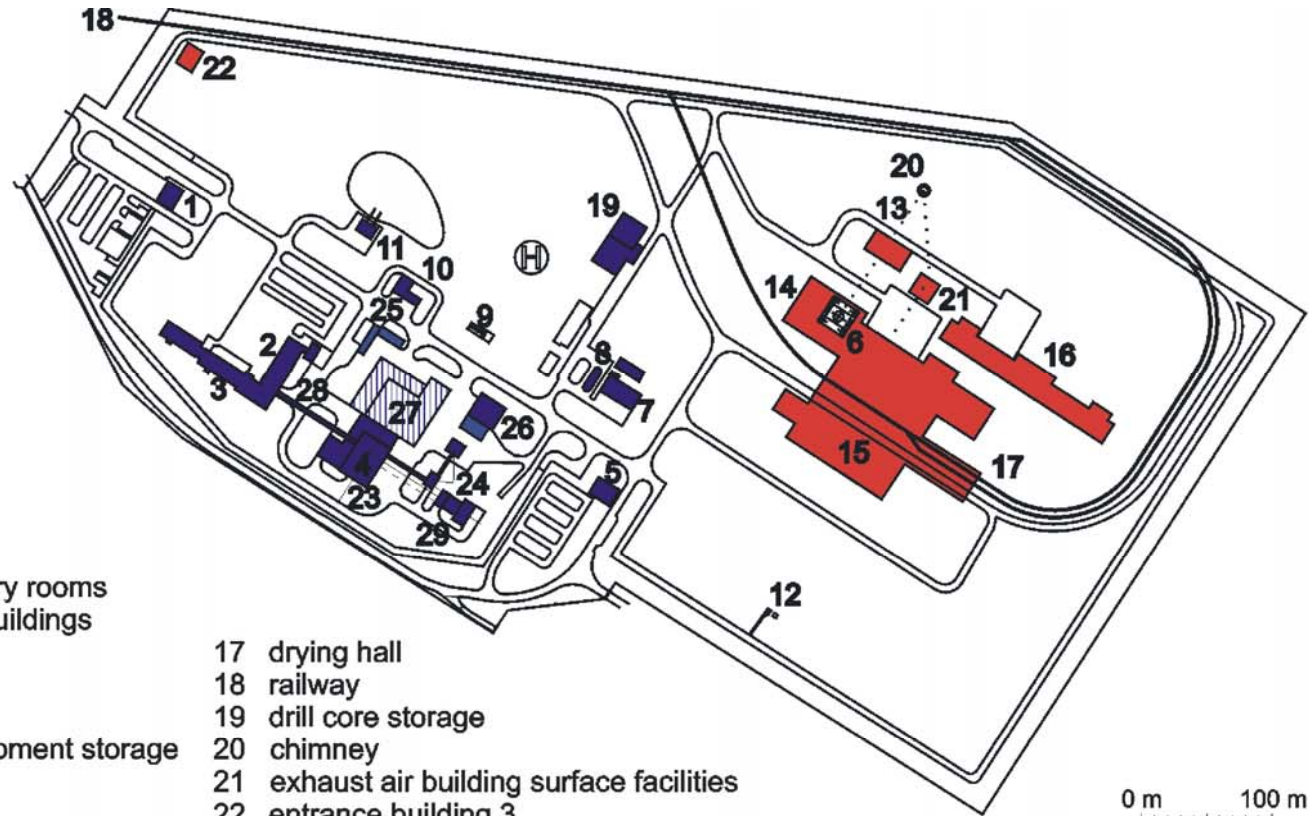
Gorleben Site Exploration Mine



DBETEC

DBE 

Gorleben



Legend:

- | | | | |
|----|--|----|---|
| 1 | entrance building 1 | 17 | drying hall |
| 2 | heating plant and dry rooms | 18 | railway |
| 3 | offices and social buildings | 19 | drill core storage |
| 4 | shaft 1 | 20 | chimney |
| 5 | entrance building 2 | 21 | exhaust air building surface facilities |
| 6 | shaft 2 | 22 | entrance building 3 |
| 7 | magazine and equipment storage | 23 | shaft hall shaft 1 |
| 8 | fuel storage | 24 | salt shipment - departure |
| 9 | pumping station
(fresh and waste water) | 25 | garages / friction hoist |
| 10 | electric power transmission | 26 | cleaning hall / storage for equipment to
pull over new ropes |
| 11 | drain water pumping station | 27 | workshop and spareparts |
| 12 | weather monitoring station | 28 | gateway - bridge to shaft 1 |
| 13 | diffusor | 29 | mine ventilation fresh air building |
| 14 | shaft hall shaft 2 | | |
| 15 | shipment - arrival | | |
| 16 | technical offices, laboratories | | |

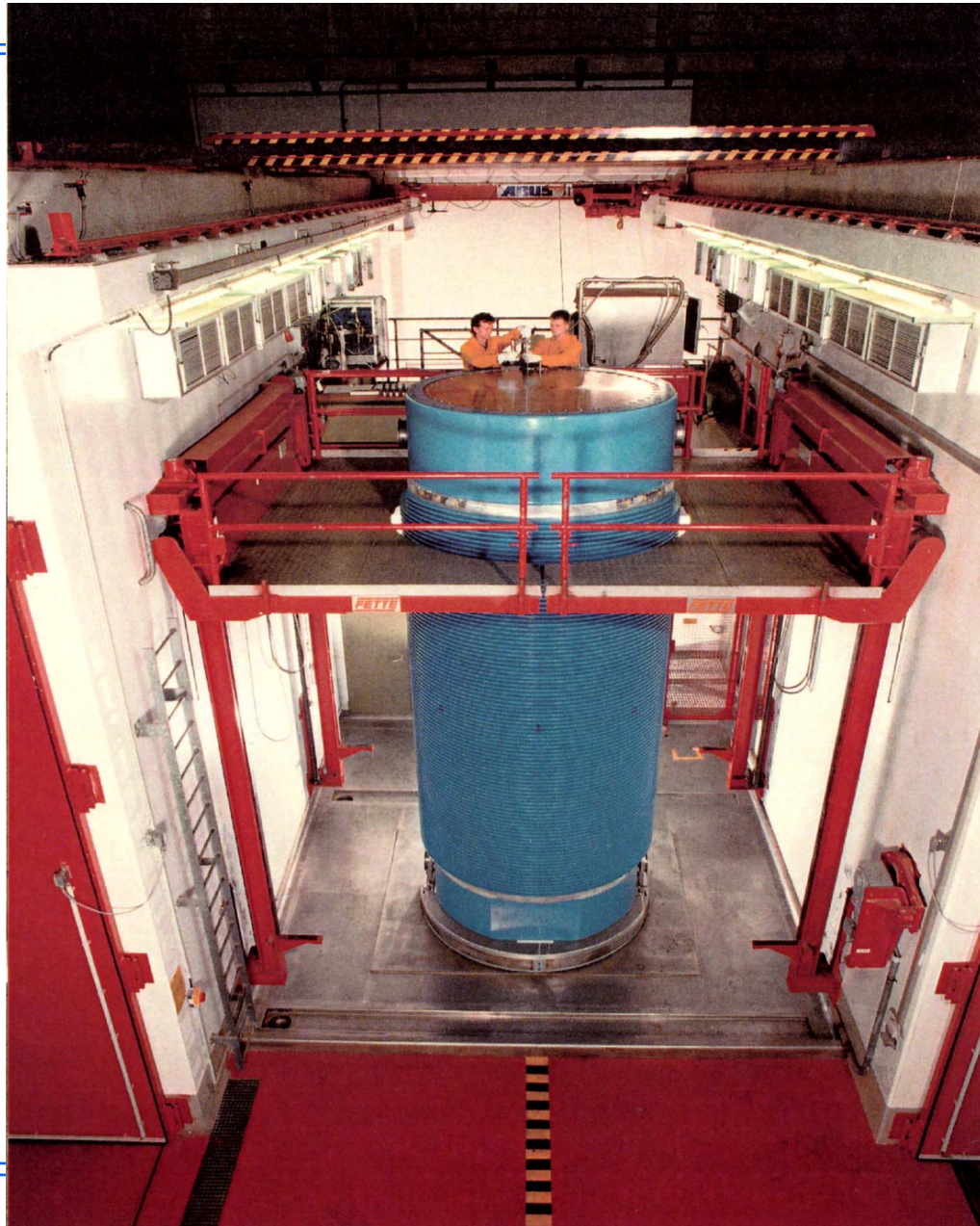
- existing
- new
- planned while exploration

Gorleben



DBETEC

DBE 



DBE-TEC

DBE 



DBE-T

DBE 

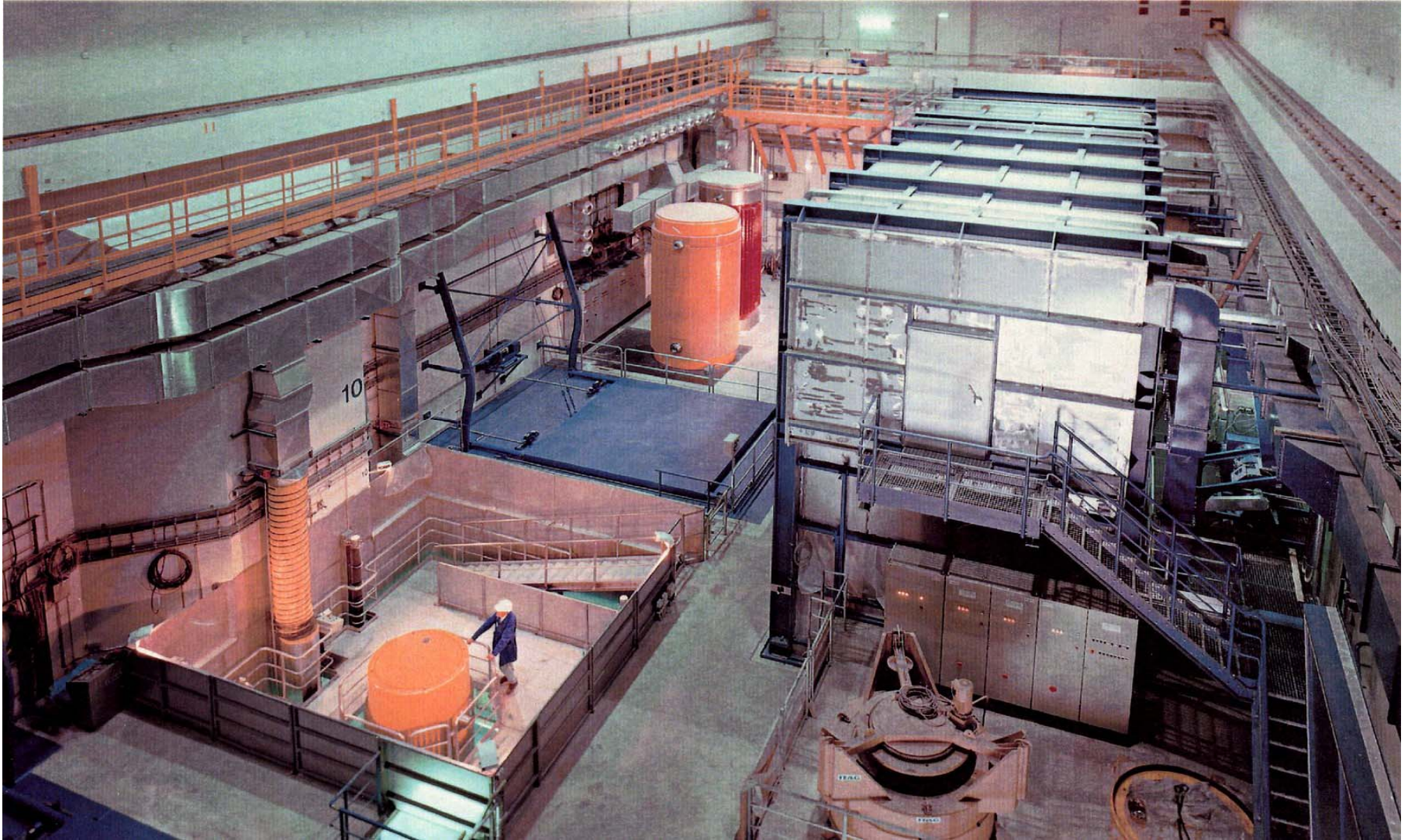
Gorleben

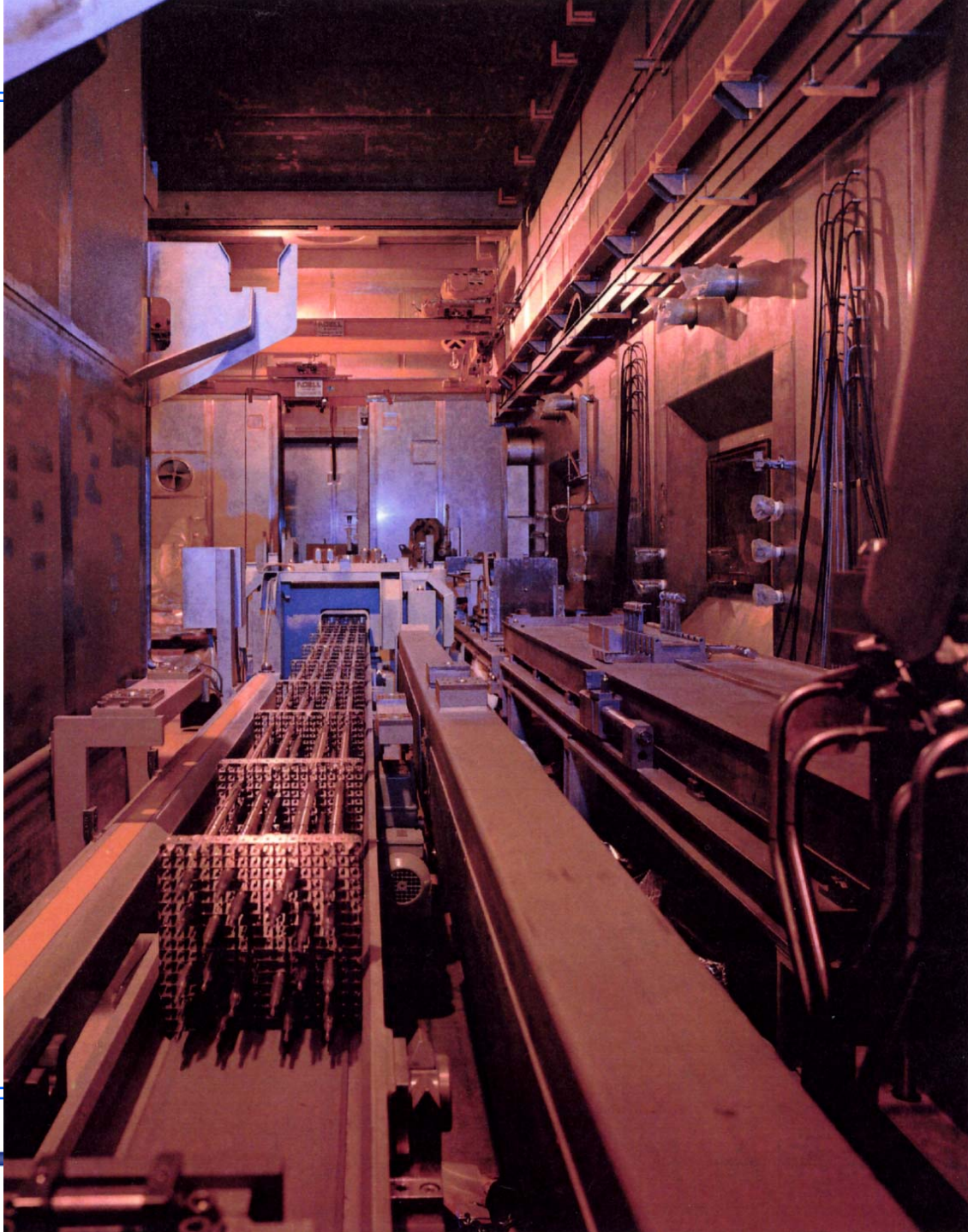


DBE-TEC

DBE 

Gorleben



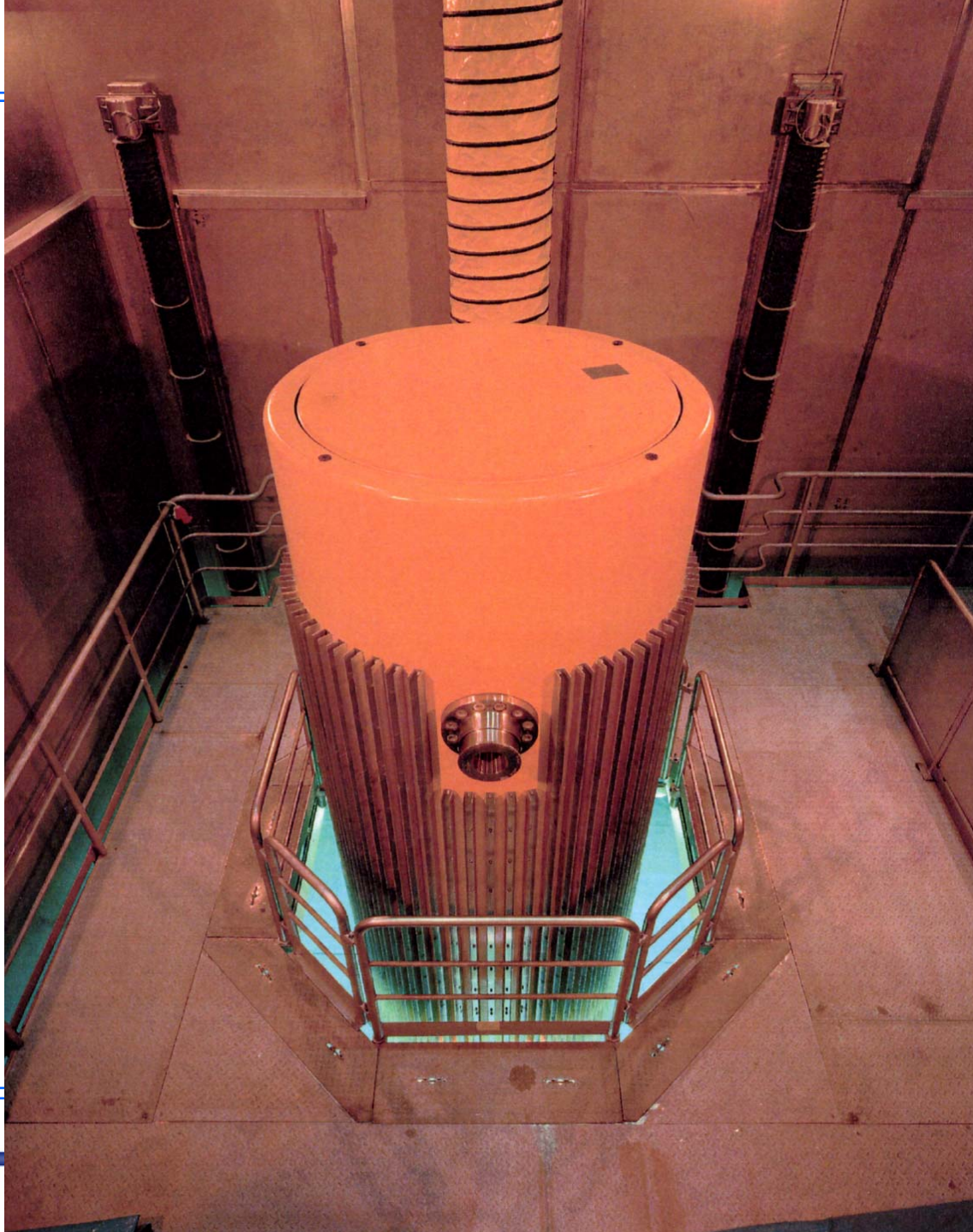


DBE-T

DBE 

Gorleben





DBE-T

DBE 

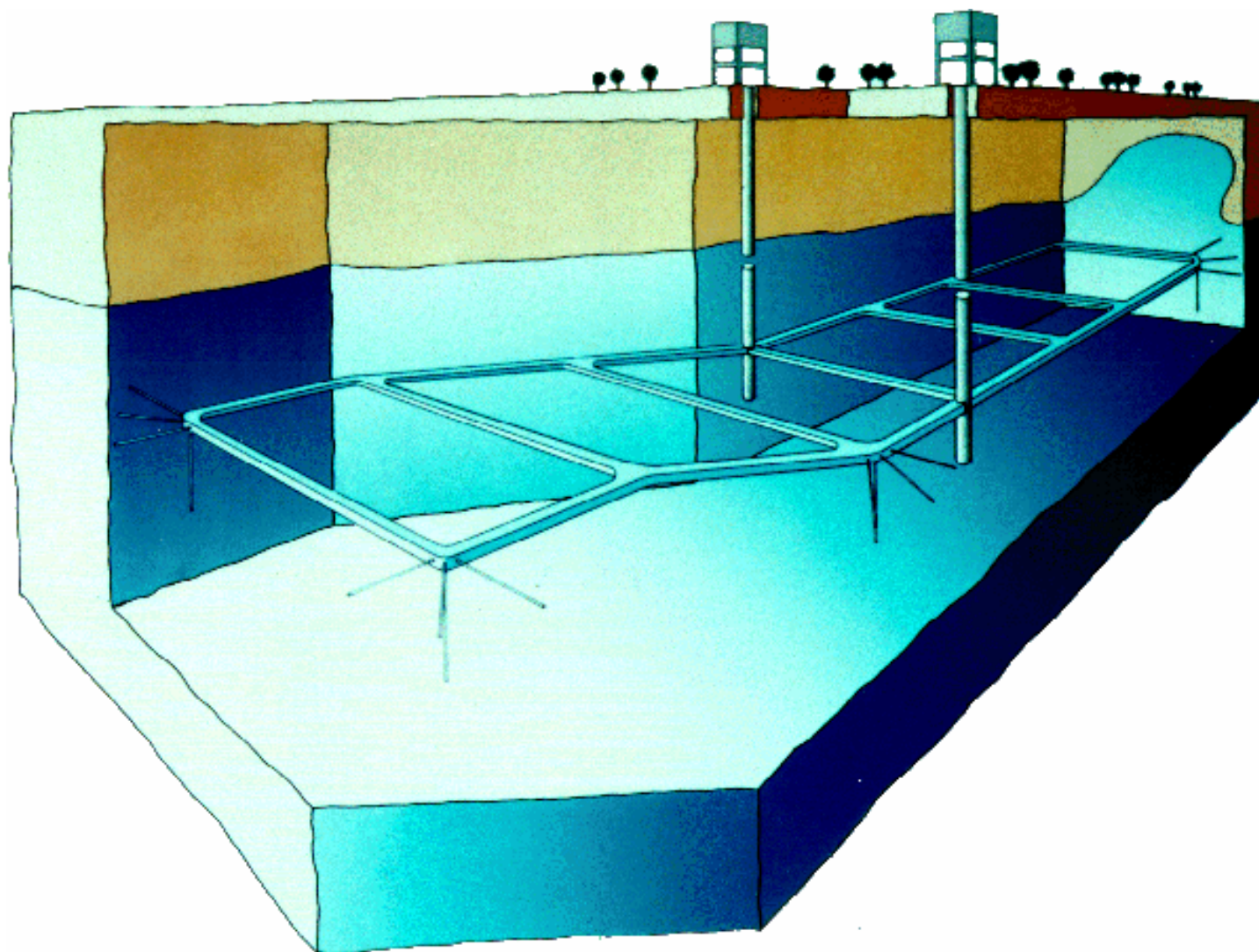
Gorleben



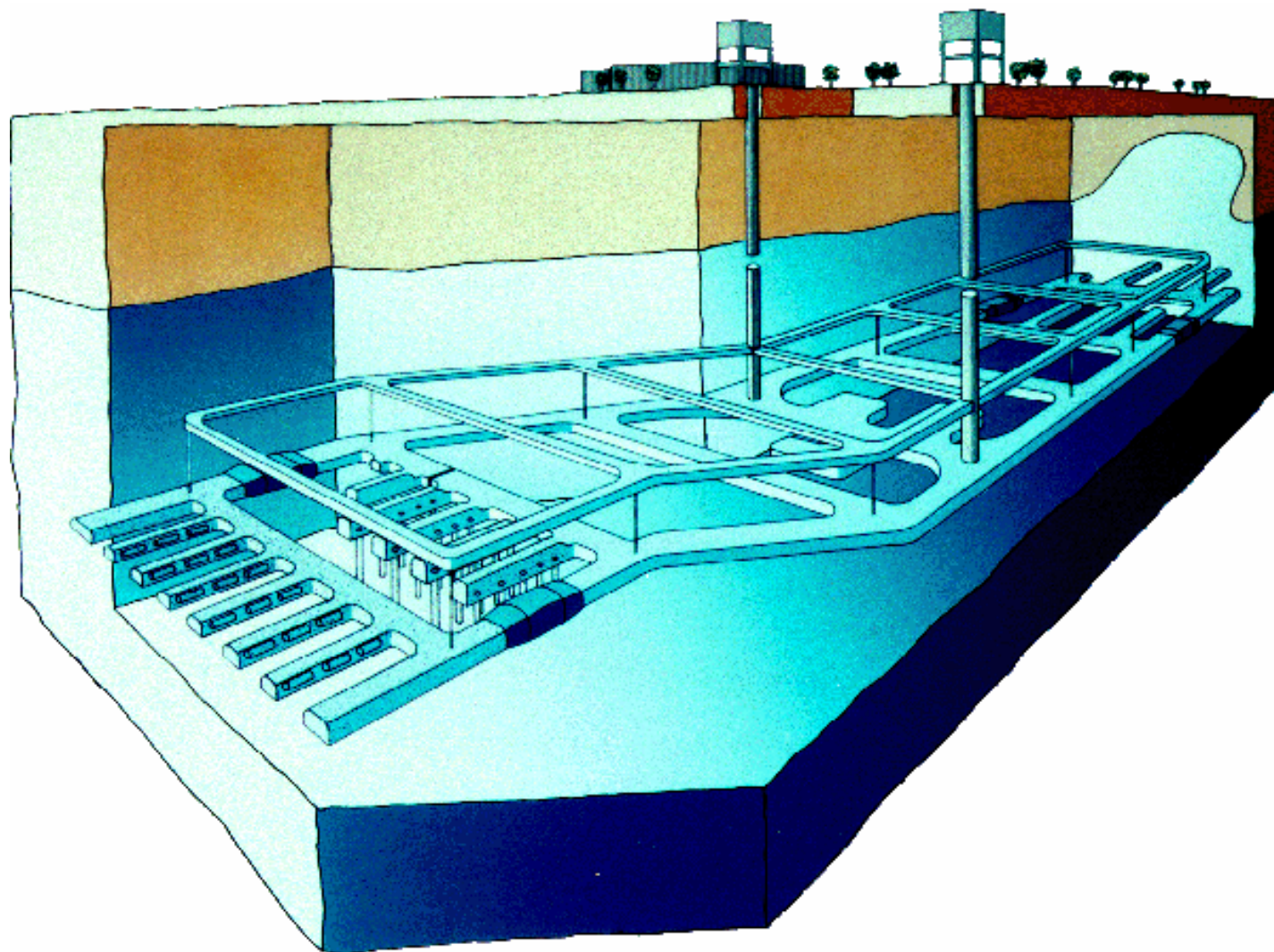
DBETEC

DBE 

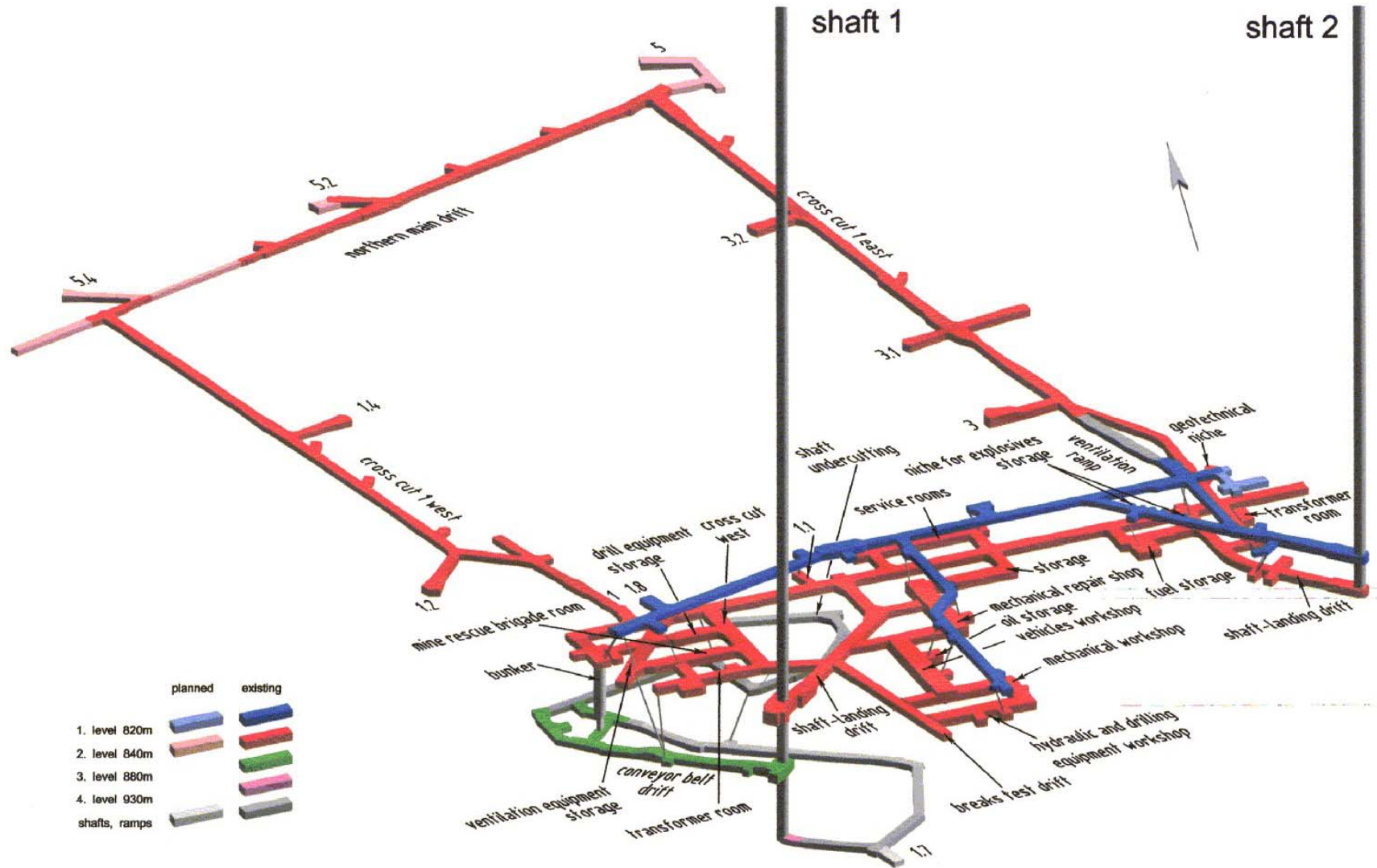
Gorleben



Gorleben



Gorleben



Gorleben



Gorleben



Gorleben



Gorleben



Gorleben



Gorleben



Peine Headquarters



DBE-TEC

DBE 

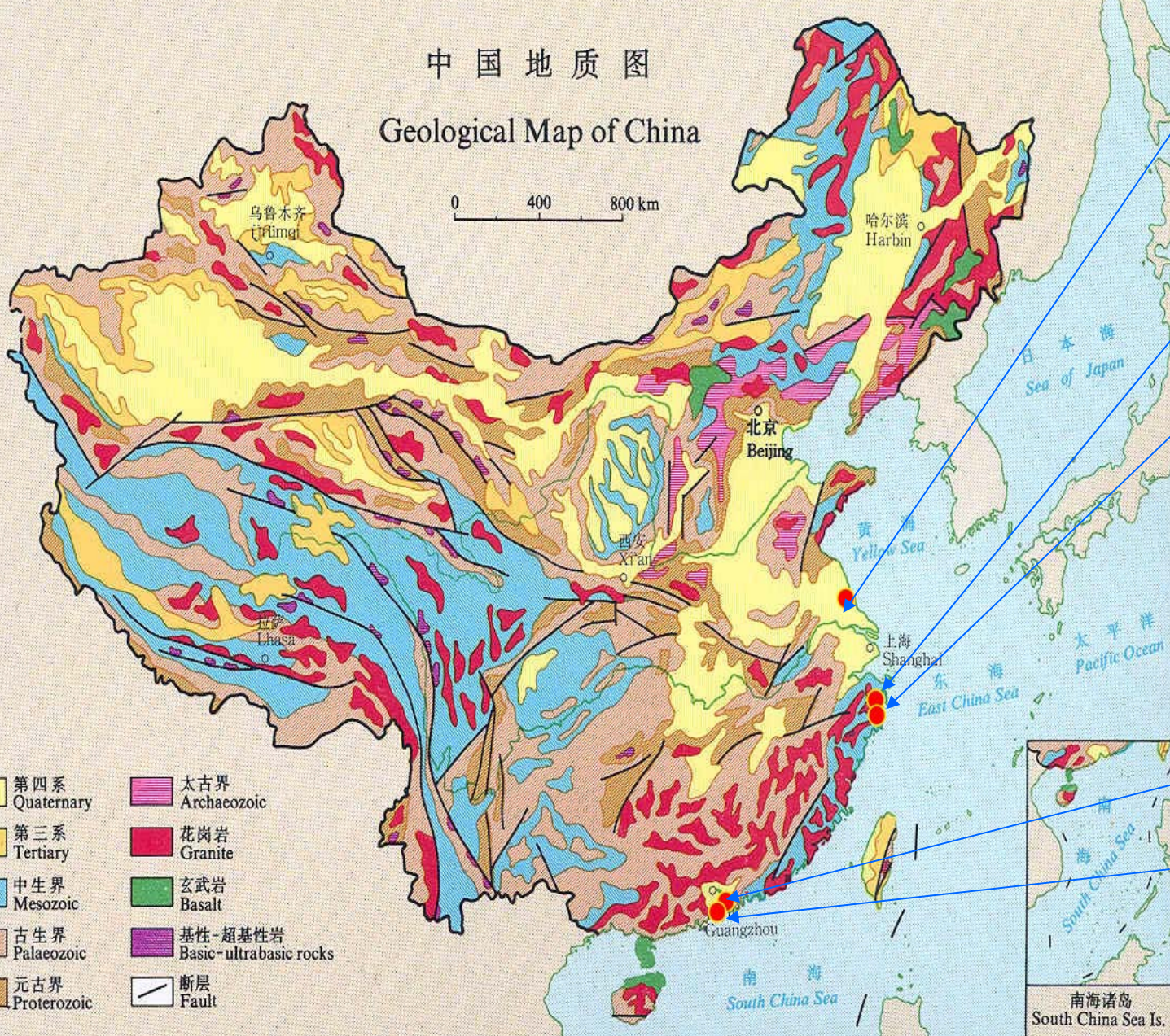
Deep Geological Disposal of High Level Radioactive Waste in China: Latest Progress by 2007

WANG, Ju (王驹)

Beijing Research Institute of Uranium Geology,
China National Nuclear Corporation

中国地质图 Geological Map of China

0 400 800 km



Tianwan



Qinshan 3



Qinshan 1, 2



Lin'ao



Daya Bay

**Nuclear power plants in Chinese Mainland in 2006:
10 reactors in operation, 1 in test operation, 4 under construction**

By 2020

- **Installed capacity of NPP: 40 GW**
18 GW under construction
- **30 more 1000 MW NPPs will be built**
in Chinese Main Land
- **Cost: 50 billion USD**
- **Right now, Sanmen NPP, Lin'ao (2nd phase),**
and Qinshan Phase 2 (2 new reactors) are
under construction

- **By 2010** **1,000 MTU from PWR**
- **By 2020** **10,300 MTU** (7000 from PWR, 3300 from CANDU)
- **After 2020** **1,000 MTU/year**

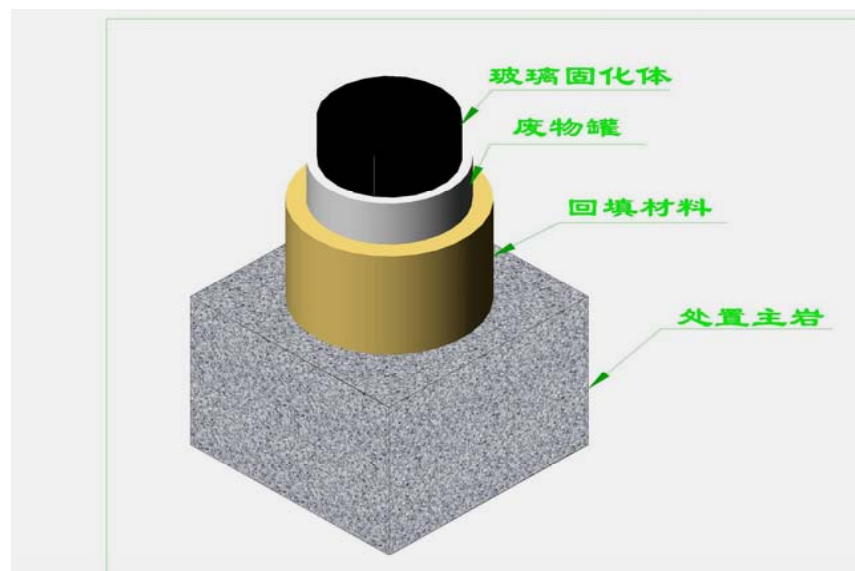
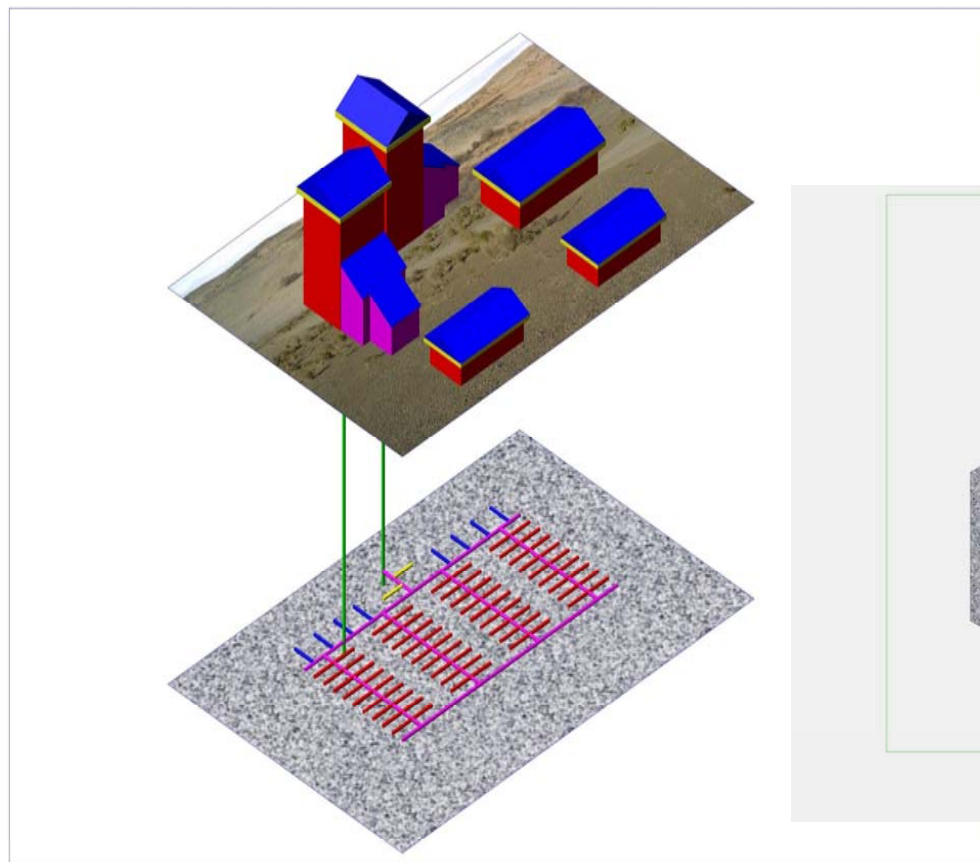
based on that the installed nuclear power capacity in China will be

20,000 MW in 2010

40,000 MW in 2020

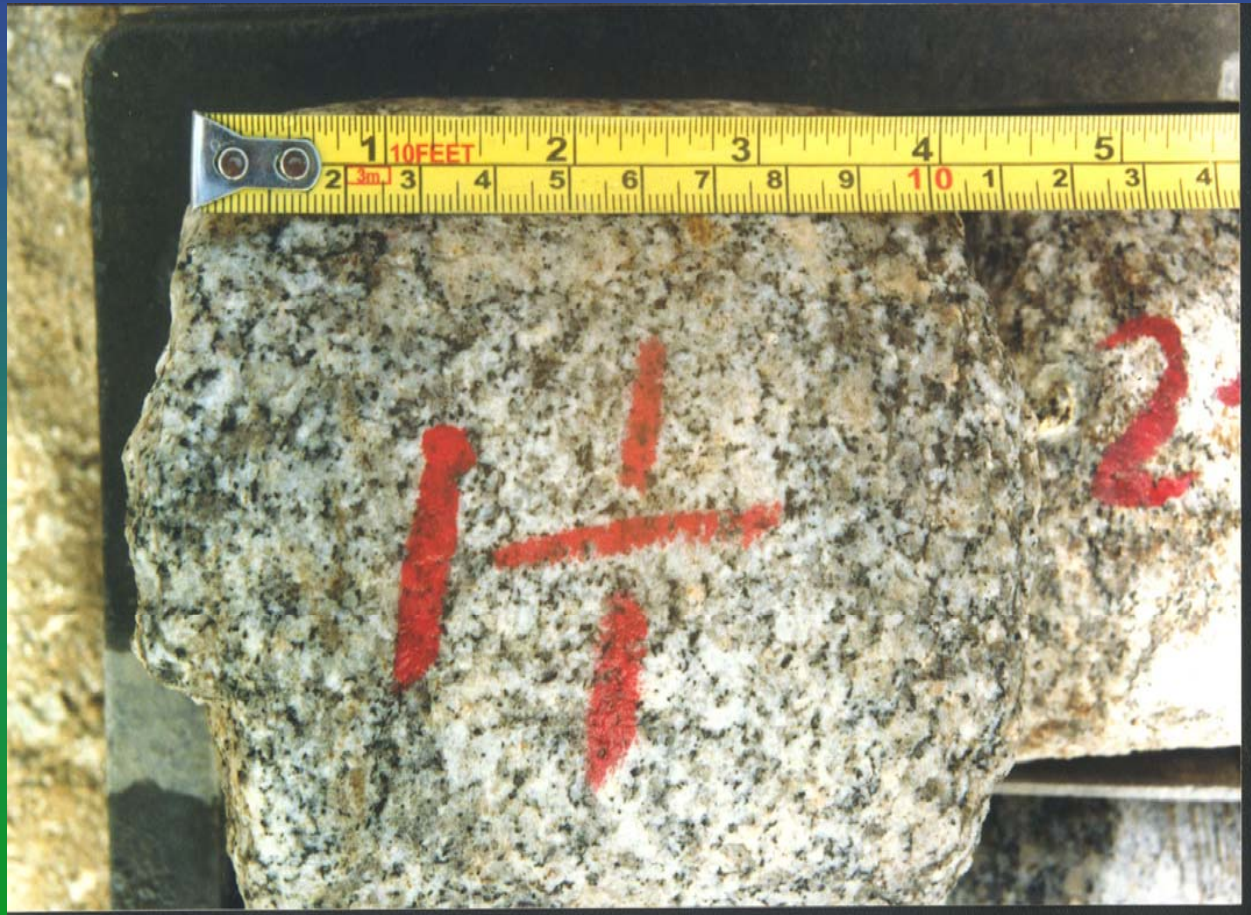
Basic Policy for HLW Disposal

- **spent fuel should be reprocessed**
- **waste form: vitrified waste, CANDU SF**
- **deep geological repository**
- **host rock: granite**
- **repository concept: shaft--tunnel-disposal hole, located in saturated zone**



Host rock for China's HLW

granite



国家环境保护总局
国家核安全局
Regulatory body

国家原子能机构
Project and fund control

State Environment
Protection Admin.
(SEPA)

National Nuclear
Safety Admin.
(NNSA)

China Atomic Energy
Authority
(CAEA)

China National Nuclear Corporation (CNNC)
-- possible implementation body

中国核工业集团公司

4 Lead Institutes

- **Beijing Research Institute of Uranium Geology (BRIUG)**
- **China Institute of Atomic Energy**
- **China Institute for Radiation Protection**
- **Beijing Institute of Nuclear Engineering**

- **other institutes and Universities**

The Law of Prevention of Radioactive Pollution entered into force:

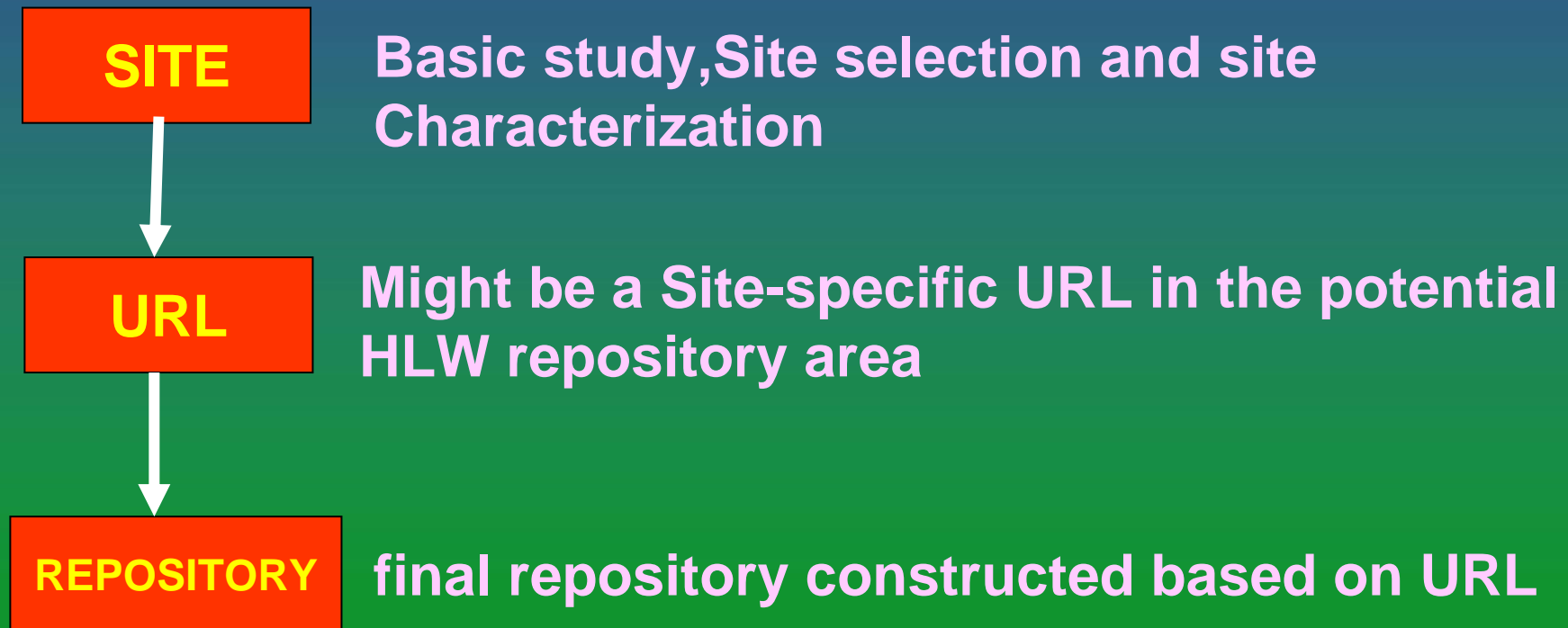
“ the high level radioactive waste and alpha-bearing waste should be disposed of in centralized deep geological repositories”

- jointly published by China Atomic Energy Authority
Ministry of Sci&Tech., State Environment Protection
Administration
- published in Feb. 2006
- First government document on HLW disposal
- the R&D on HLW in China entered into a new stage

Objectives of HLW disposal Program

- To select an site with stable geological and suitable social-economical conditions
- To build a geological repository in the middle of 21st century
- To protect the public health and the environment from the unacceptable harm from HLW through the containment, retardation by engineered and natural barriers.

3-step strategy (“三部曲”战略)



Long term plan for HLW disposal

- 2006--2020 :
Basic Study and Site Selection
- 2020--2040
Underground Research Laboratory
- 2040--middle of 21st Century
Repository

- Strategies, planning and management
- Engineering Design
- Site selection and site characterization
- Radiochemical studies for disposal
- Safety assessment

Studies on strategy, regulation, plan and standards

- **studies on disposal strategies**
- **establishment of framework of standards**
- **compilation of R&D network**
- **framework for management system**
- **comparison among geological disposal, P&T and long-term storage**

Studies on site selection and site evaluation

- deep geological environment of Beishan site
- regional geology of Beishan site
- hydrogeology of Beishan site
- geophysical survey
- another pre-selected region
- technologies for site evaluation
- digital geoscience database
- facility establishment for site evaluation

Focus: Beishan granite site

Studies on Engineering design

- **conceptual design of URL,**
- **conception design of repository**
- **engineered barrier system study**
- **bentonite study**
- **facility establishment for engineering design**

Radiochemical studies for disposal

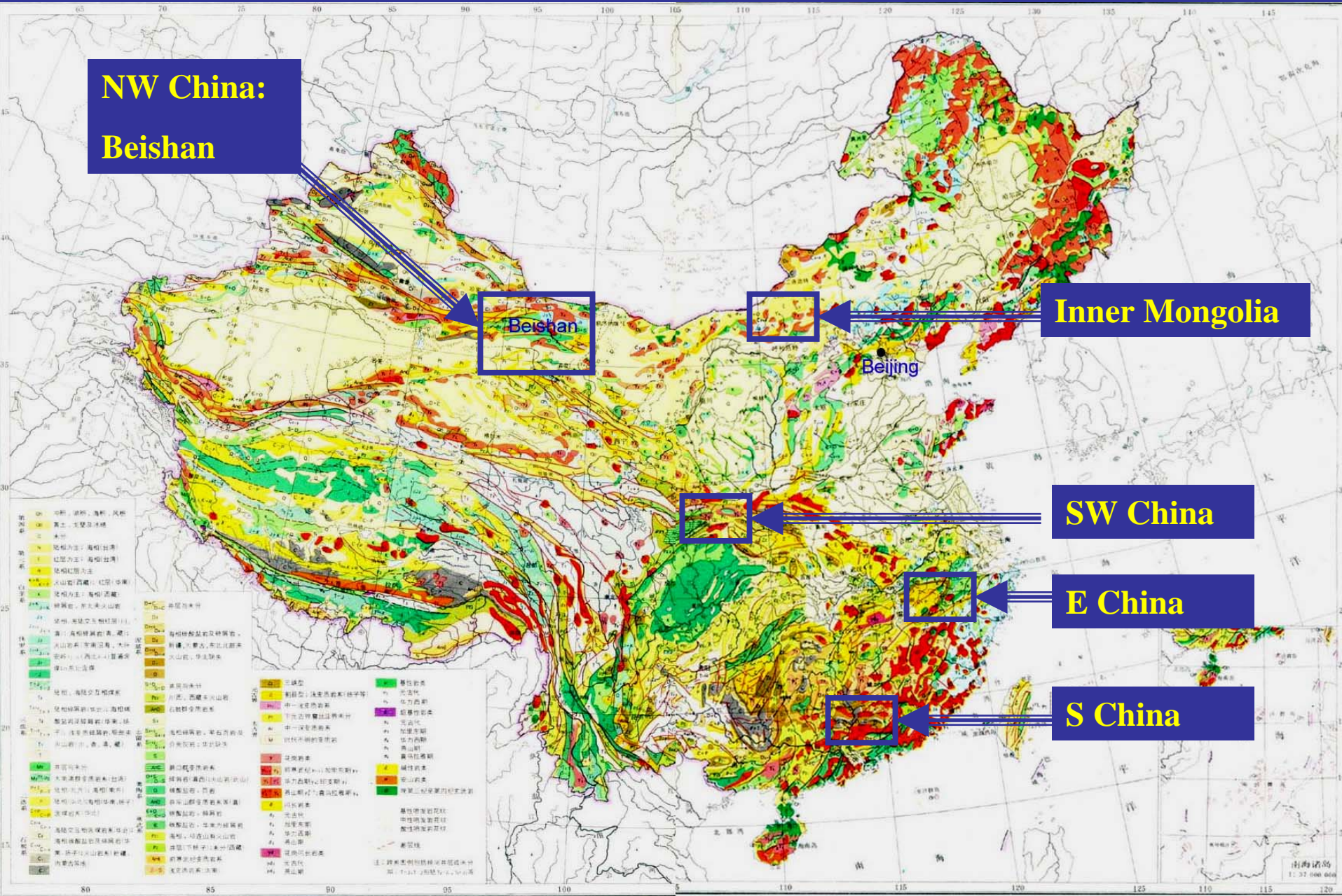
- **performance of glasses, containers**
- **chemical behavior of radionuclides under simulated repository conditions**
- **migration behavior of radionuclides**
- **database for radionuclide migration**
- **facility construction for radionuclide migration study**

Studies on safety assessment

- **methodologies for safety assessment**
- **study on safety standards**
- **safety cases**
- **studies of computer codes for SA**
- **study platform for SA**

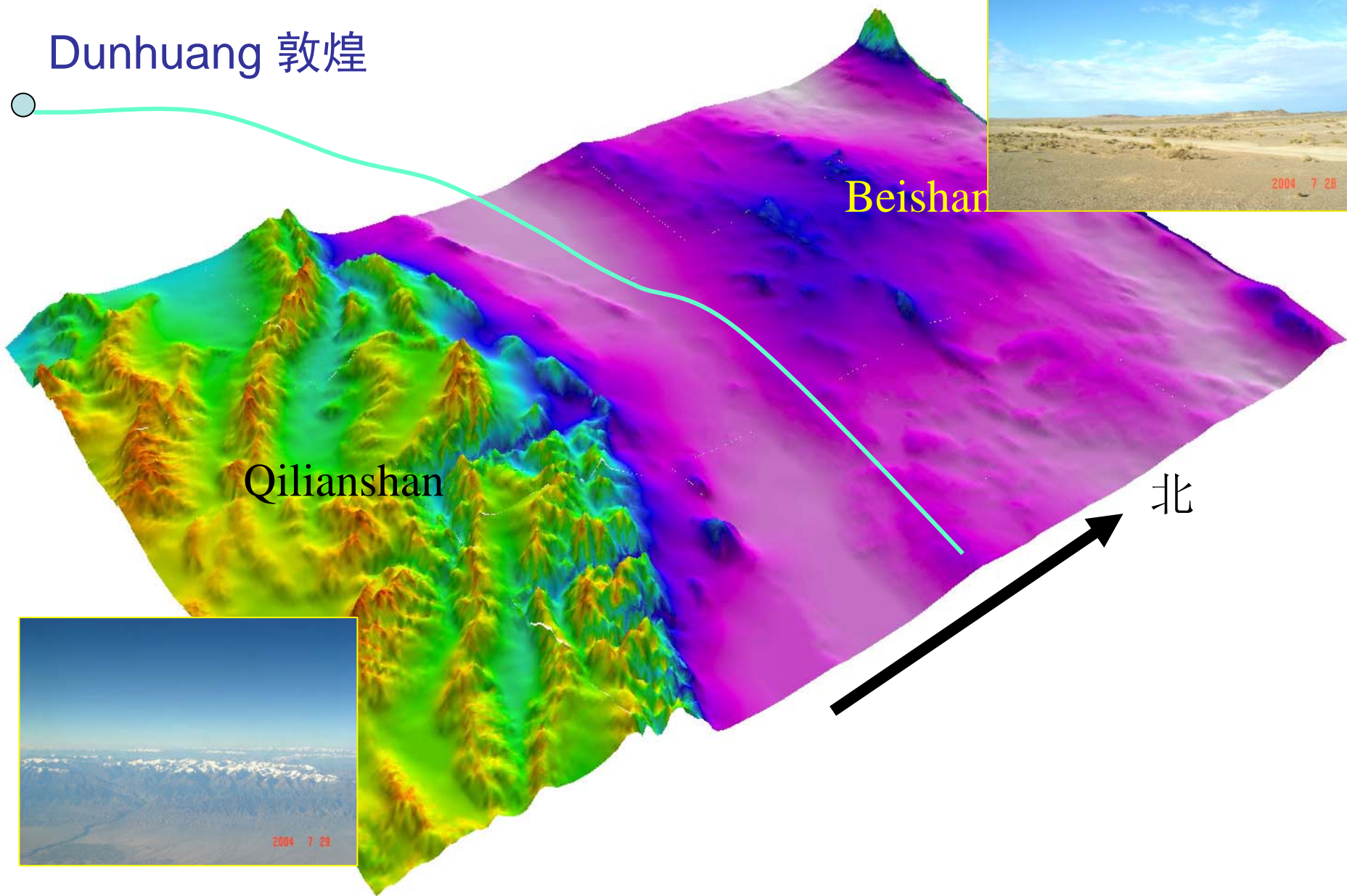
- **Site selection and Site characterization: since 1986**
- **Backfill material study: Bentonite from Inner Mongolia**
- **migration behavior of radionuclide**
- **Natural analogue**

Major activities: Site selection and site characterization



5 Pre-selected regions for China's HLW repository since 1986

Dunhuang 敦煌



3-D DEM of Beishan and Qilianshan

Beishan site 北山场址

- in Gansu (甘肃) province, NW China
- the most potential area for China's repository
- Gobi desert area
- low population density
- low precipitation : 60--80 mm/a
- high evaporation: 2900-3200 mm/a
- no economical prospect
- no important mineral resources
- convenient transportation
- stable crust
- favorable hydrogeological conditions
- host rock: granite and diorite

Beishan site 北山场址





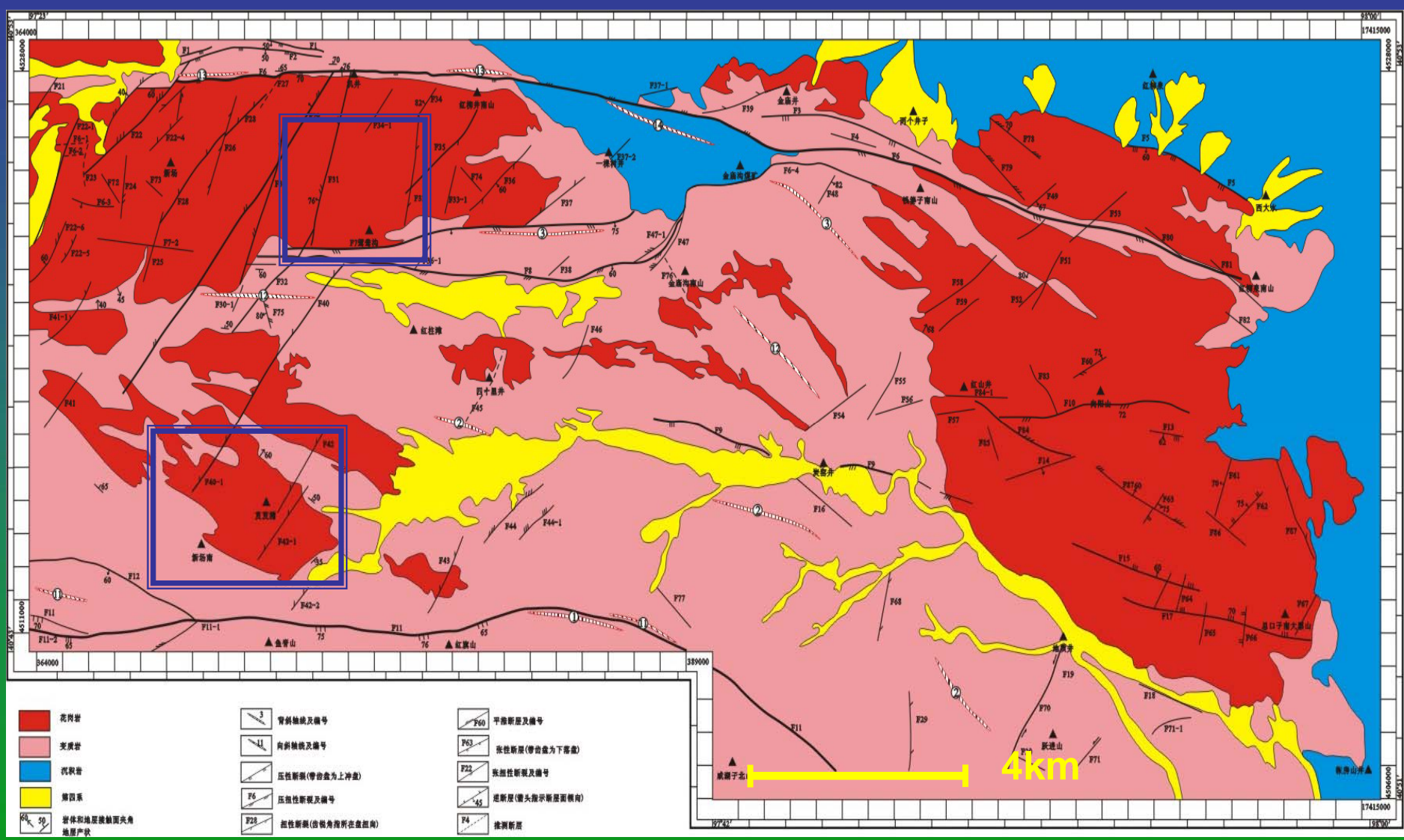
Landscape of Beishan site

Outcrops of granite



Major Activities 2000--2007

- **surface geological, hydrogeological and survey at Jiujing, Yemaquan and Xinchang-xiangyangshan sections**
- **bore hole drilling for BS01, 02, 03, 04**
- **geophysical survey**
- **in situ tests in bore holes**
- **application of remote sensing technology**
- **Regional crust stability study**
- **evaluation of site suitability**

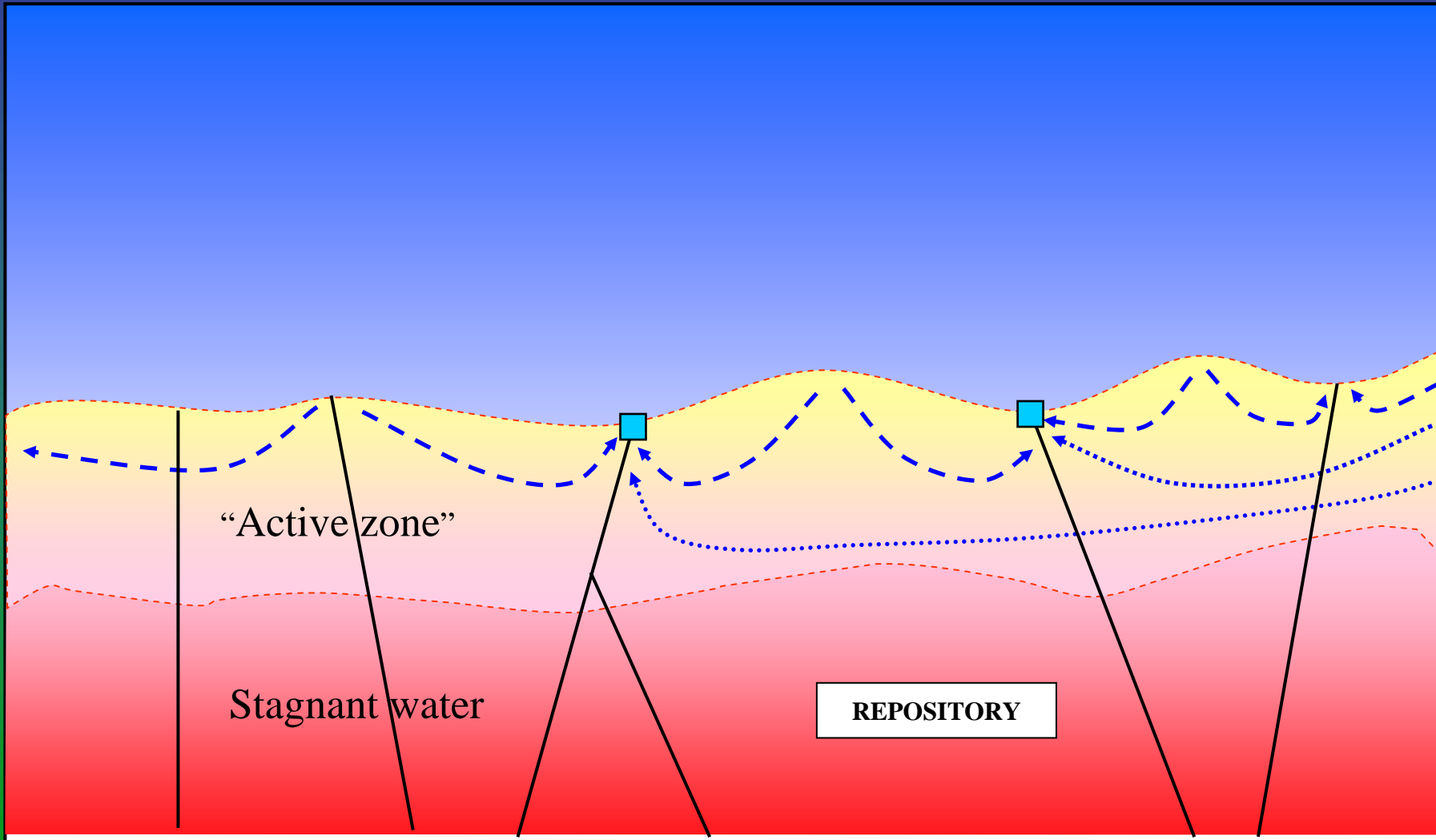




drilling sites at BS01, BS02, BS03, BS04 boreholes



Conceptual model of the groundwater flow



Hydrogeologic Characterization

Dynamics of deep groundwater

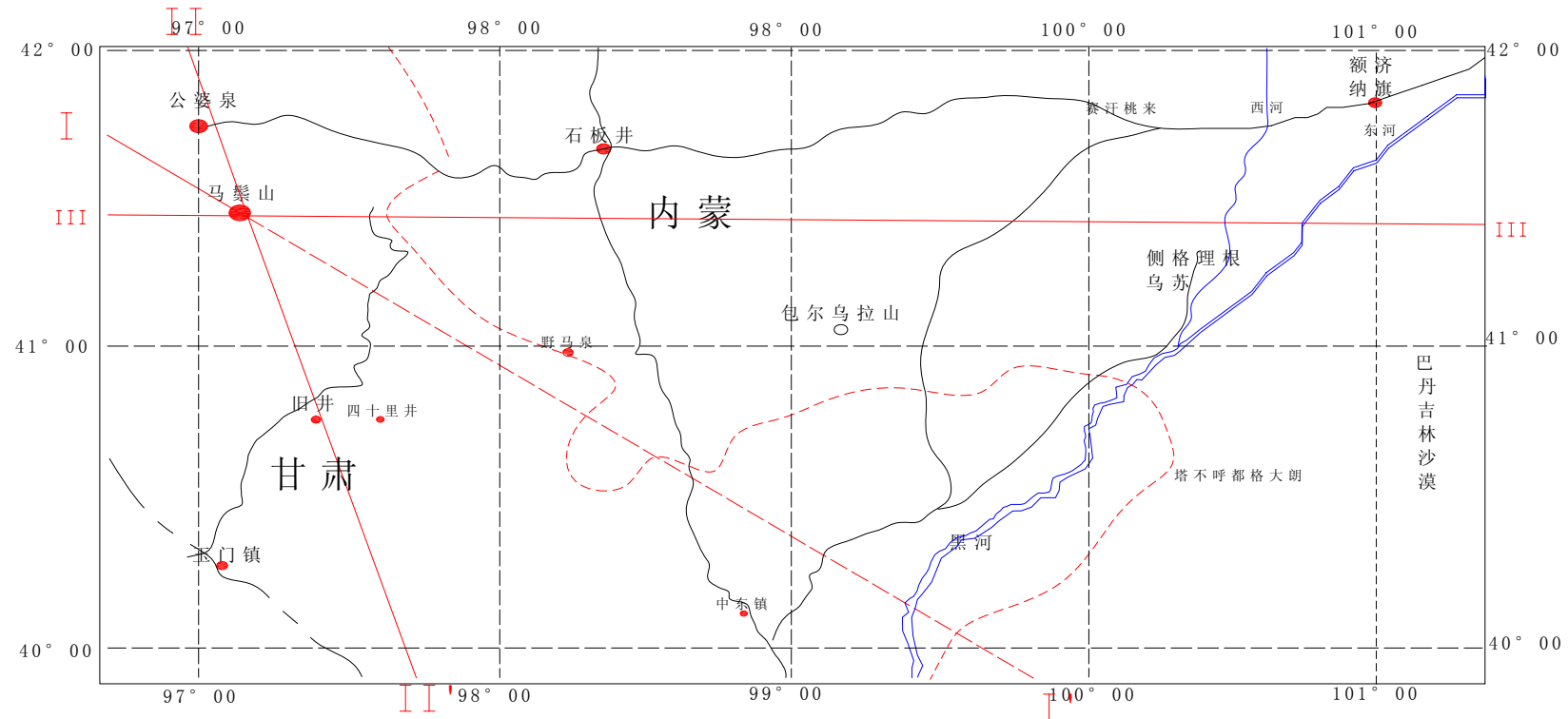
- **low water outflow** 弱含水性
- **low permeability** 低渗透性
- **low velocity** 低流速性

- High salinity 高矿化性,
- slight-alkaline 偏碱性,
- reducing 还原状态

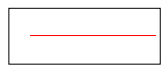
which is not favorable for the transportation of radionuclide

Regional Hydrogeological profile

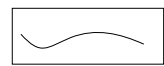
北山地区地理位置示意图



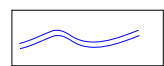
图例



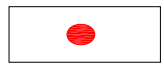
剖面线



普通公路



河流



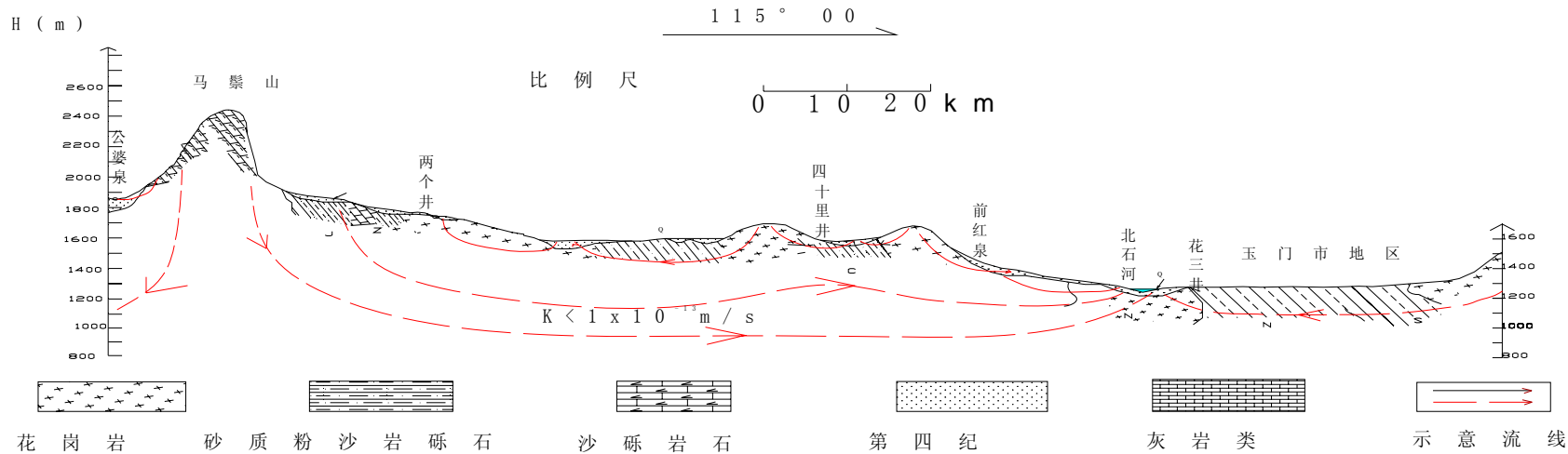
城镇



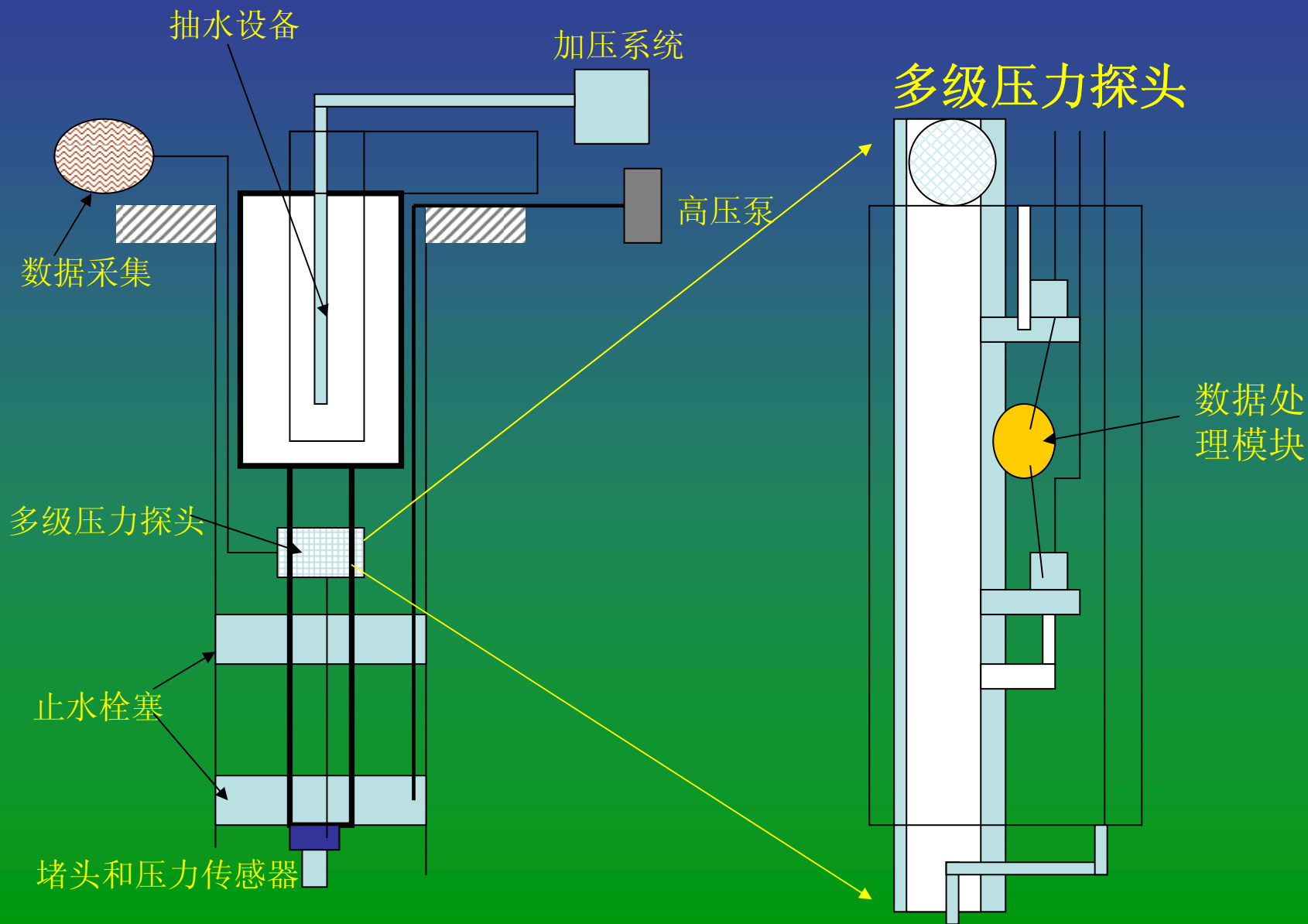
省界

Hydrogeological profile

马鬃山 - - - - 玉门市水文地质剖面示意图 (II - - II')



Double packer system



Double packer test at BS03 in 2005



Double packer system

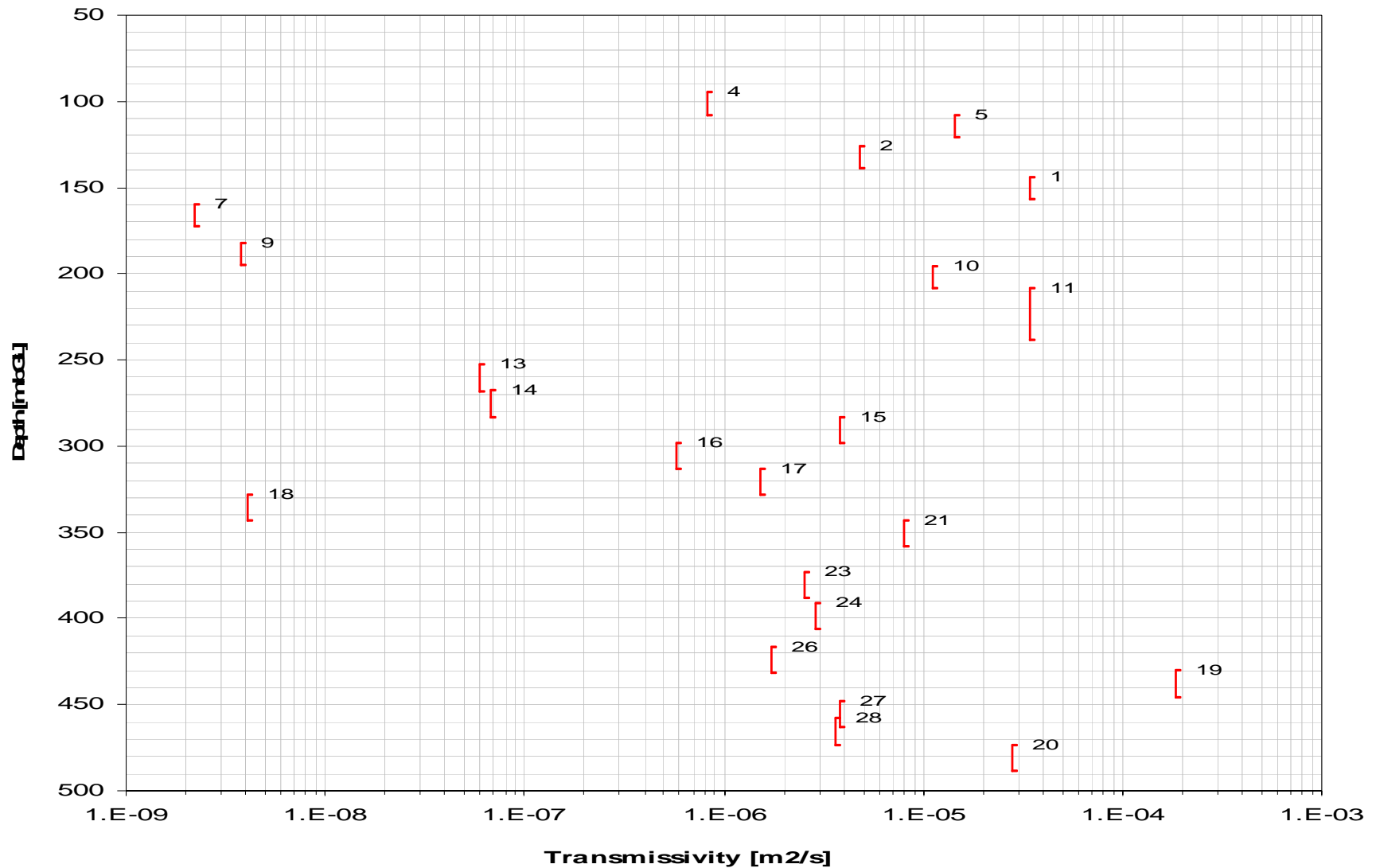


Stator of Moyno Pump



Rotor of Moyno Pump

Transitivity Profile in BS03: 95m-489m,

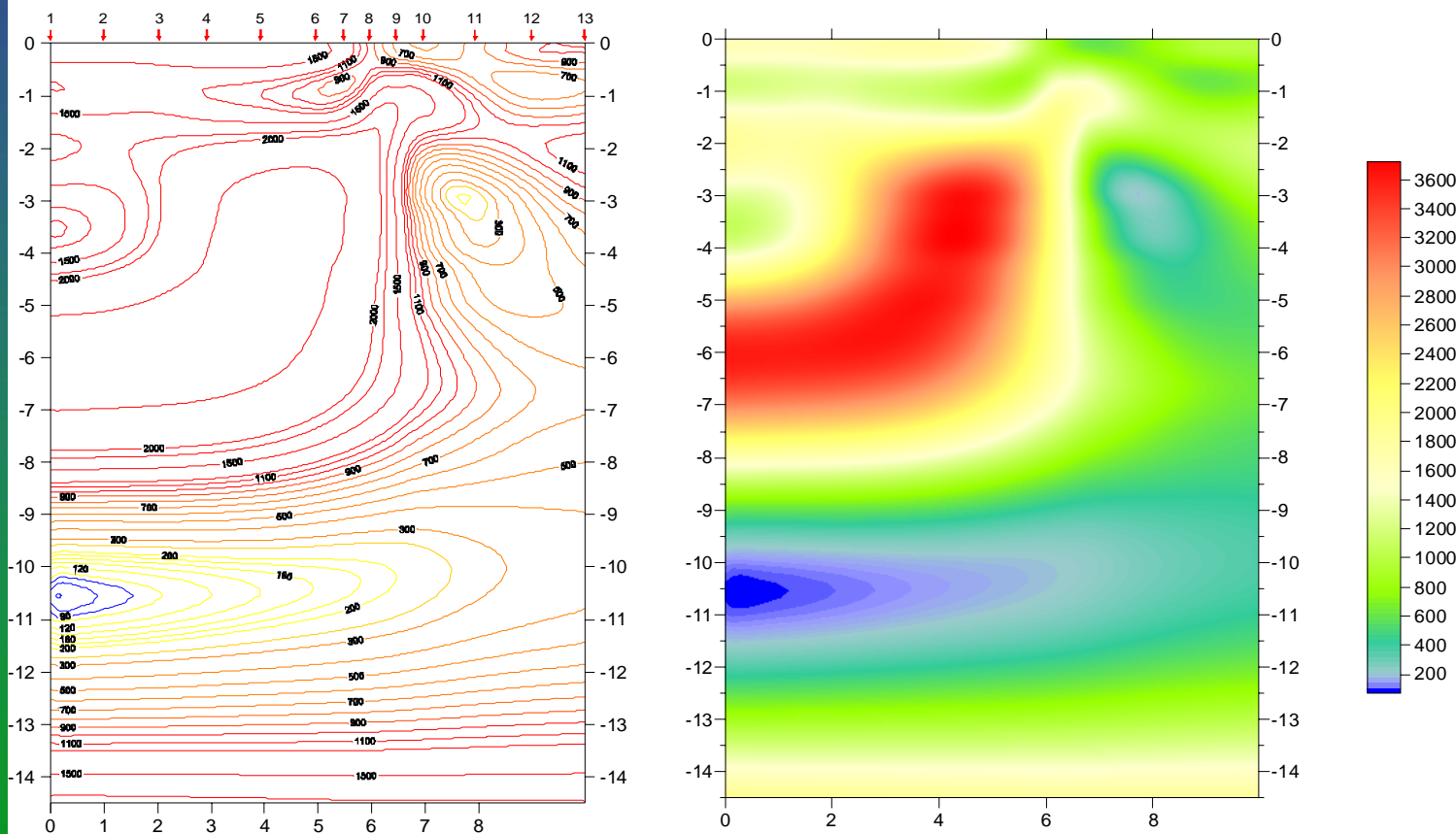


Major geophysical activities

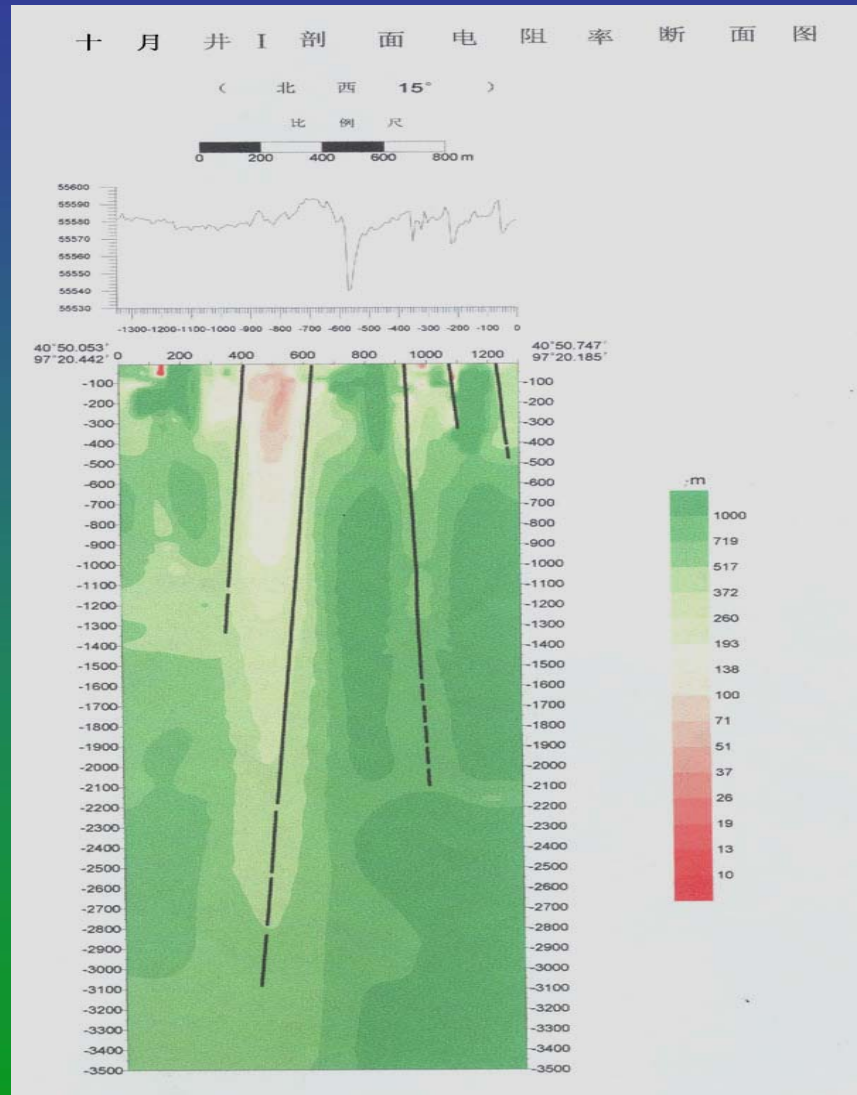
- 1 **Electromagnetic measurement: EH4**
- 2 **high-resolution magnetic survey**
- 3 **Magnetotelluric survey: MT-1**
- 4 **bore hole geophysical logging:
dipole, resistivity, potential,
temperature, gamma etc.**

MT survey in Caishichang

采石场岩体MT结果



EH4 survey in Shiyuejing



3D Electromagnetic Imaging in Beishan

Survey Specification (Sino-Japan cooperation)

◆ Components

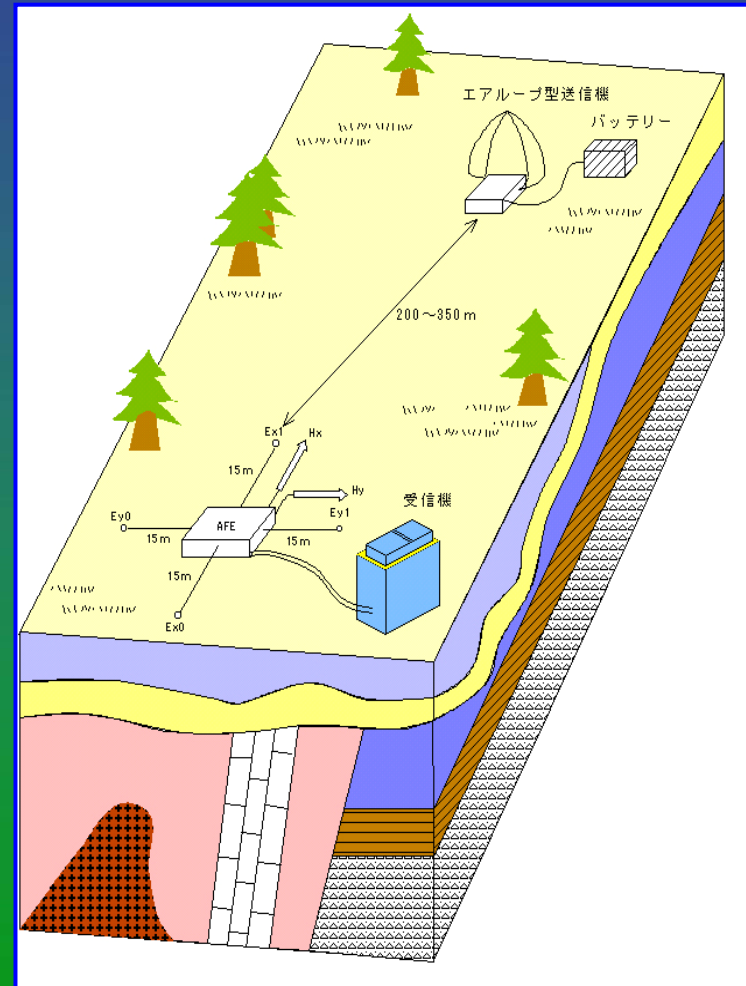
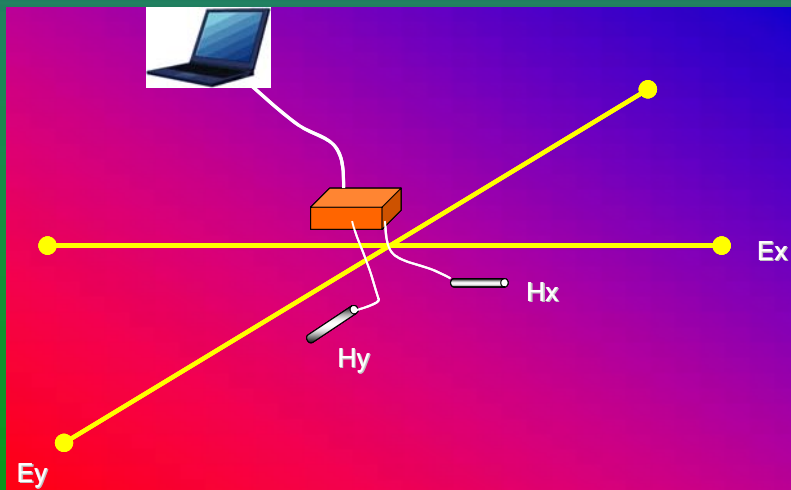
E_x, E_y (=30m)

H_x, H_y

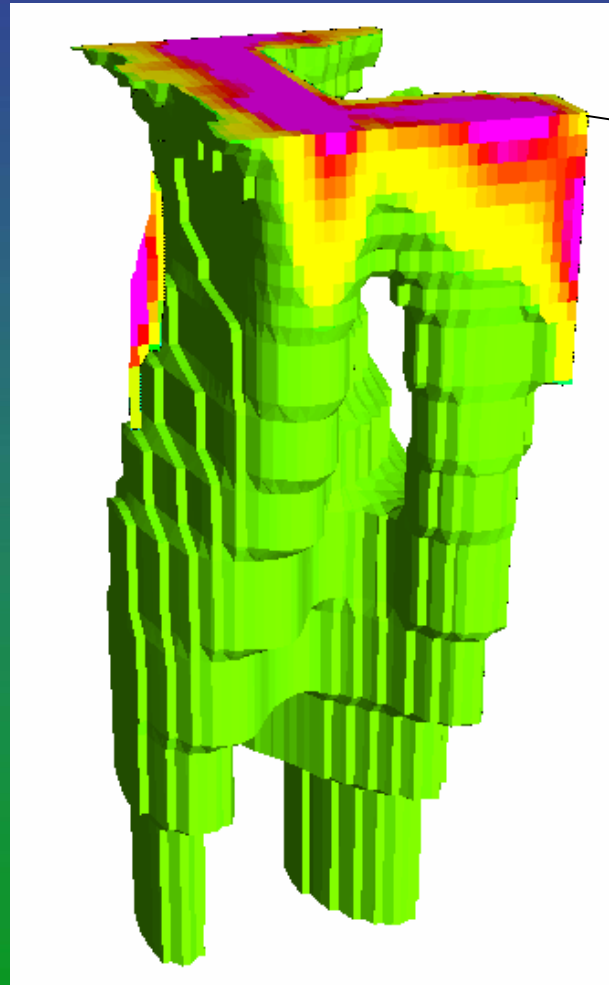
Frequency

100k – 1k Hz : CSMT

1k – 10 Hz : MT



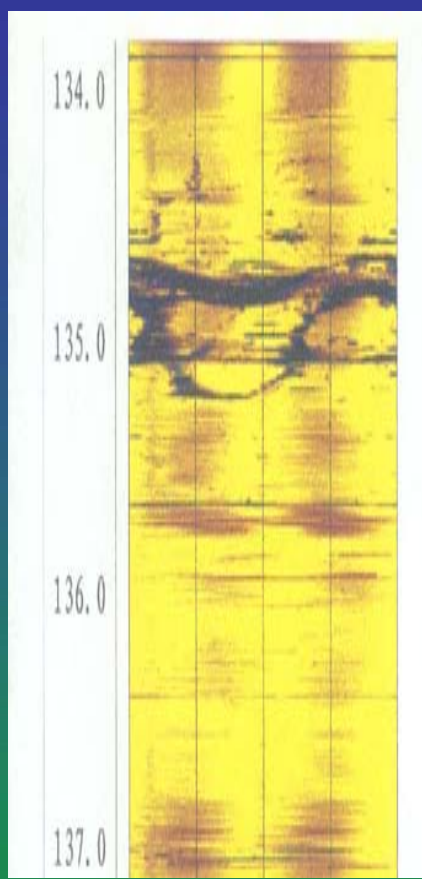
3-D Inversion Results



Blocks with less than $700 \Omega \cdot \text{m}$

Major bore hole survey

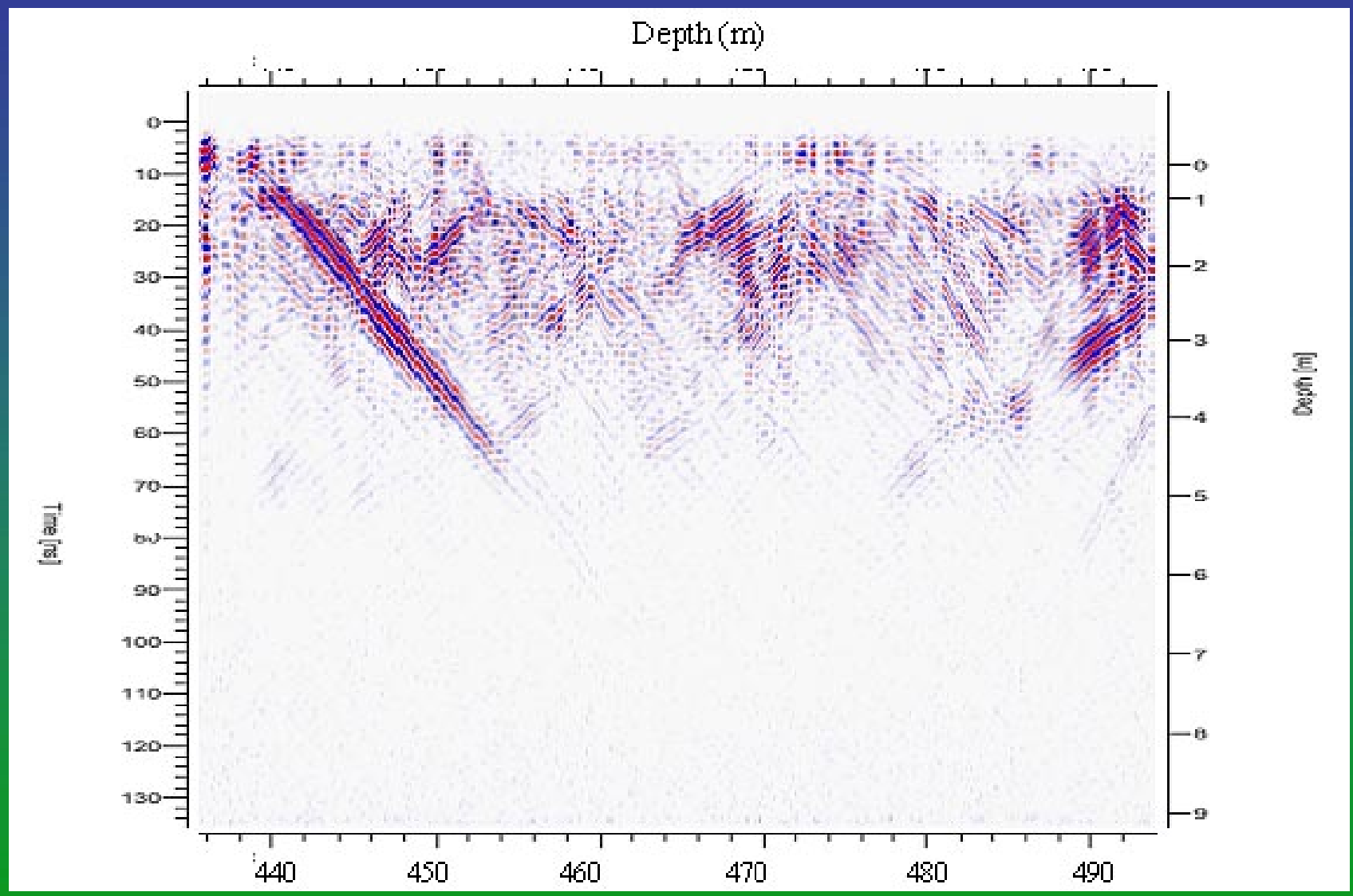
- **Bore hole optical camera**
- **Bore hole acoustic televiewer**
- **Bore hole hydrogeochemical logging**
- **Bore hole radar survey**
- **Bore hole geostress measurement**
- **Vertical seismic profile**



bore hole televiewer survey

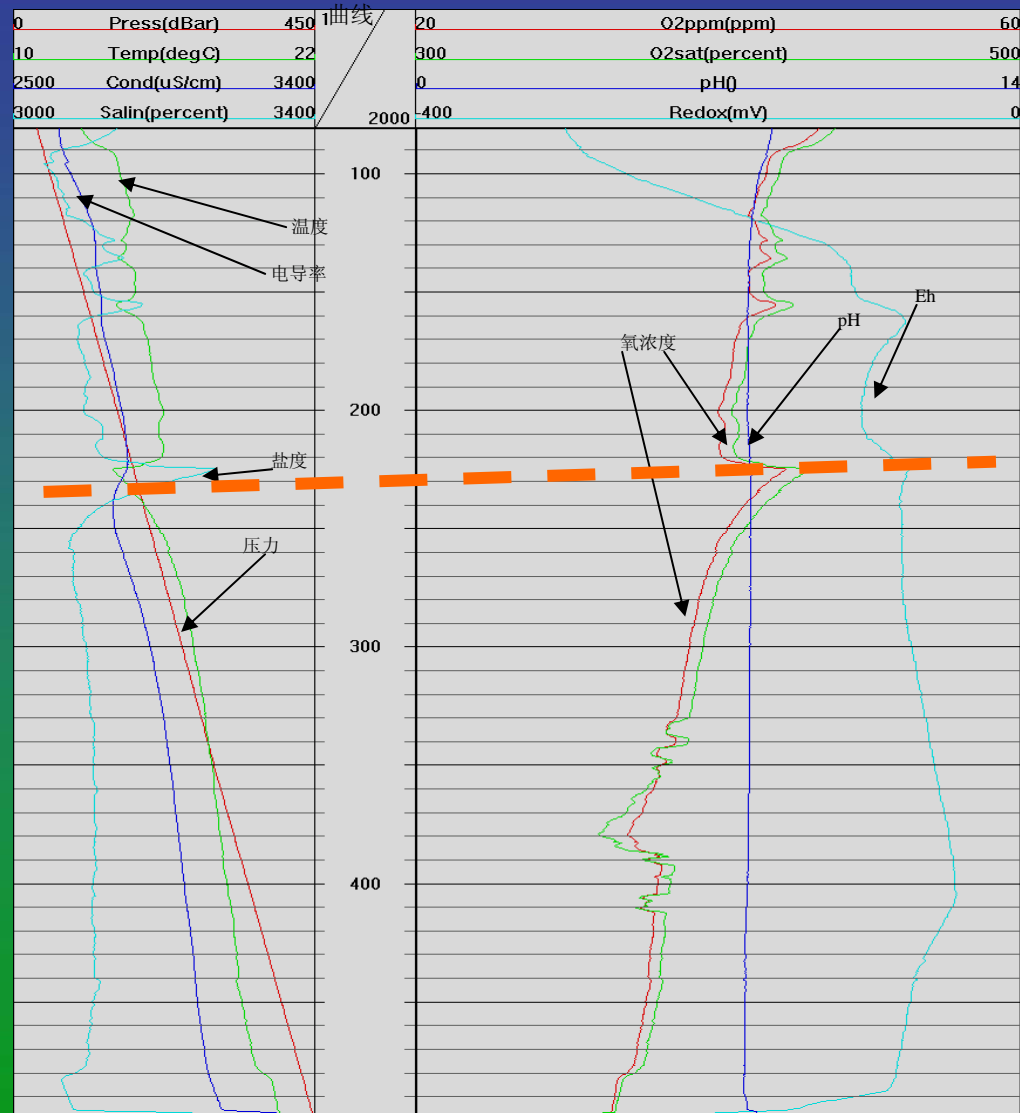
钻孔电视测量

Image of bore hole radar measurement, BS03

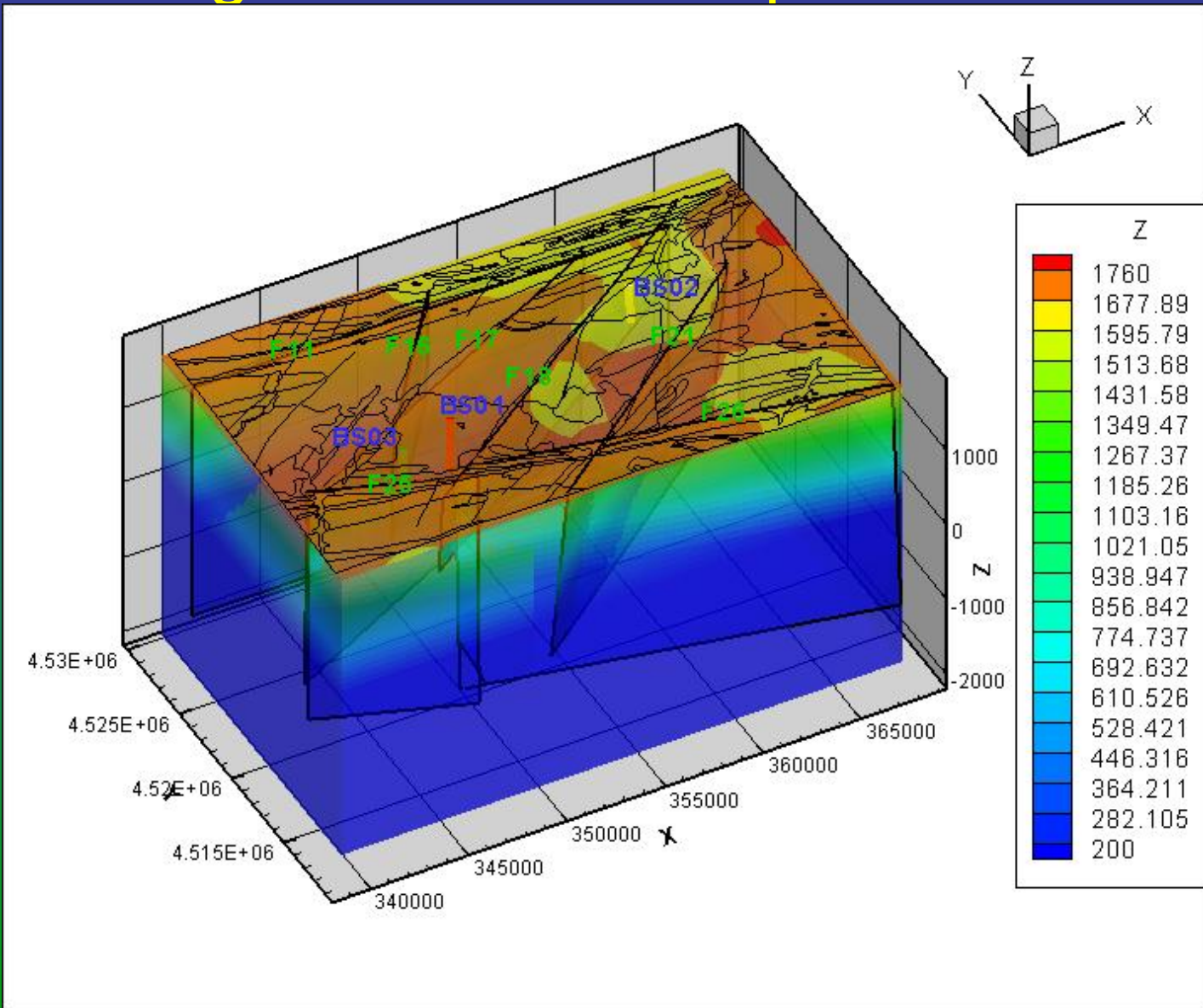


Fluid logging for BS03

图 11-2 BS03多参数水质测量



3D Geological model—cooperation with BGR



Rock mechanical study



BS01, 深度 556-676m, 总长度 19.54m



BS03, 深度 411-420m, 总长度 2.95m

Rock mechanical test : samples before test



直径

---- 5cm

长度

---- 10cm

Rock mechanical test: samples after test

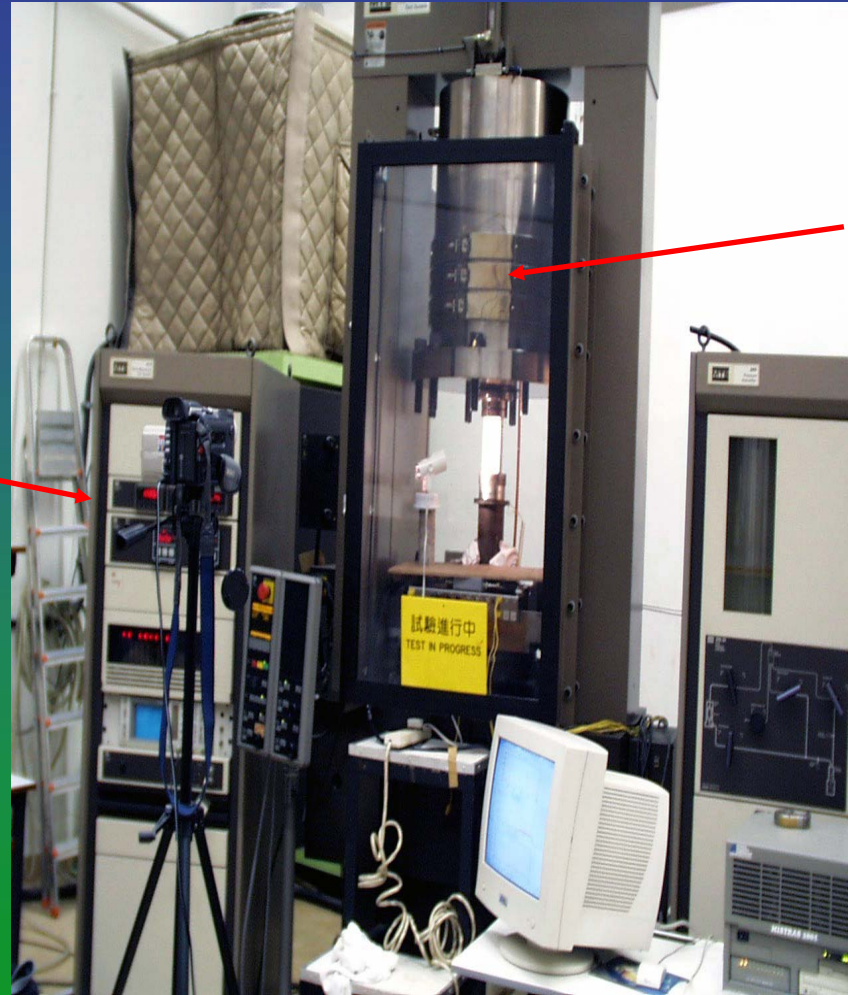


脆性
破坏

MTS 815 岩石力学试验机



高温条件下的试验



温度控制面板

加热条带

样品破坏—sample broken



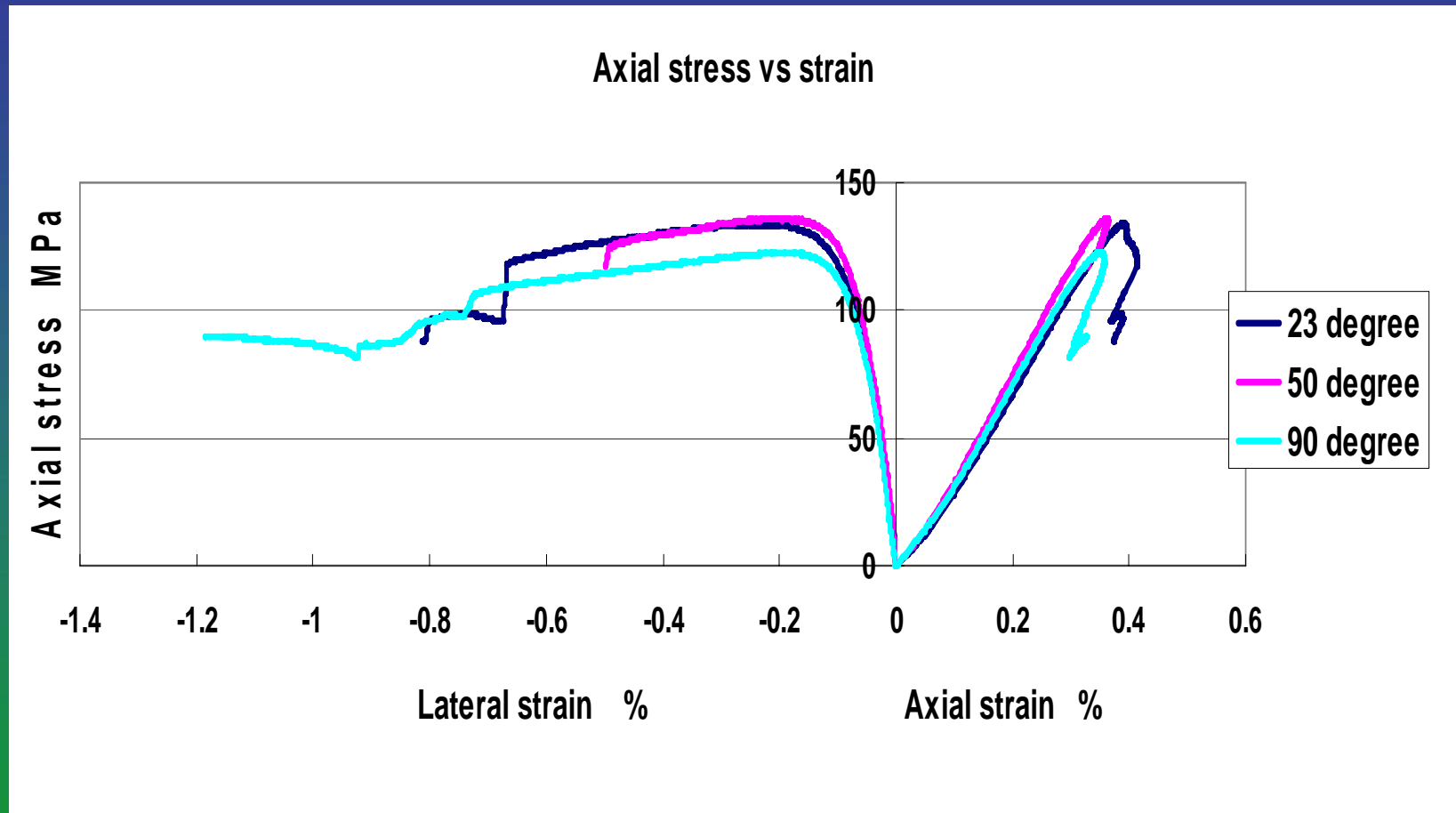
$\Phi 50 \times 125$ mm, 90°C , 恒载223KN,
破坏时响声很大, 岩样分为两大块

2004. 07. 2—07. 20



- Uniaxial stress-strain tests under room temperature, **50**、**90**
- Uniaxial long-term loading test under room temperature, **50**, **90**
- Triaxial stress-strain tests, long term loading tests

Stress-strain test at elevated temperature



- 室温至60度，强度无明显变化
- 60度后，强度明显降低，塑性增大

2. Recent progress in HLW disposal—backfill material

Geological features



The GMZ bentonite deposit is a large-scale deposit. In China, the proved reserves of GMZ deposit ranks the third of its kind and the reserves of sodium bentonite ranks the second.

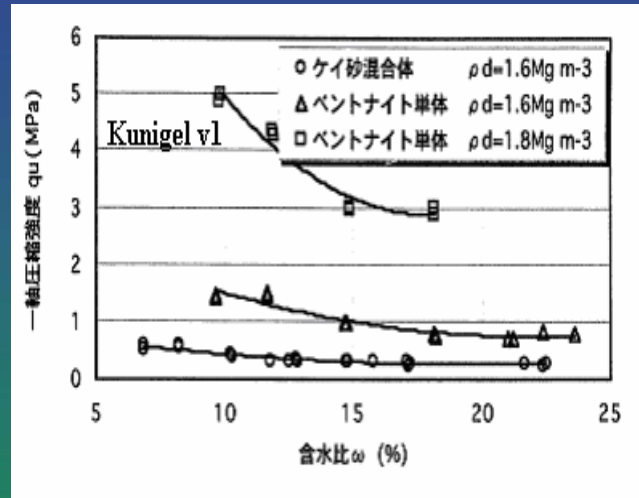
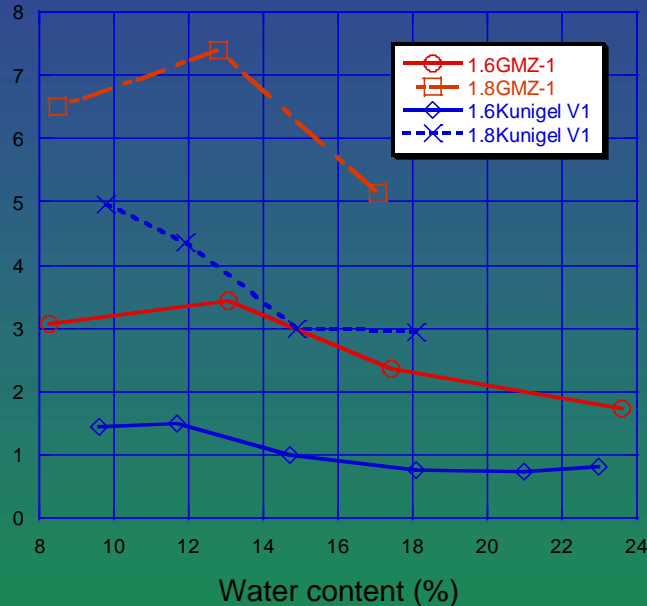
GMZ deposit

The reserves in GMZ is about 160 million tons with 120 million tons Na-bentonite reserves.



Mechanical characteristics of Gaomiaozi bentonite

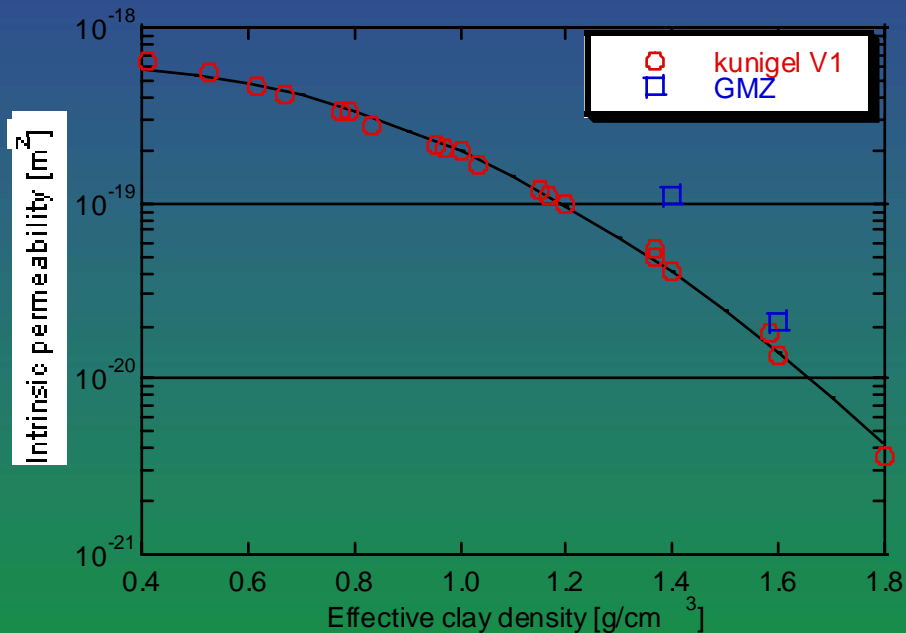
1-axial compressive strength [MPa]



GMZ-1: 2 times of Kunigel V1(1.6g/cm³);
50% higher than Kunigel V1 (1.8g/cm³);

The trend of change for GMZ-1 is a little different from that of Kunigel V1. There is a peak point of GMZ-1 curve for both densities.

Hydraulic property of Gaomiaozi bentonite

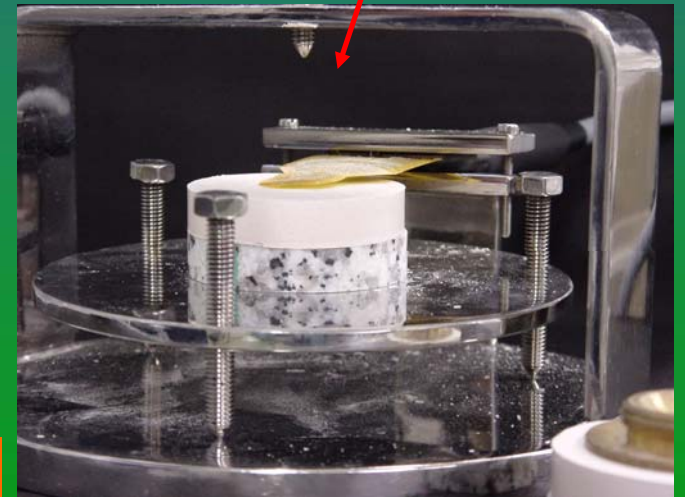
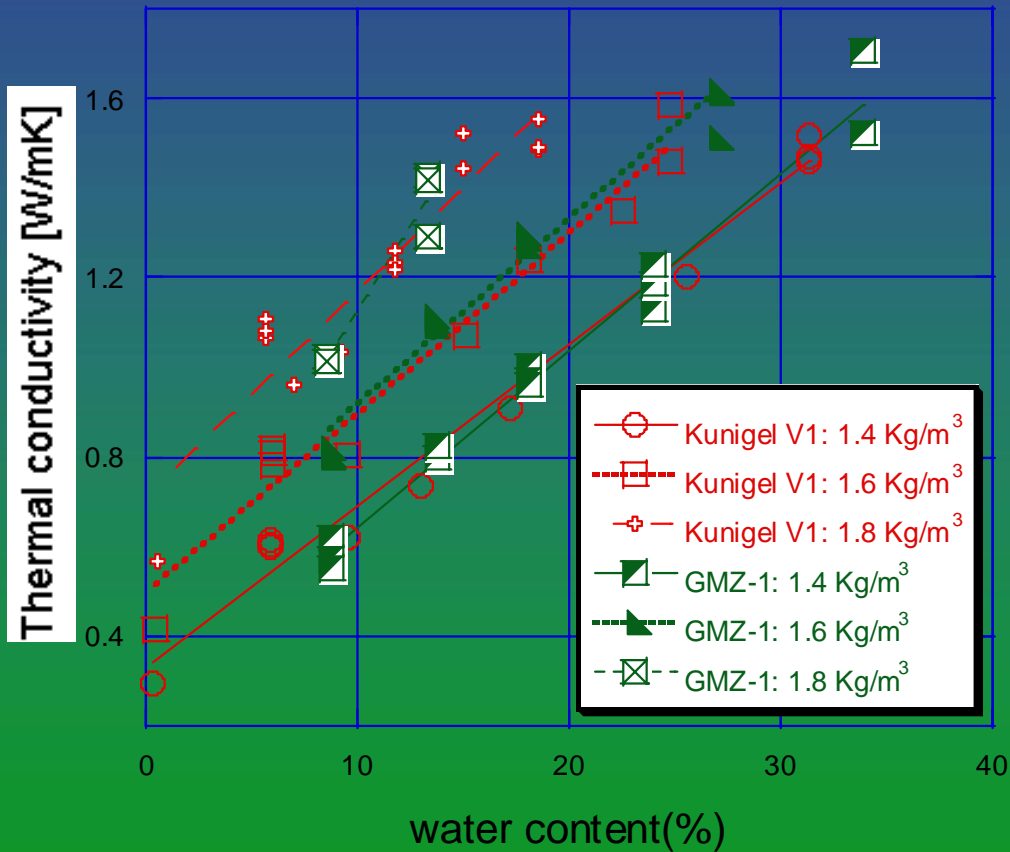


The intrinsic permeability: GMZ-1 > Kunigel V1. higher content of Na-montmorillonite in Kunigel V1.

Due to a little difference of experimental condition (i.e. pressure of compressed air), it is possible that data obtained to some extent didn't reveal the fact of difference.

Thermal property of Gaomiaozi bentonite

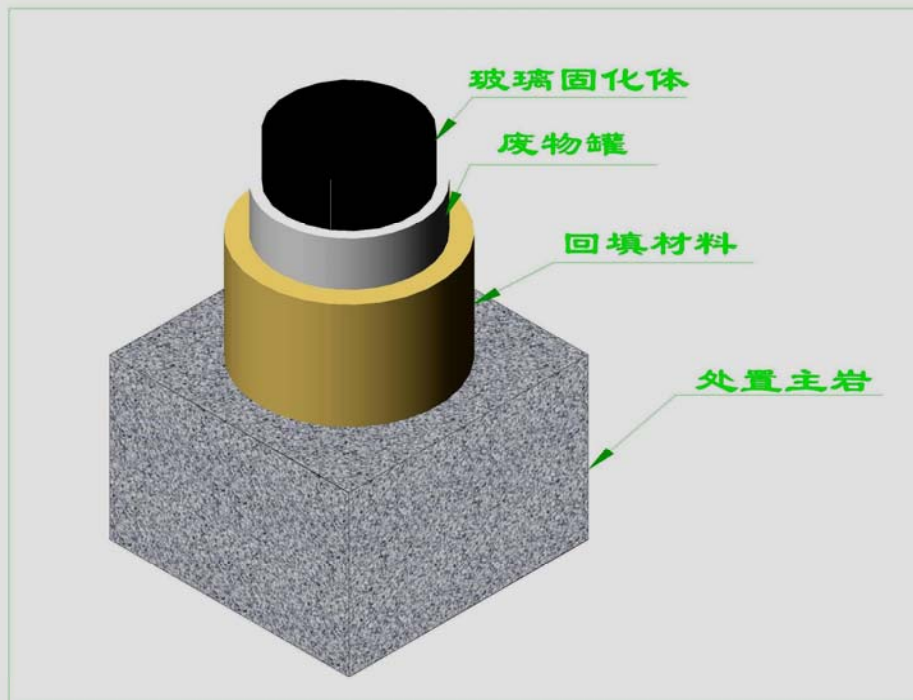
Thermal conductivity Vs water content



Thermal conductivity : no significant difference

Radionuclide used

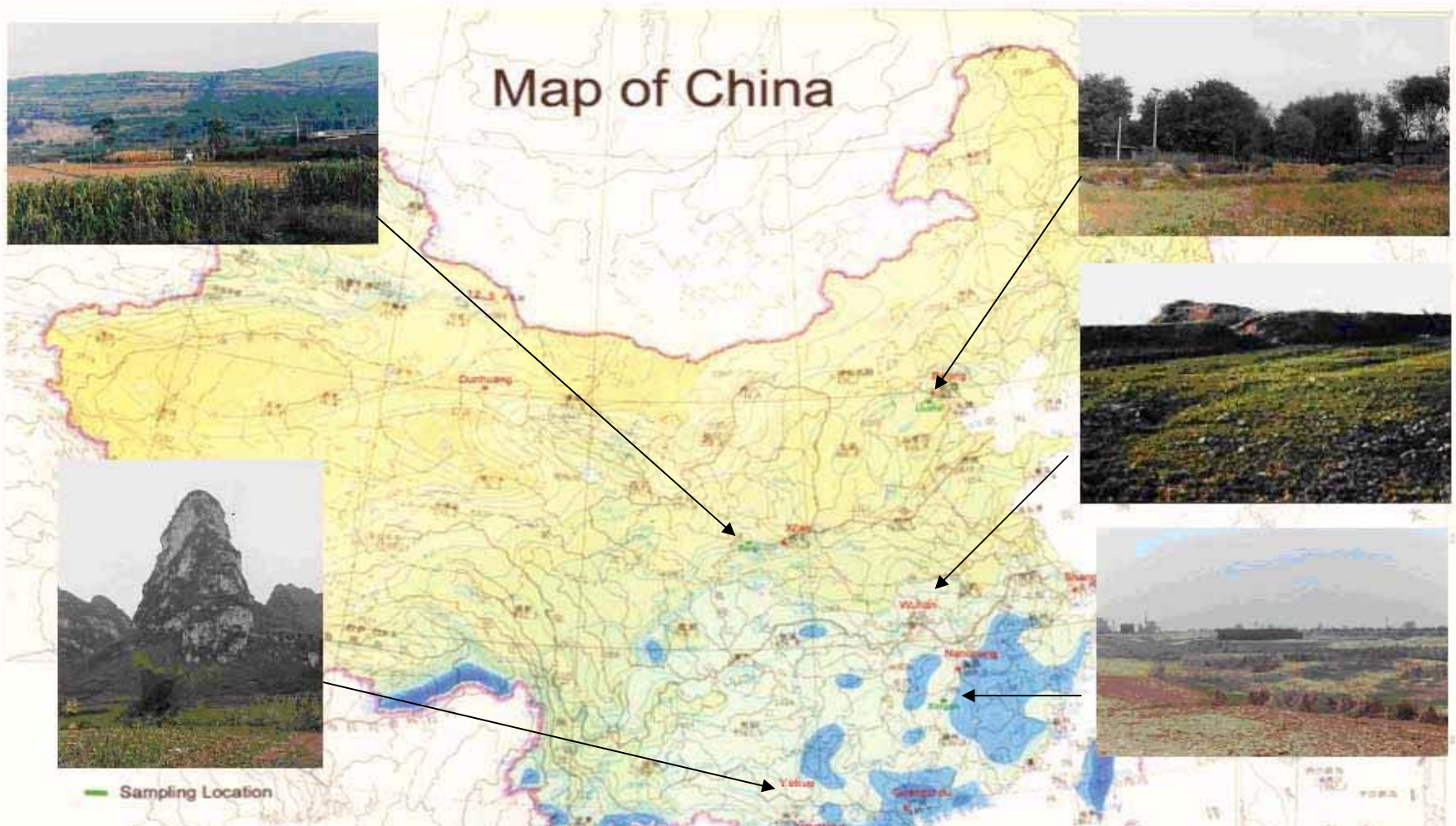
Np-237,
Pu-239,
Tc-99,
Am-241
Sr-85, 89, 90
Cs-134,
I-129 等,



Media used:

- **Bentonite-膨润土**
- **Stibnite 辉锑矿**
- **Active carbone of apricot shell杏壳活性炭**
- **Granite, Beishan granite**
- **Altered granite**
- **fracture**

Major Activities: analog study



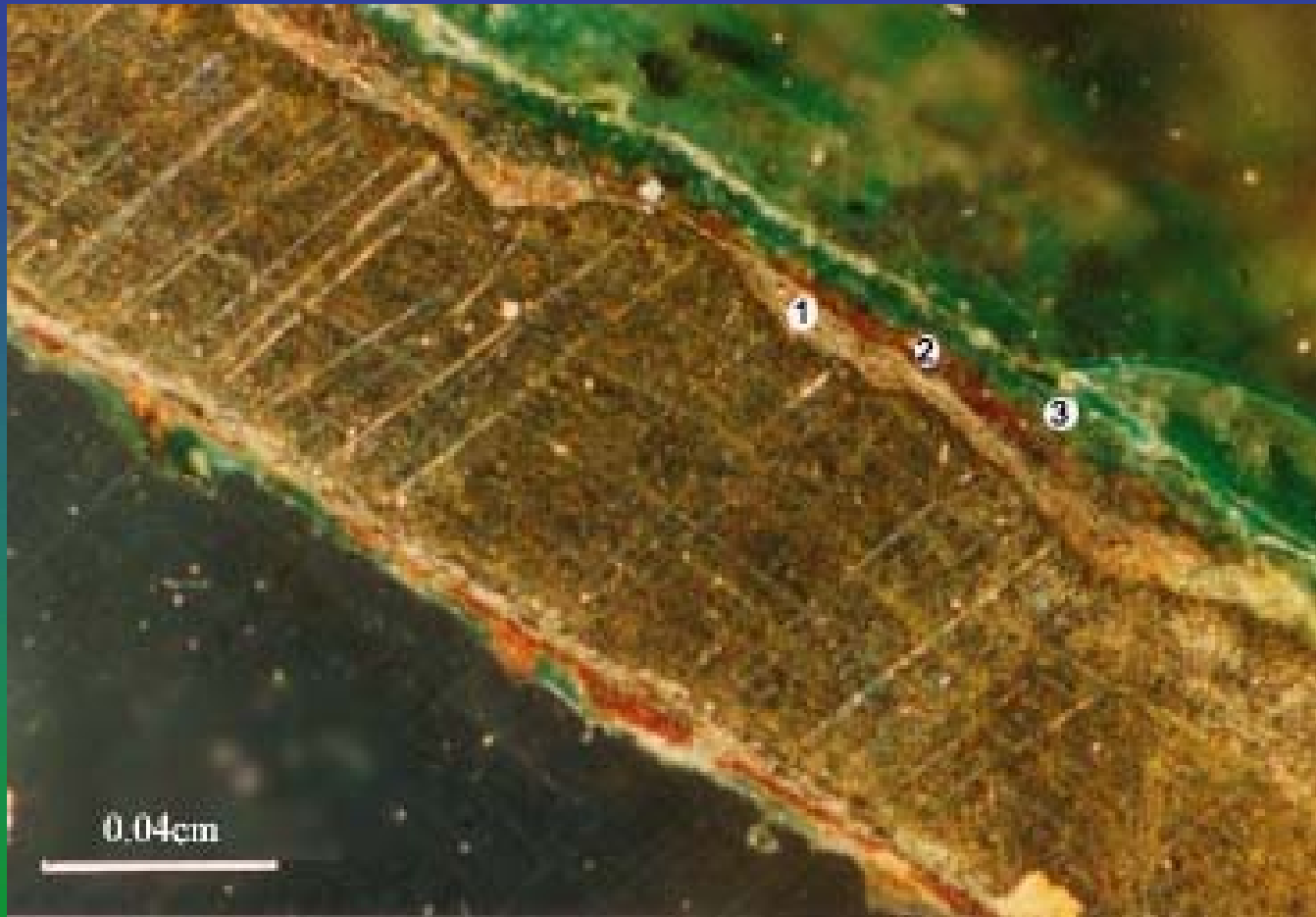
Location of bronze relics as natural analog

Major Activities: natural analog study

Bronze wares at Liulihe site and Wuhan site

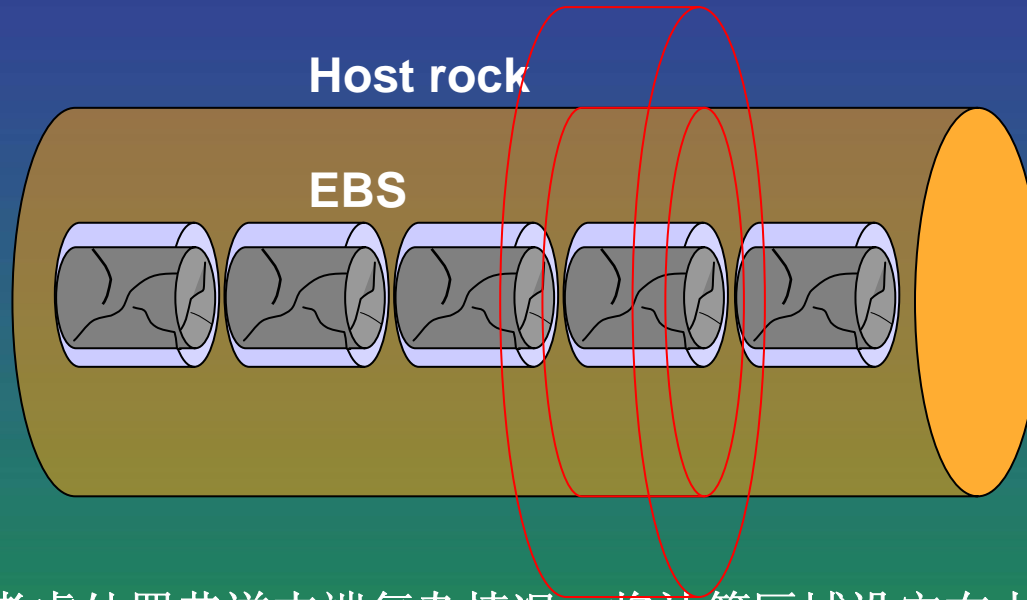


Corrosion of bronze ware



① - 疏松亚层; ② - Cu氧化物亚层; ③ - Cu碳酸盐亚层

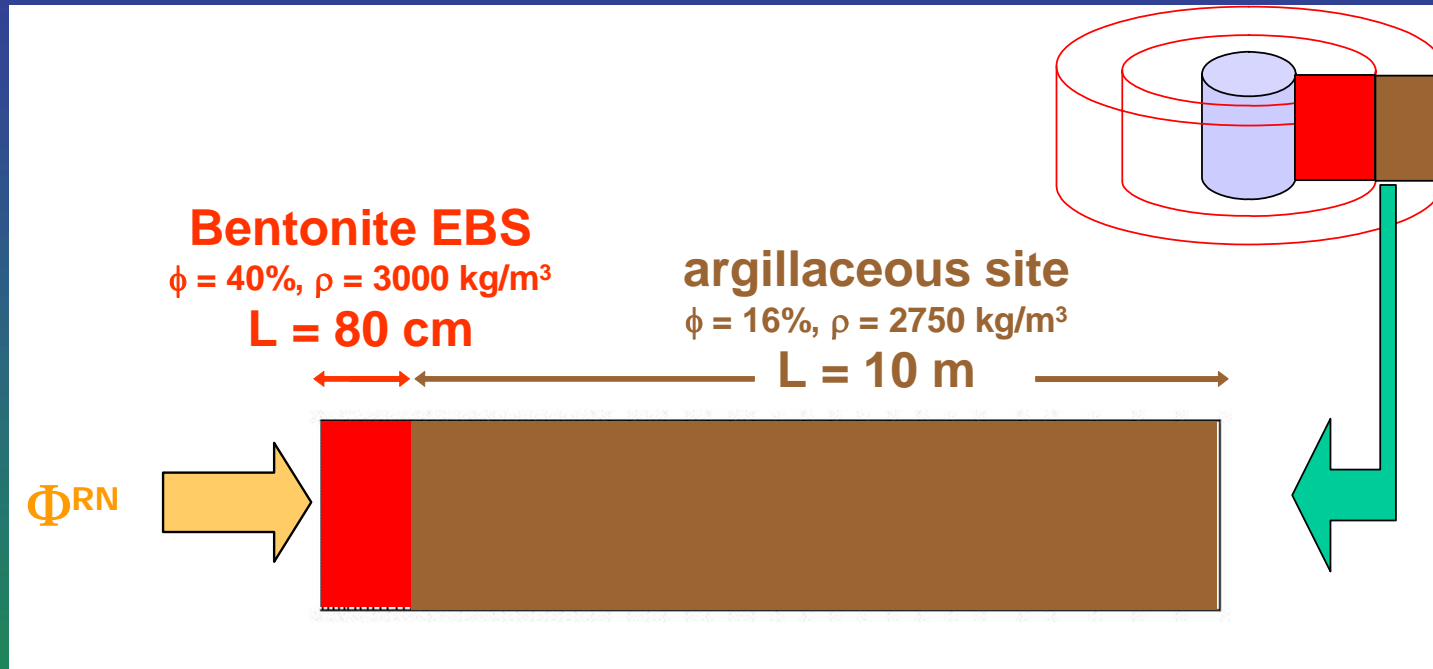
Concept:



本次计算不考虑处置巷道末端复杂情况，将计算区域设定在上图的红色圆柱体区域。考虑该概念模型为对称结构，特将模型简化为1维环状模型

- 最内层为玻璃固化体，内径为**0.3米**，高**1.1m**
- 外层为**0.07m**厚废物罐
- **0.8m** 的回填材料
- **10m**厚的处置

2. Recent progress in HLW disposal--PA

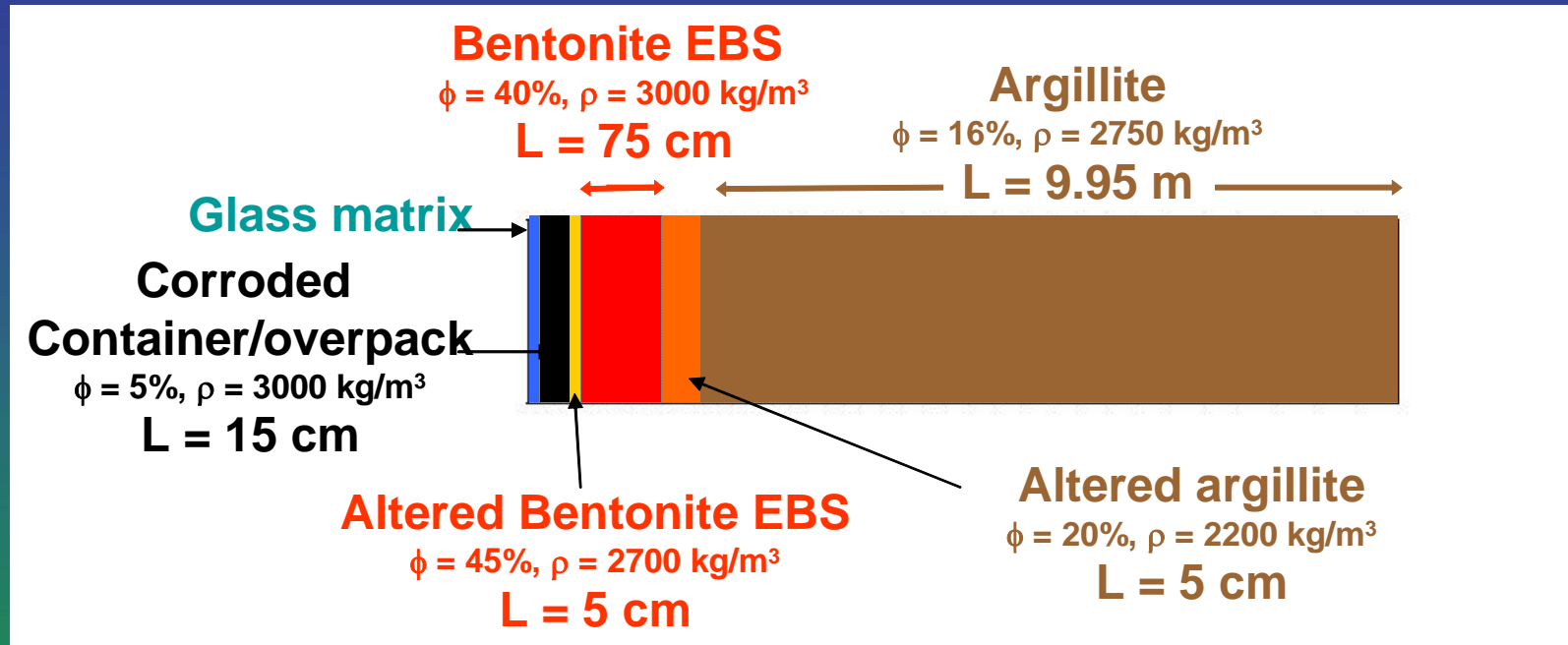


Scenario1 Cylindrical computational domain for RN migration in reference case.

The system comprises only the **unaltered, initial bentonite based EBS argillaceous EDZ.**

The density and effective porosity are 3000 kg/m^3 and 40% for the EBS, and 2750 kg/m^3 and 16% for EDZ.

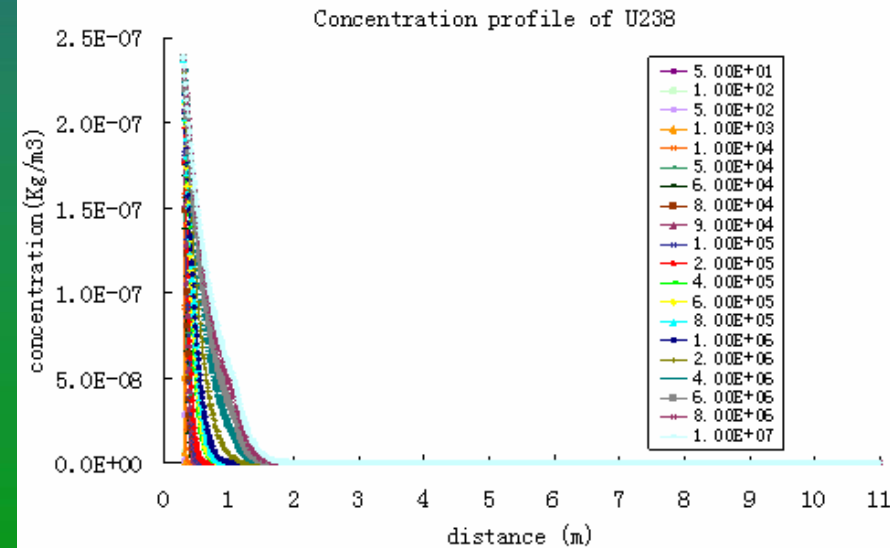
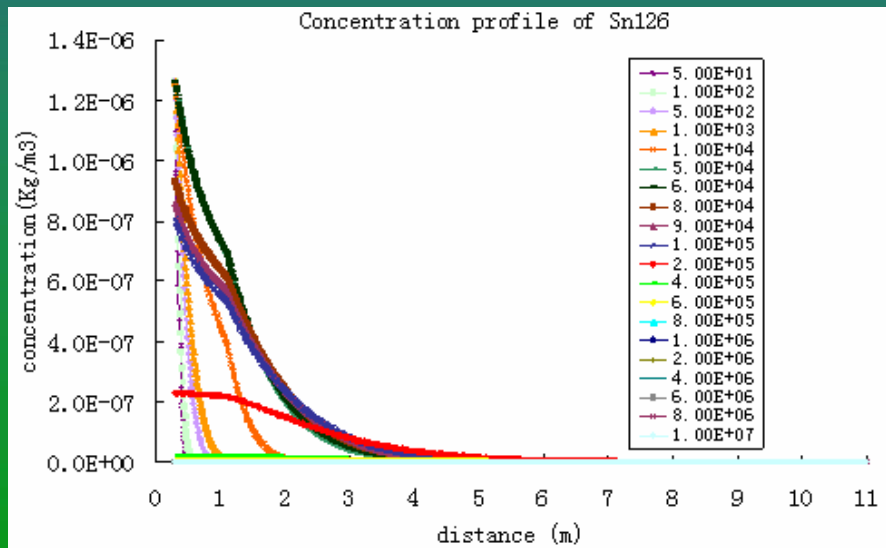
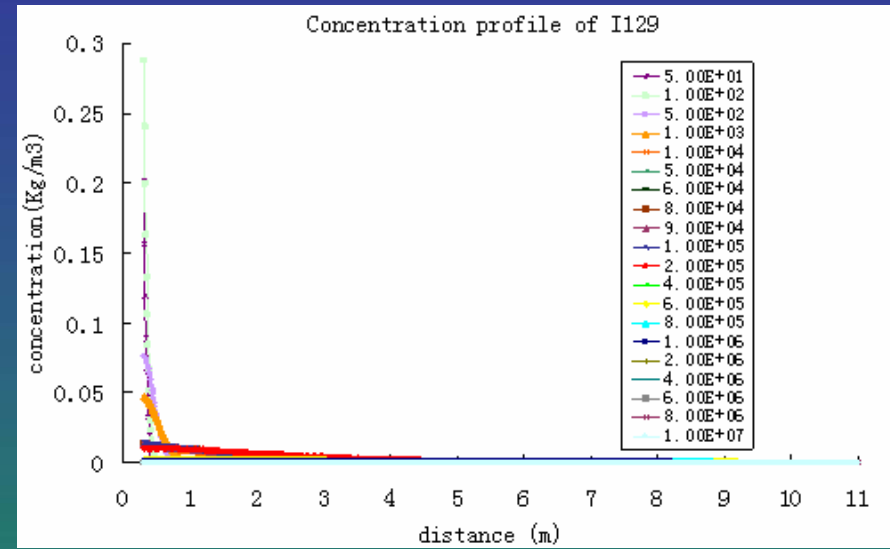
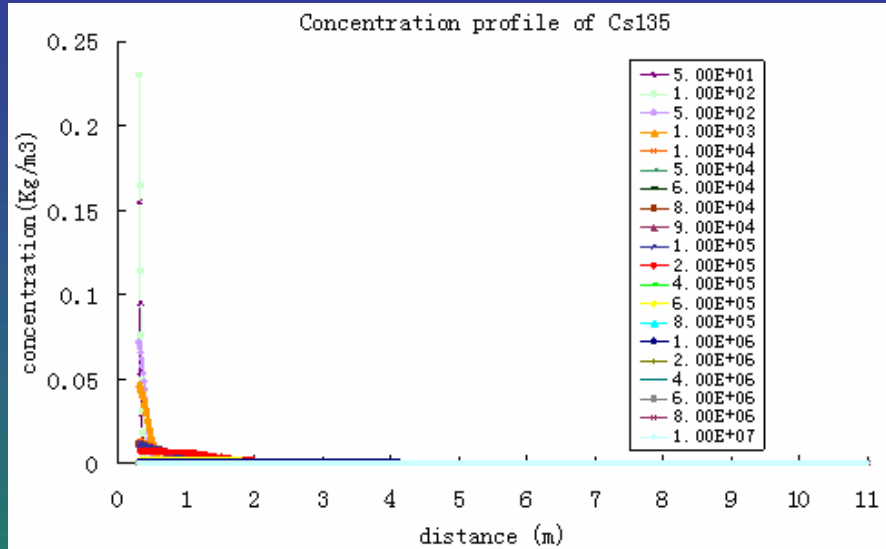
2. Recent progress in HLW disposal--PA

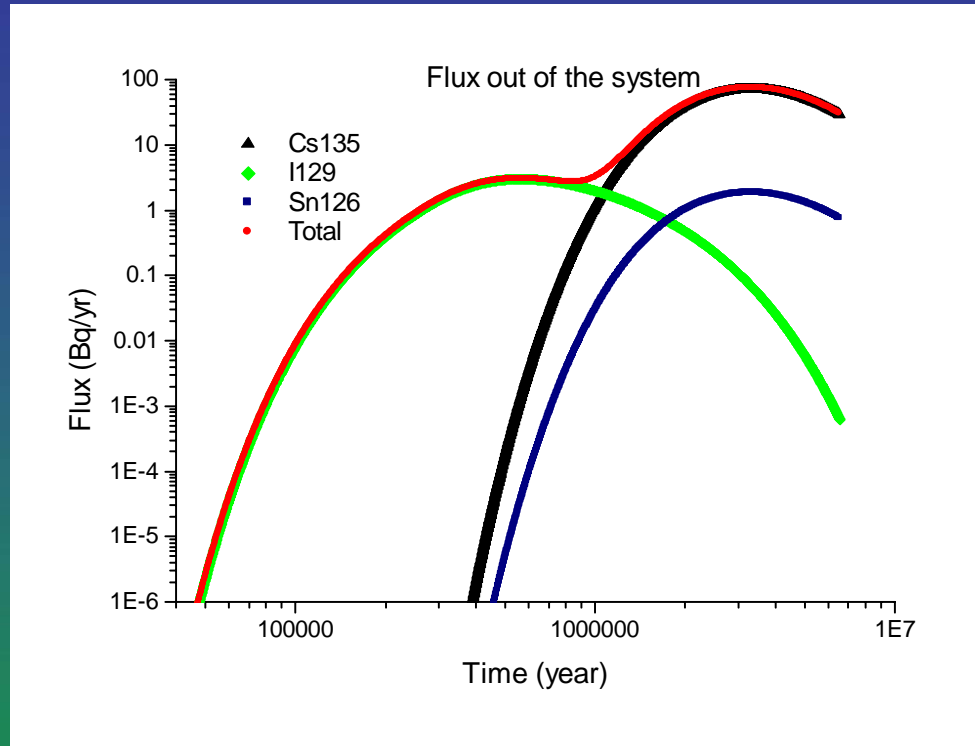


Scenario2 Cylindrical computational domain for RN migration in altered case.

As a result of canister/overpack corrosion, additional domains are created by the corrosion products and the argillite and/or EBS are altered

模拟计算结果-(1) 参考情景的浓度变化剖面





1. ^{238}U ($T_{1/2}=4.47 \times 10^9$ years), ^{239}Pu ($T_{1/2}=2.41 \times 10^4$ years) and ^{243}Am ($T_{1/2}=7.73 \times 10^3$ years) did not come out of the system,
2. ^{135}Cs ($T_{1/2}= 2.30 \times 10^6$ years), ^{129}I ($T_{1/2}= 1.57 \times 10^7$ years) and ^{126}Sn ($T_{1/2}=1.0 \times 10^5$ years) contribute the release rates,
3. ^{129}I is the first one come out of the system due to no sorption,
4. ^{135}Cs contribute 50 times more to the total release rate with the value 100Bq/a than ^{129}I , ^{126}Sn .

- Germany
- Finland
- Korea
- Japan
- France,
- Sweden,
- Canada,
- Switzerland,
- USA
- IAEA

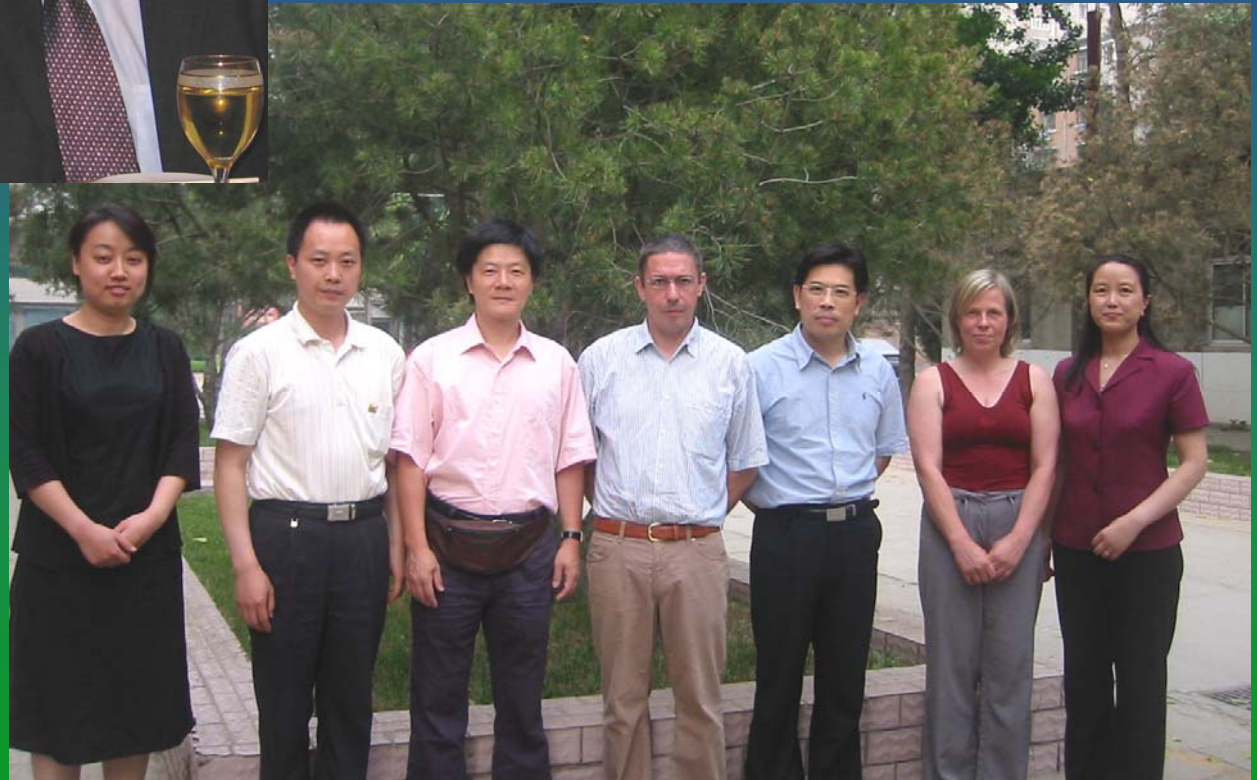




国外专家在北山参观选址地点



Experts from BGR visit Beishan, April, 2002



Experts from BGR, GRS visit BRIUG, 2006



China-Germany meeting, May 2005



Experts from US NWTRB visit Beishan, Oct. 1999



Experts from Canada, Korea, France, Switzerland and USA visited Beishan site on June 3, 2002



**IAEA workshop on HLW disposal,
May 27--June 4, Beijing, China**



日本核燃料循环研究所(原动燃团,PNC) 访问北山(1999.6.10)

JNC experts visit Beishan site, June 10, 1999



IAEA expert visit Beishan site, May 2000



**Experts from France, Switzerland dispatched by IAEA
Working at Beishan site in September 2003**

Experts from US DOE, EPA, NRC visit Beishan site in June 2005





A photograph of a sunrise over a mountain range. The sun is a bright yellow semi-circle on the horizon, partially obscured by the dark silhouettes of the mountains. The sky is a gradient of orange and yellow, with some light clouds. The overall mood is peaceful and serene.

Thank you

北山日出 Sun Rising in Beishan



Bundesministerium
für Bildung
und Forschung



Decommissioning of Nuclear Facilities: German R&D

Michael Weigl

**CHINESE-GERMAN WORKSHOP ON RADIOACTIVE
WASTE DISPOSAL**

MAY 28 – 31, 2007

Sino-German Science Centre, Beijing



Bundesministerium
für Bildung
und Forschung



Federal Ministry of Education and Research
Division 713: Decommissioning of Experimental
Nuclear Installations and Waste Management
Head of Division: Dr. Komorowski



Building of the Ministry in Bonn

Project Management Agency
Forschungszentrum Karlsruhe
Water Technology and Waste
Management Division



Research Center Karlsruhe

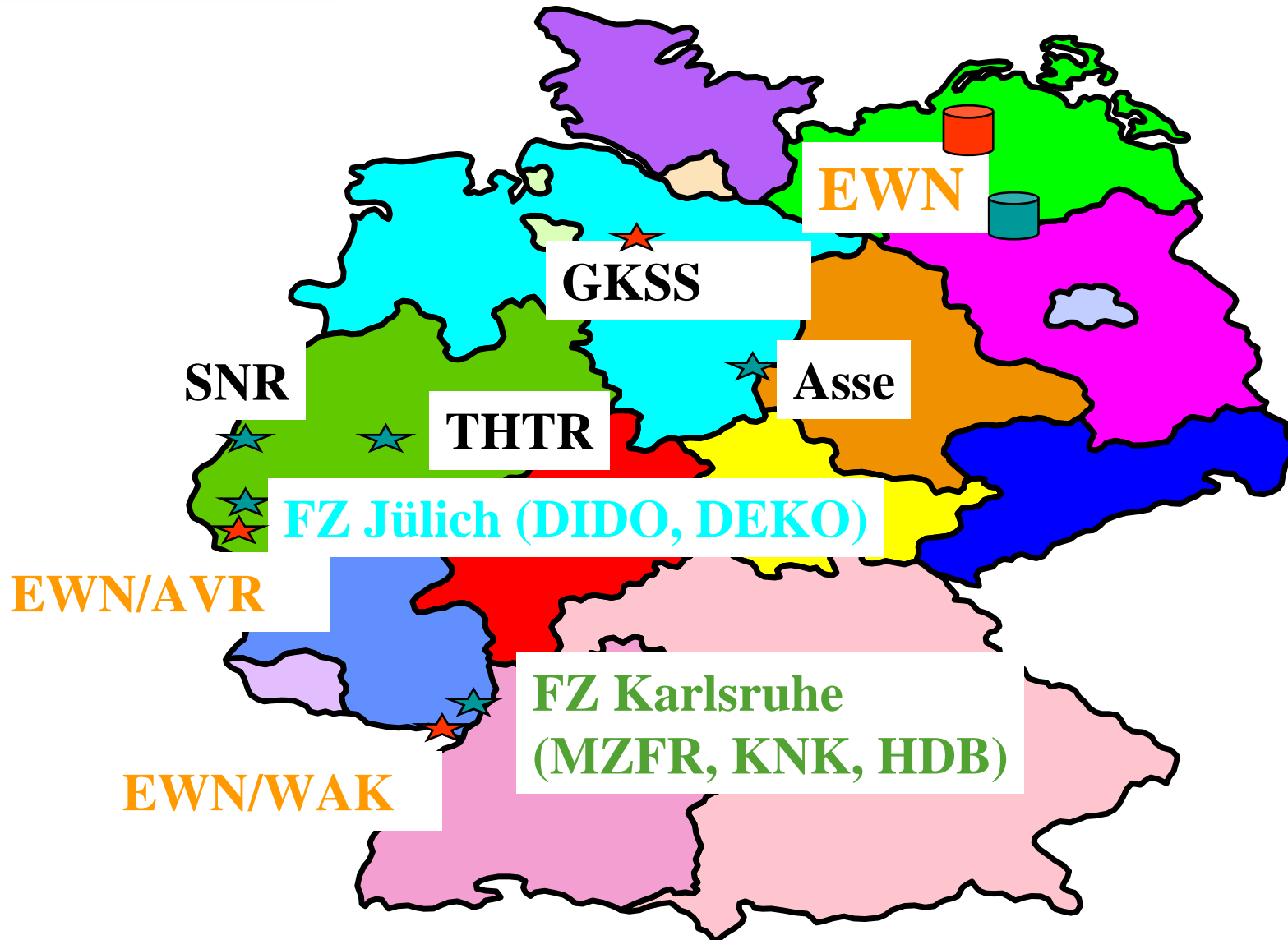


Outline

- **Decommissioning of Experimental Nuclear Installations in Germany – Past, Present and Future**
- **R & D Projects in the field of Decommissioning and Dismantling of Nuclear Facilities (founded by the Federal Ministry of Education and Research)**
- **Decommissioning of the MZFR: An example for the application of new technologies**
- **Outlook**

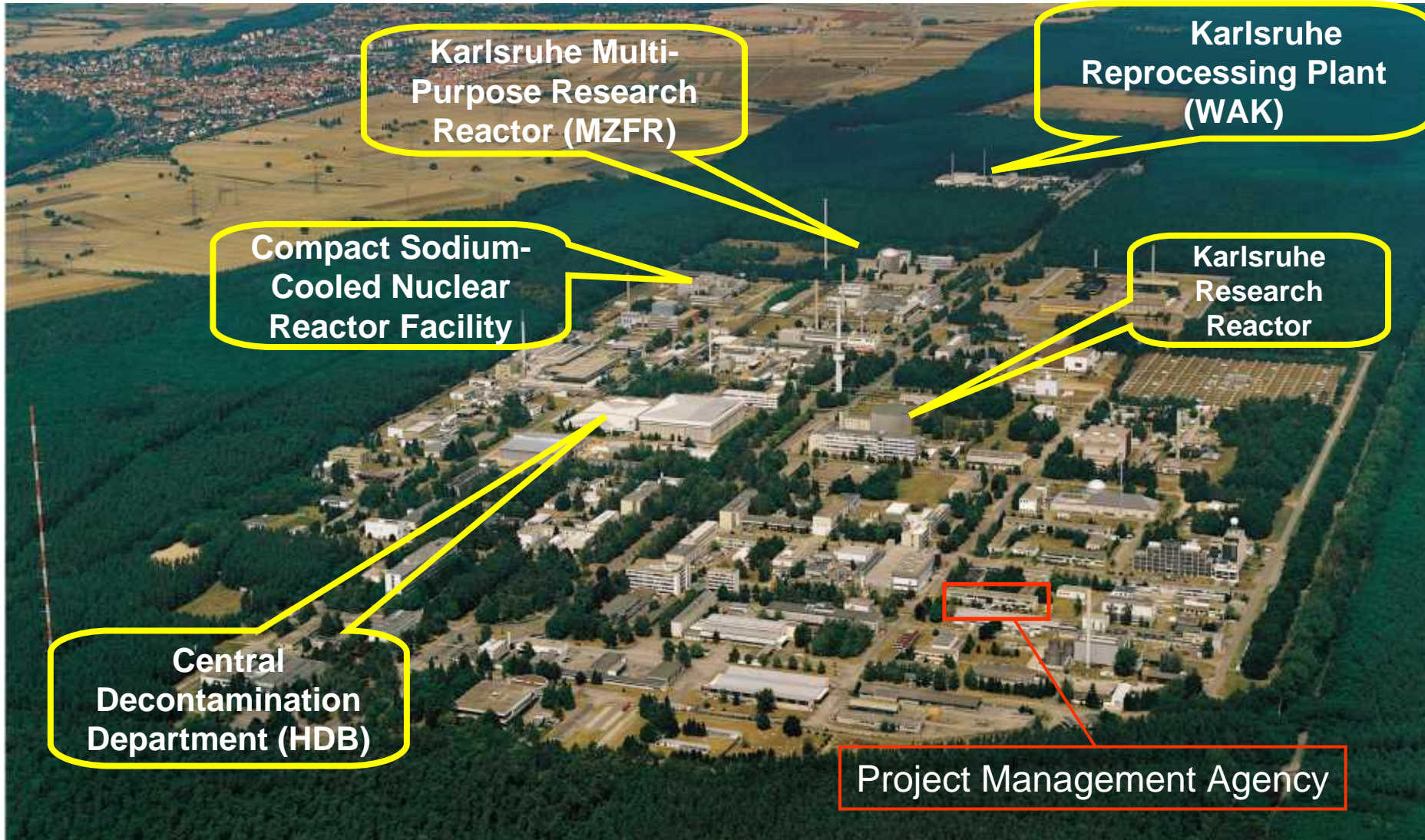


Decommissioning Projects of the Federal Ministry of Education and Research





Decommissioning Projects at the Forschungszentrum Karlsruhe





Tasks already finished



- **Niederaichbach Nuclear Power Plant (KKN)**



- **Karlstein Superheated Steam Reactor (HDR)**



- **Karlsruhe Research Reactor (FR2) (Safe storage)**

- **Thorium High temperature reactor THTR (Safe storage)**

- **TRIGA II Heidelberg (decommissioning completed)**



Present and Future Tasks

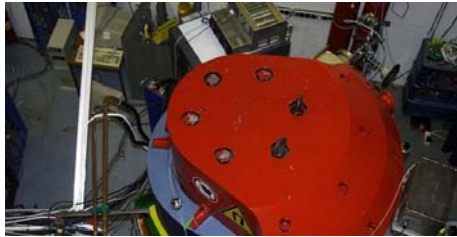
- **DIDO (Research Center Jülich)**
- **FRG1 u. 2 (Research Center Geesthacht) decommissioning starts in 2009**
- **HAWC-Vitrification: VEK (Vitrification Plant Karlsruhe)**
- **Closing of the Asse Research Mine**
- **Start of Operation of Konrad repository (LAW, MAW)**



R & D Projects



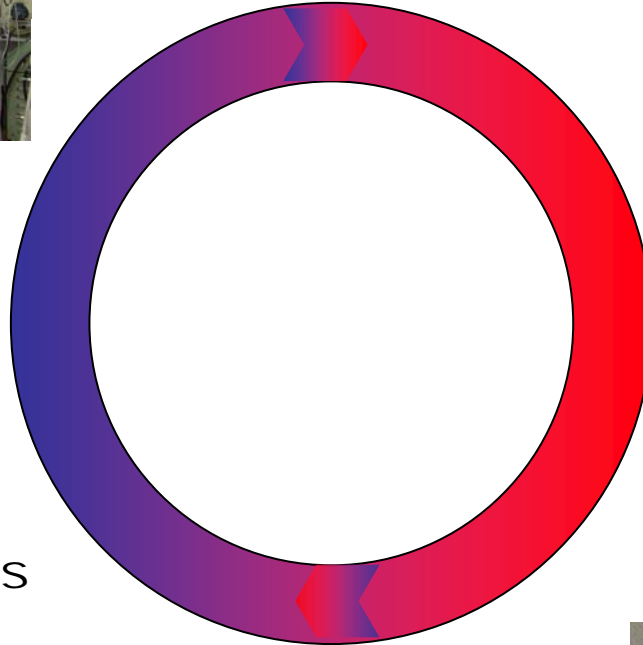
Applied
Radio Chemistry



New Analytic Methods



Radiation Research



Cutting technologies



Decontamination



Biological
dump recultivation



Remote-controlled
techniques



1. Decontamination Technology

Decontamination of concrete surfaces using Laser ablation and simultaneous conditioning

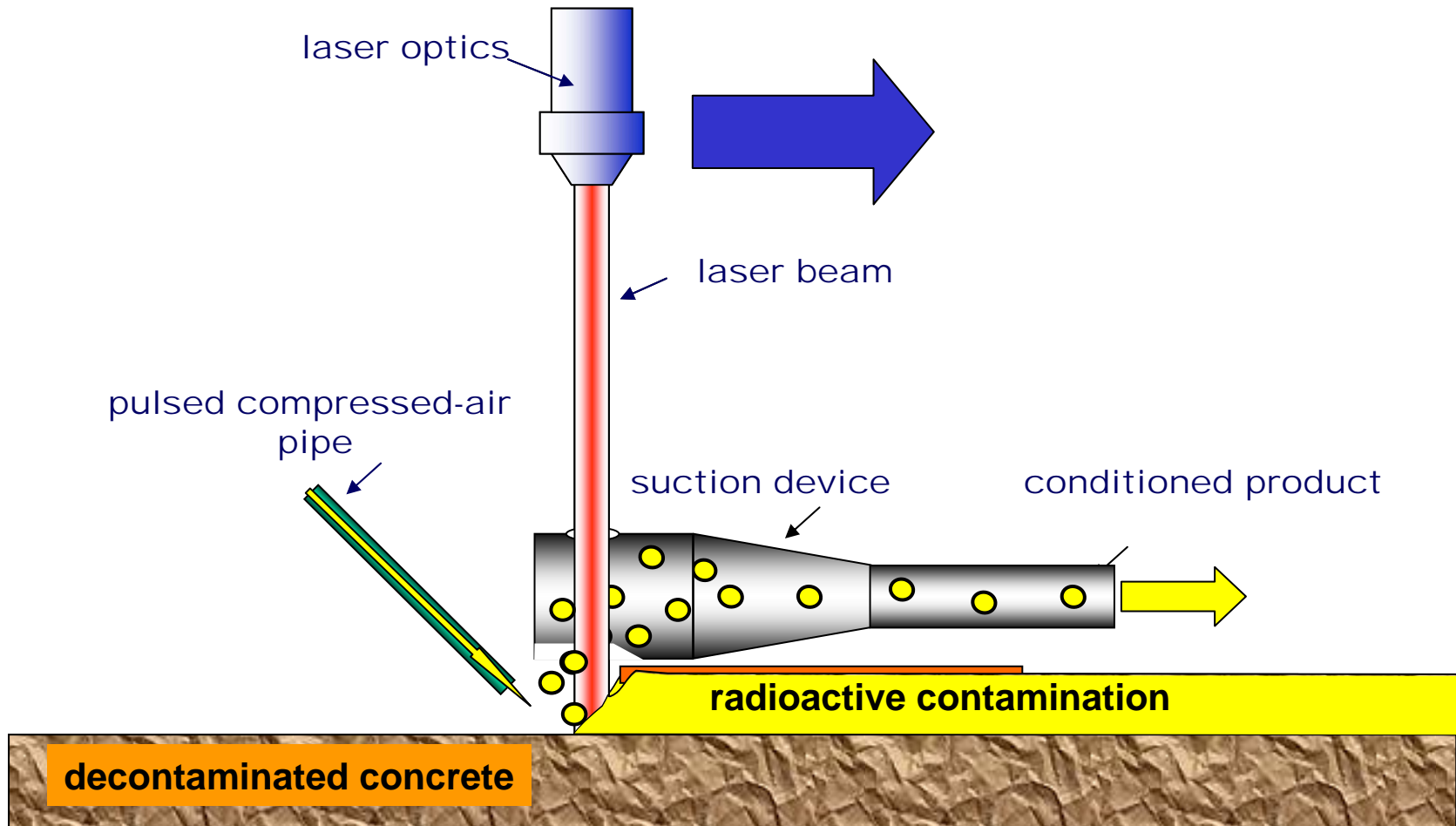
„LASABA“

W. Lippmann, J. Knorr, M. Herrmann, R. Wolf, A.-M. Reinecke, A. Zeuner

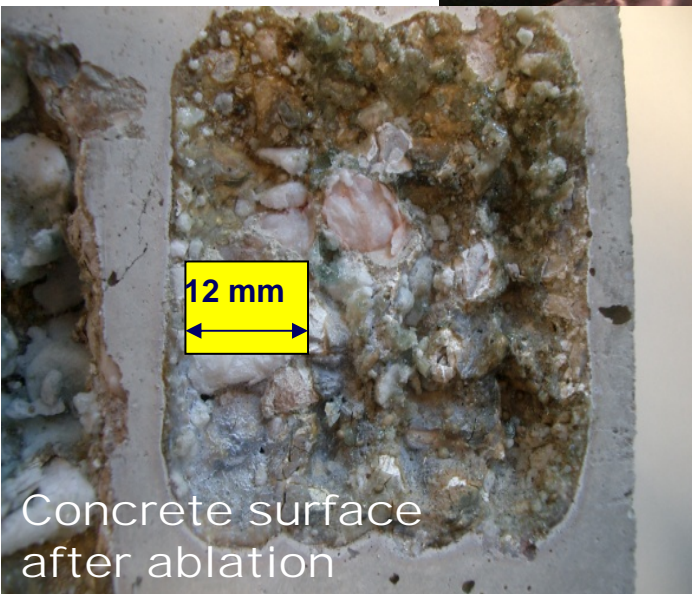
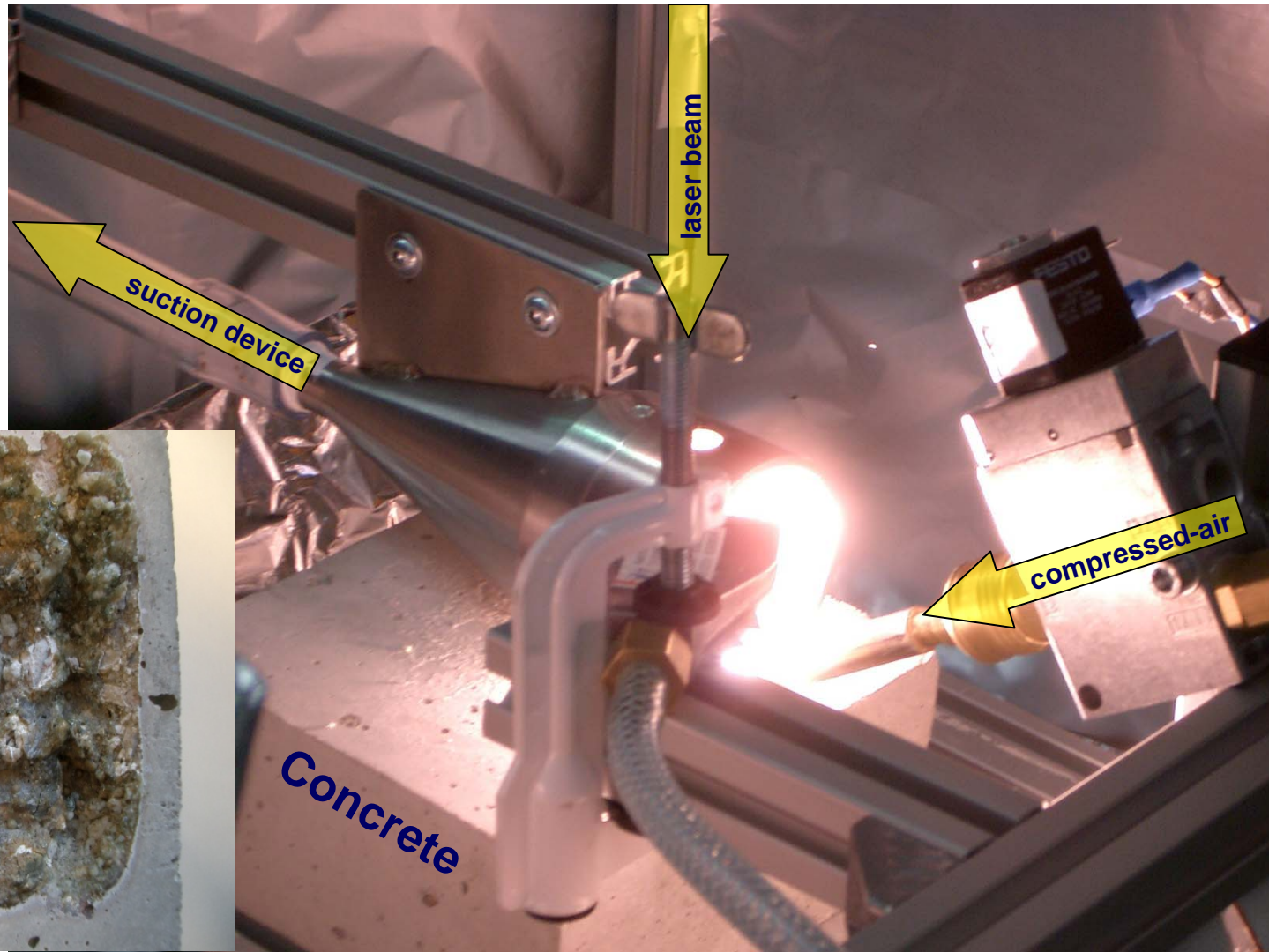
Projekträger: Forschungszentrum Karlsruhe
Wassertechnologie und Entsorgung
(PTKA-WTE)

Projektkoordinator: TU Dresden
Partner: Laserinstitut Mittelsachsen e.V. (LIM)
VKTA Rossendorf e.V.

Principle of the Ablation and Conditioning Process



Laser Ablation




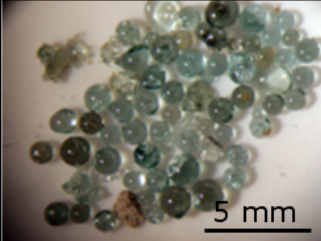
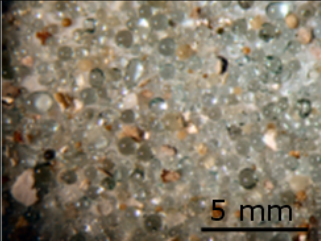
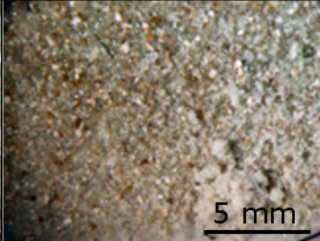
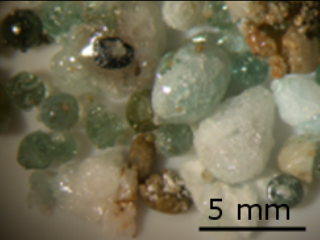
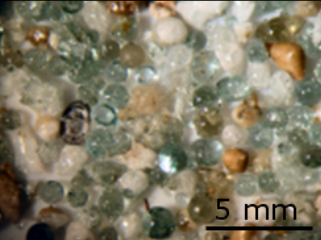

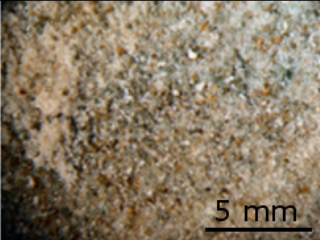
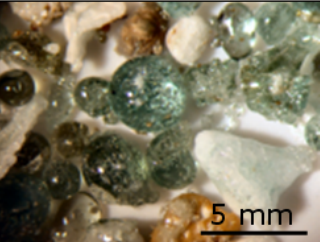
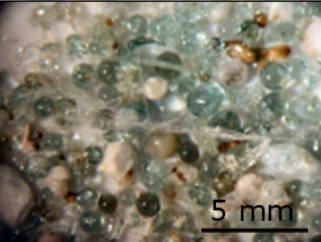
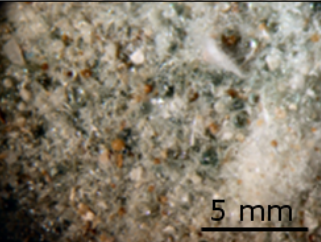

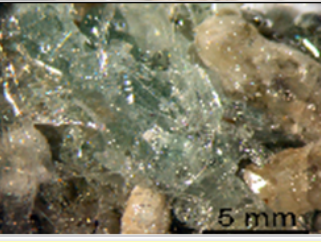
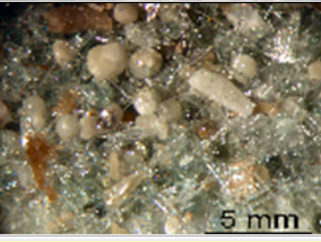
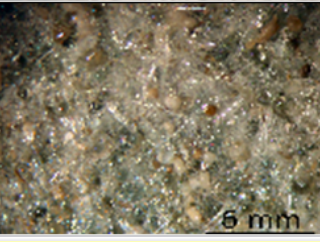
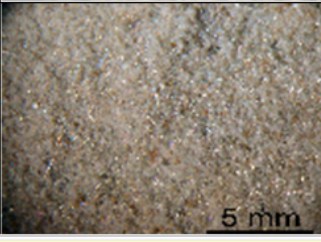
Conditioned Product

Classification of the product:

Yield of different particle fractions depending on process parameters

compressed air flow

**More than 90 %
of the initial
radioactivity is
fixed in the
product !**

		particle fractions			
		Nr.1 (1,6mm)	2 (1mm)	3 (0,3mm)	4 (0,125mm)
5a					
5b					
5c					
7b					

particle size



2. Cutting Technologies

CAMC

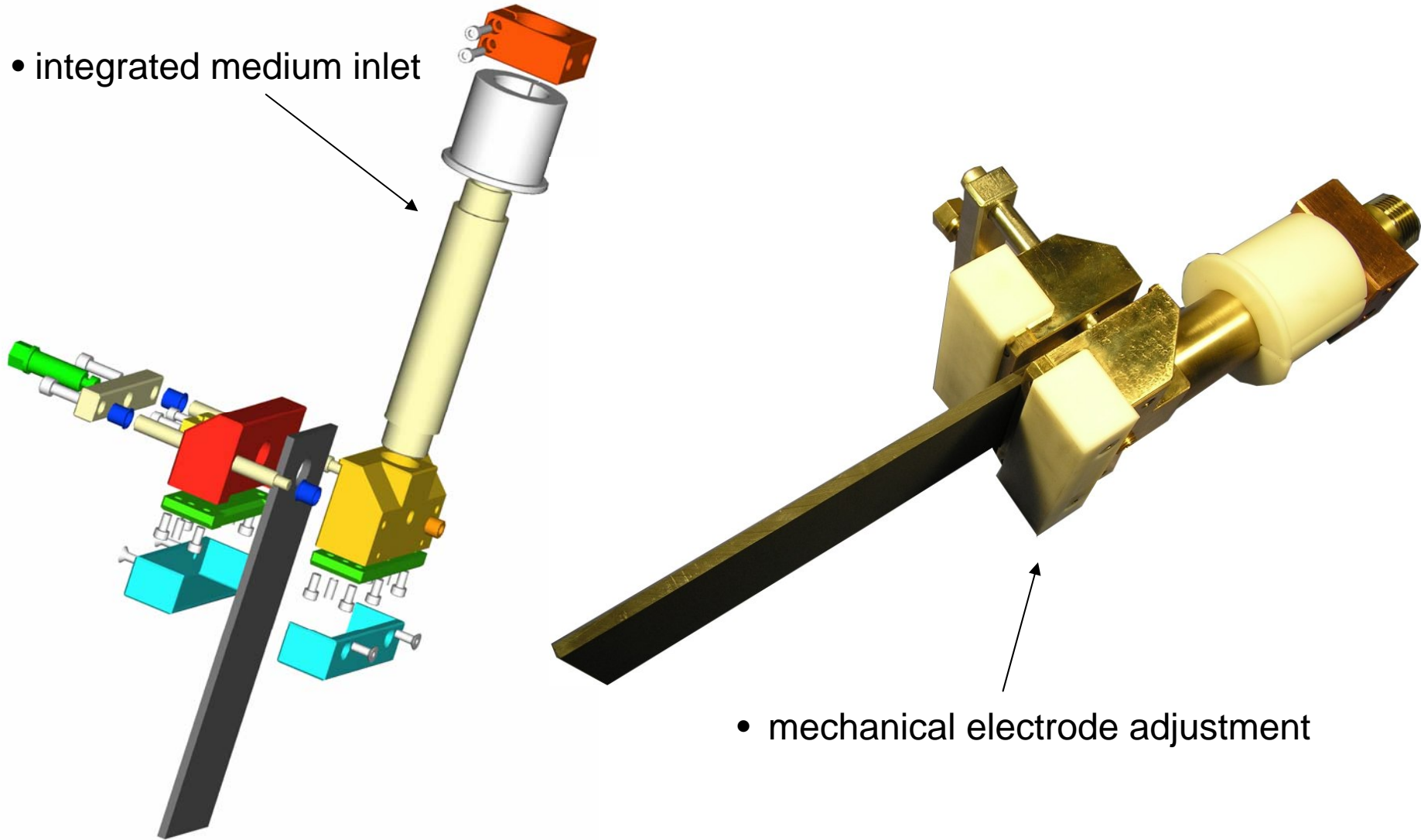
Contact-Arc-Metal-Cutting (CAMC)

Guido Kremer, Friedrich-Wilhelm Bach



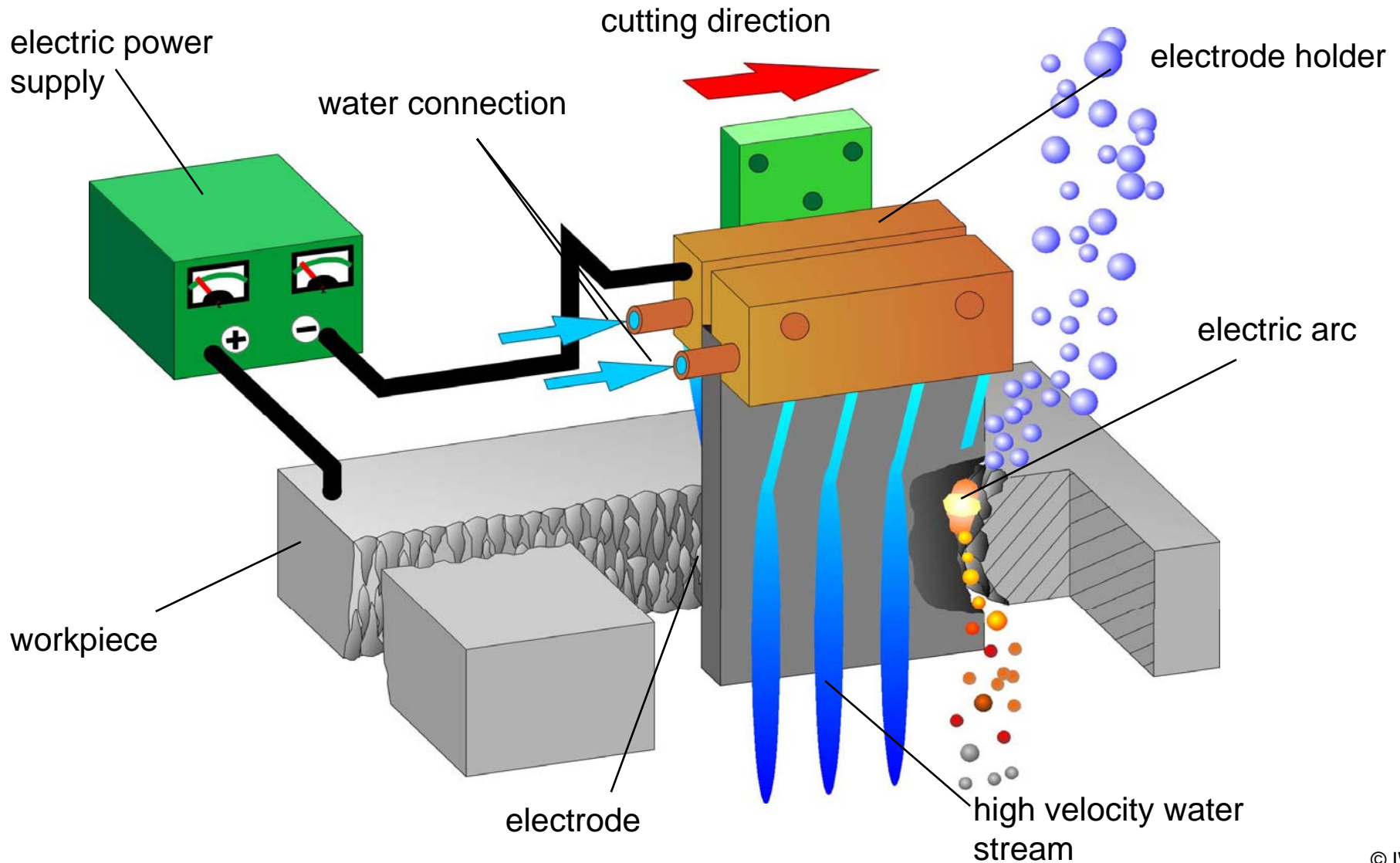
CAMC-Tool – Electrode holder with Electrode

- integrated medium inlet



- mechanical electrode adjustment

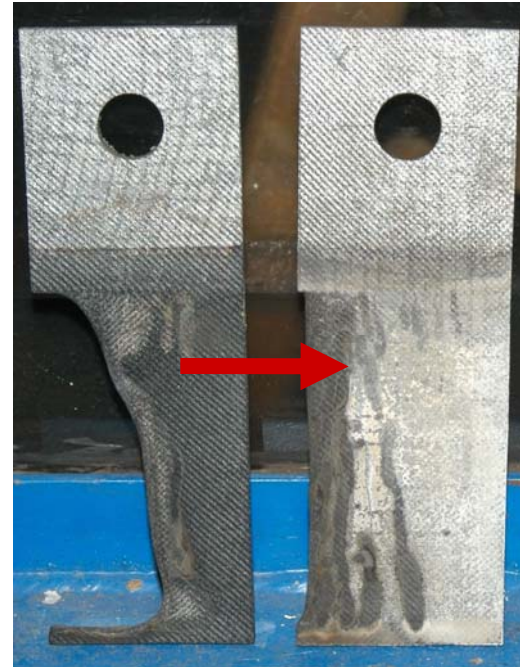
Contact-Arc-Metal-Cutting (CAMC) – principle



CAMC-Cuts into 130 mm solid material

Parameter

	initial	optimized
cutting voltage:	42 Volt	58 Volt
cutting current:	2000-3500 A	max. 700A (much smaller supply!)
water pressure:	5 bar	11 bar
quantity of water flow:	5-6 m ³ /h	17m ³ /h
electrode material:	fiber-reinforced graphite	pure graphite

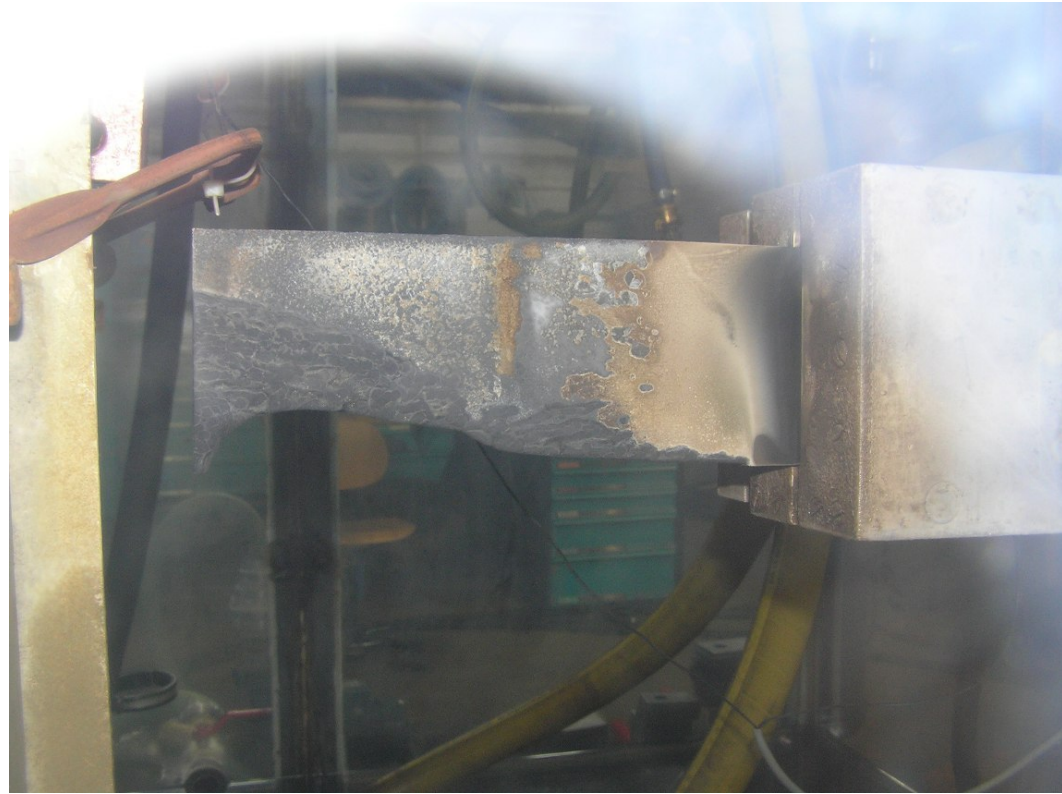


abrasion was reduced to 10 %

CAMC-CUT through a Mock-Up – pure graphite electrode



CAMC-CUT: 70-130 mm



abrasion at the graphite electrode after complete cut through the mock-up



Decommissioning of MZFR: An example for the application of new technologies

Decommissioning and Dismantling of the MZFR



E. Prechtl, B. Eisenmann
Hauptabteilung Projekte, Rückbauprojekt MZFR
Forschungszentrum Karlsruhe GmbH
W. Süßdorf, Fa. Studsvik
A. Loeb, Fa. Nukem

Decommissioning and Dismantling of the MZFR



Typ:

**Pressurized Water Reactor
Heavy Water Cooling
and Heavy Water Moderated**

Power:

200 MW_{th}, 57 MW_{el}

Build:

1961 – 1965

Operation:

1965 – 1984

Aim:

Complete Dismantling

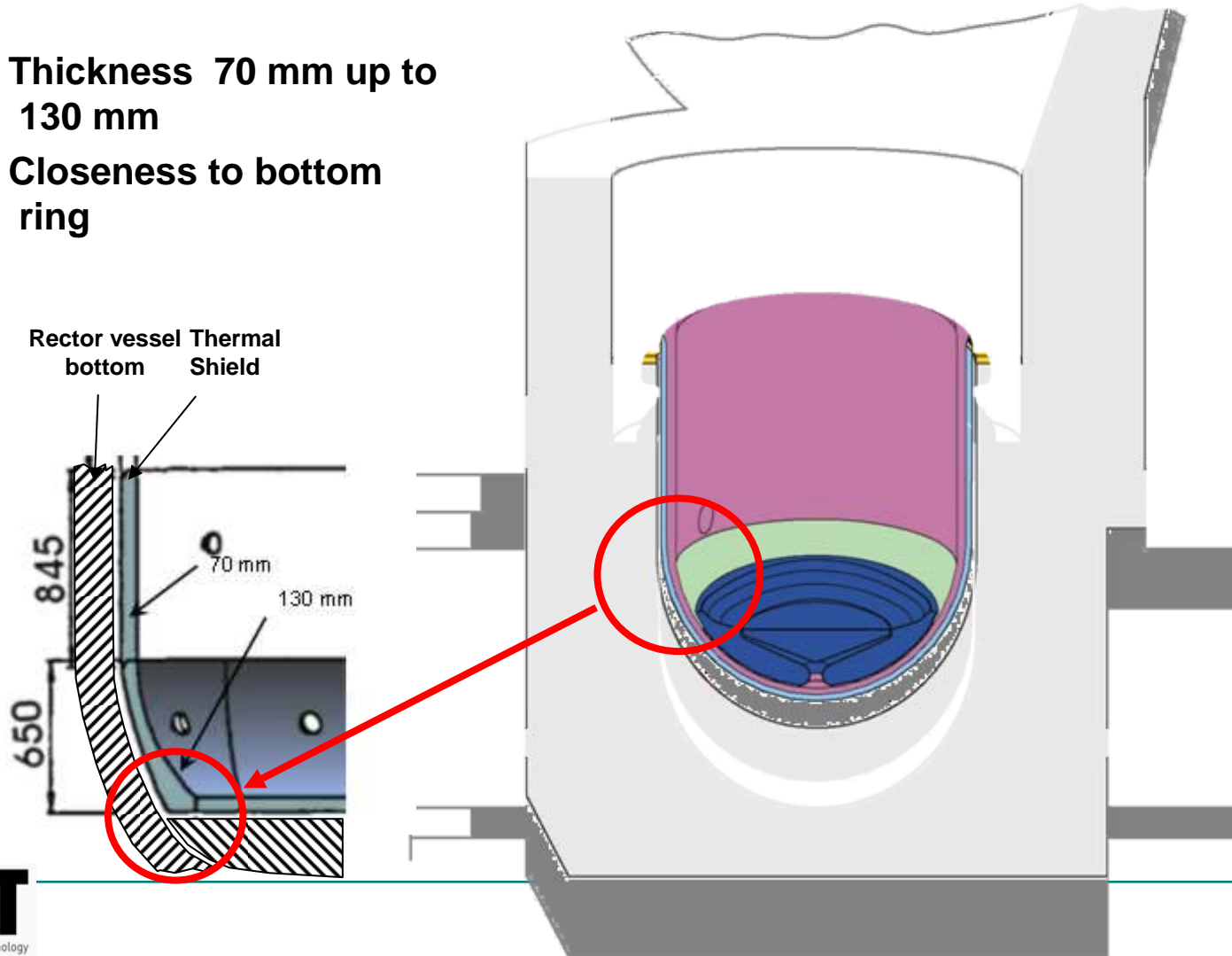
Reactor vessel of the MZFR



Fabrication in 1964

Remote-controlled Cutting of the Thermal Shield: Cutting of part 5, Special task due to very special geometry

1. Thickness 70 mm up to 130 mm
2. Closeness to bottom ring

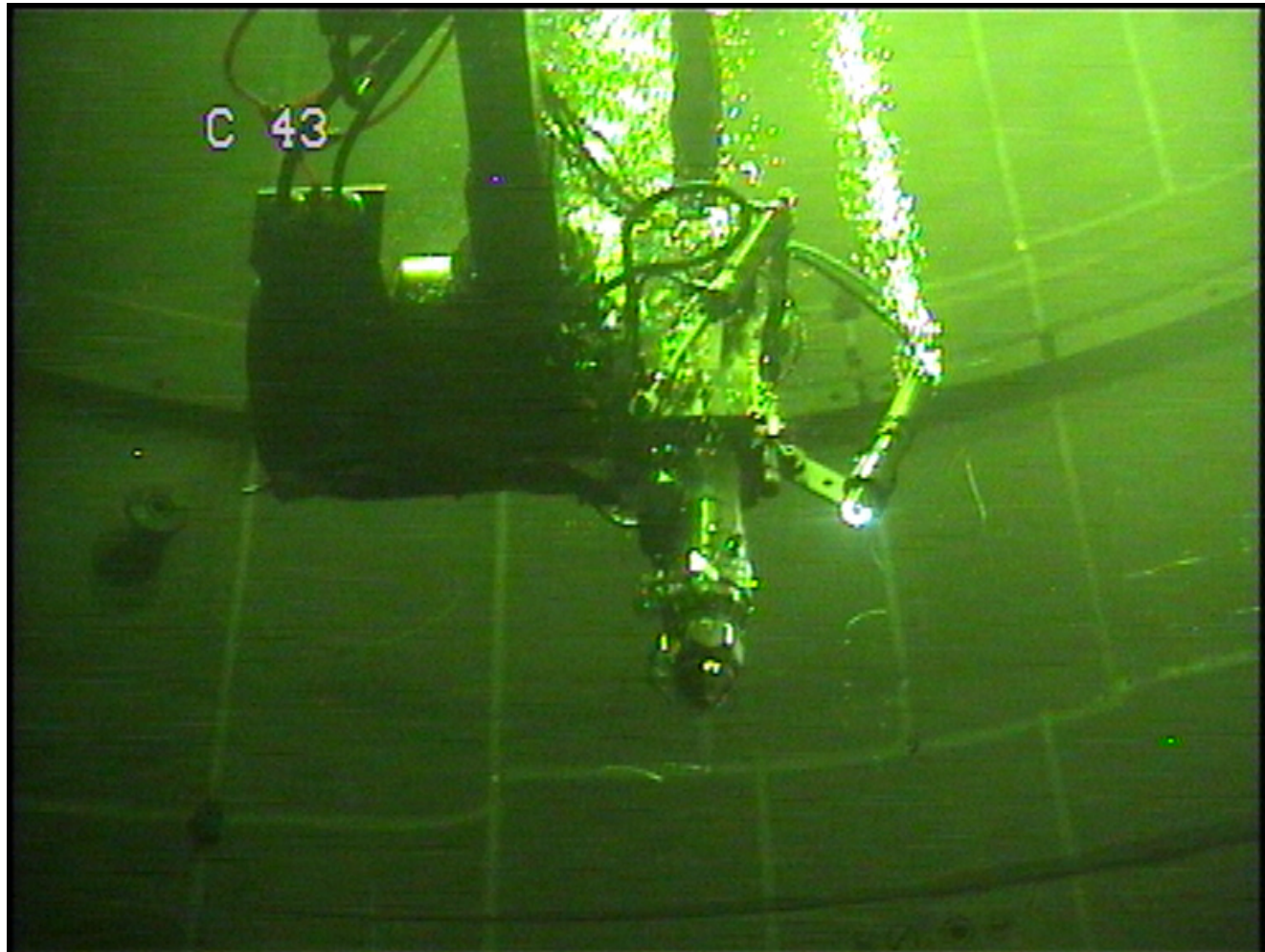


Test on a Dummy of Part 5 of the Thermal Shield

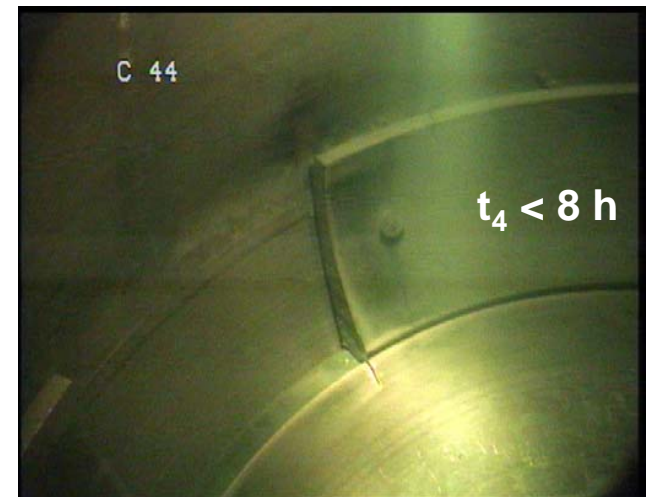
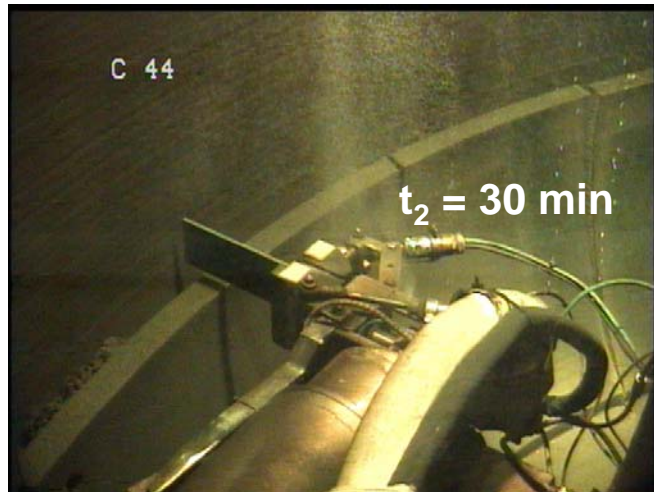
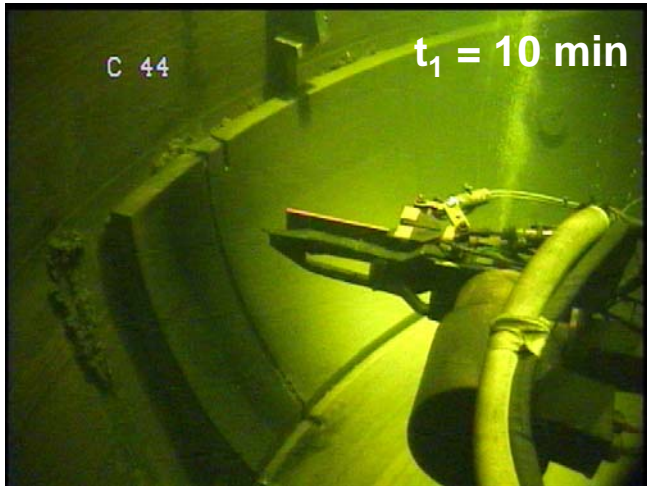


Underwater lab at Universität Hannover
CAMC Cut: Thickness 70 – 130 mm)

Remote-controlled Tool Carrier



Remote-controlled CAMC Cutting of the Thermal Shield, Part 5

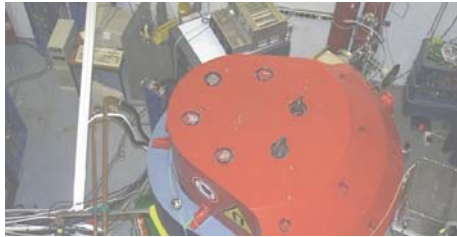




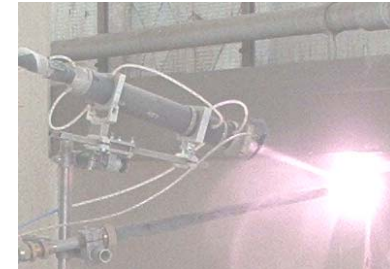


Outlook

- Techniques for decommissioning and dismantling of nuclear facilities are already available
- Improvement of common techniques and use of innovative techniques for special problems could reduce costs and improve safety of both the workers and the public
- Management of radioactive waste from decommissioning is a key consideration, therefore the availability of a final waste disposal is an increasing demand
- In future design of nuclear facilities considerations about decommissioning and dismantling have to be implemented.



Thank You for
Your Attention !



Endlagerung radioaktiver Abfälle
in tiefen geologischen Formationen
Deutschlands



Untersuchung und Bewertung von
Tongesteinsformationen

Clay formations – a possible alternative as host rocks for radioactive waste disposal in Germany ?

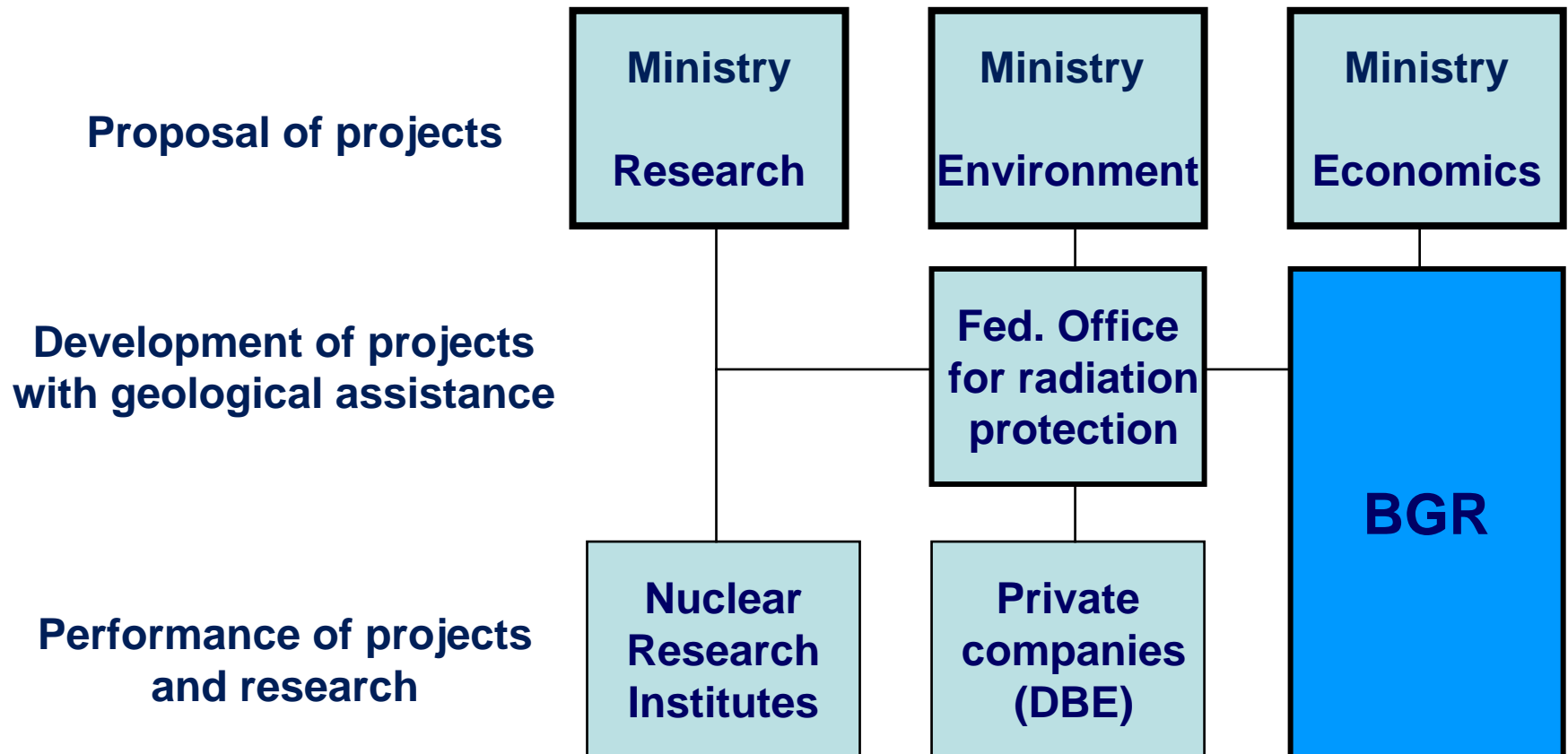
Volkmar Bräuer

Peer Hoth
Holger Wirth
Klaus Reinhold
Paul Krull
Hagen Feldrappe

BGR- „Clay report“
by order of the German
Federal Ministry of Economics
and Technology

Nuclear waste disposal in Germany

- Responsibilities -



Repository/Exploration Sites in Germany



Konrad



Gorleben



Morsleben



BGR activities on radioactive waste disposal

- Research since more than 30 years
- Site specific investigations
Morsleben, Gorleben, Konrad
- Research and development
Host rocks, geotechnical barriers,
scenario analyses
- International co-operation
International URLs, bilateral
agreements

Site Selection



Research



Site Exploration



Long-Term Safety

Properties	Rock Salt	Clay/Clay Stone	Crystalline Rock (granite)
thermal conductivity	high	low	medium
permeability	almost impermeable	very low to low	very low (not fractured) to permeable (fractured)
stability	medium	low to medium	high
deformation behaviour	viscous (creep)	plastic to brittle	brittle
excavation stability	inherent stability	support required	high (unfractured) low (fractured)
in situ stress	lithostatic isotropic	anisotropic	anisotropic
solution behaviour	high	very low	very low
sorption capacity	very low	very high	medium to high
temperature resistivity	high	low	high

Properties of potential host rocks

 favorable

 unfavorable

 medium

Components	Rock Salt	Clay/Clay Stone	Crystalline Rock
emplacement level	approx.. 900 m	approx.. 500 m	500 - 1200 m
disposal technique*	drifts and deep boreholes	drifts respectively . short boreholes	boreholes or drifts
design temperature	max. 200° C	max. 100° C	max. 100° C (bentonite backfill)
backfill material*	crushed salt	bentonite	bentonite
duration of interim storage (fuel element container and high active waste container)	min. 15 years	min. 30 - 40 years	min. 30 - 40 years
support	not necessary	necessary, under certain conditions very complex	necessary in fractured areas
waste container concept	existing	to be developed in Germany	to be developed in Germany
mining experience	wide experience (salt mining)	less experience	at lot of experience (ore mining)

Disposal concepts in different host rocks



favorable

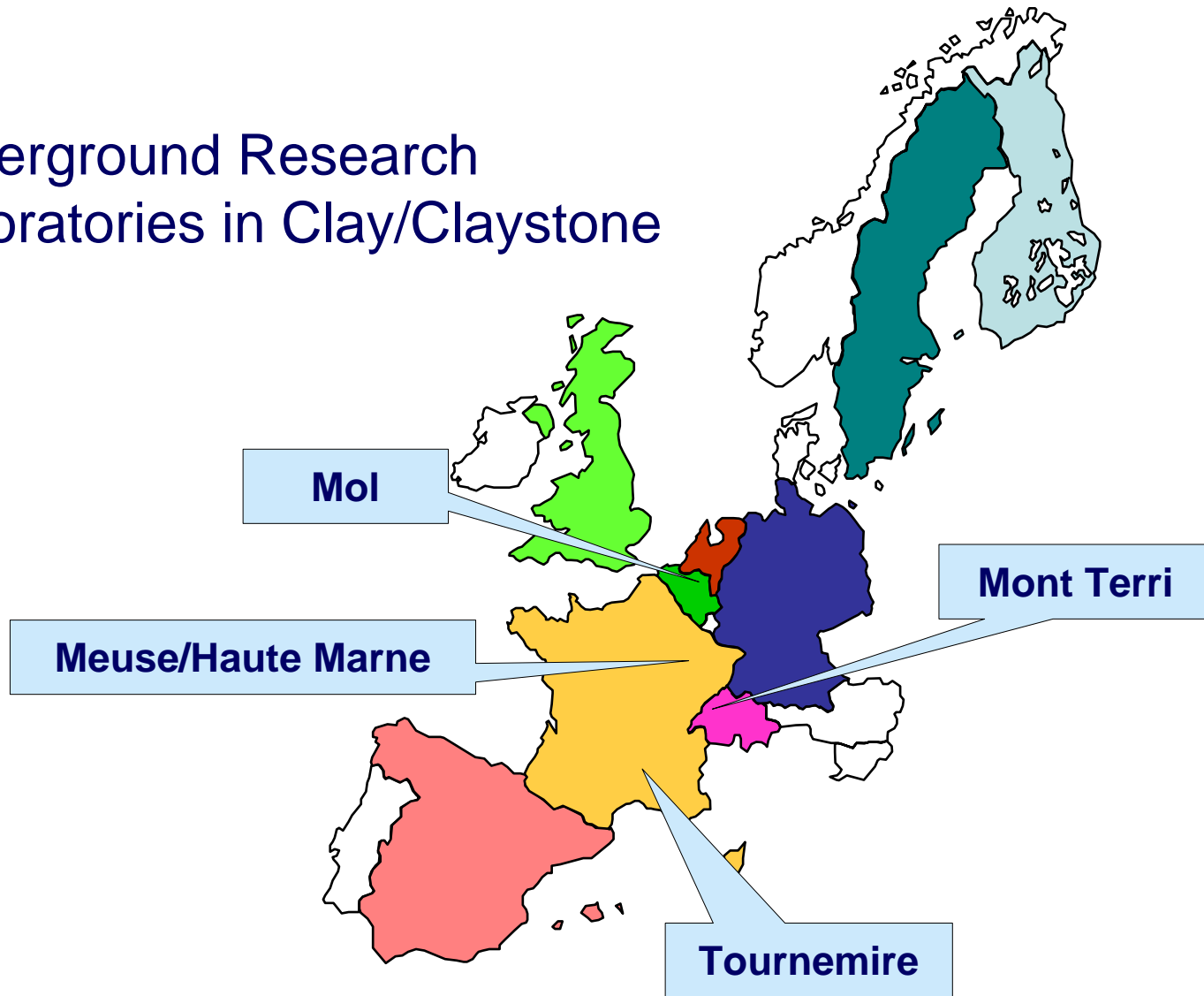


unfavorable

* has to be adopted to the host rock

International Co-operation

Underground Research Laboratories in Clay/Claystone



Period / Epoch		Series / Stage	Northern Germany		Southern Germany		
			W	E	W	E	
Tertiary	Quaternary	ca. 1.8	Quartär				
	Neogene		Pliozän				
			Miozän				
			Oligozän				
	Paleogene		Eozän				
			Paläozän				
			Dan				
			Mastricht				
	Cretaceous	Upper Cretaceous	ca. 65	Campan			
				Santon			
			Coniac				
			Turon				
			Cenoman				
Lower Cretaceous			Alb				
			Apt				
			Barrême				
			Hauterive				
			Valangin				
Jurassic	Upper Jurassic (Malm)	ca. 145	Berrias				
			"Serpulit"				
			"Münder Mergel"				
			"Eimbeckhäuser P.-K."				
			"Gigas-Schichten"				
			Kimmeridge				
	Middle Jurassic (Dogger)		"Korallenoolith"				
			"Heersumer Sch."				
			Callov				
	Lower Jurassic (Lias)		Bathon				
		Bajoc					
		Aalen					
		Toarc					
Triassic	Upper Triassic Keuper	ca. 205	Pliensbach				
			Sinemur				
			Hettang				
			Rhät				
			"Steinmergelkeuper"				
	Middle Triassic Muschelkalk	M	"Oberer Gipskeuper"				
			"Schilfsandstein"				
			"Unterer Gipskeuper"				
	Lower Triassic Buntsandstein	L	"Lettenkeuper"				
			"Ob. Muschelkalk"				
		"Mittl. Muschelkalk"					
		"Unt. Muschelkalk"					
		"Röt"					
		"Solling-Folge"					
Permian	Upper Permian (Zechstein)	ca. 250	"Hardeggen-Folge"				
			"Detfurth-Folge"				
			"Volpriehausen-Folge"				
			"Quickborn-Folge"				
			"Bernburg-Folge"				
Lower Permian (Rotliegend)		"Calvörde-Folge"					
		"Möln-Zyklus"					
	"Friesland-Zyklus"						
	"Ohre-Zyklus"						
	"Aller-Zyklus"						
	"Leine-Zyklus"						
	"Staufurt-Zyklus"						
	"Werra-Zyklus"						
	Oberrotliegend						
	Unterrotliegend						

Stratigraphic position of clay/claystone formations in Germany



Formation with shales and claystone



regional / local distribution of argillaceous rocks with good spatial characterisability
- possible host rocks for nuclear waste repositories



regional / local distribution of argillaceous rocks with limited spatial characterisability

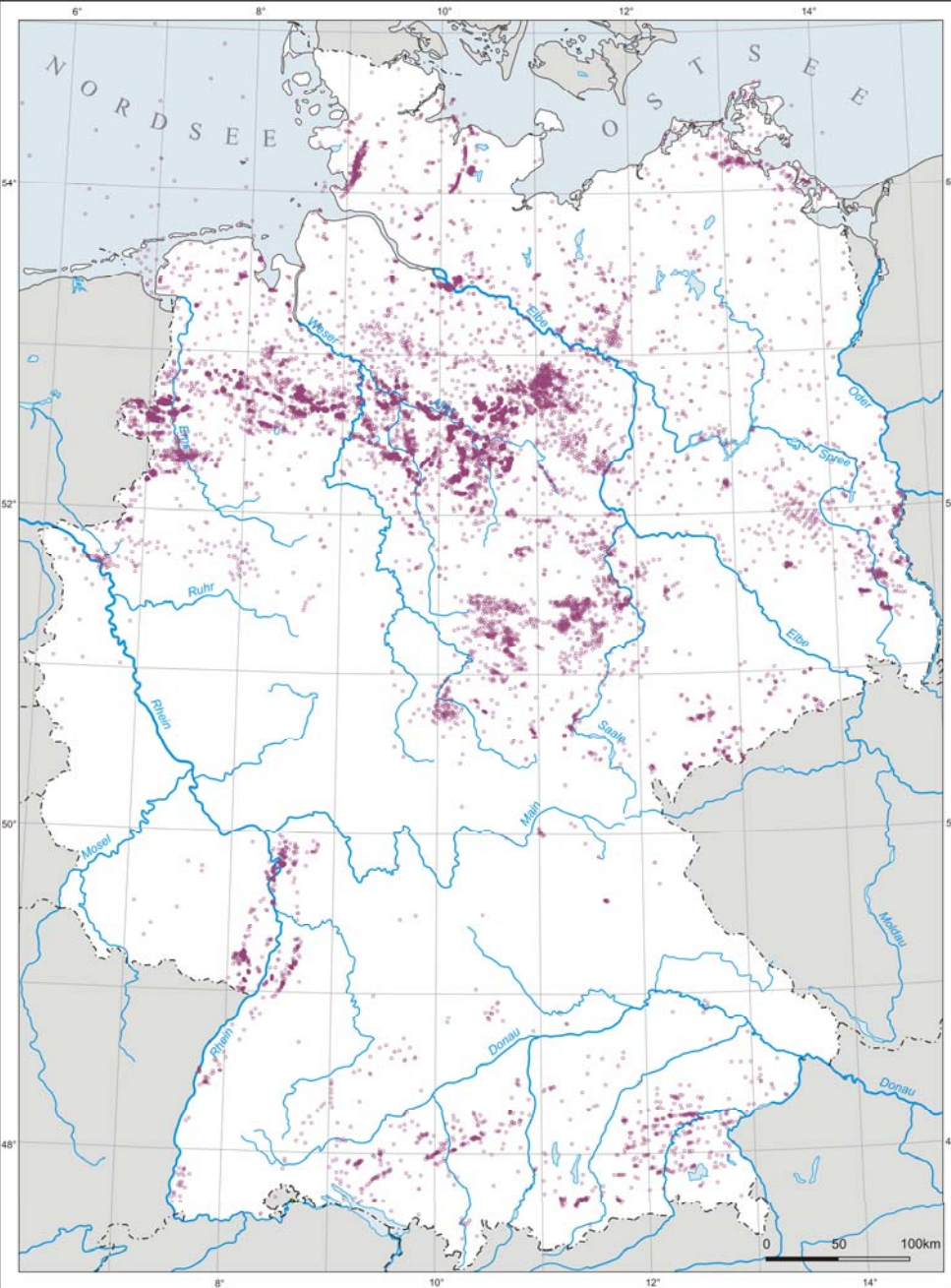


Formation with sandstone and siltstone facies

Data base for the „BGR-clay report“

- Literature
- Drilling records
- Borehole logs
- Seismic-Data
- Borehole-correlations
- No in-situ tests

Boreholes in Germany (approx. 25.000)



● Deep boreholes (depth > 300m)

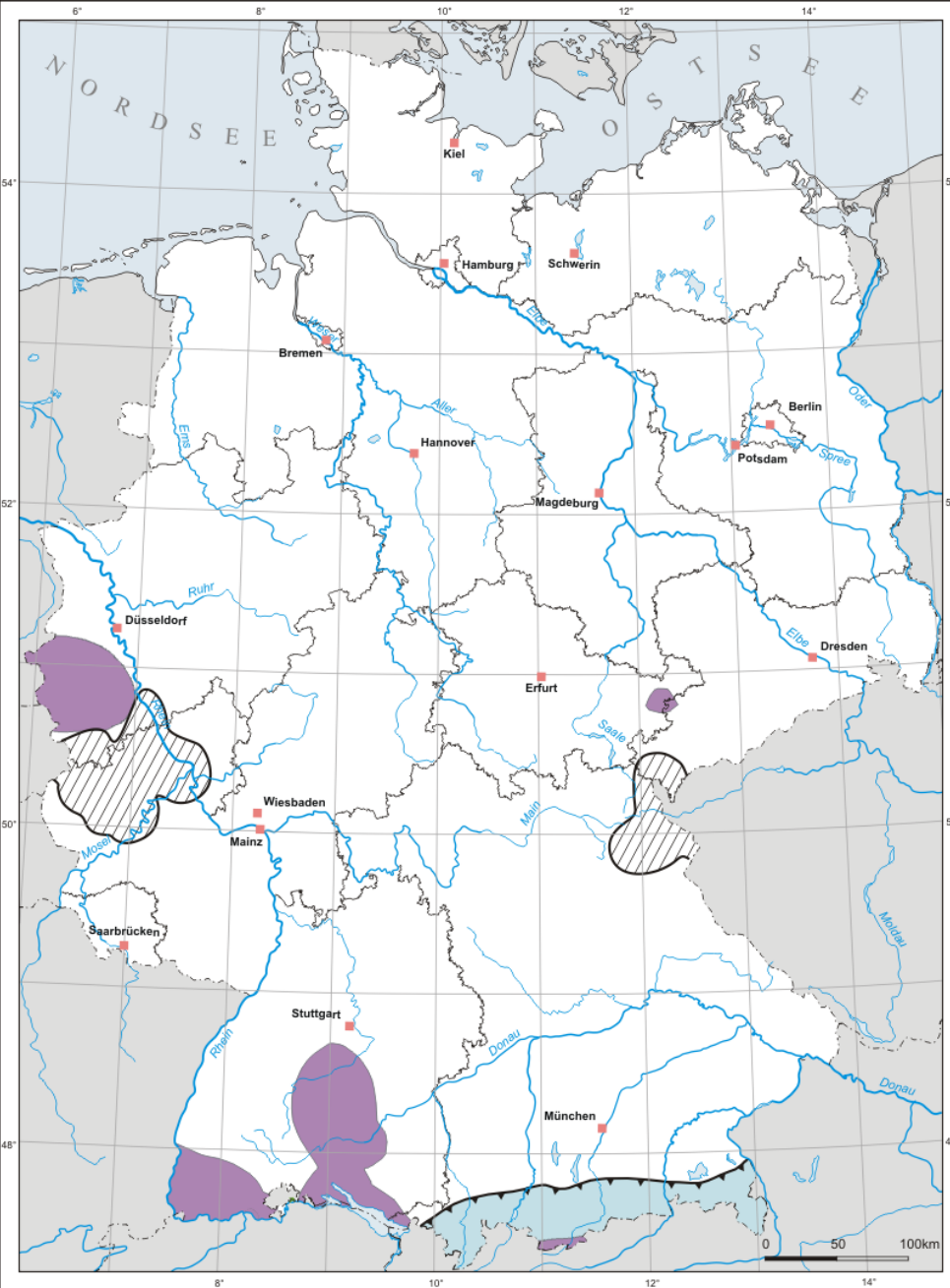
Fundamental requirements on the geological environment of a deep repository (IAEA, Nagra (CH), Andra (F))



- Long-term geological stability
- Favorable host rock properties
- Sufficient extent of host rock body
- Avoidance of, and insensitivity to, detrimental phenomena and perturbations
- Explorability
- Predictability

Basic exclusion criteria

- Large-area vertical movements
- Active fault zones
- Seismic activity
- Volcanic activity

Areas with seismic and volcanic risks in Germany



-  Seismic zone > 1 (DIN 4149)
-  Areas with increased risk of volcanism

Minimum requirements for disposal sites (1)

- The isolating rock zone must consist of rock types to which a field hydraulic conductivity of less than 10^{-10} m/s can be assigned
- The thickness of the isolating rock zone must be at least 300 m
- The repository mine must lie no deeper than 1,500m
- The isolating rock zone must have an areal extension that permits the realization of a repository (e. g. approximately 3 km² in salt or 10 km² in clay or granite)

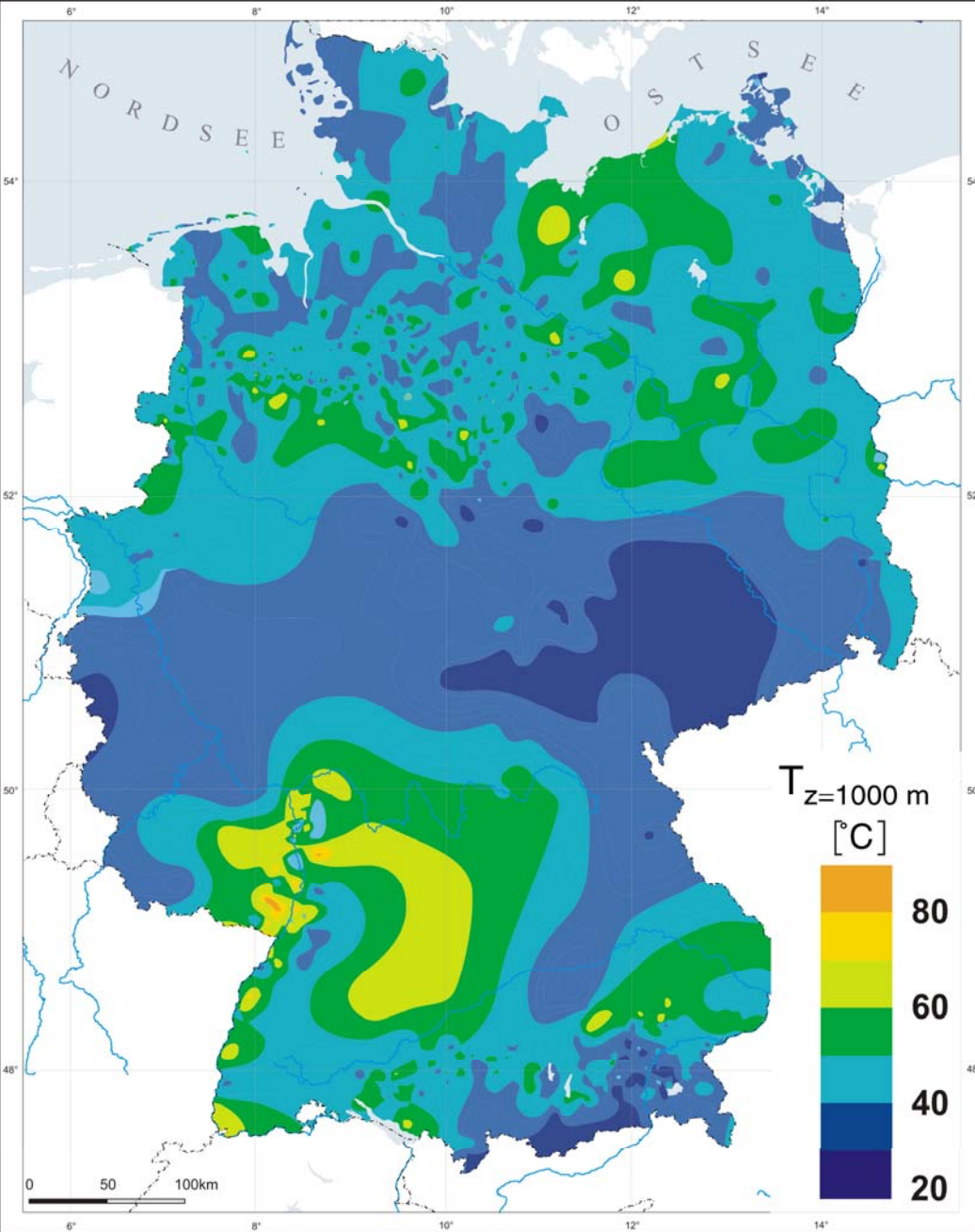
Minimum requirements for disposal sites (2)

- Neither the isolating rock zone nor the host rock must be at risk from rock burst
- There must be no findings or data which give rise to doubts whether the geoscientific minimum requirements regarding field hydraulic conductivity, thickness and extent of the isolating rock zone can be fulfilled over a period of time in the order of magnitude of one million years

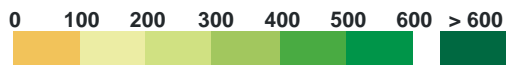
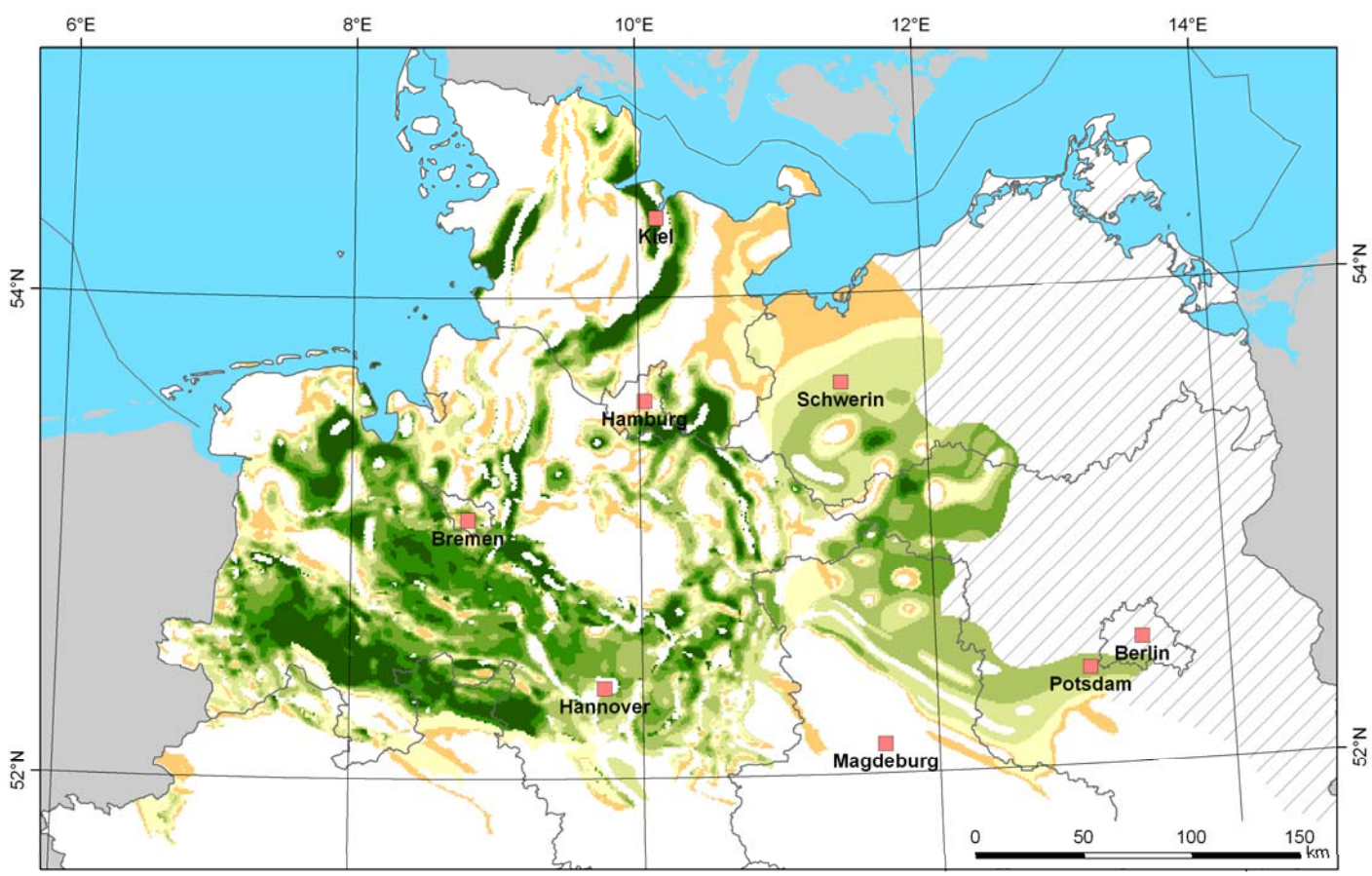
Additional specific exclusion criteria in Germany


- Repository must lie no deeper than 1000 m
- Clay with plastic behavior was excluded
- Additional regional restrictions

Temperature distribution in Germany

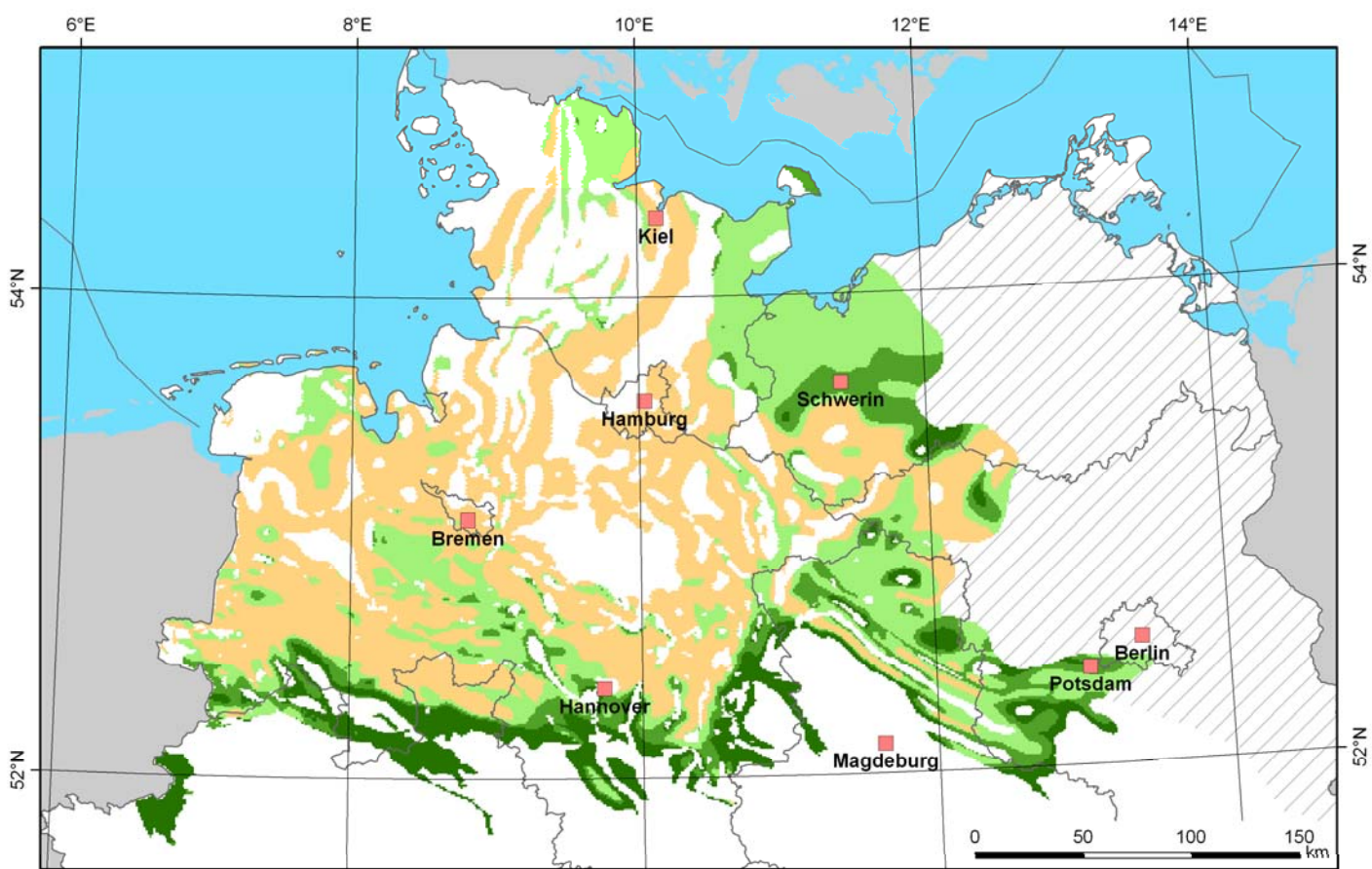


Temperature distribution (depth = 1000m)

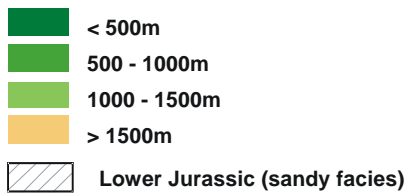


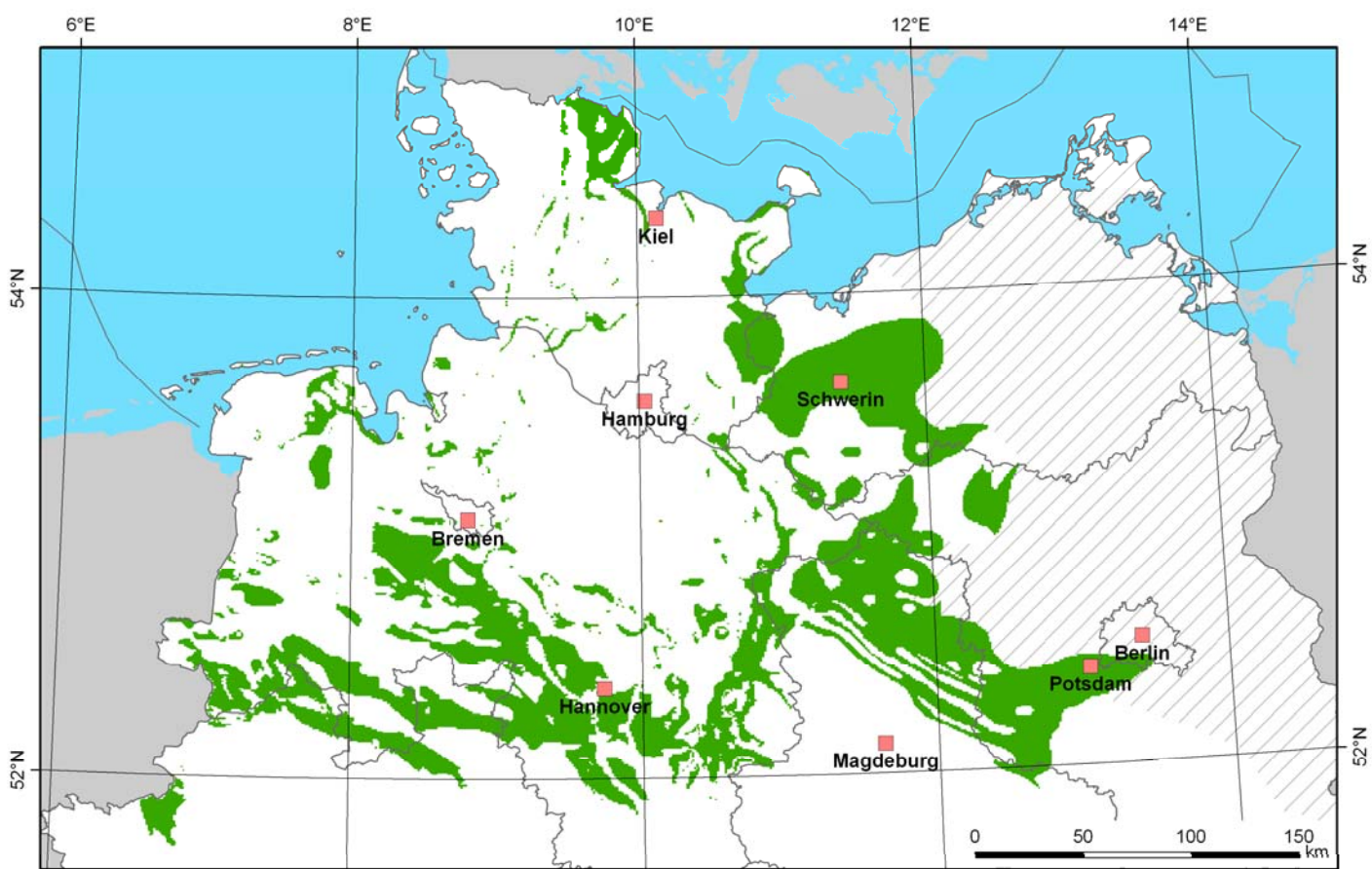
 Lower Jurassic (sandy facies)

Thickness [meter] of Lower Jurassic



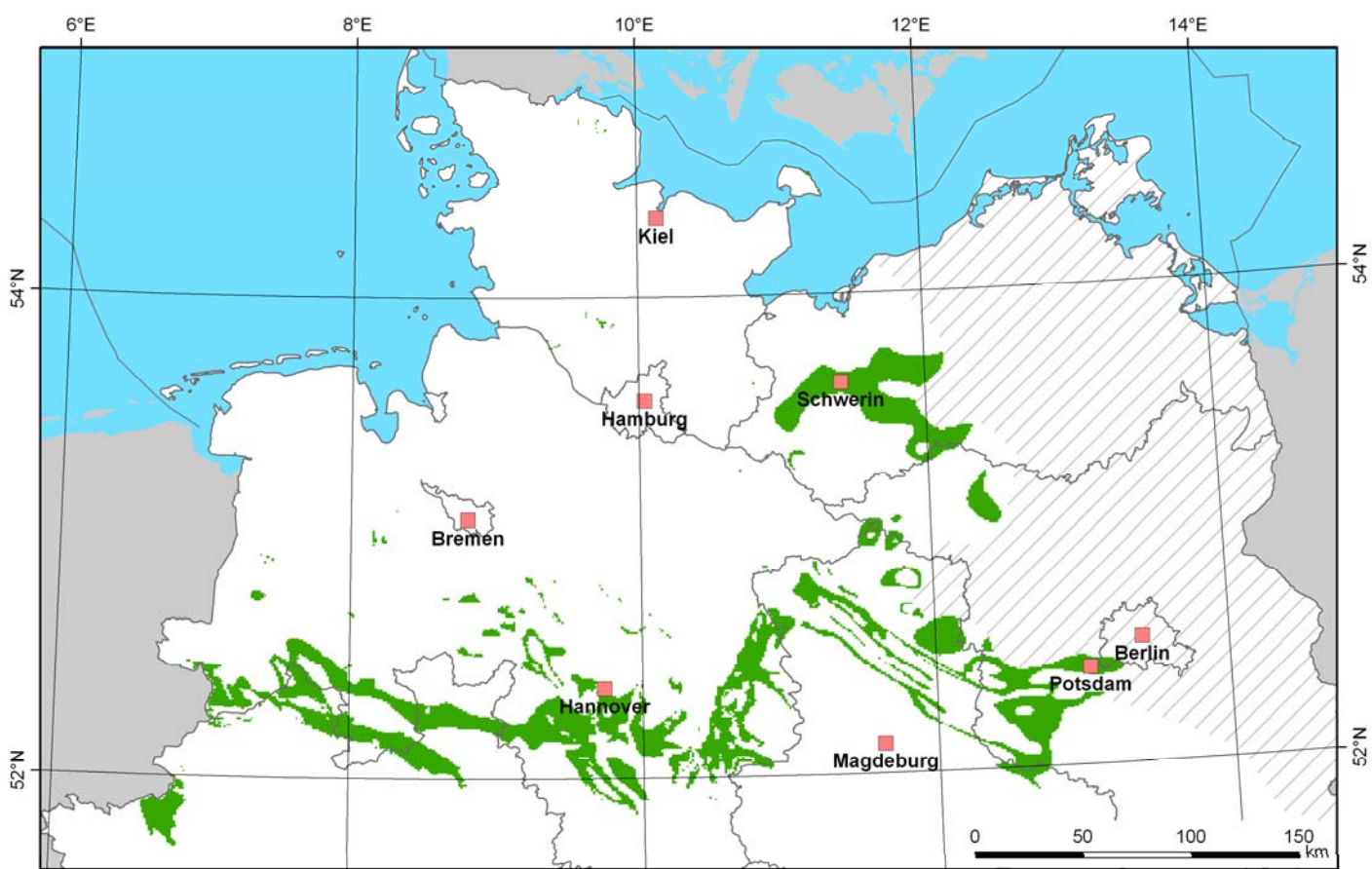
Depth of surface of Lower Jurassic [below Sea level]





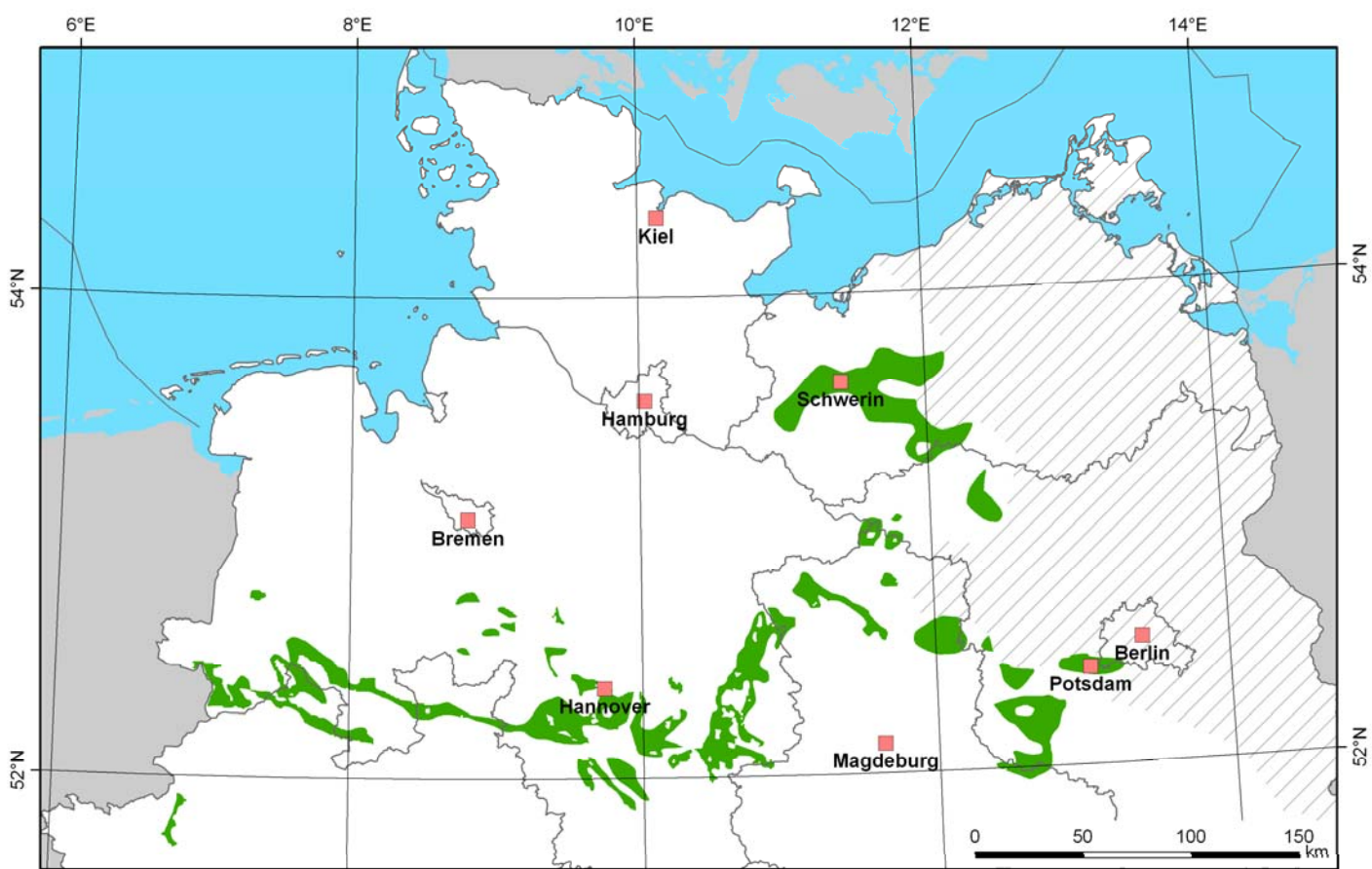
- Thickness > 100m
Depth < 1500m
(below ground surface)
- Lower Jurassic (sandy facies)

Minimum requirements / Lower Jurassic



- Thickness > 100m
Depth < 1000m
(below groundsurface)
- Lower Jurassic (sandy facies)

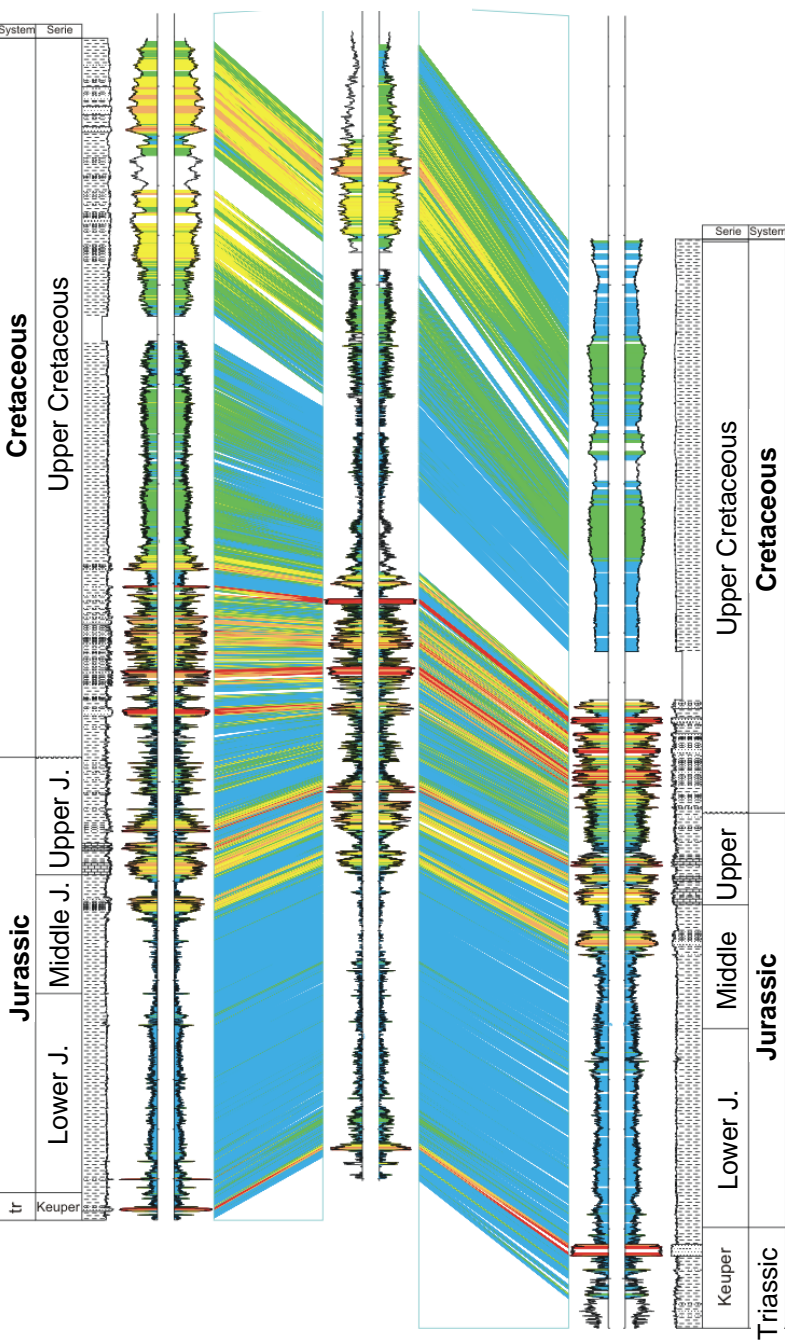
Claystone specific criteria / Lower Jurassic



- Thickness > 100m
- Depth > 300m and < 1000m
(below groundsurface)
- area > 10km²
(in good special characterisation)
- Lower Jurassic (sandy facies)

Application of all claystone specific criteria / Lower Jurassic

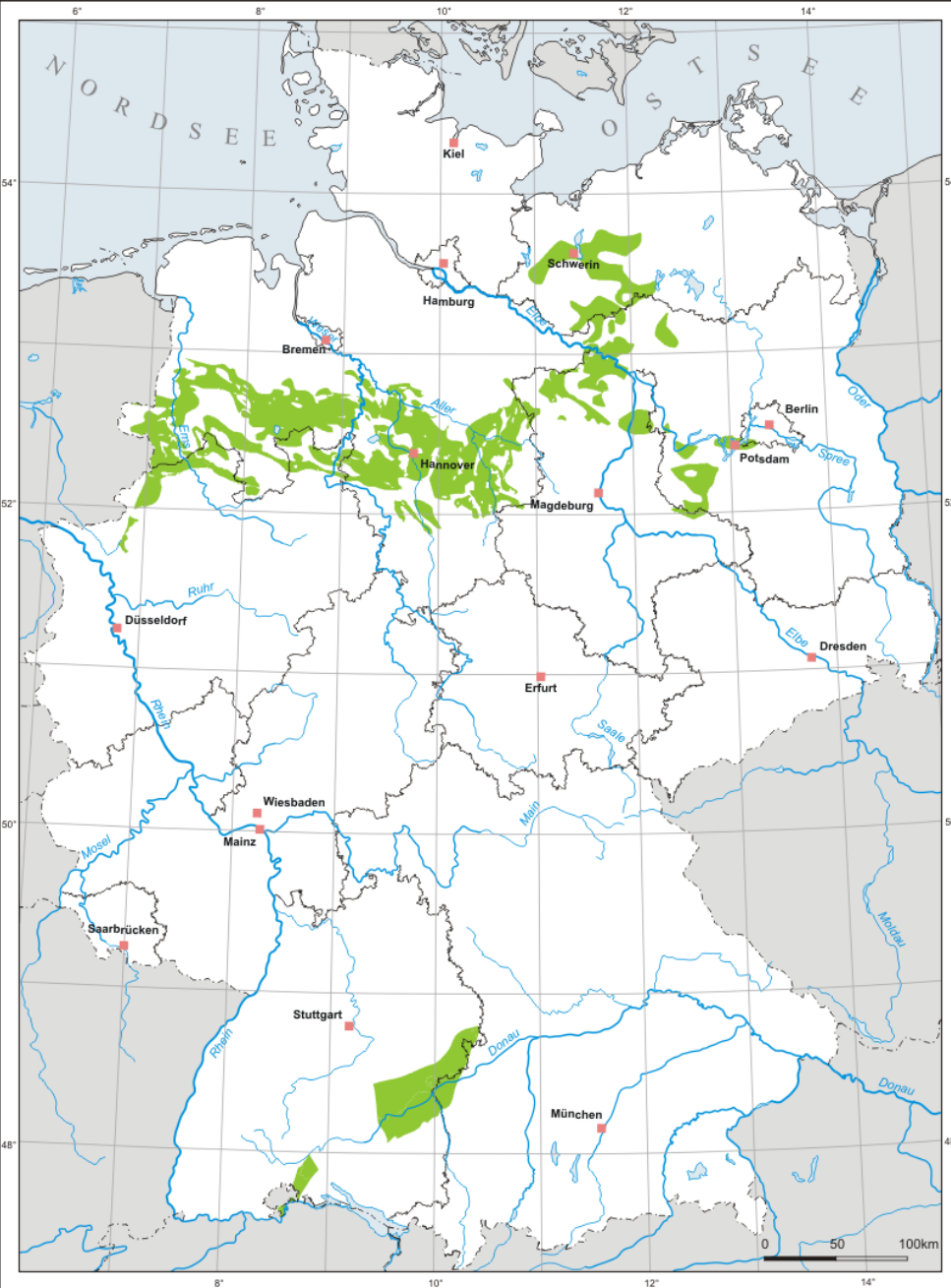
Borehole 1 Borehole 2 Borehole 3



Claystone formations

Example of borehole correlation

(Code CORRELATOR)



Claystone formations

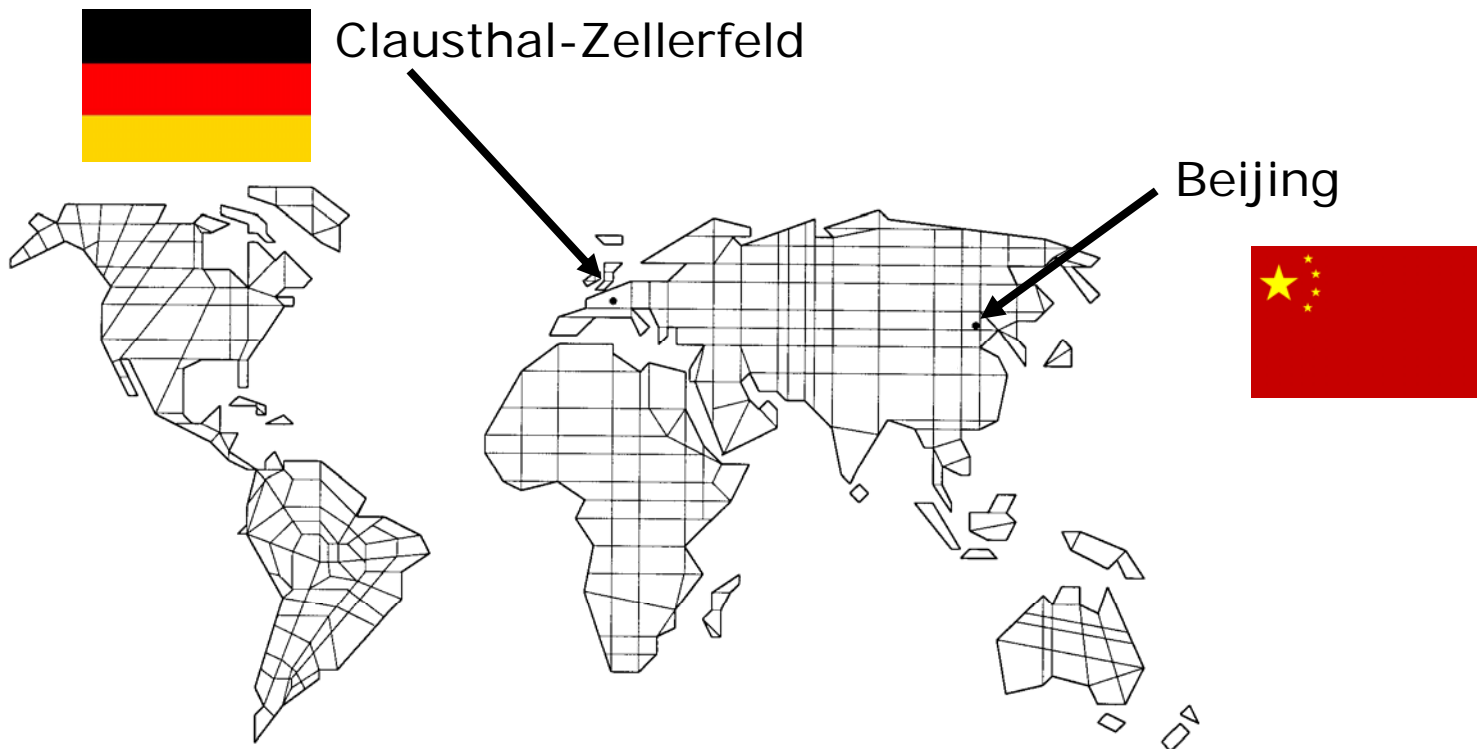
potentially suitable for further investigations in Germany

Future Research Activities

R+D	Salt	Claystone	Granite
Charakterisation of potential host rocks	x	X	(X)
Geotechnical barriers, Excav. Disturbed Zone	X	X	X
Siting of potential host rocks in Germany	(X)	X	(X)
Safety assessment	X	X	--



Chinese-German Workshop on Radioactive Waste Disposal



Sino-German Science Center, Beijing May 28-31, 2007

K.-H. Lux

Radioactive Waste Disposal in Various Host Rock Formations – *Some Geomechanical Aspects* *(Fundamentals)*

Short Version with selected aspects...

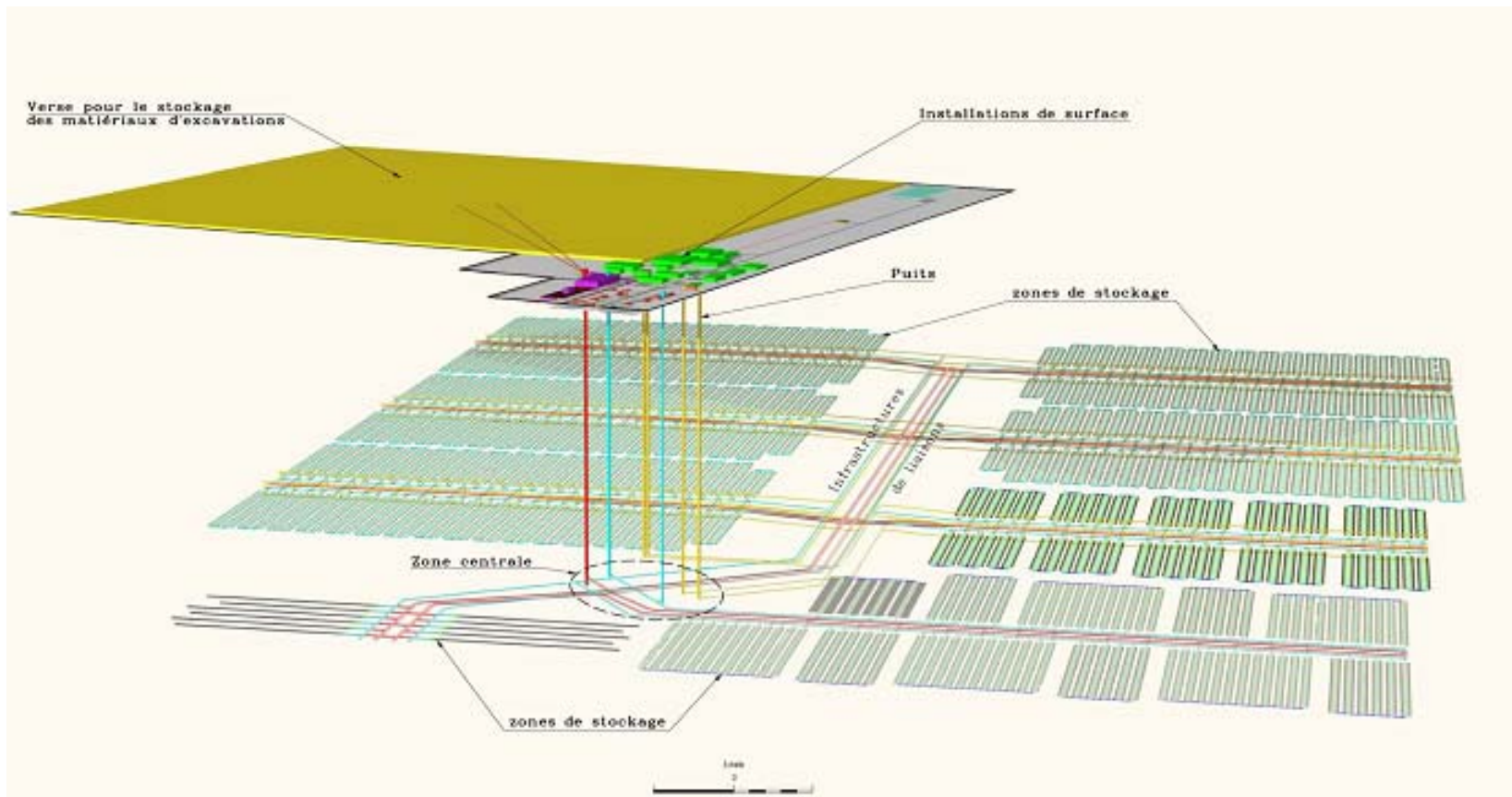


Contents

- Demonstration of Safety / General Aspects
- Waste Quantities and Properties
- Site Selection
- Physico-chemical Modelling / Coupled Processes
- Thermo-Mechanical – Hydraulic Aspects
- Geomechanical Aspects
- The Best Repository ?
- Conclusions



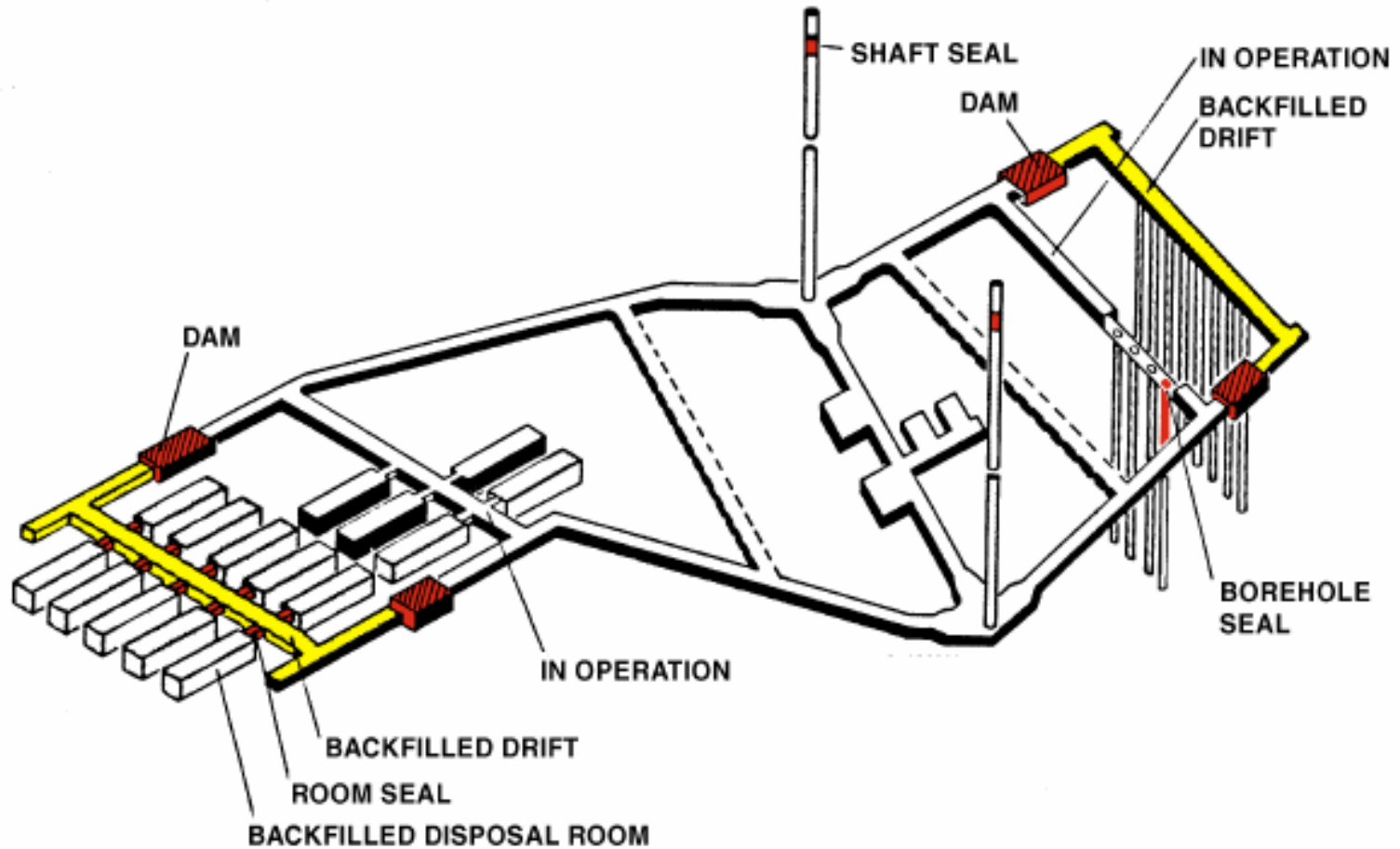
Reality and Prognosis: Disposal system (example)



⇒ Waste Repository = Complex geologic, geometric and physico-chemical system in space and time



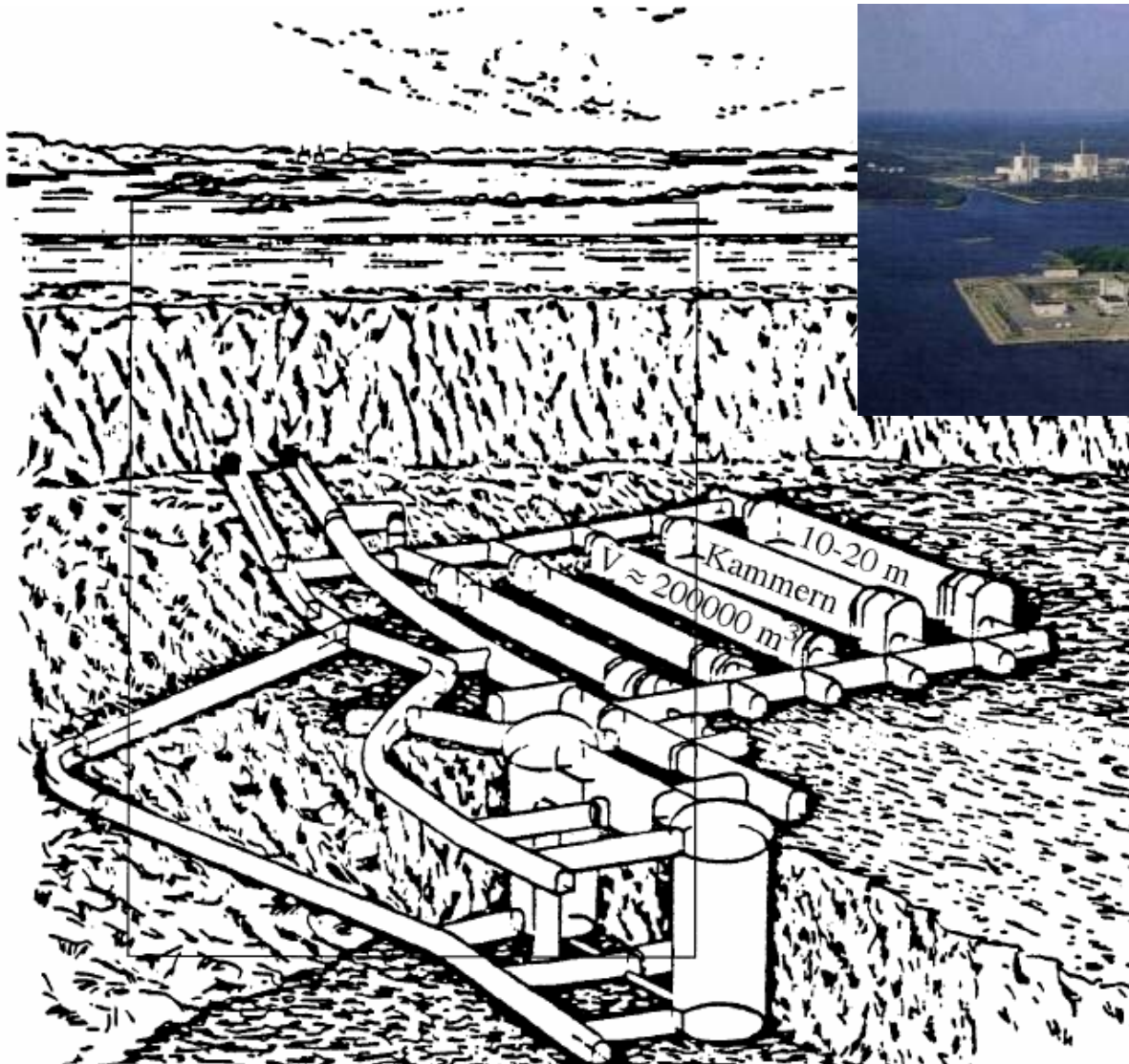
Schematic design of HA-Waste repository / rock salt



GRS (2005)



Schematic design of RN-Waste repository / granite



Final Repository Concepts for guarantee of long-term Safety

General demand:

Long-term safe and maintenance-free isolation of hazardous substances from the biosphere (cc-principle)

Basic concept:

- disposal of hazardous waste in (deep) underground formations
- identification of natural barriers against contaminant release
- design and construction of geotechnical and technical barriers
- development of site-specific multi-barrier system (Redundancy and Diversity)

⇒ *Appropriate Geosystems ?*



General Concepts:

Geological Barrier(s)

Geotechnical Barrier(s)
(borehole-/ drift-/ shaft-sealing)

Technical Barrier(s)

Concept 1

Concept 2

Final Repository Concepts for guarantee of long-term Safety

Granit, Claystone / Clay, Rock Salt

Geological Barrier(s)

Geotechnical Barrier(s)

(borehole-/ drift-/ shaft-sealing)

Technical Barrier(s)

Concept 1 **Requirement:**
Rock mass with sufficient
low permeability

Concept 2 **Requirement :**
Containers with sufficient
functionality in the rele-
vant ambience (M,H,T,C)

? Long-term Behaviour / Long-term Safety ?

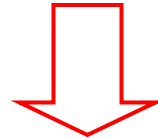
⇒ favourable Geosystems ?

⇒ site selection procedure?



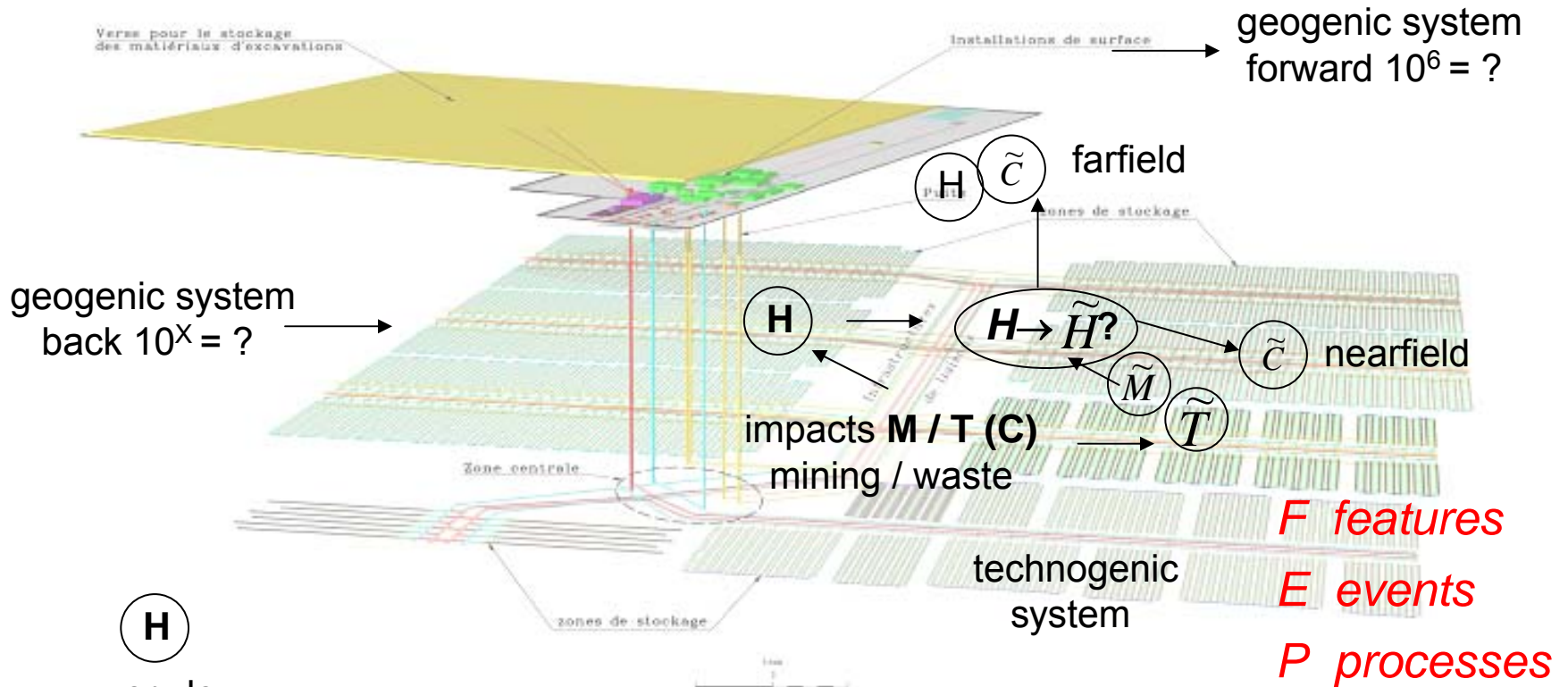
Basic experiences of Geoscience / Geotechnics

- Geosystems are exposed to natural/technical impacts
- Geosystems are changing with time at different rates depending on impacts and related physicochemical processes
- Processes active in geosystems are of different kind and intensity influencing each other:



thermal, hydraulic, mechanical, chemical as well as biological processes are possible, acting in space and time and depending on the individual geosystem and the technical activity.

Physico-chemical Modelling / Coupled processes Repository-system and Effects / Processes



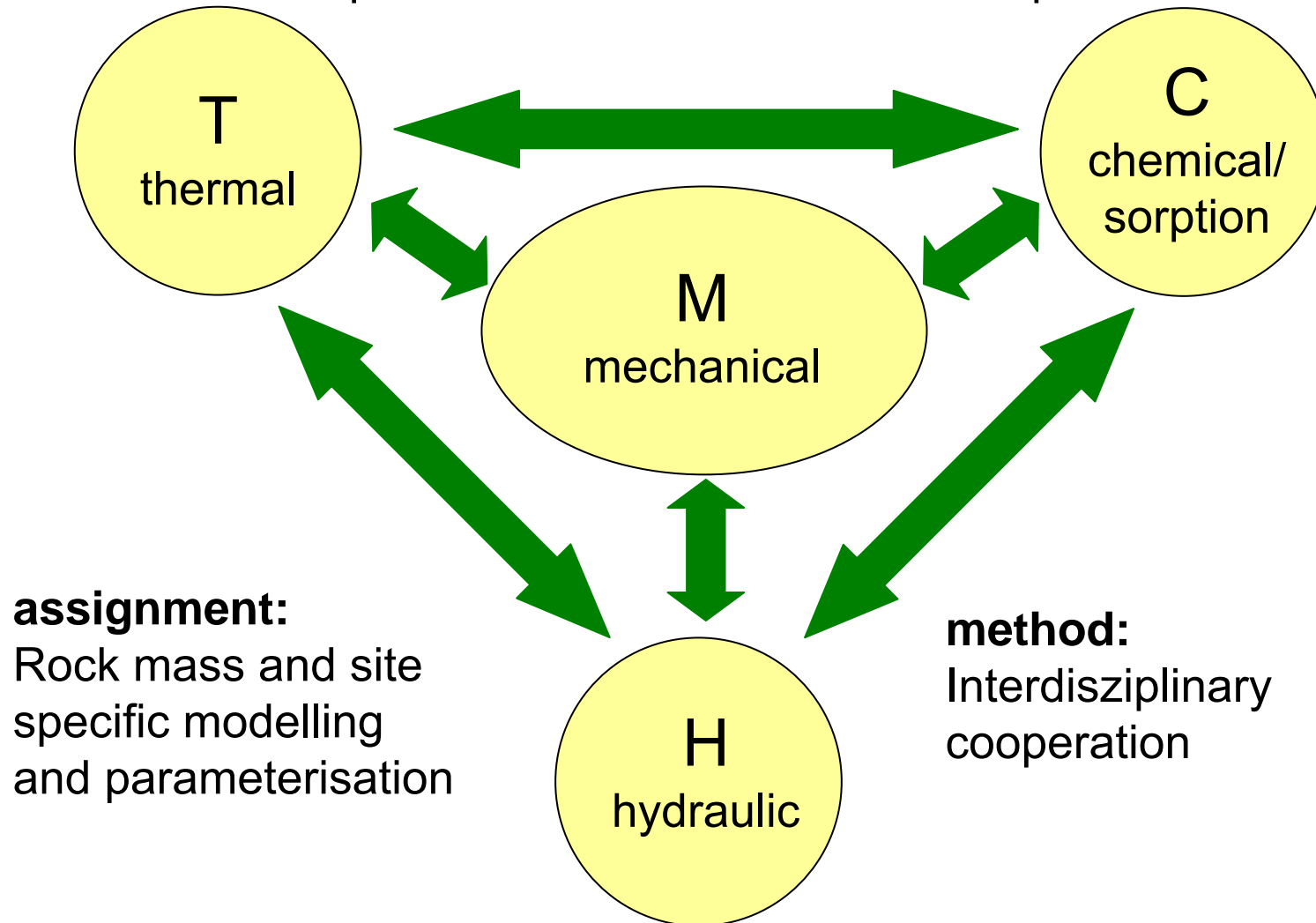
\textcircled{H}
 very low
 permeability

probability of occurrence of **FEP's** (impacts on geosystem)
 high \rightarrow ordinary development \Rightarrow complete isolation
 low \rightarrow case scenario \Rightarrow admissible release

F features
E events
P processes

Coupling of processes – general/present state and further development

from present state \Rightarrow to further development



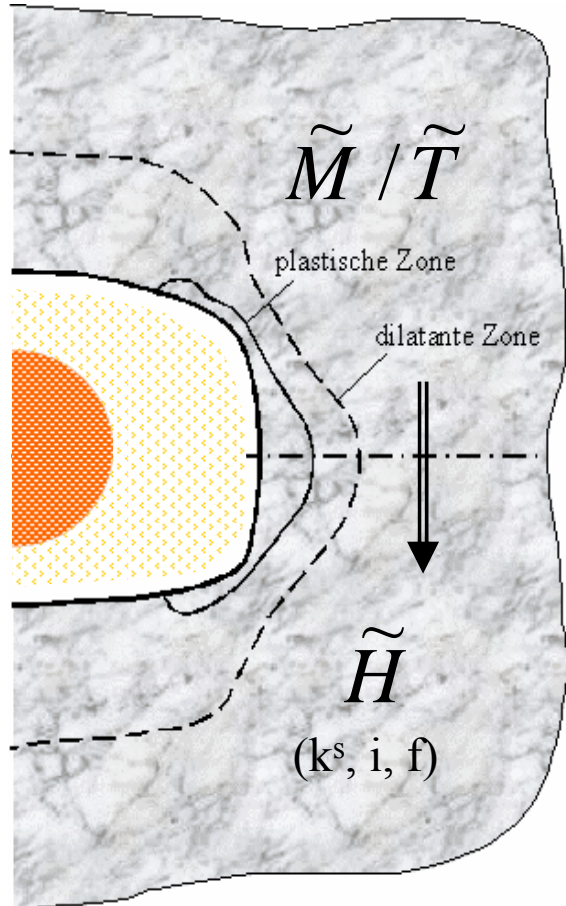
- Some Aspects with respect to change of mechanical / hydraulic properties
 - *Nearfield processes/EDZ*
 - *Damage process – rock salt*
 - *Damage process – claystone*
 - *Recreation of damage/Rehealing – rock salt*
 - *Pressure-forced infiltration of fluids (liquids, gas) in primarily impermeable or nearly impermeable rock formations*
 - *Damage process - granite*

- Some Aspects with respect to change of mechanical / hydraulic properties
 - *Nearfield processes/EDZ - basics*
 - *Damage process – rock salt*
 - *Damage process – claystone*
 - *Recreation of damage/Rehealing – rock salt*
 - *Pressure-forced infiltration of fluids (liquids, gas) in primarily impermeable or nearly impermeable rock formations*
 - *Damage process - granite*

THM-Processes in the nearfield of a drift with disposed waste (EDZ)

rock salt - clay stone/clay - granite

Nearfield processes - Excavation Damage Zone (EDZ)



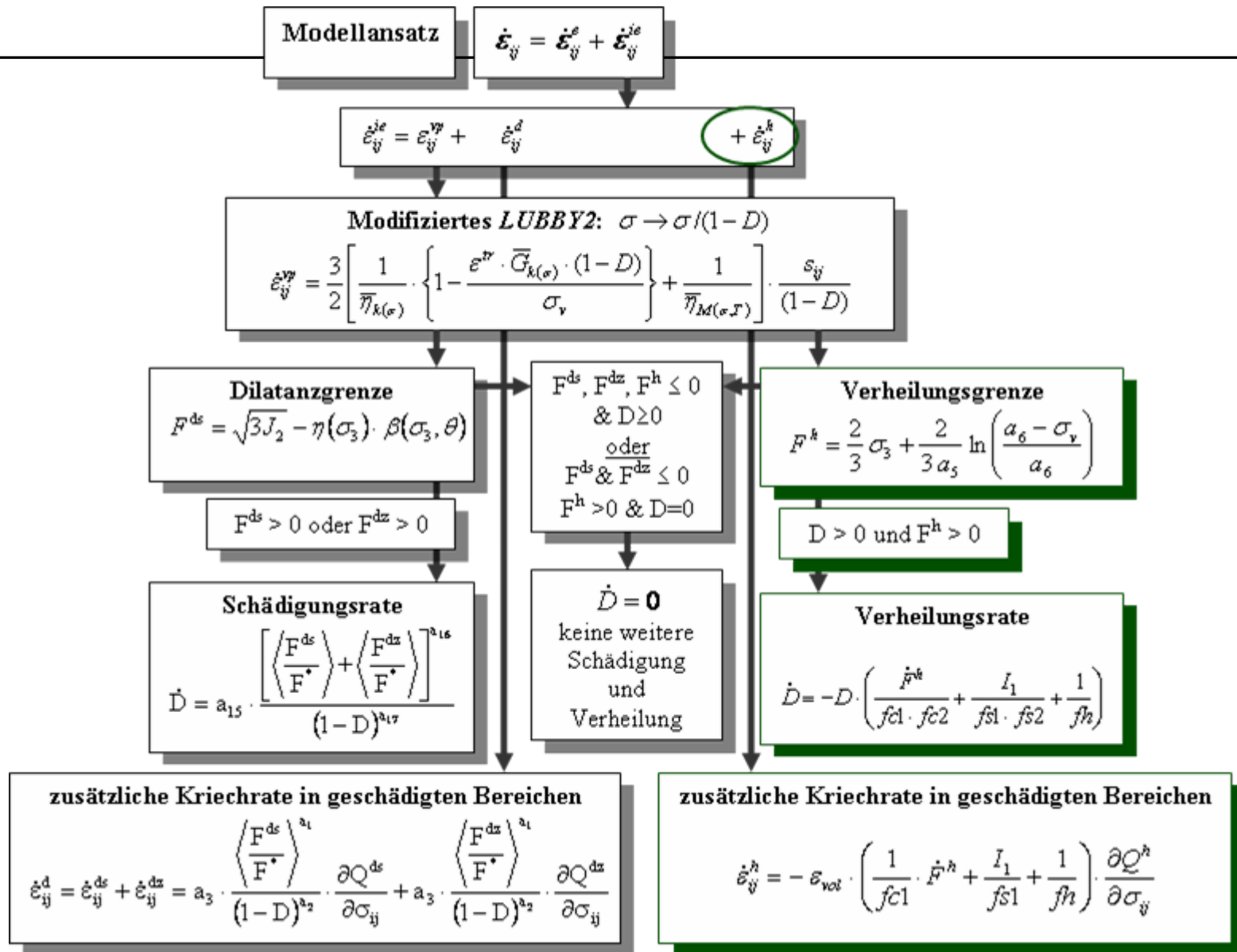
process	⇒	influenced properties
mechanical	M	stress rearrangement deformation rock mass loosening rock mass instability contour fracture
thermal	T	additional stress additional deformation strength strain
hydraulic	H	fluid viscosity (water, brine, gas) fluid pressure porosity permeability

secondary pathways?

⇒ dilatancy limit / rupture limit ?



Constitutive Model including creep, damage and re-healing of damage



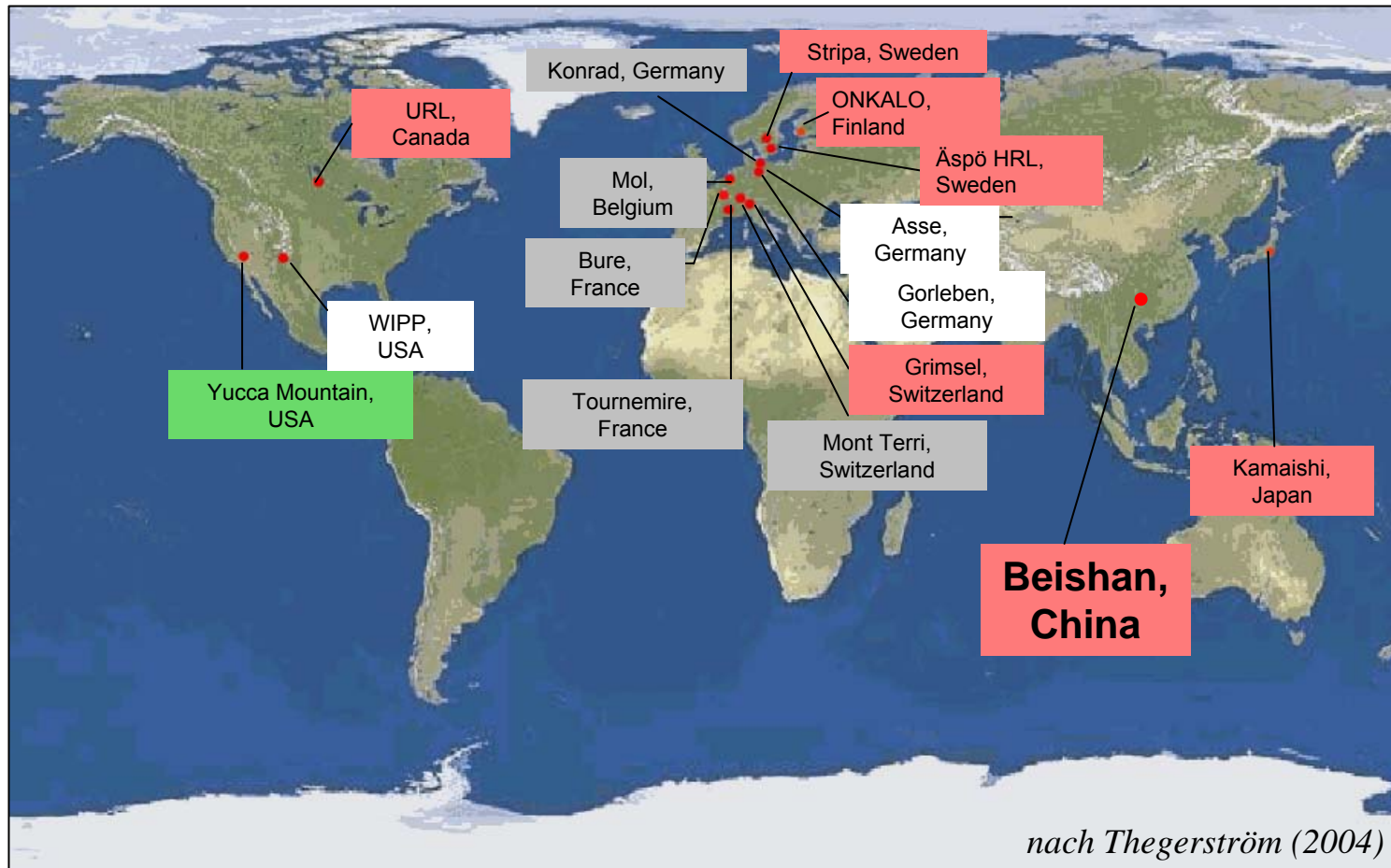
Rock salt samples and laboratory investigation



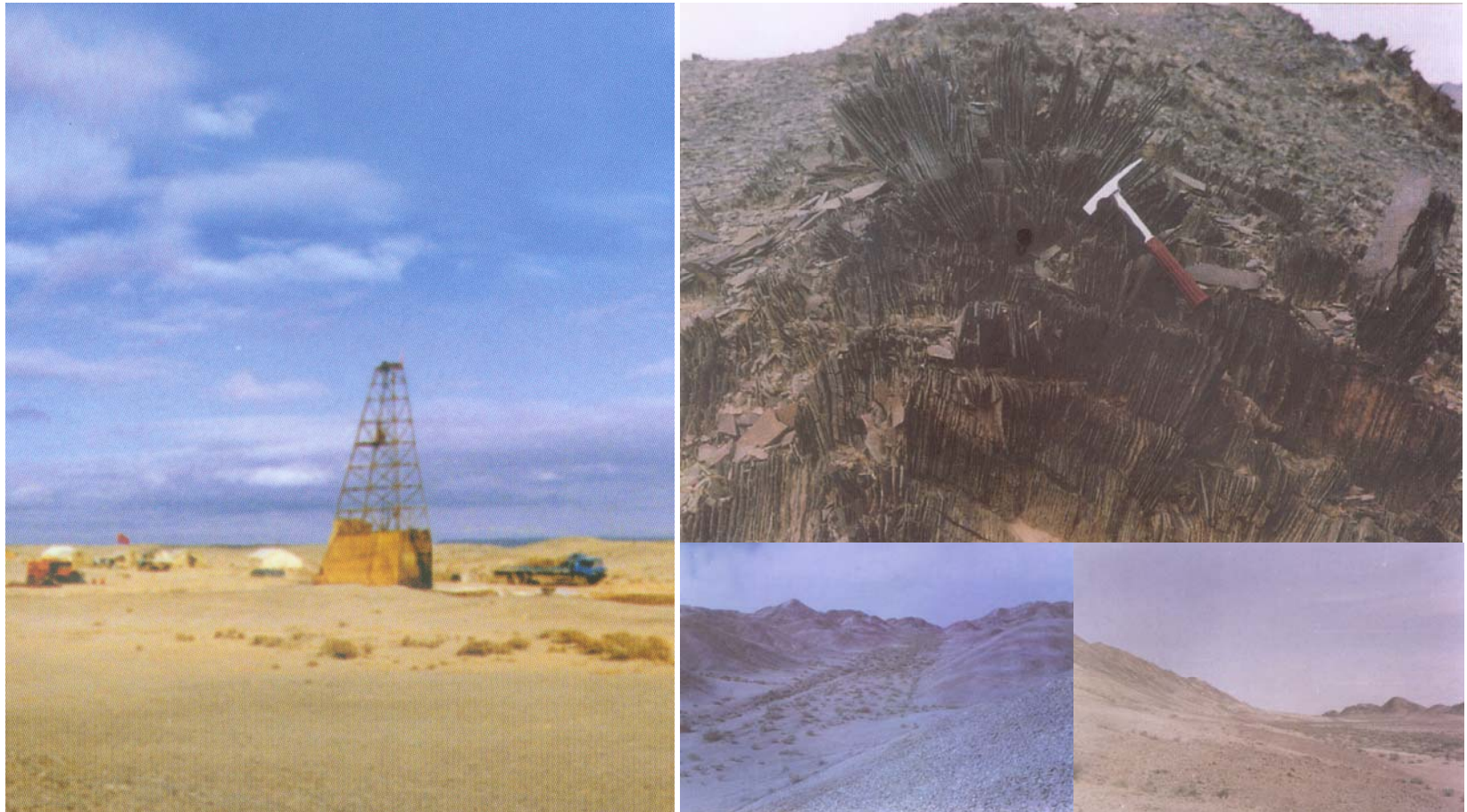
- Some Aspects with respect to change of mechanical / hydraulic properties
 - *Nearfield processes/EDZ - basics*
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 - *Recreation of damage/Rehealing – rock salt*
 - *Pressure-forced infiltration of fluids (liquids, gas) in primarily impermeable or nearly impermeable rock formations*
 - **Damage process – granite**
 - Lab Investigations:
 - **Some preliminary calculations with respect to static stability/ EDZ evolution - granite**

Repository sites and URL– Geographic Positions

HLW-Repository site in China



HLW-Repository in China – Some Impressions of Site



HLW-Repository in China – Investigation 2004

Rock Material / Granite



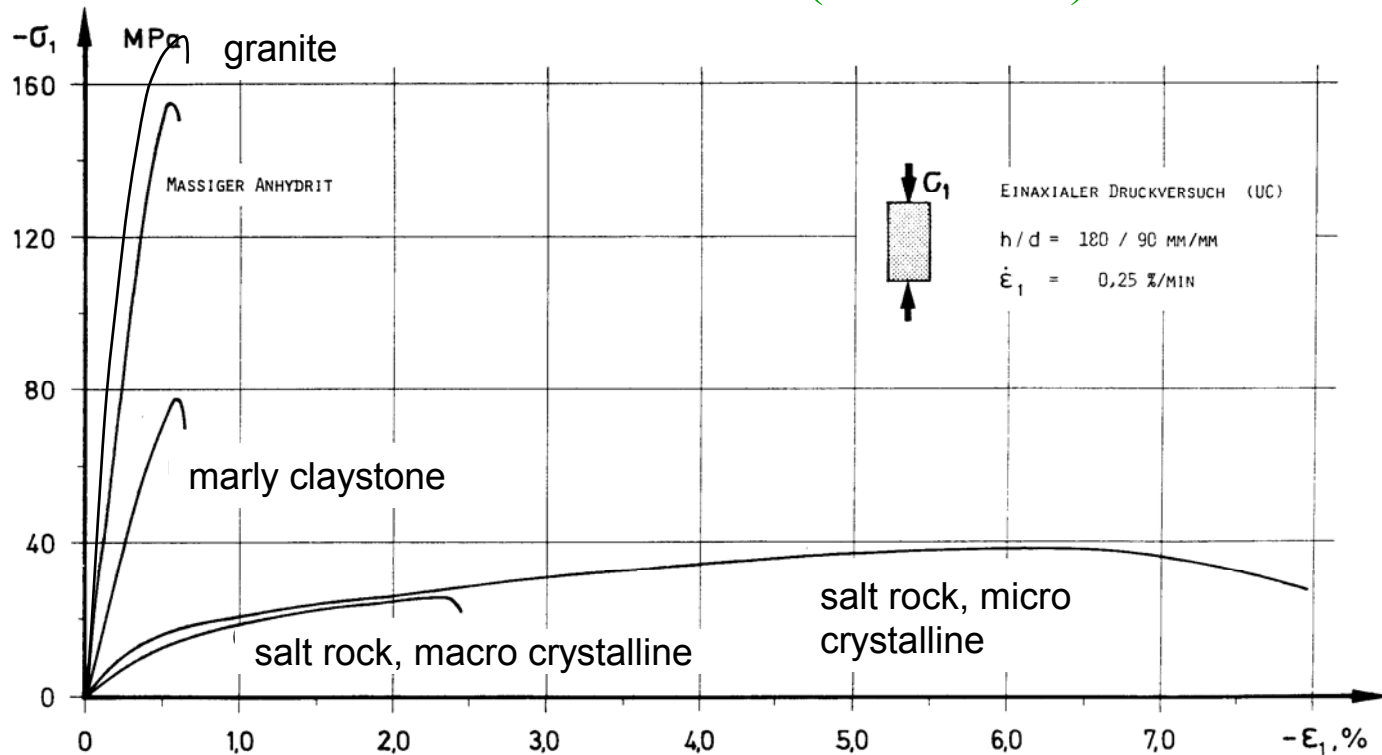
Test sample before and after failure with single macro-fracture (different scale)



Thermo mechanical – hydraulical Aspects

Exemplary drift – **granite** / operation mode (1/2)

No viscous deformation rates (rock matrix)

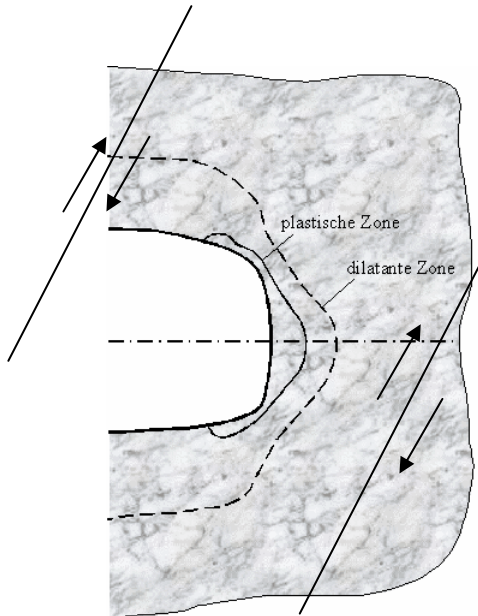


Deformation rates of different rocks of uniaxial compression load at room temperature, *Lux (1984)*



Thermo mechanical – hydraulic Aspects

Exemplary drift – granite / operation mode (2/2)



fissure opening/
-enlargement?

$\beta = f(\text{rock, discontinuities})$

$\beta_D = f(\text{rock})$

Modelling of geomechanical Processes (M)

$$\dot{\epsilon} = \dot{\epsilon}^{el} (+ \dot{\epsilon}^{vp})$$

$$\dot{\epsilon} = f(\sigma, T, E, \nu, \beta, \beta_S, \beta_D)$$

Modelling of geomechanical / geohydraulic Processes (M→H)

$$K^P = K^P_{\text{Matrix}} + K^P_{\text{Fis}} (?)$$

K^S caused by the type of excavation (blasting, TBM)?

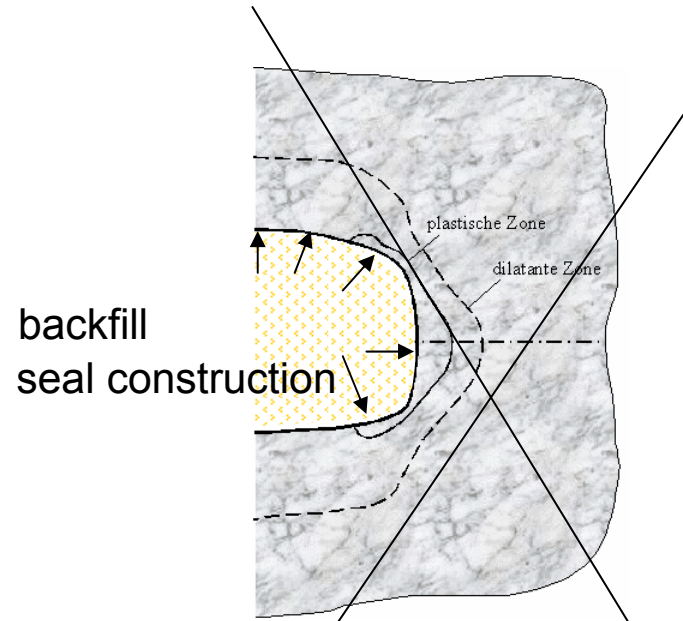
K^S because of excavation?

K^S because of temperature change?

PorPerm-Model: ...

Thermo mechanical – hydraulic Aspects

Exemplary drift – **granit** / post operation mode (2/2)



**Fissure degeneration
caused by P_A ?**

$\beta = f(\text{rock, discontinuities})$

$\beta_D = f(\text{rock})$

Modelling of geomechanical Processes (M)

$$\dot{\varepsilon} = \dot{\varepsilon}^{el} (+\dot{\varepsilon}^{vp})$$

$$\dot{\varepsilon} = f(\sigma, T; E, \nu; \beta, \beta_S, \beta_D)$$

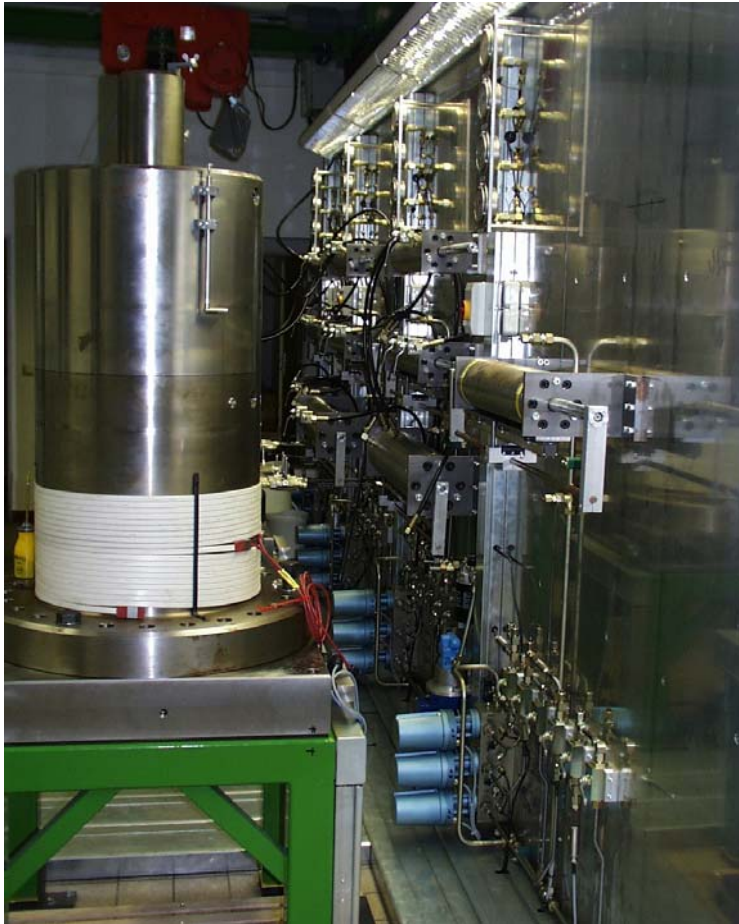
Modelling of geomechanical / geohydraulic Processes (M→H)

$$K_{\text{Matrix}}^S \ll K_{\text{Fis}}^S \text{ bzw. } K_{\text{Fis}}^P$$

⇒ fissure permeability dependent (in situ-tests)

Thermo mechanical – hydraulic Aspects

Exemplary drift – **granit** / post operation mode (1/2)

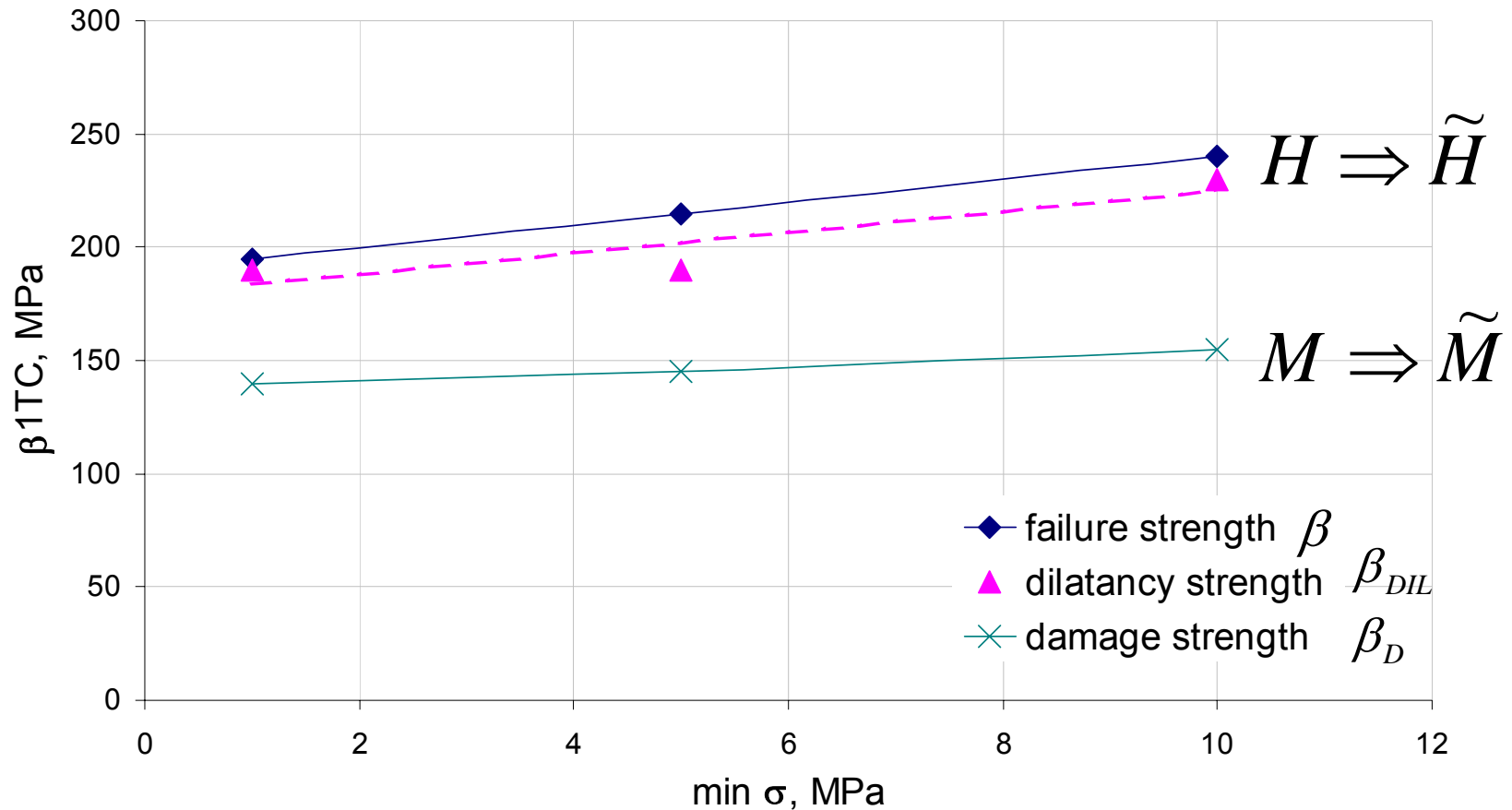


Current assessment:

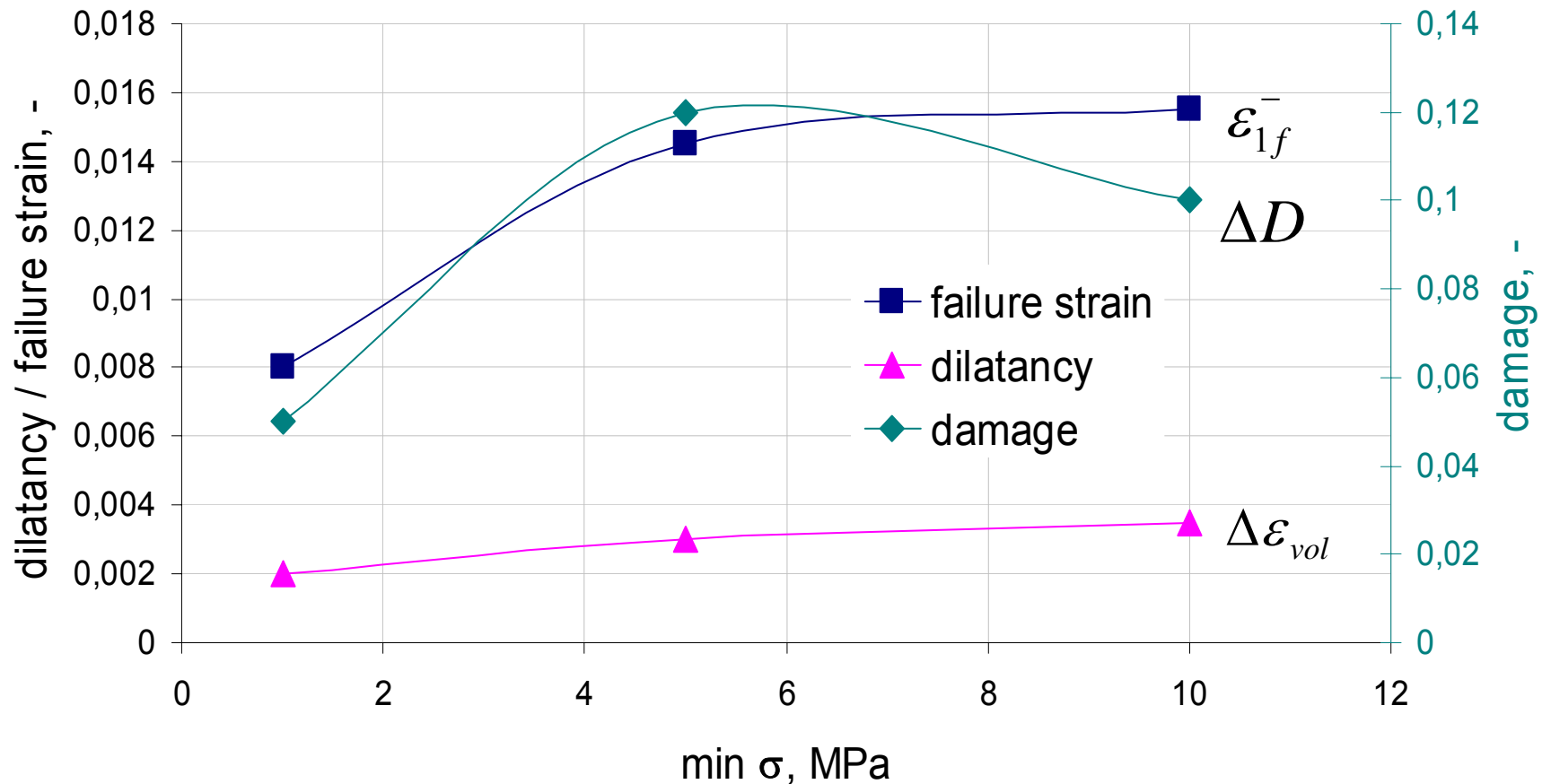
Only marginal fissure regeneration

- elastic recompaction
- no fissure healing without secondary mineralisation caused by precipitation

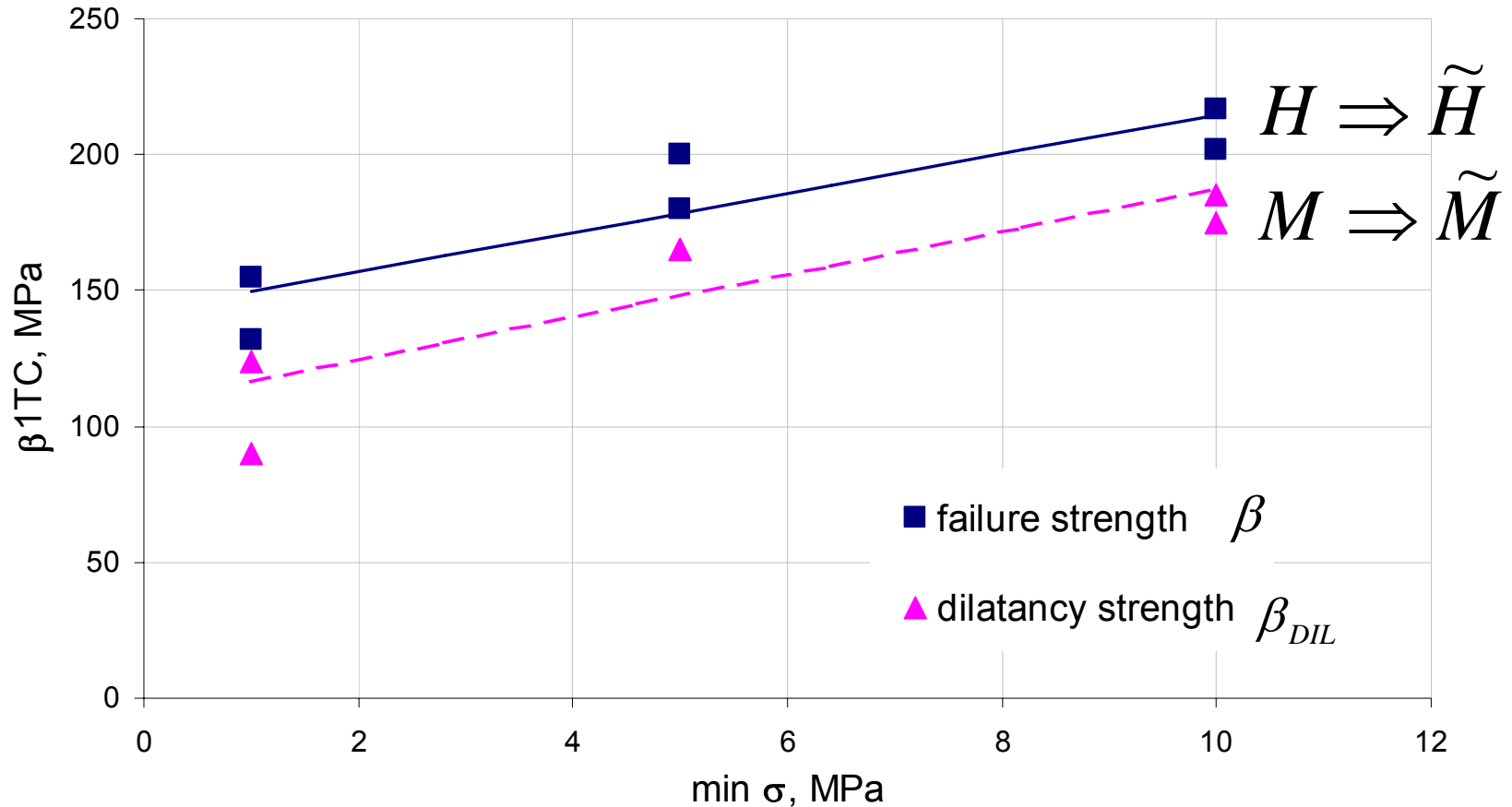
Mechanical data for granite type 1 with respect to minimal stress: failure strength, dilatancy strength, damage strength



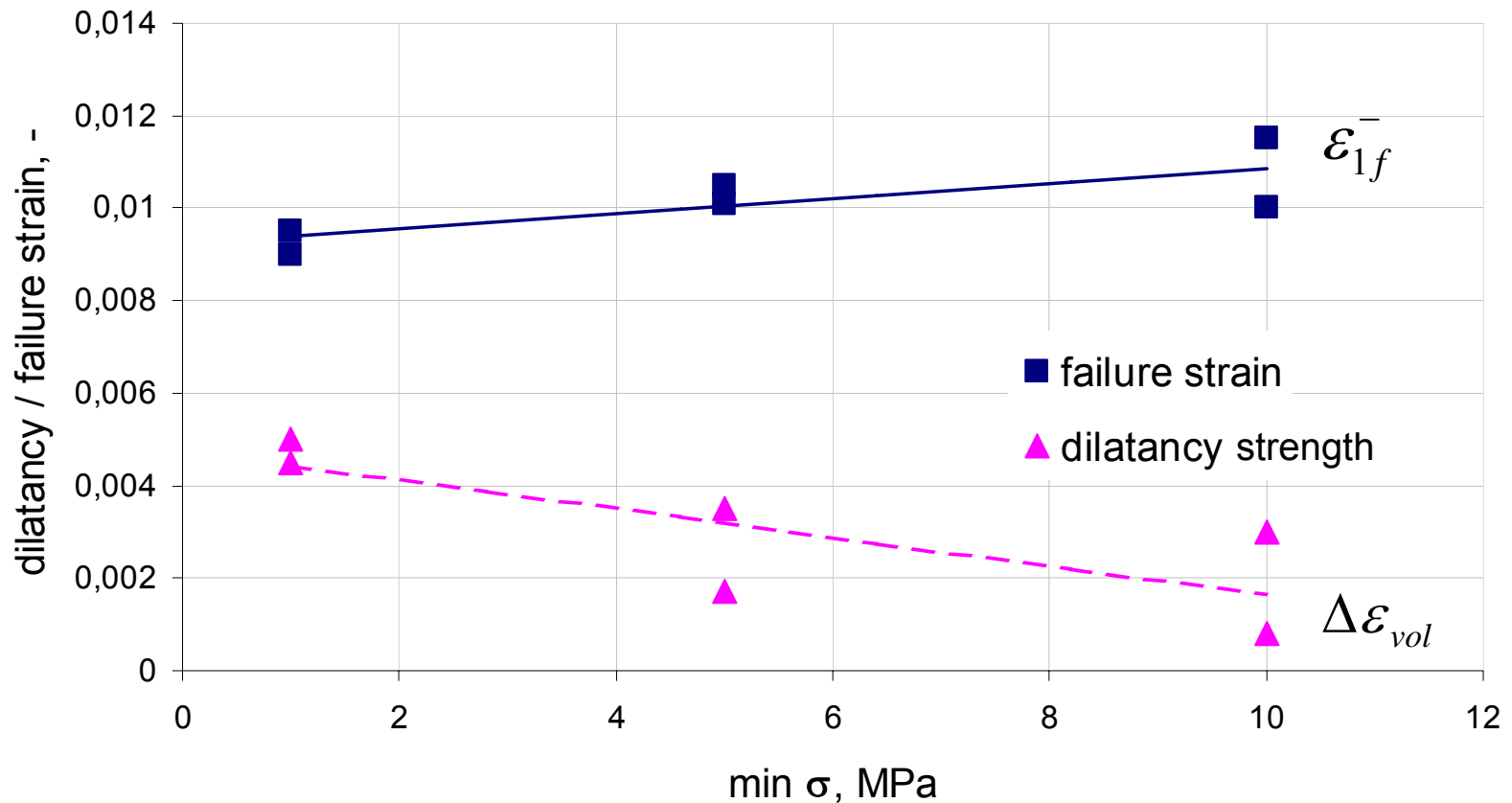
Mechanical data for granite type 1 with respect to minimal stress: failure strain, dilatancy, damage



Mechanical data for granite type 2 with respect to minimal stress: failure strength, dilatancy strength, damage strength



Mechanical data for granite type 2 with respect to minimal stress: failure strain, dilatancy, damage



Investigation 2007...

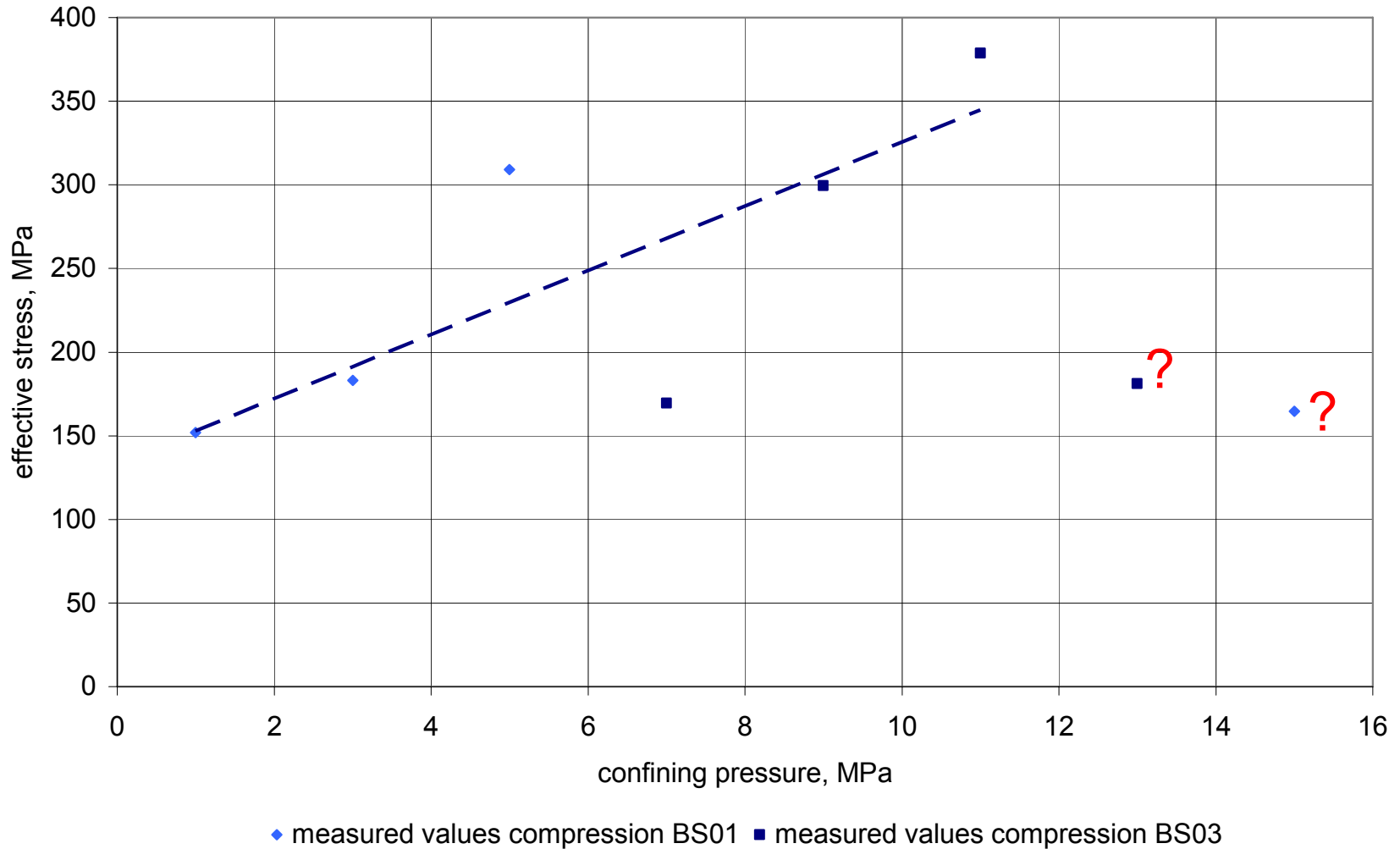
Granite samples from Beishan locations BS01 and BS03



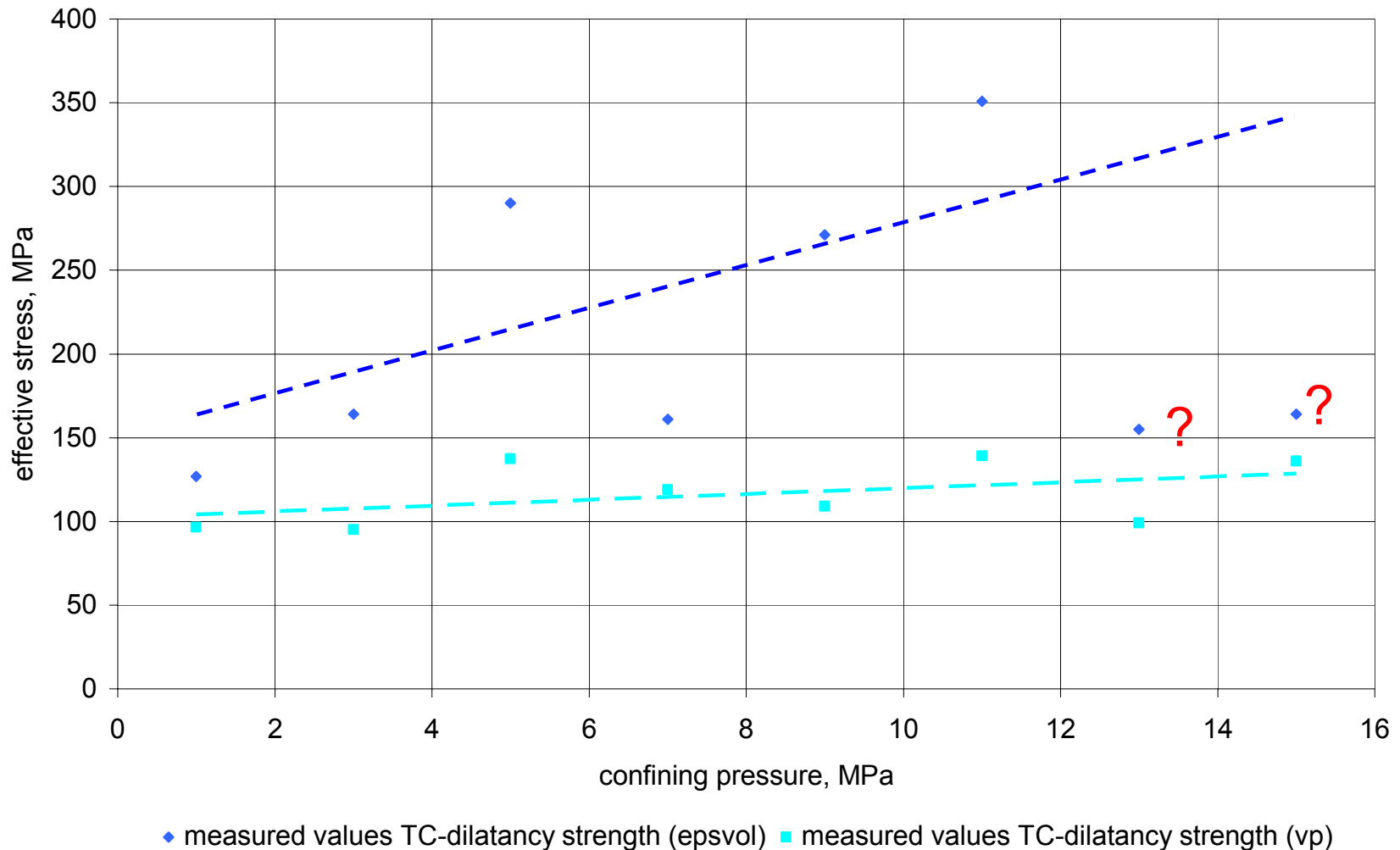
...within the context of an agreement between CNNC and TUC on research in the field of radioactive waste disposal in granite formations



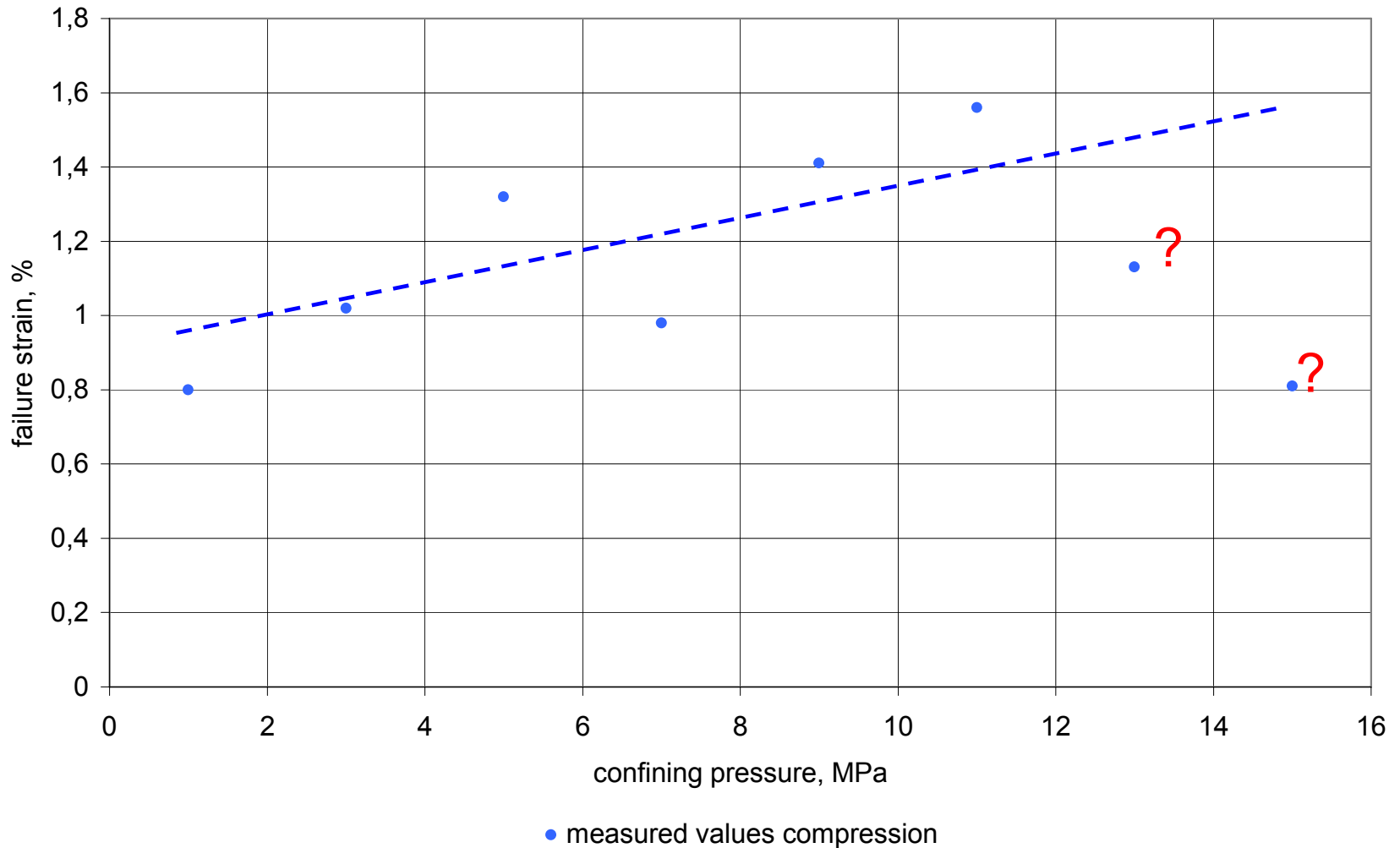
Failure strength of granite from Beishan locations BS01 and BS03



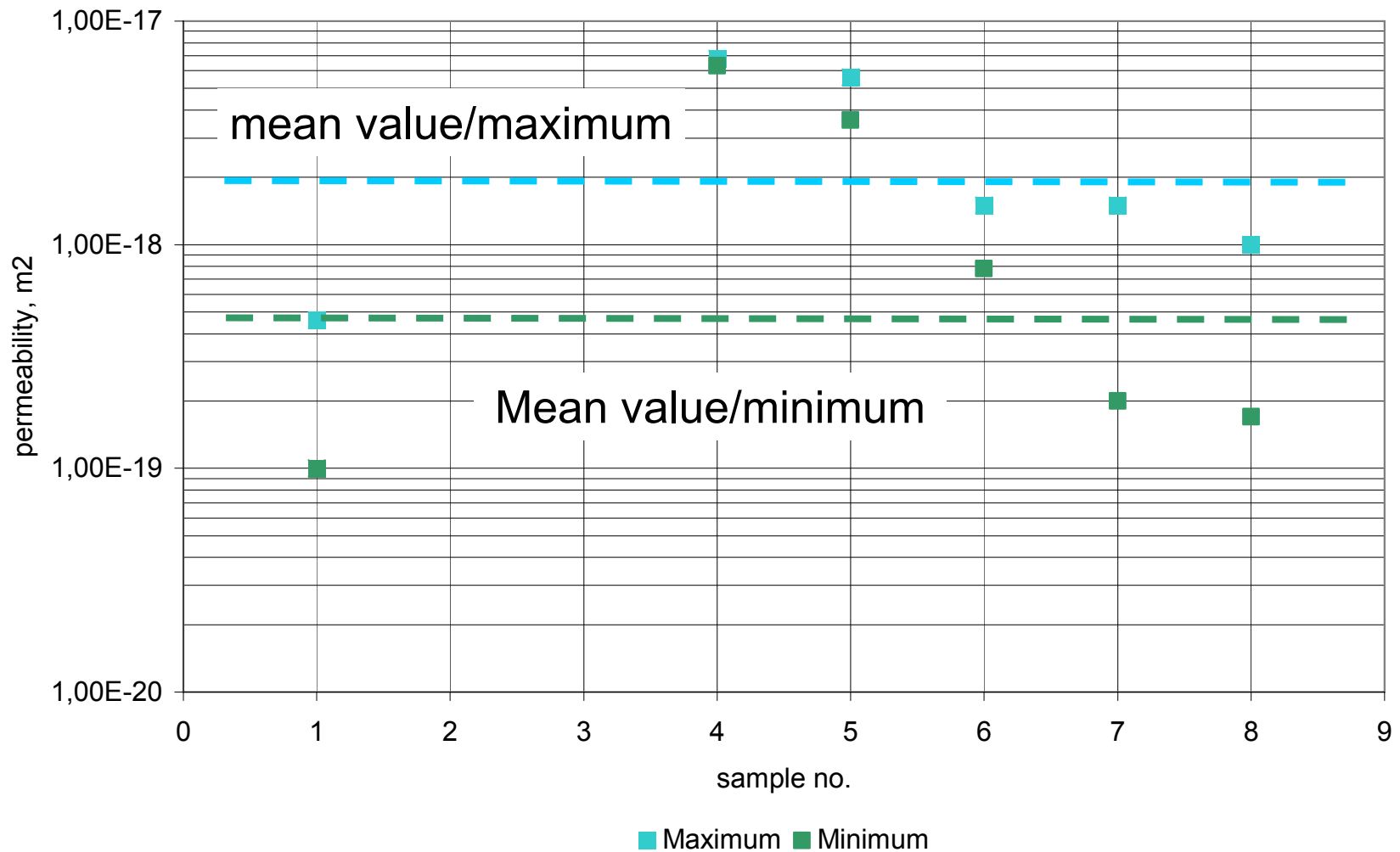
Dilation strength of granite from Beishan locations BS01 and BS03



Failure strain (TC) of granite from Beishan location BS01 and BS03



Permeability of granite from Beishan locations BS01 and BS03

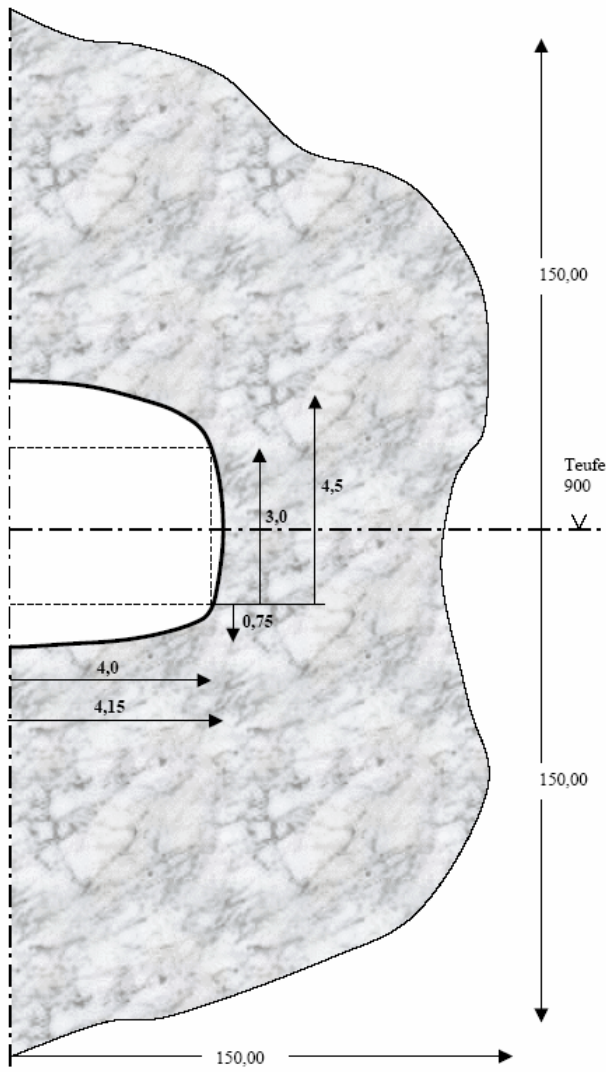


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 - Damage process – granite
lab investigations
 - Some preliminary calculations with respect to static stability /
EDZ evolution - granite
- The Best Repository ?
- Conclusions



Drift in granitic rock mass - example



Basic assumptions:

- Homogeneous isotropic rock mass
- linear - elastic ideal plastic material behavior
- Material properties

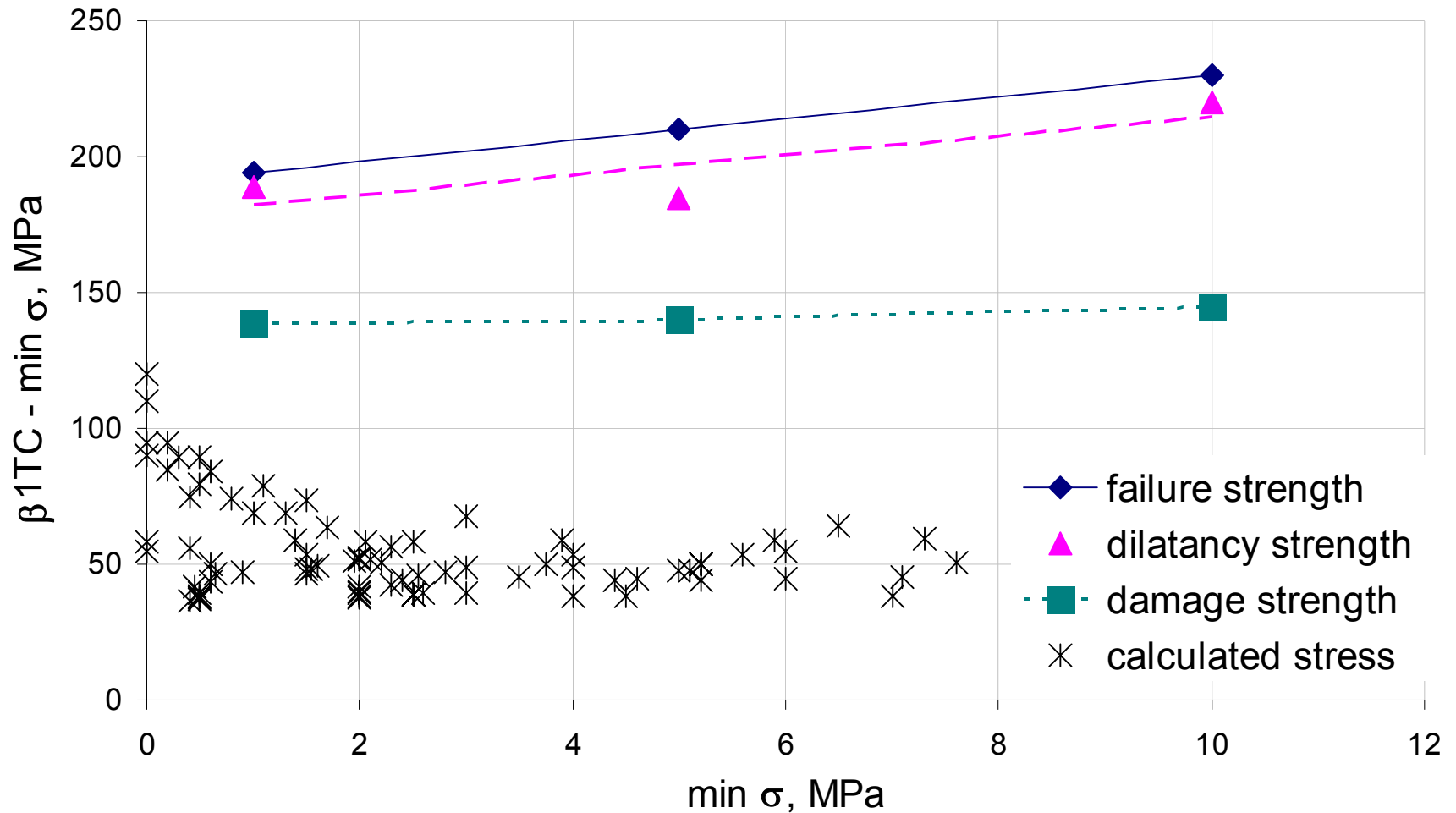
Granite type 1: $E = 40.000 \text{ MPa}$

$\varphi = 48,8^\circ$ $c = 31,3 \text{ MPa}$

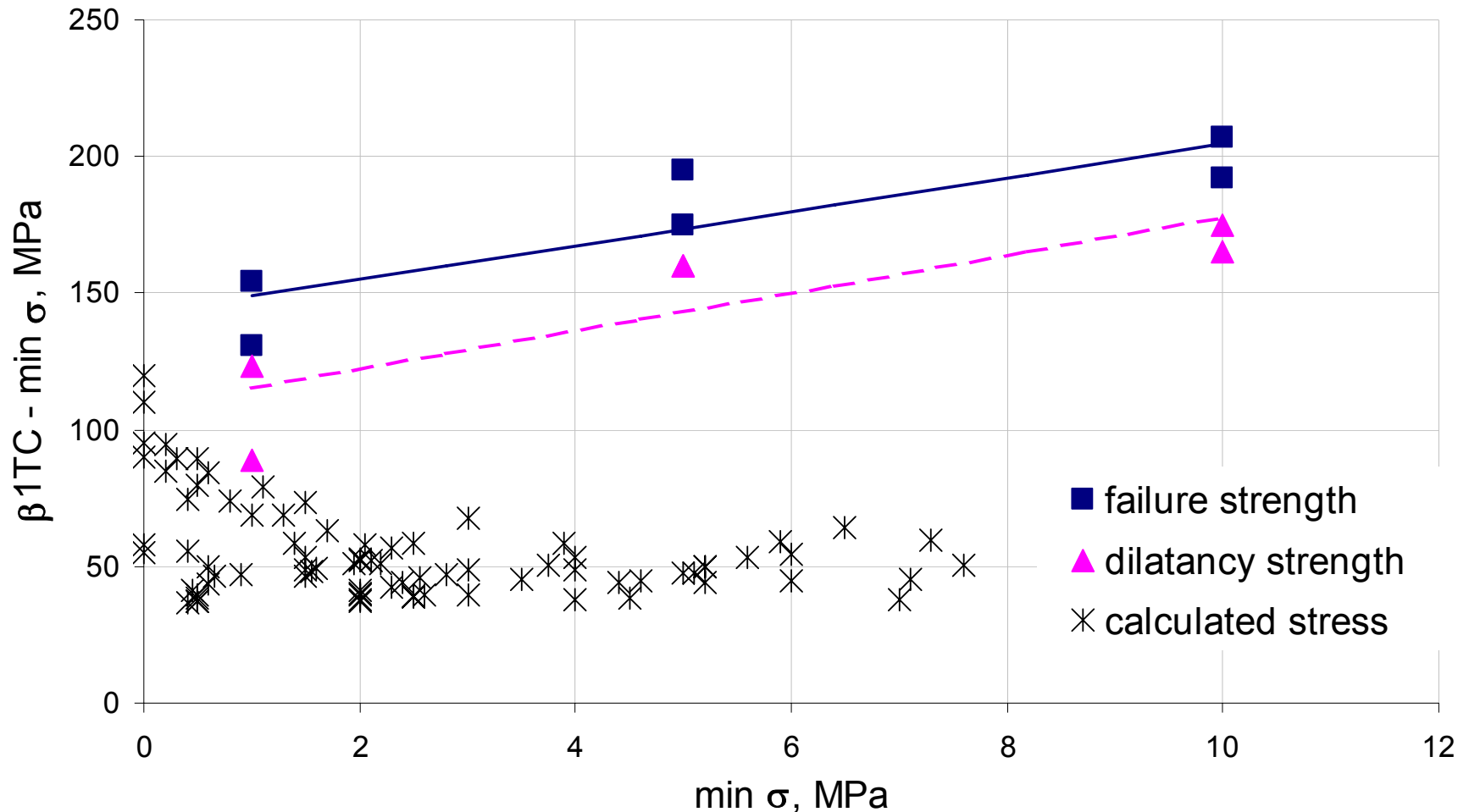
Granite type 2: $E = 30.000 \text{ MPa}$

$\varphi = 45,6^\circ$ $c = 15,1 \text{ MPa}$

Comparison of rock mass strength (= rock strength **granite type 1**) and rock stress caused by mining and **waste disposal** (z = 900m)



Comparison of rock mass strength (=rock strength **granite type 2**) and rock stress caused by mining and waste disposal (z=900m)



Conclusions



Germany's situation today / Waste disposal sites

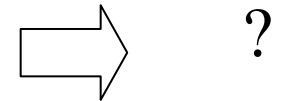
Licensed now / in operation in
some years



partly explored/exploration stopped



New site
selection
procedure



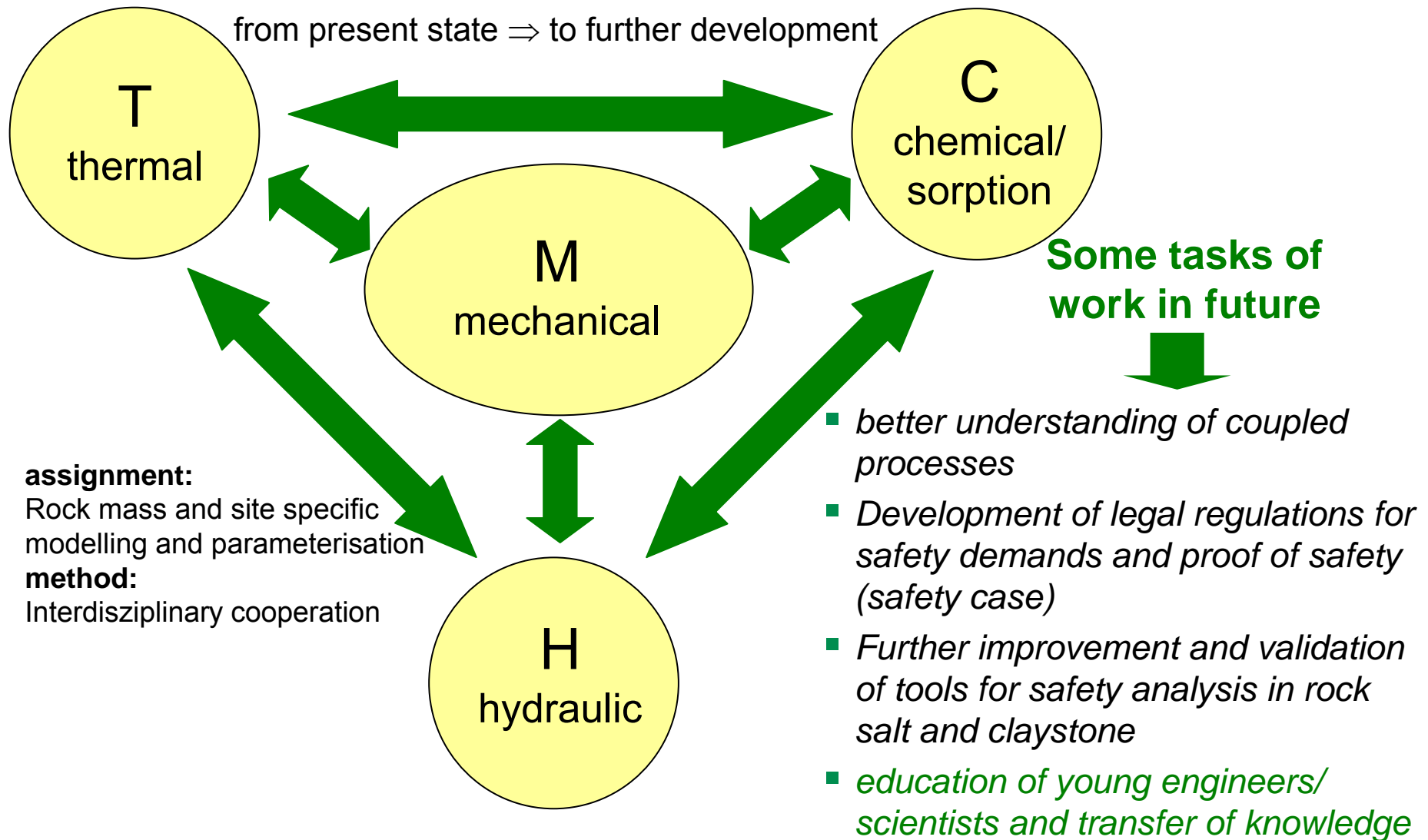
Rock salt
claystone

LAW/MAW – repository Konrad
(lime stone/claystone)

HAW-repository
Gorleben (rock salt)



Scientific work – selected aspects



Curriculum

Radioactive and Hazardous Waste Management

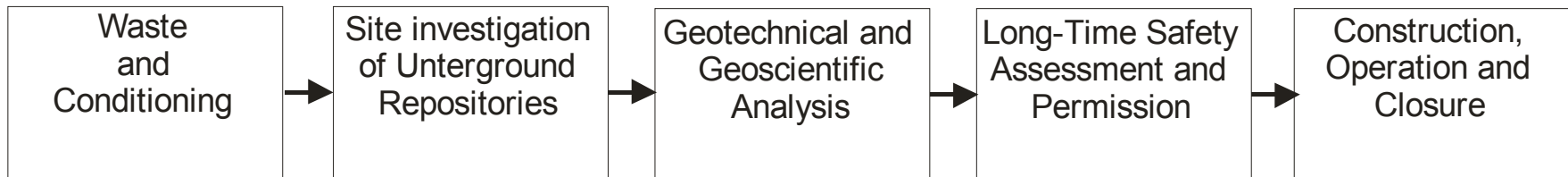
120 ECTS



Master of Science in Radioactive and Hazardous Waste Management

Competence in Engineering and Geoscience

for all Processes and Phases of
Radioactive and Hazardous Waste Management



General construction of the curriculum

- **11 compulsory modules** **96 ECTS**
 - **10 Lectures / courses / seminars** **66 ECTS**
 - **Master thesis** **30 ECTS**

- **7 compulsory optional modules** **36 ECTS**
 - **3 or 4 out of 7 lectures / courses with 6 ECTS each**

- **4 complementary modules** **18 ECTS**

Compulsory modules (1)

▪	Module 1: Site Characterization	9 ECTS
	- Methods of site characterization	6,0 ECTS
	- Fluid flow in porous media II	3,0 ECTS
▪	Module 2: Geomechanics	6 ECTS
	- Static of tunnels and mechanics of salt	3,0 ECTS
	- Geological and geotechnical barriers - Safety assessment	3,0 ECTS
▪	Module 3: Numerical Simulation	6 ECTS
	- Geological and geotechnical barriers - numerical modelling	3,0 ECTS
	- THMC – processes and numerical simulation	3,0 ECTS
▪	Module 4: Waste Inventory	6 ECTS
	- Radioactive Waste and legal regulations	2,0 ECTS
	- Origin, quantity and conditioning of radioactive waste	2,0 ECTS
	- Radiation physics and radiation protection	2,0 ECTS
▪	Module 5: Permission and Legal Regulations	5 ECTS
	- Permission process	2,0 ECTS
	- Energy politics	1,0 ECTS
	- Special waste and waste industry	2,0 ECTS
▪	Module 6: Petrology and Geochemistry	6 ECTS
	- Petrology and geochemistry of repository relevant host rocks	3,0 ECTS
	- Petrophysics	3,0 ECTS



Compulsory modules (2)

- | | |
|--|----------------|
| ■ Module 7: Repository Concepts | 7 ECTS |
| - Repository concepts | 2,0 ECTS |
| - Planing of final repositories | 2,0 ECTS |
| - International strategies in long term safety assessment | 3,0 ECTS |
| ■ Module 8: Long-Term Safety | 8 ECTS |
| - Principles of long term safety assessment and monitoring | 5,0 ECTS |
| - Numerical simulation in long term safety assessment | 3,0 ECTS |
| ■ Module 9: Repository Technics | 5 ECTS |
| - Underground disposal | 3,0 ECTS |
| - Transport and intermediate storage | 3,0 ECTS |
| ■ Module 11: Main Seminar and Field Trips | 8 ECTS |
| - Main seminar | 6,0 ECTS |
| - Field trips | 2,0 ECTS |
| ■ Module 12: Master Thesis | 30 ECTS |



Compulsory optional modules

▪	Module 1: Handling of Hazardous Waste	6 ECTS
	- Processing of hazardous waste	3,0 ECTS
	- Combustion technics	3,0 ECTS
▪	Module 2: Course Geochemistry	6 ECTS
	- Course geochemistry I	3,0 ECTS
	- Course geochemistry II	3,0 ECTS
▪	Module 3: Course Petrology	6 ECTS
	- Course petrology I	3,0 ECTS
	- Course petrology II	3,0 ECTS
▪	Module 4: Isotope Geochemistry	6 ECTS
	- Introduction to isotope geochemistry	3,0 ECTS
	- Applied isotope geochemistry	3,0 ECTS
▪	Module 5: Applied Hydrogeochemical Flux Modelling	6 ECTS
▪	Module 6: Environmental Monitoring	6 ECTS
	- Environmental monitoring	2,5 ECTS
	- Mine surveying in underground repositories	1,0 ECTS
	- Cartography and map of mine	2,5 ECTS
▪	Module 7: Risk Management and Communication	6 ECTS
	- Risk management	3,0 ECTS
	- Project management and project planning	3,0 ECTS



Complementary modules

- **Module 1: Characterization and Groundwater flux** **6 ECTS**
 - Fluid flow in porous media 3,0 ECTS
 - Cycles of matter in the environment 3,0 ECTS

- **Module 2: Course Hydrogeology** **6 ECTS**
 - Flux calculation of water and matter in the hydrogeosphere - hydrogeochemistry 3,0 ECTS
 - Flux calculation of water and matter in the hydrogeosphere – geohydraulic systems 3,0 ECTS

- **Module 3: Principles of Hydrogeology and Geochemistry** **6 ECTS**
 - Hydrogeology 3,0 ECTS
 - Geochemistry I 3,0 ECTS

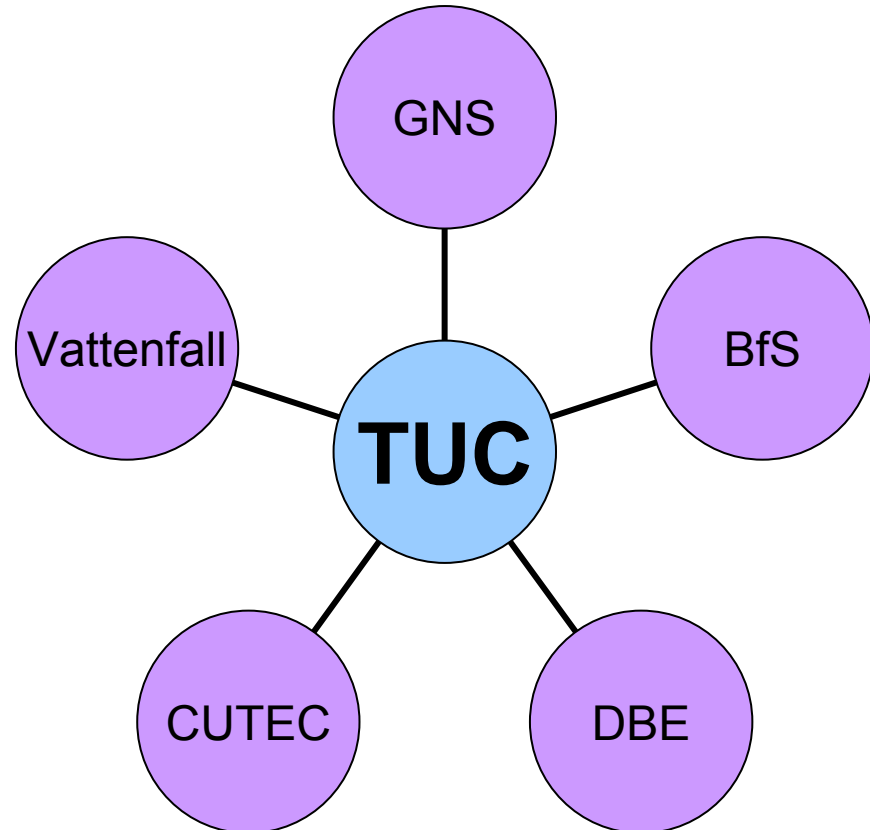
- **Module 4: Investigation of Geological Structures** **6 ECTS**
 - Geophysical investigation 3,0 ECTS
 - Geological and tectonical principles of site investigation 3,0 ECTS



25 % of lectures and seminars are given by experts of industrial companies (energy suppliers as well as research bureaus) and legal authorities.

The main part of teaching is accomplished by the TUC departments

- **Petrology and Geochemistry**
- **Geomechanics**
- **Hydrogeochemistry**
- **Mining Engineering**
- **Geophysics**

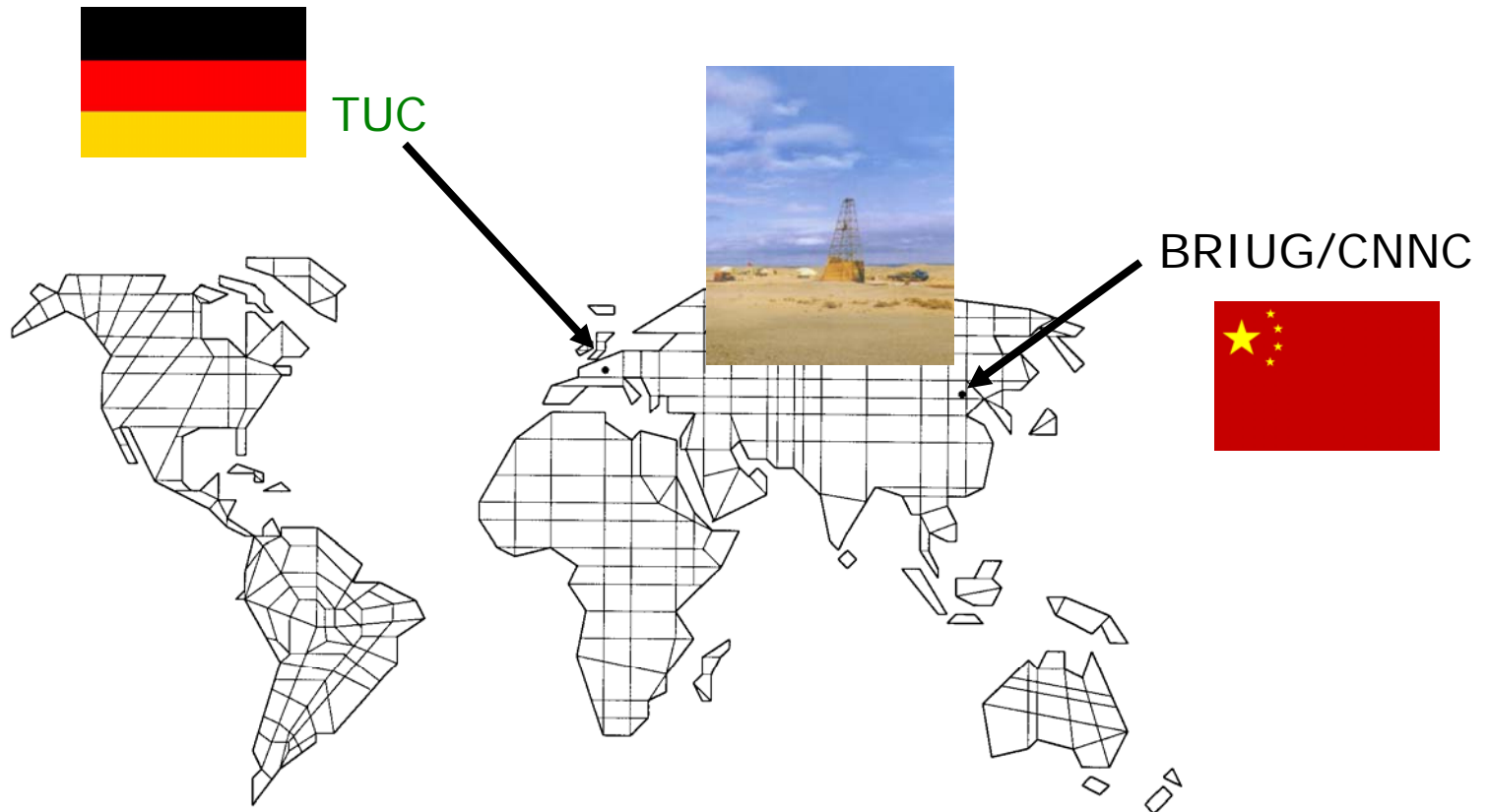


Internal (TUC) and external (waste industry and authorities) lecturers

	1. Semester	2. Semester	3. Semester	4. Semester	
C O M P U L S O R Y M O D U L E S	1	Methods of site characterization	Origin, quantity and conditioning of radioactive waste	THMC-processes and numerical simulation	
	2		Fluid flow in porous media II	Numerical simulation in long term safety assesement	
	3				
	4				
	5	Underground disposal	Geological and geotechnical barriers - numerical modelling	Planing of final repositories	Master thesis
	6				
	7	Petrophysics I	Radioactive waste and legal regulations	International strategies in long-term safety assessment	
	8				
	9	Static of tunnels and mechanics of salt	Repository concepts	Energy politics	
	10			Radiation physics and radiation protection	
	11	Geological and geotechnical barriers - safety assessment	Principles of long-term safety assessment and monitoring	Permission process	
	12				
	13				
	14				
	15		Special waste and waste industry	Main seminar and field trips	
	16				
	17		Petrology and geochemistry of repository relevant host rocks		
	18				
	19		Transport and intermediate storage		
	20				



Thanks for attention as well as ...



... Good luck for further fruitful and interesting cooperation





Site selection and characterization for China's HLW repository in Beishan, Gansu

Rock mass mechanical properties and Seepage Characteristics

Yang Chunhe

Institute of Rock and Soil Mechanics,
Chinese Academy of Sciences

2007.5

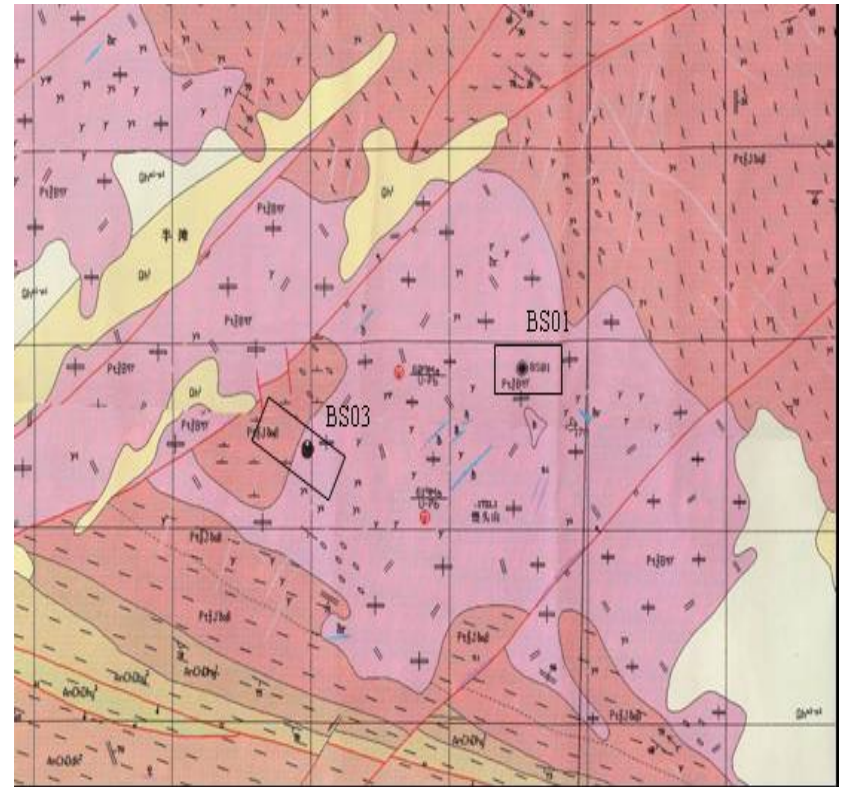


Outline

- **Introduction**
- **Field survey and tests**
- **Joint characteristics**
- **Mechanical properties**
- **Geostress and seepage characteristics**
- **Conclusions**

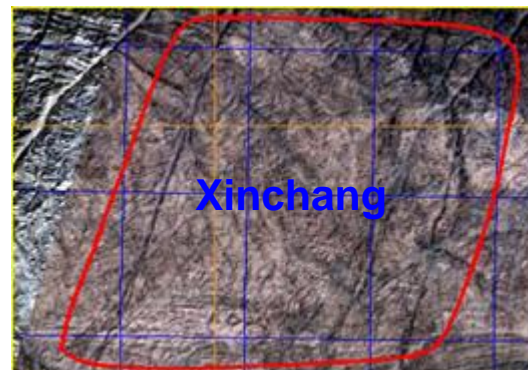
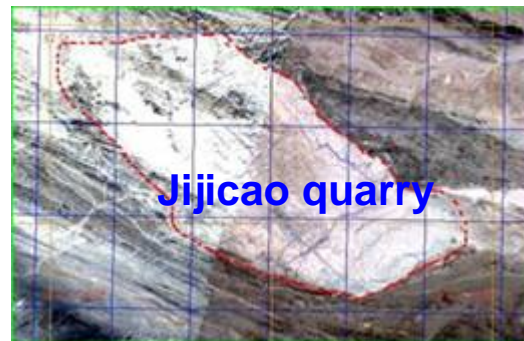
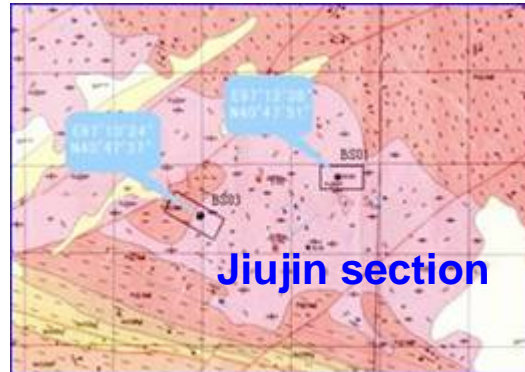
Introduction

- **Jiujin section, Jijicao quarry and Xinchang are candidates in Beishan-the preselected area for China's HLW repository**
- **During 2001-2006, series of investigation were done by **Wuhan Institute of Rock and Soil mechanics, CAS****





Rock mass mechanical properties and Seepage Characteristics

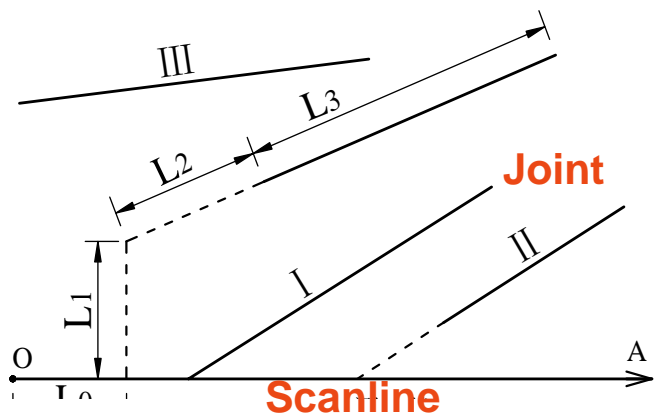




Rock mass mechanical properties and Seepage Characteristics

- Introduction
- **Field survey and tests**
- Joint characteristics
- Mechanical properties
- Geostress seepage characteristics
- Conclusions

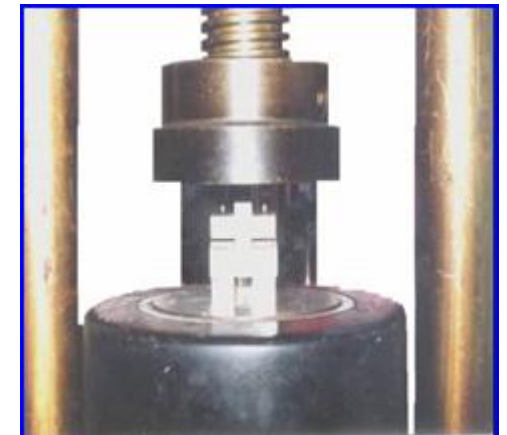
Field Joint Survey



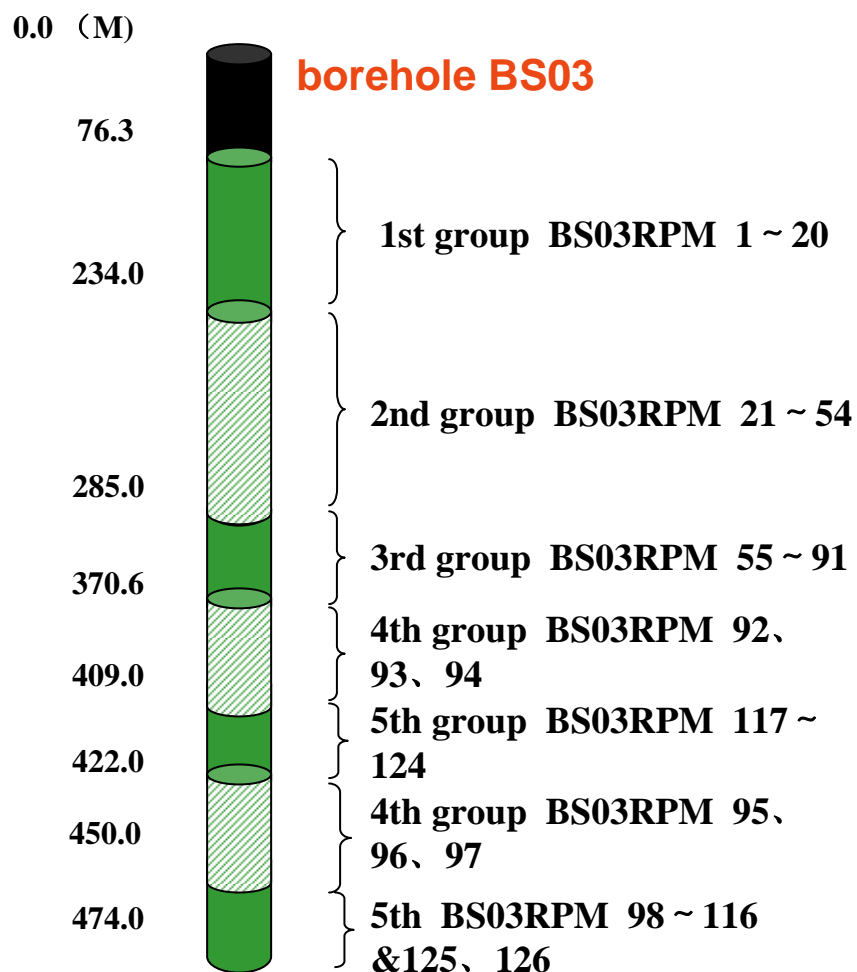
Schematic Joint survey method



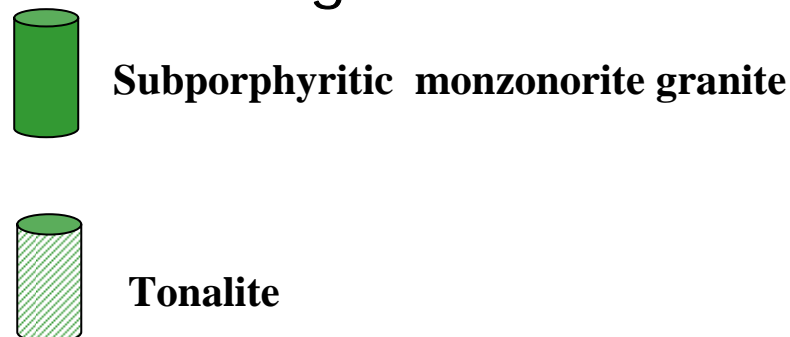
Rock Sampling and Laboratory Tests



Rock mass mechanical properties and Seepage Characteristics



Legend



The lithology is mainly monzonorite granite and partially tonalite .

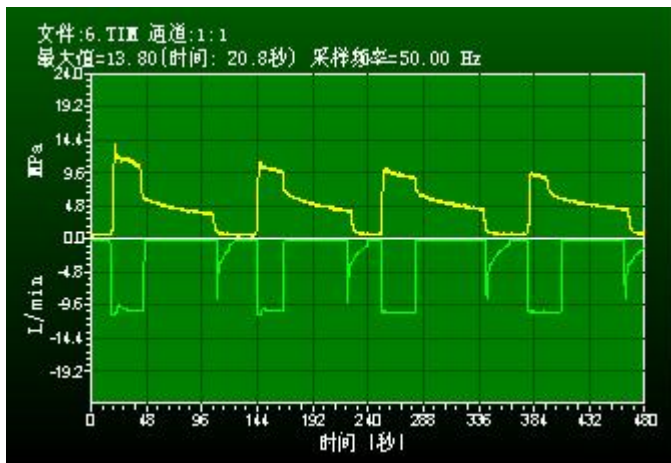
Five groups of rock samples were chosen from different depths

Depth Borehole Specimen



Rock mass mechanical properties and Seepage Characteristics

Hydraulic Fracture and High-pressure
Injection were done in borehole BS03





Rock mass mechanical properties and Seepage Characteristics

- Introduction
- Field survey and tests
- **Joint characteristics**
- Mechanical properties
- Geostress and seepage characteristics
- Conclusions

Rock mass mechanical properties and Seepage Characteristics

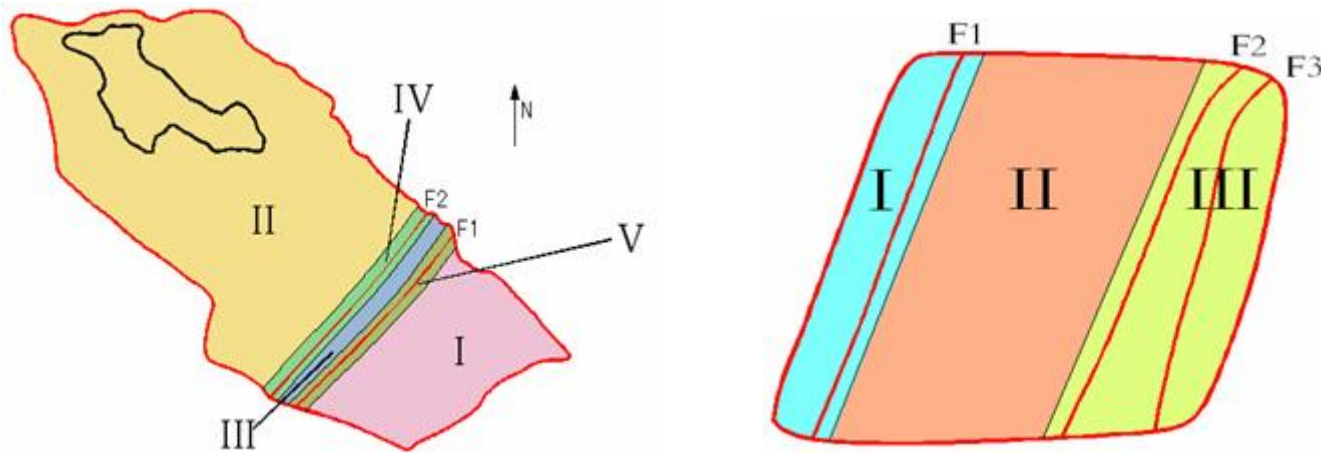




- ✓ **Joints are principally steep shear joints.**
- ✓ **Joints of dip angle greater than 60° are about 90.89%.**
- ✓ **X shear joints can be observed in some outcrops.**
- ✓ **One set joints is visible for most joints.**
- ✓ **Joint is flat, smooth with stable strike and long extension.**

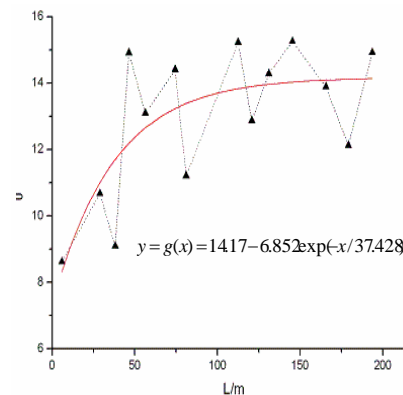
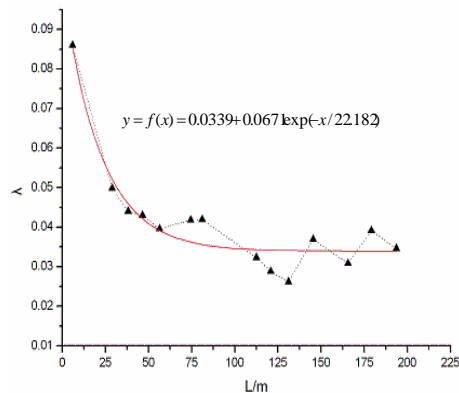


Rock mass mechanical properties and Seepage Characteristics

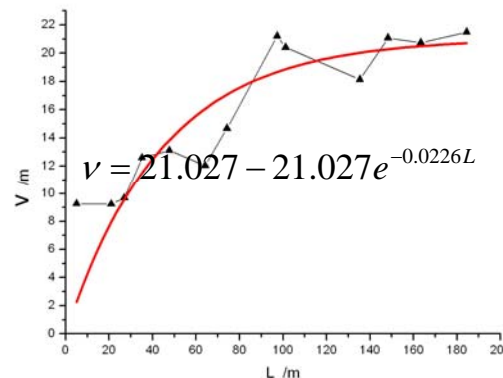
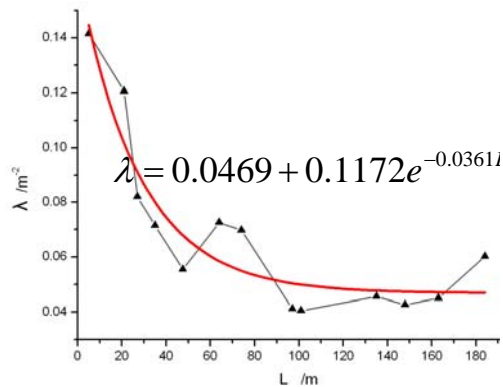


According to the faults, Jijicao quarry and Xinchang are roughly divided into statistical homogeneities and the region which is influenced by the faults.

Rock mass mechanical properties and Seepage Characteristics



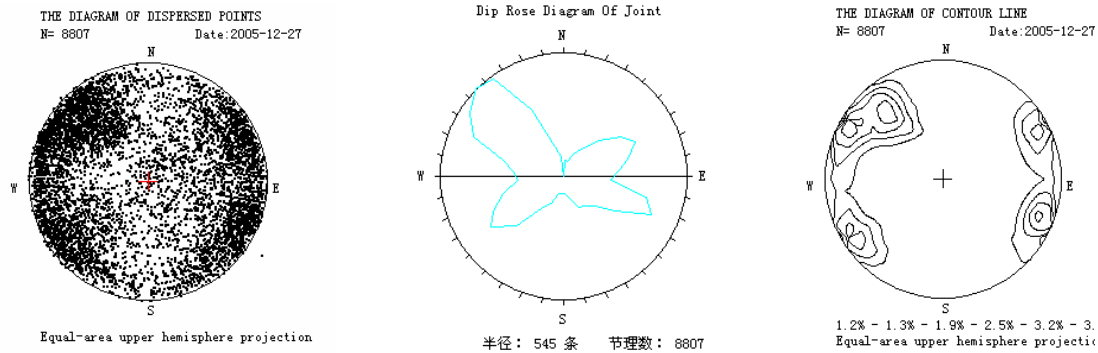
Mean trace length and trace midpoint density-L in Jiji quarry



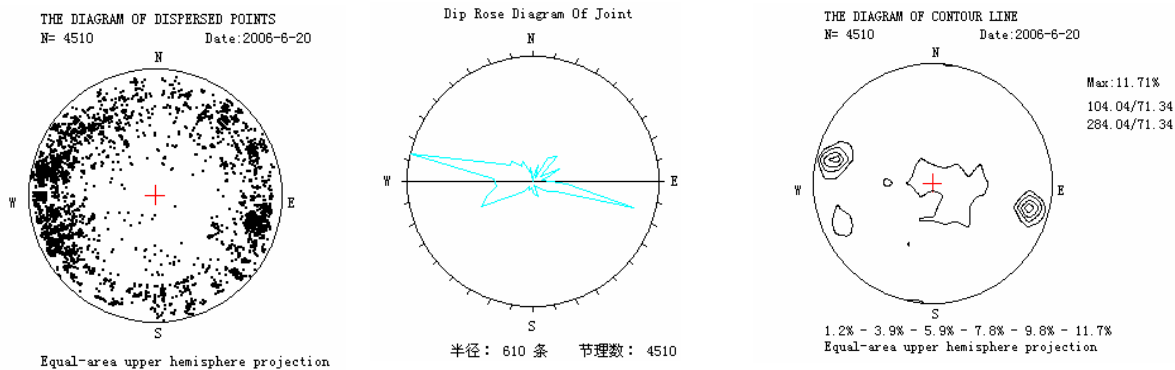
Mean trace length and trace midpoint density-L in Xingchang

➤ The boundary of the statistical homogeneous domains is determined

Statistic of joint orientation

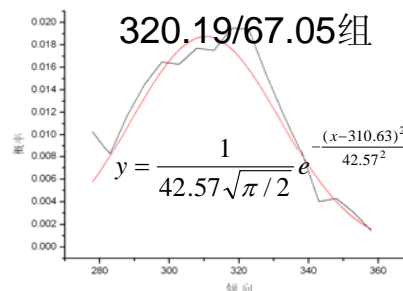
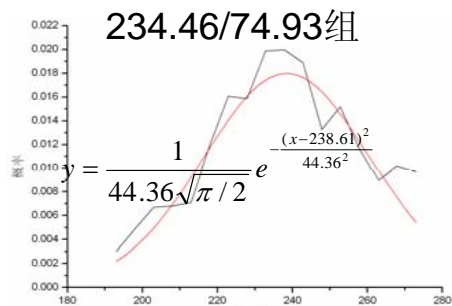


Joint polar points and Dip rose diagram of II statistical homogeneity of Jiji quarry



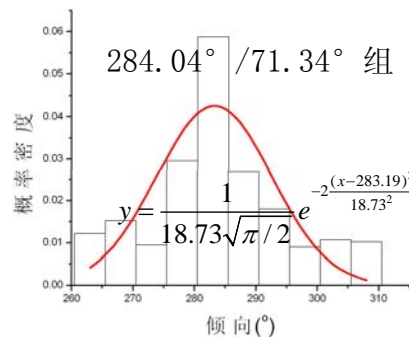
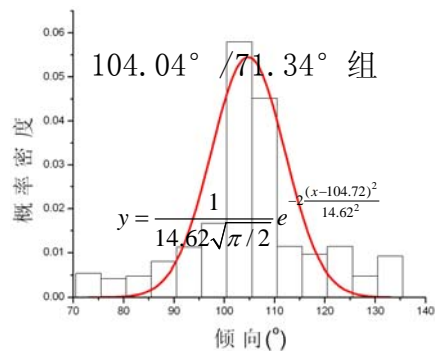
Joint polar points and Dip rose diagram of II statistical homogeneity of Xingchang

Probability analysis of joint orientation



Fitted dip distribution curve and formula of

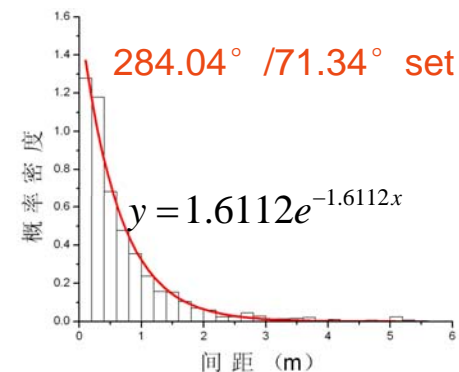
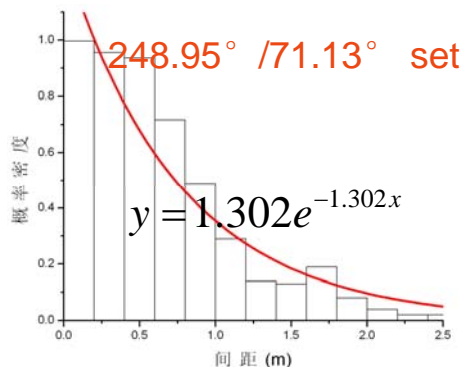
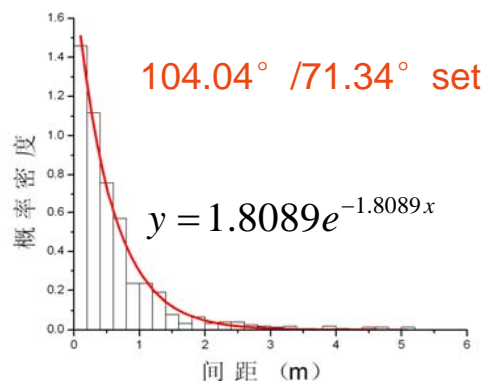
II statistical homogeneity of Jiji quarry



Fitted dip distribution curve and formula of

II statistical homogeneity of Xingchang

Statistic of joint space



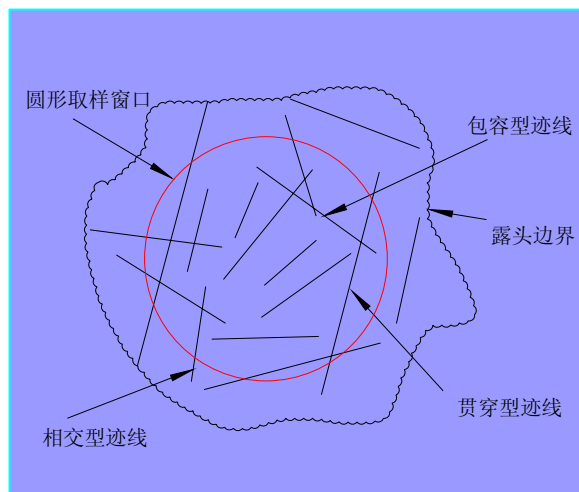
**Fitted joint space distribution and formula
of II statistical homogeneity of xingchang**

Joint spacing of Xingchang

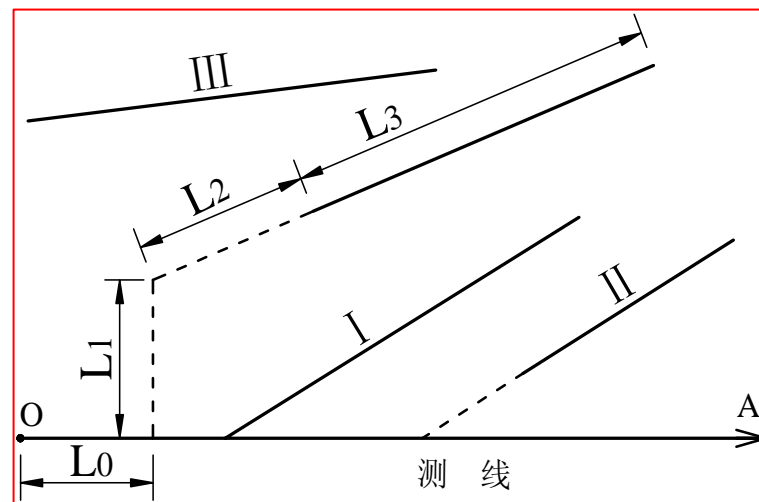
	SET	ORIENTATION	SPACING (m)
II	1	104.04 ° / 71.34 °	0.55
	2	248.95 ° / 71.13 °	0.77
	3	284.04 ° / 71.34 °	0.62

According to ISRM (1978) joint space of the 104.04 / 71.34 set of Xinchang is moderate spacing and the others are wide spacing.

Estimation of mean trace length and midpoint density



Schematic circular sample window



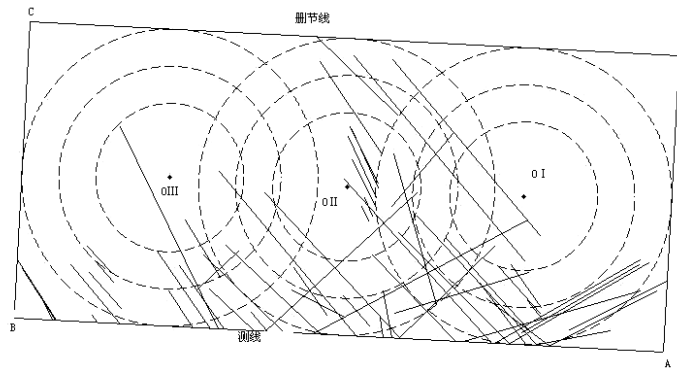
Types of endpoints of joint traces

$$\text{Mean trace length } \bar{v} = \frac{\pi(N + N_2 - N_0)}{2(N - N_2 + N_0)} c$$

$$\text{Midpoint density } \lambda = \frac{N - N_2 - N_0}{2\pi c^2}$$

Estimation of mean trace length and midpoint density (continued)

Concentric circles method

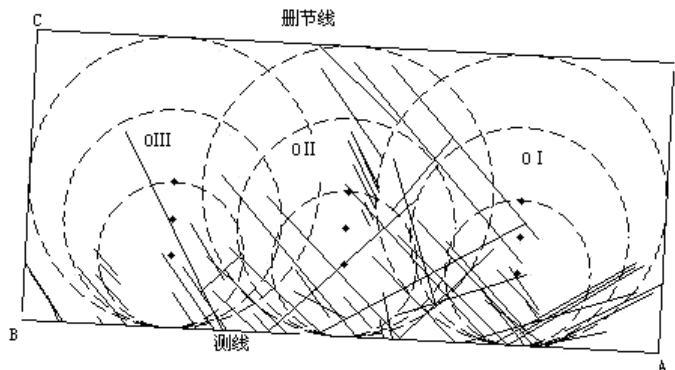


Results of Concentric circles

同心圆法所得露头F90°平均迹长和迹线中点的面密度

窗口半径 /m	窗口编号	各类迹线条数			迹线中点面密度 λ	平均迹长估计值 ν/m
		N_0	N_1	N_2		
13.5287	O I	7	16	4	0.0261	17.001
	O II	12	16	3	0.0348	11.688
	O III	5	10	0	0.0174	10.625
10.1465	O I	0	14	0	0.0216	15.938
	O II	6	13	2	0.0386	10.838
	O III	1	9	0	0.0170	13.040
6.7644	O I	0	5	0	0.0174	10.625
	O II	6	7	1	0.0661	5.033
	O III	0	3	0	0.0104	10.625

Tangent circles method



Results of tangent circles

相切圆法所得露头F90°平均迹长和迹线中点的面密度

窗口半径 /m	窗口编号	各类迹线条数			迹线中点面密度 λ	平均迹长估计值 ν/m
		N_0	N_1	N_2		
13.5287	O I	7	16	4	0.0261	17.001
	O II	12	16	3	0.0348	11.688
	O III	5	10	0	0.0174	10.625
10.1465	O I	4	11	5	0.0294	17.6158
	O II	9	14	3	0.0495	9.9613
	O III	5	10	0	0.0309	7.9691
6.7644	O I	3	9	6	0.0522	14.8756
	O II	5	8	6	0.0626	11.8060
	O III	3	8	1	0.0487	7.5896

➤ Stable and reasonable results can be obtained from Tangent circles method

Estimation of mean trace length and midpoint density (continued)

Trace length and midpoint density for each statistical homogeneous domains of Jiji quarry

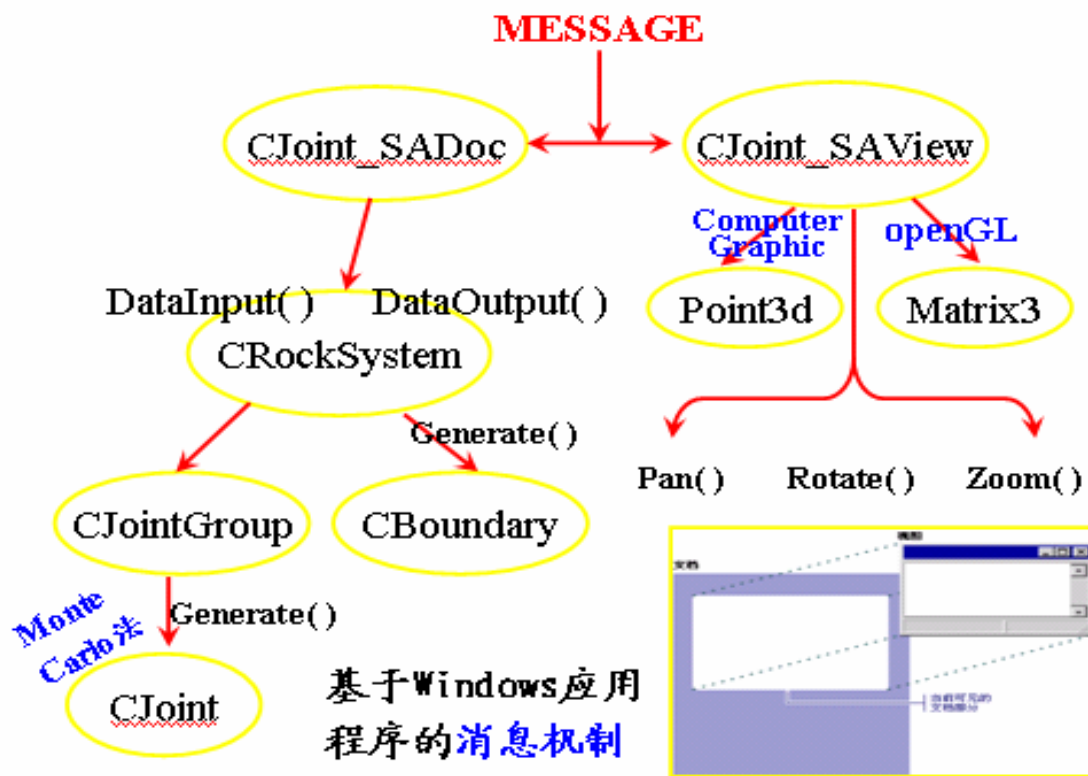
NO.	I	II	III	IV	V
/m	14.834	14.398	15.167	15.667	12.184
/m ⁻²	0.034	0.0387	0.034	0.0408	0.0414

Trace length and midpoint density for each statistical homogeneous domains of Xingchang

NO.	I	II	III
/m	14.129	18.671	14.173
/m ⁻²	0.1058	0.0586	0.0827

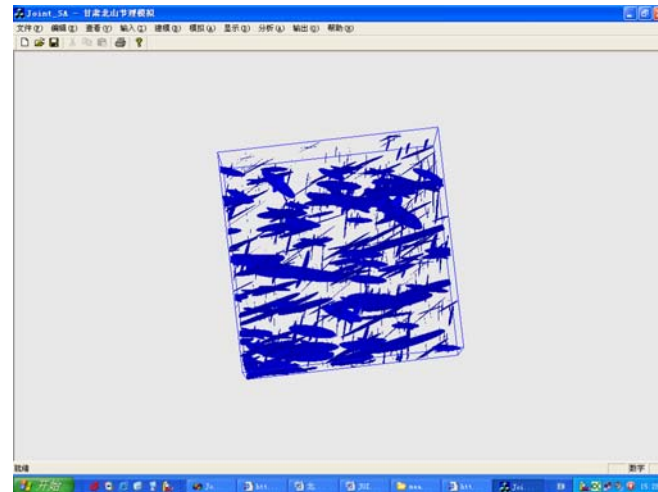
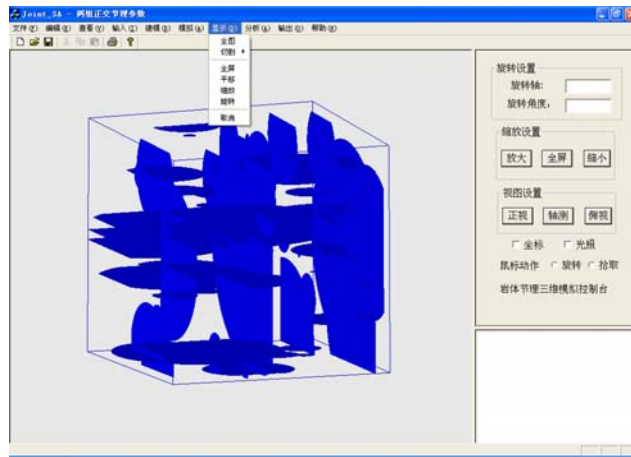
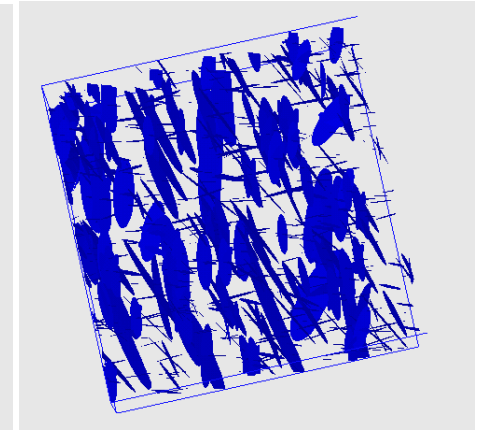
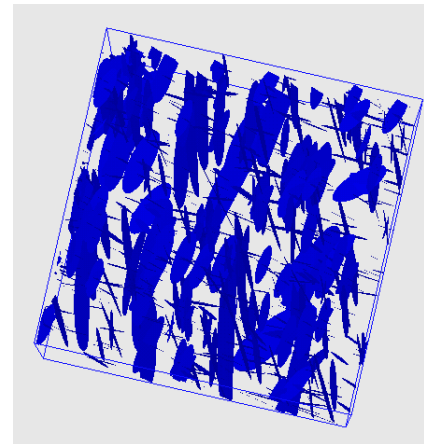
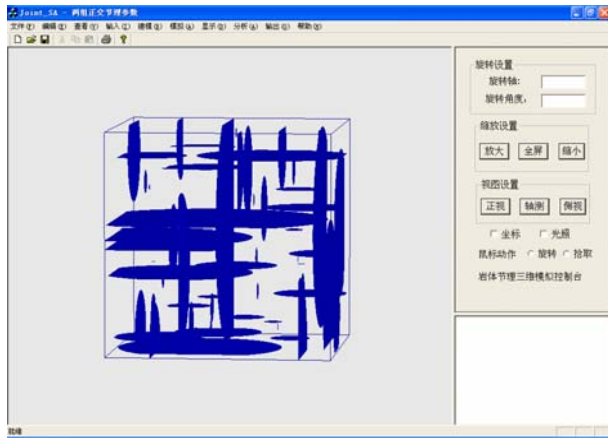
➤ Mean trace length is smaller and midpoint density is greater in the region that influenced by faults than that in statistical homogeneity

Development of 3-D joint simulation system





Development of 3-D joint simulation system (continued)



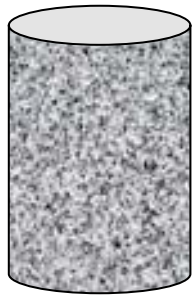


Rock mass mechanical properties and Seepage Characteristics

- Introduction
- Field survey and tests
- Joint characteristics
- **Mechanical properties**
- Geostress and seepage characteristics
- Conclusions

mechanical properties of intact rock

Specimen size



$\phi 50 \times 100$



$\phi 60 \times 30$



$40 \times 40 \times 20$

Test items

Water-content coefficient ; Hygroscopic coefficient;
Dry density ; Acoustic wave measurement ;
Uniaxial compression strength and deformation;
Triaxial strength and deformation

Water-content coefficient ; Hygroscopic coefficient;
Dry density ; Brazil test

Shear strength

Broken blocks

Specific gravity ; specific heat

Specimen after tests

Uniaxial compression



Triaxial compression



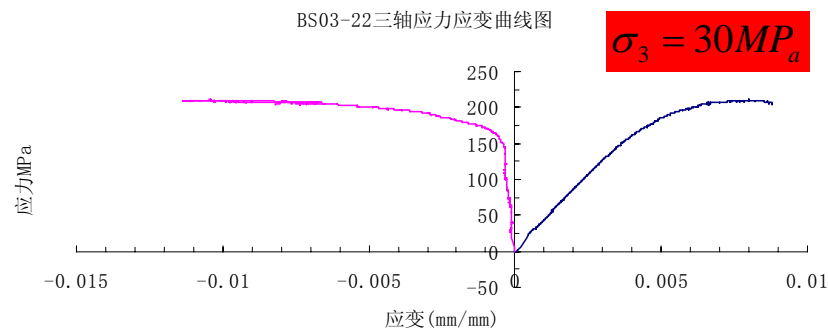
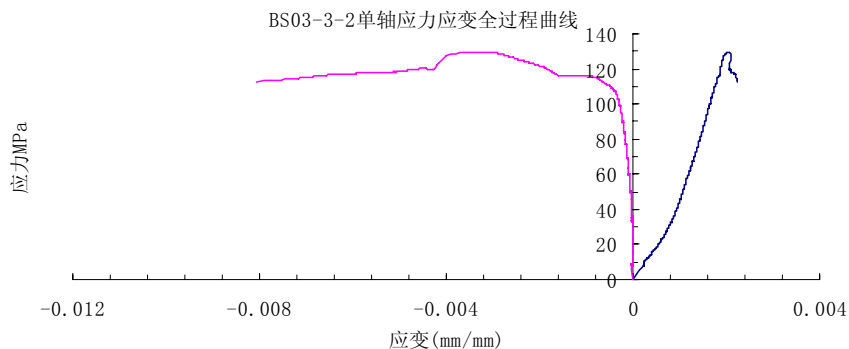
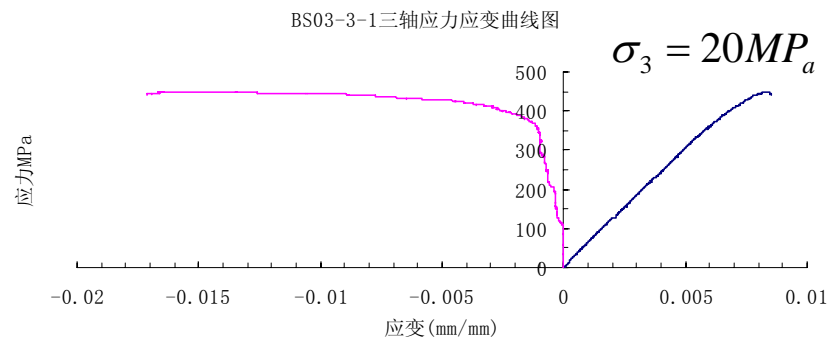
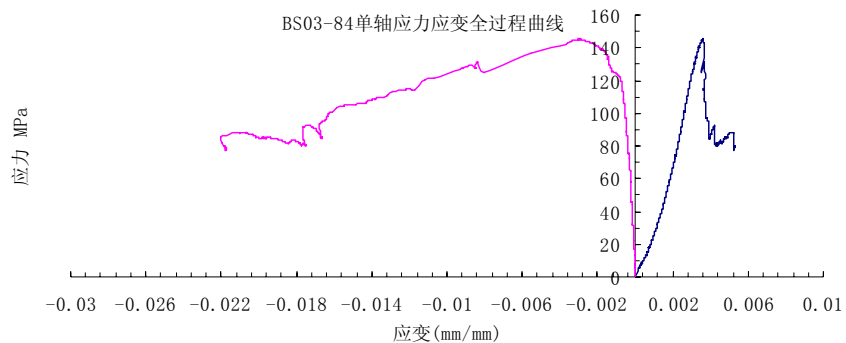
Direct shear



BRAZIL split



Curve of uniaxial and triaxial compression test



Uniaxial compression test

Triaxial compression test



Conclusions of rock mechanics characteristics

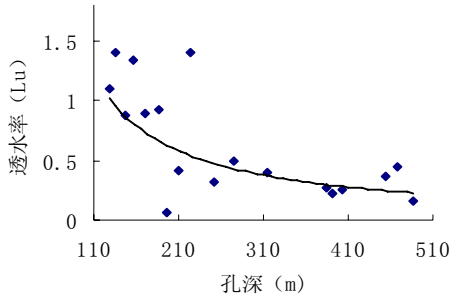
- **Both have high mechanical strength, small deformation, high brittleness.**
- **Subporphyritic monzonite granite is more homogeneous and has high mechanical strength.**
- **Tonalite is inhomogeneous and its mechanical strength is enhanced with depth.**
- **Homogeneity of shallow rock is inferior. Homogeneity of rock under 300m is superior and mechanical strength is high.**



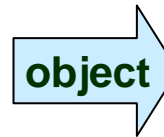
Rock mass mechanical properties and Seepage Characteristics

- Introduction
- Field survey and tests
- Joint characteristics
- Mechanical properties
- **Geostress and seepage characteristic**
- Conclusions

Seepage characteristic



Permeability coefficient of individual sections can be measured with high pressure injection water tests.

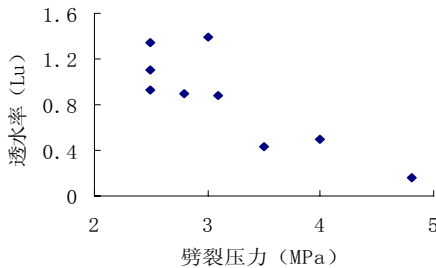


Average permeability character definite units was obtained.

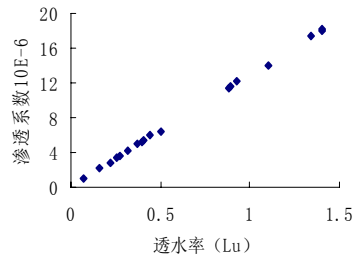


The mean value of permeability coefficient for individual sections can be used to describe permeability coefficient of definite geological units.

Permeability rate-depth curve



Splitting water pressure- Permeability rate curve



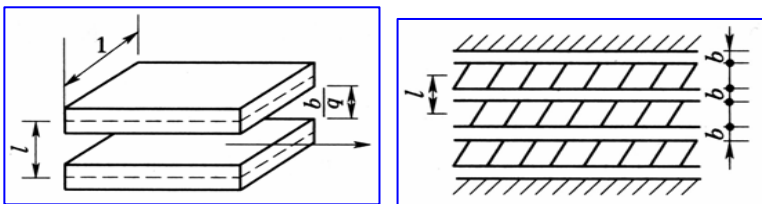
Permeability coefficient -permeability rate curve

$$\bar{K} = \sqrt[n]{K_1 K_2 \cdots K_n}$$

➤ The geometric mean permeability coefficient of borehole BS03 is 4.4×10^{-6} cm/s .

Seepage characteristic (continued)

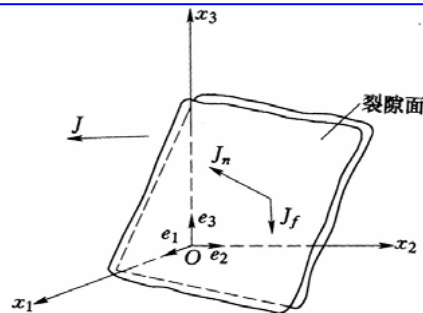
Flow in single fracture is the basis to determination of hydraulic conductivity tensor for fractured medium.



Permeability figure of hydraulic gradient parallel with fracture plane

$$K = \sum_{i=1}^n K_{ei} \begin{bmatrix} 1 - \cos^2 \beta_i \sin^2 \gamma_i & -\sin \beta_i \cos \beta_i \sin^2 \gamma_i & -\cos \beta_i \sin \gamma_i \cos \gamma_i \\ -\sin \beta_i \cos \beta_i \sin^2 \gamma_i & 1 - \sin^2 \beta_i \sin^2 \gamma_i & -\sin \beta_i \sin \gamma_i \cos \gamma_i \\ -\cos \beta_i \sin \gamma_i \cos \gamma_i & -\sin \beta_i \sin \gamma_i \cos \gamma_i & 1 - \cos^2 \gamma_i \end{bmatrix}$$

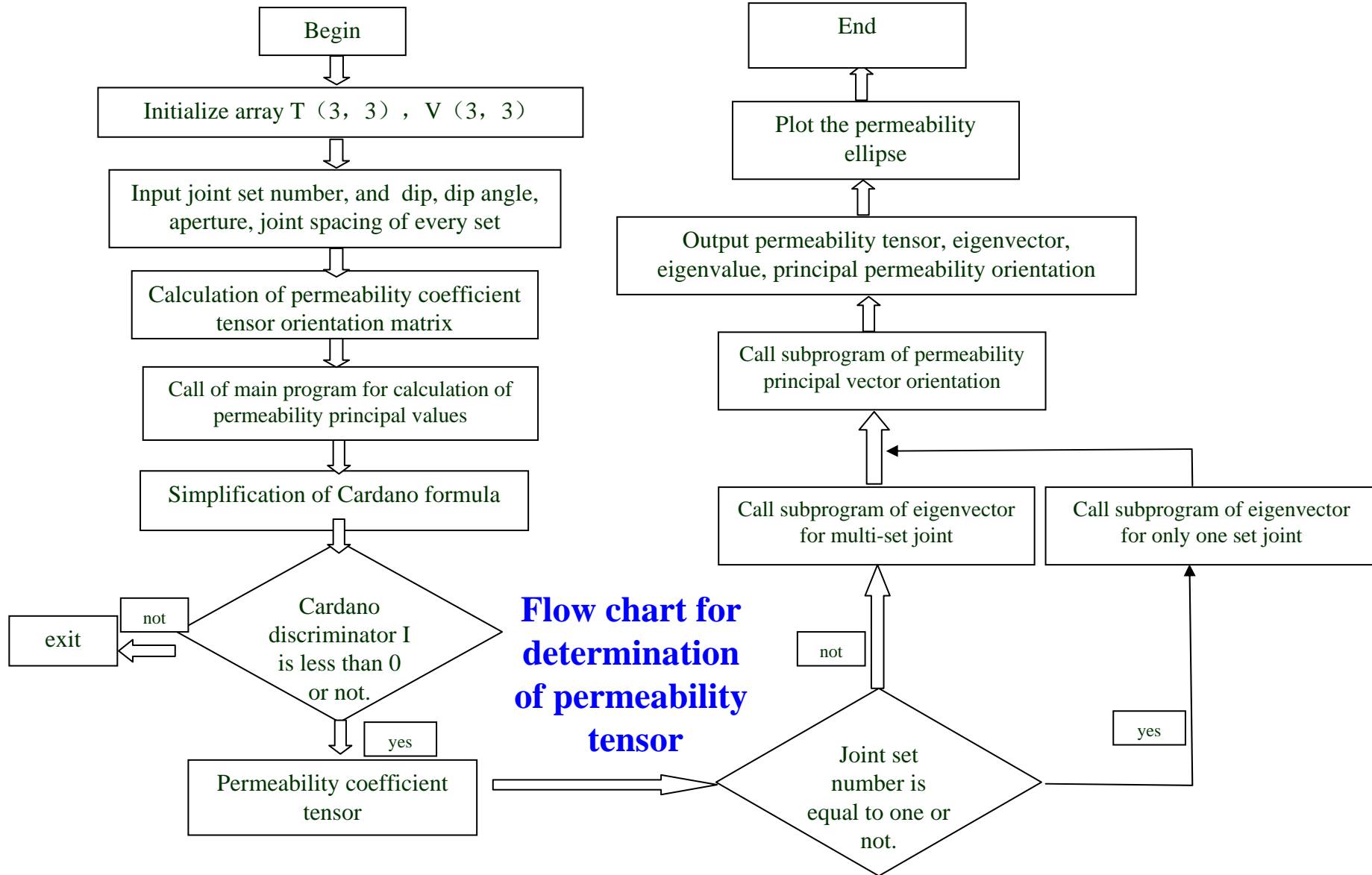
Generally, in permeability domain, hydraulic gradient is unparallel with fracture plane. But water flow velocity in fractures is related to hydraulic gradient which is parallel with fracture plane.



Permeability figure of hydraulic gradient unparallel with fracture plane



Rock mass mechanical properties and Seepage Characteristics



Rock mass mechanical properties and Seepage Characteristics

Seepage characteristic (continued)

Hydraulic parameters of 4 set joint :

- 1st: dip 43.19° , dip angle 70.58° , spacing 2.75m
- 2nd: dip 141.75° , dip angle 60.75° , spacing 5.03m
- 3rd: dip 223.23° , dip angle 67.05° , spacing 2.11m
- 4th: dip 348.03° , dip angle 68.14° , spacing 8.64m



渗透张量计算程序V1.0

输入

裂隙组数 4

	倾向°	倾角°	隙宽cm	隙间距m
第一组	43.19	70.58	0.006	2.75
第二组	141.75	60.75	0.006	5.03
第三组	223.23	67.05	0.006	2.11
第四组	348.03	68.14	0.006	8.64
第五组	0	0	0	0
第六组	0	0	0	0

渗透张量

0.823E-05	-0.763E-05	0.194E-05
-0.763E-05	0.107E-04	-0.161E-06
0.194E-05	-0.161E-06	0.139E-04

渗透主矢量

-0.763	0.146	0.630
-0.637	-0.338	-0.692
0.112	-0.930	0.351

渗透主值

0.157E-05	230.12	6.42
0.135E-04	336.61	68.36
0.177E-04	137.70	20.57

渗透矢量方位

230.12	6.42
336.61	68.36
137.70	20.57

计算 清空

渗透椭圆 退出

共有 4 组裂隙

ct=-.7326E-43

Hydraulic conductivity tensor

$$K = \begin{bmatrix} 0.823 \times 10^{-5} & -0.763 \times 10^{-5} & 0.194 \times 10^{-5} \\ -0.763 \times 10^{-5} & 1.070 \times 10^{-5} & -0.016 \times 10^{-5} \\ 0.194 \times 10^{-5} & -0.016 \times 10^{-5} & 1.390 \times 10^{-5} \end{bmatrix}$$

Permeability principal value

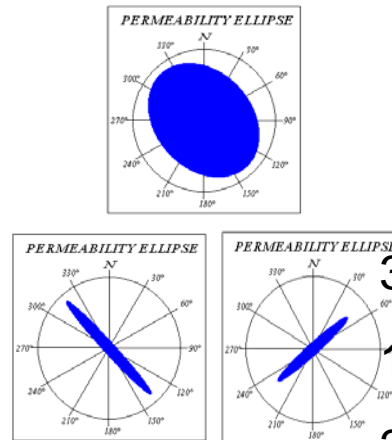
$$0.157 \times 10^{-5} \quad 0.135 \times 10^{-4} \quad 0.177 \times 10^{-4}$$

Permeability principal vector

$$\alpha_1(-0.763, -0.637, 0.112)$$

$$\alpha_2(0.146, -0.338, -0.930)$$

$$\alpha_3(0.630, -0.692, 0.351)$$



3 permeability principal orientation:

1 dip 230.12° , dip angle 6.42°

2 dip 336.61° , dip angle 68.36°

3 dip 137.70° , dip angle 20.57°

Permeability ellipse



Geostress characteristic

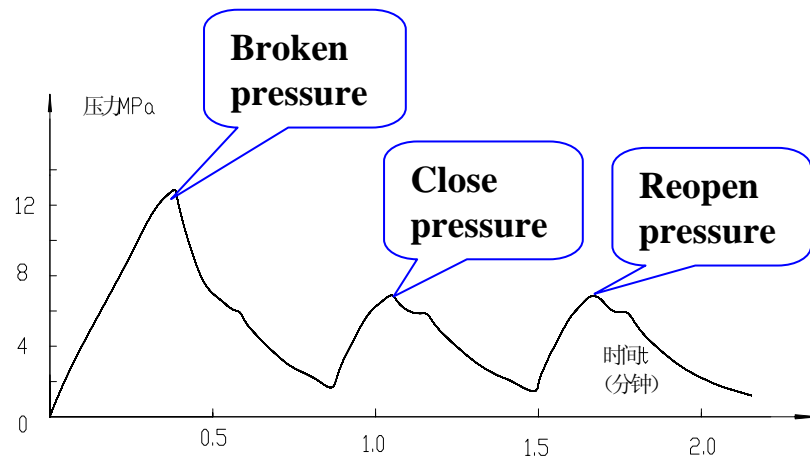
Geostress measured by hydraulic fracture method



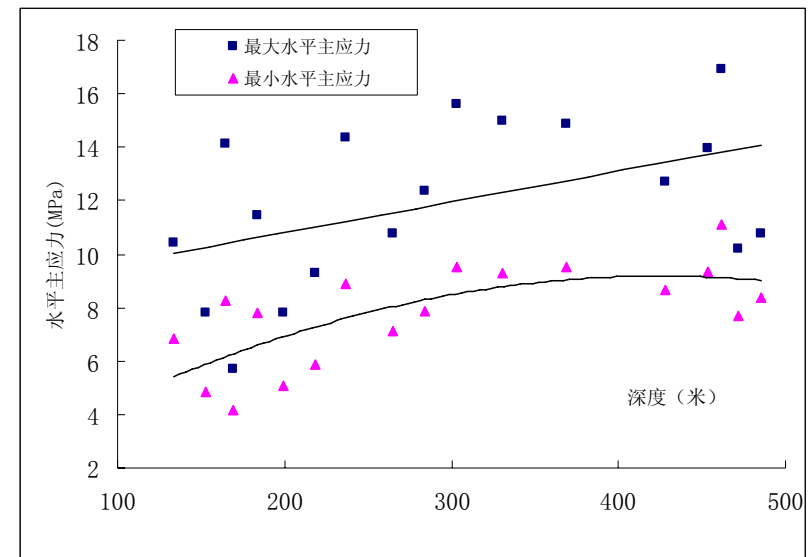
Hypothesis:

1. Host rock is the linear, homogeneous, isotropic elastic medium.
2. Injection water flow obey the Darcy's law in rock pore .
3. Perpendicular stress σ_V is one of principal stress

Results of measurement of geostress



**Pressure-time curve
of 283.51-284.51m**



➤ **The geostress of Beishan a is moderate and the magnitude of geostress increases with the depth.**



Conclusions

- **The quantitative parameters of joint characteristic are obtained**
- **Rock in the research area is high density, low Water-content, low Hygroscopic coefficient, low porosity, low permeability**
- **Rock in the research area is high mechanical strength, small deformation, high brittleness.**
- **The geostress of Beishan a is moderate and the magnitude of geostress increases with the depth.**



中国科学院武汉岩土力学研究所
INSTITUTE OF ROCK AND SOIL MECHANICS
CHINESE ACADEMY OF SCIENCES

Rock mass mechanical properties and Seepage Characteristics

Thank you!

BGR Research Activities in Crystalline Rock

- Grimsel Test Site (CH), Hard Rock Laboratory Äspö (SE) -

Dr. SHAO, Hua

Federal Institute for Geosciences and Natural Resources (BGR)
Hanover, Germany

Objects of investigation programs

- ▶ Additional research work to salt rock
- ▶ Test and examination of the methods for characterising rock mass,
- ▶ Collection of the geological, hydraulic and geomechanical data for developing a structural model and validation of developed model,
- ▶ Determination of the effective parameter values for the numerical modelling,
- ▶ Exchange of experiences with international partners

Focuses of the BGR's investigation programs

- ▶ German - Swiss co-operation: Grimsel Test Site, 1984 –

- ! ***Development of methodology***

- Geology, Rock mechanics, Hydraulics/mass transport and THMC

- Projects: BK, GS, ZPK, CTN, EFP, GMT, FEBEX

- ▶ German - Swedish co-operation: Hard Rock Laboratory Äspö, 1996 –

- ! ***Application of methods and models***

- Hydraulics/mass transport and THMC coupling

- Projects: TURE, TASK 5, TPF, PR, EBS, LASGIT

BGR's investigation programs in granite (Grimsel Test Site)

In situ activities

- Geological characterisation of fractured rock
- Rock stress measurements to determine the stress distribution around the tunnel
- Fracture flow test to determine potential flow paths in fractures/fracture network
- **Near-field characterisation**
- **Tracer tests in different scales (1 / 10 / 70 / > 100 m)**

Participation & co-operation

- *Engineered barrier system and interface between geological and engineered barrier systems*

Theory and modelling

- Development and validation of conceptual models
- **Development of computer code for numerical simulations (flow and transport, two-phase flow, and coupled THMC)**

BGR's investigation programs in granite (HRL Äspö)

In situ activity

- Two-phase flow and gas tracer transport experiment in water saturated fractured rock (laboratory test, in situ experiment, and numerical modelling)
- Large-Scale Gas Injection Test (LASGIT)

Theory and modelling

- *Modelling Task Force 4 (TRUE – Tracer Retention Understanding Experiments): Modelling of groundwater flow and solute transport*
- *Modelling Task 5: Hydrological and hydro-chemical modelling*
- *Prototype Repository (THM modelling)*
- *Modelling Task Force on Engineered Barrier System (EBS)*

Properties of granitic rock types

- Mechanical and constructional stability of rock mass
- Heterogeneity (discontinuity and fracture network) for potential flow
- High permeability
- High sorption and matrix diffusion property
- Small extension of EDZ

==> **Engineered Barrier System**

Grimsel Test Site (Switzerland)

Bird's-eye view

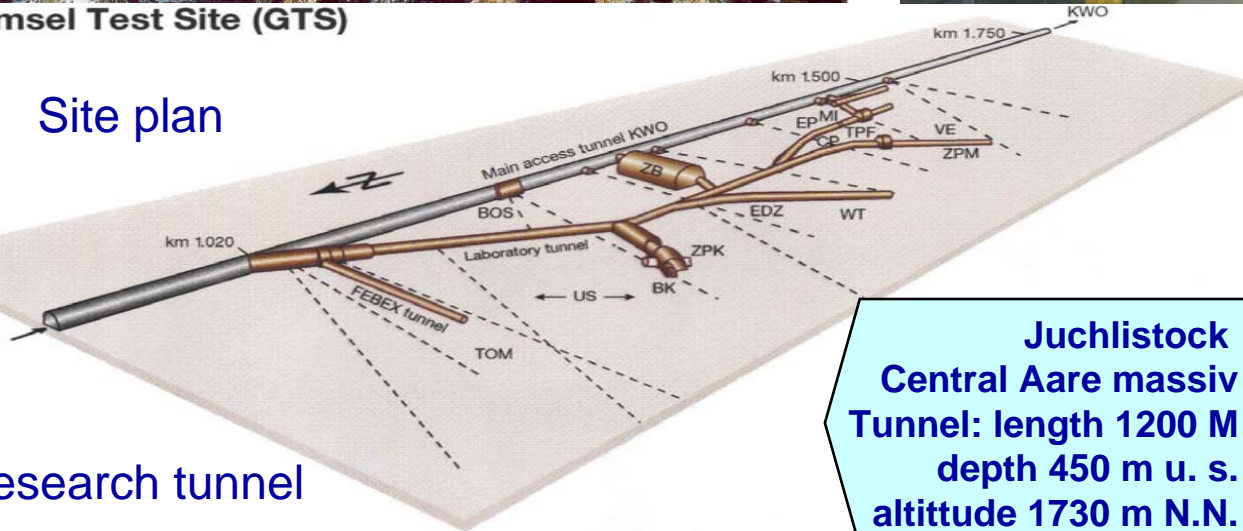


Grimsel Test Site (GTS)



BGR cavern
(BK-area)
Blasted in lamprophyre
and fractured zone

Site plan

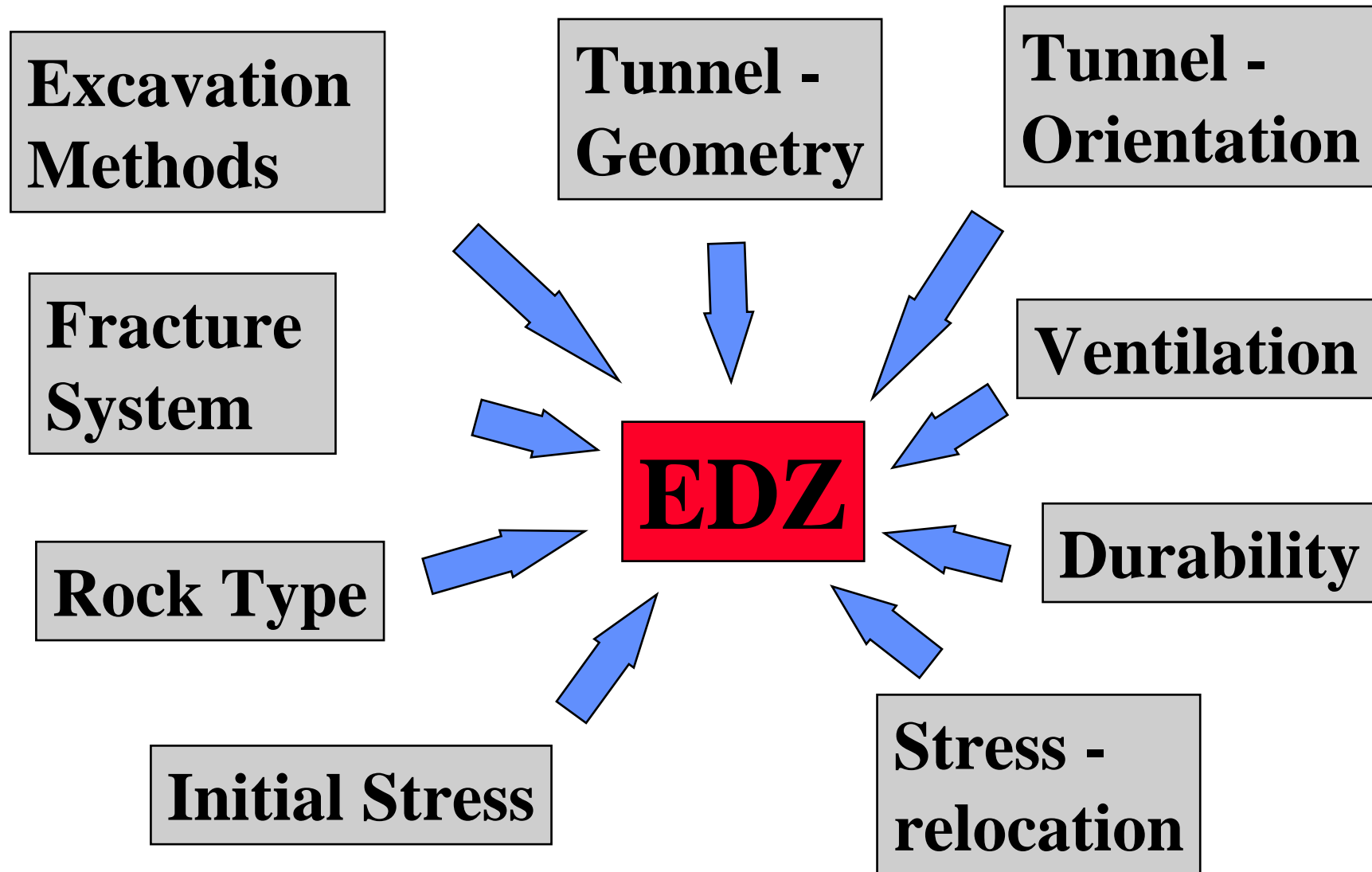


Research tunnel

Juchlistock
Central Aare massiv
Tunnel: length 1200 M
depth 450 m u. s.
altitude 1730 m N.N.

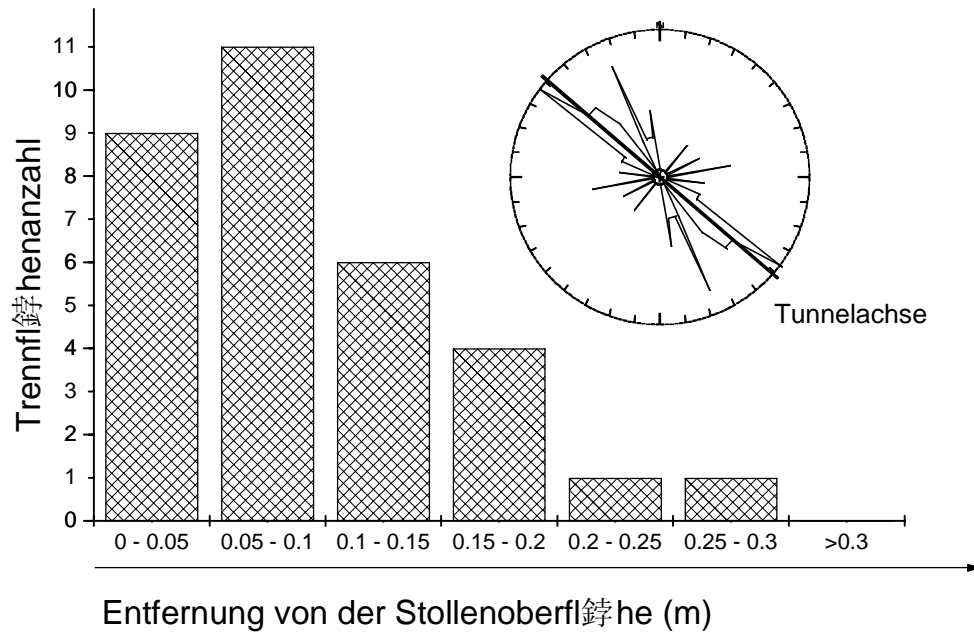


Near-field characterisation - Parameters affect EDZ



Near-field geology

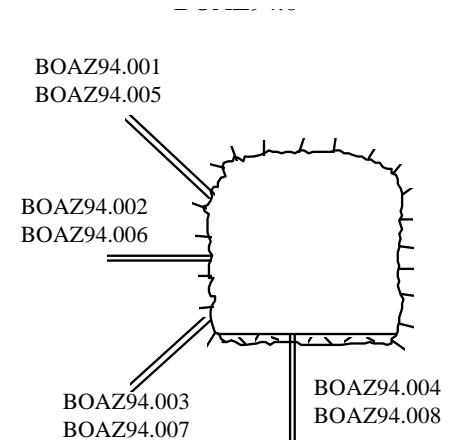
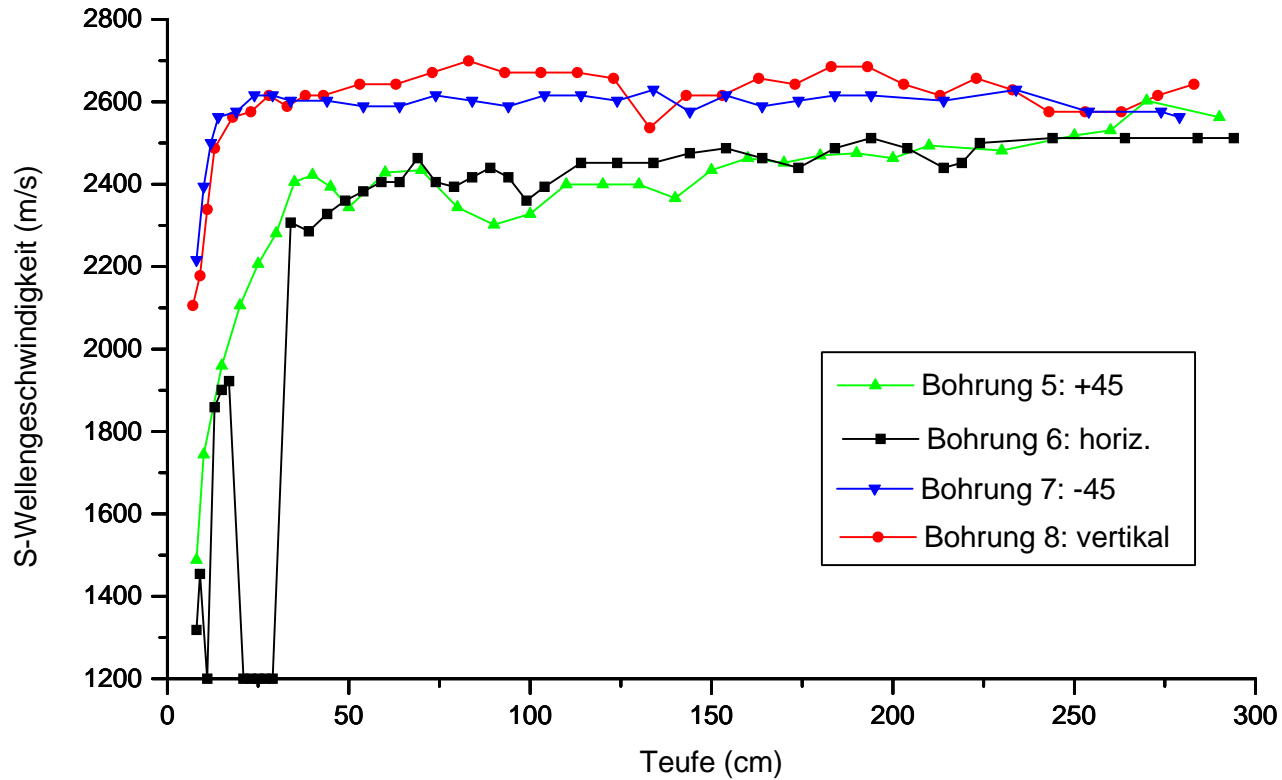
Fracture frequency



Thin section photo: micro fissure network marked with the fluoresced resin (picture 1.2 mm)



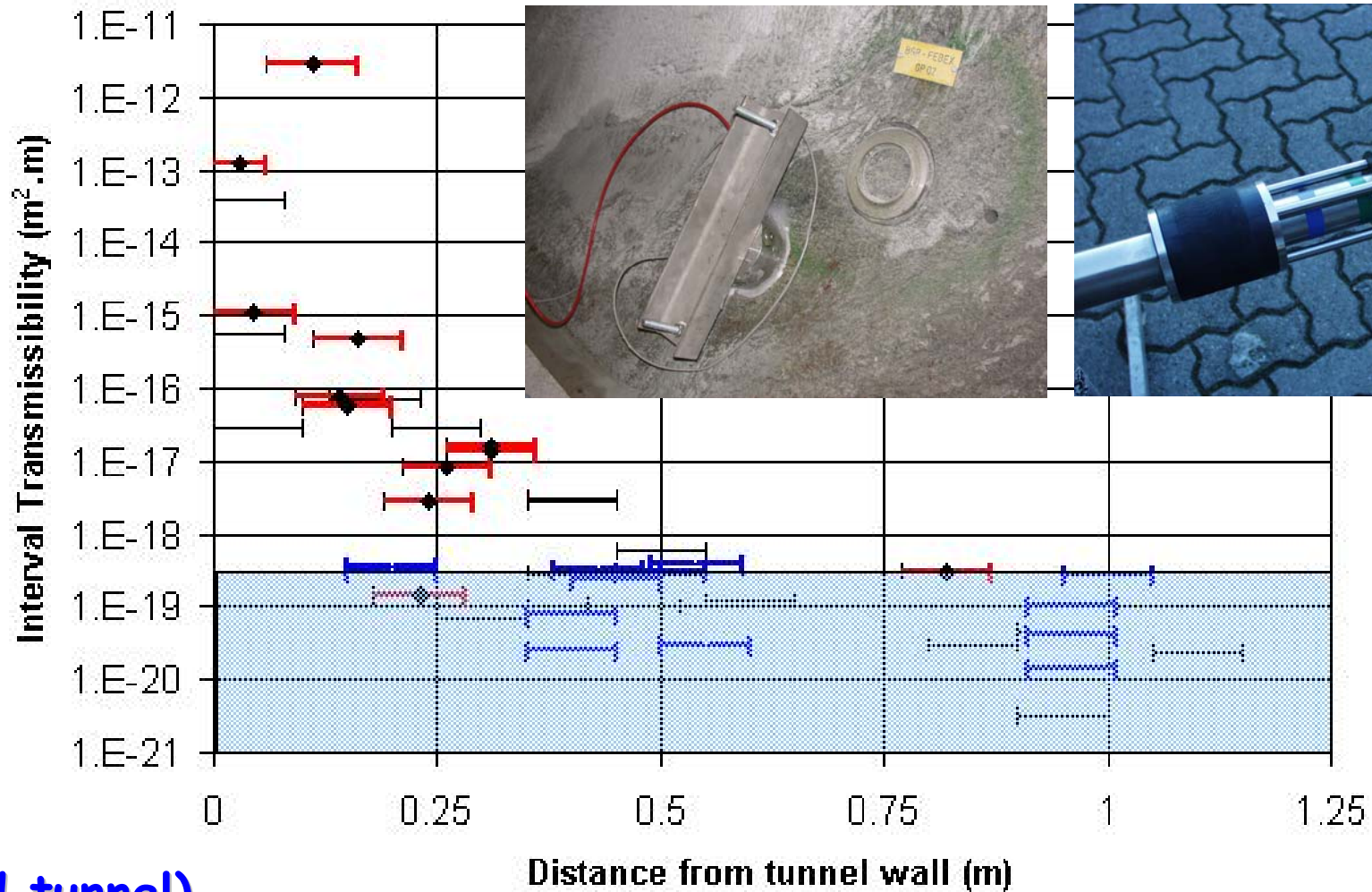
Borehole seismic measurements



Querschnitt und Lage der Bohrungen

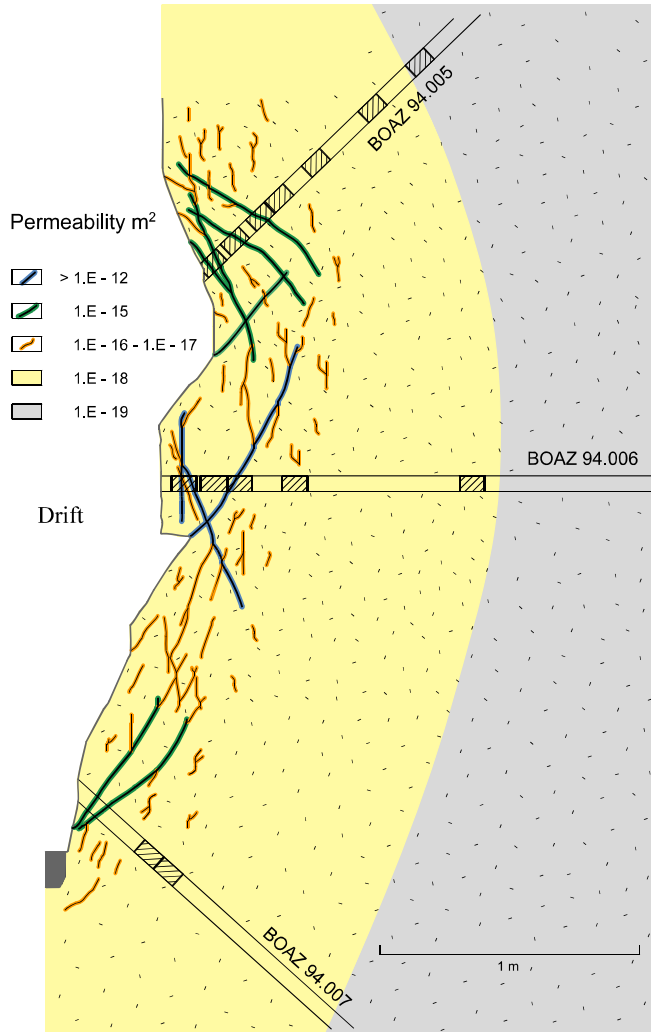
Distribution of near-field hydraulic permeability

Interval Transmissibility Air Injection Tests at BK Area



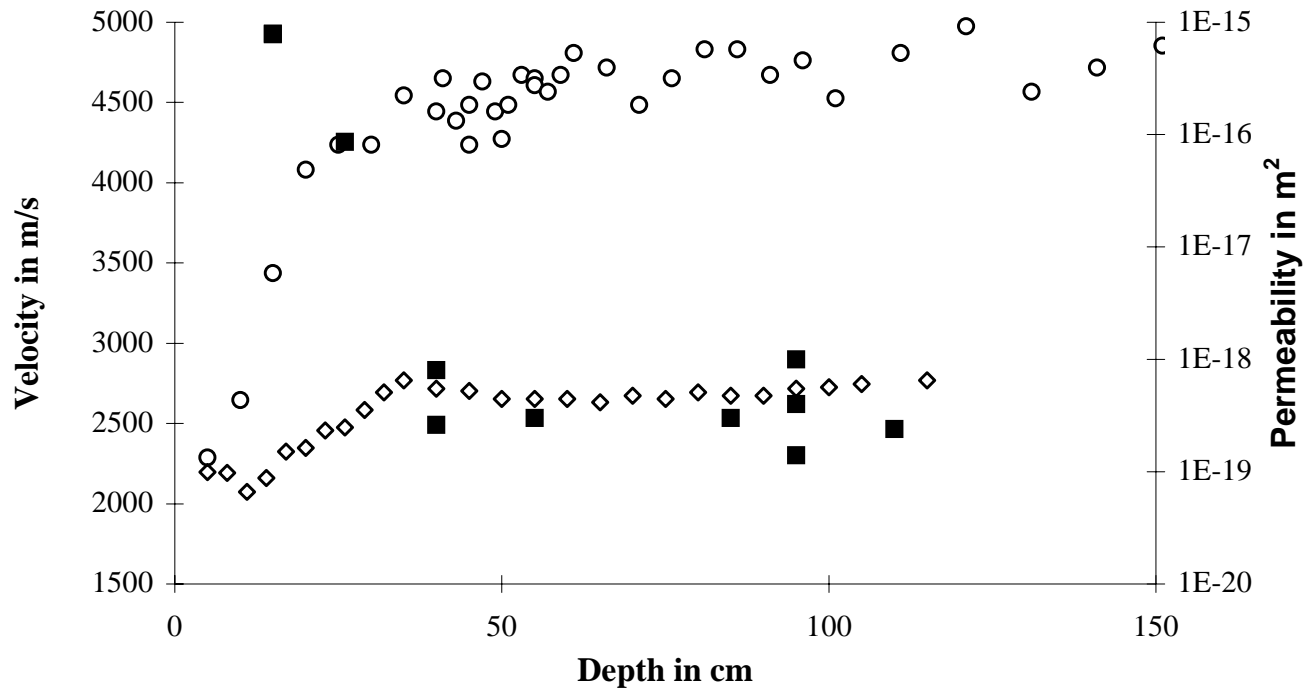
(blasted tunnel)

Near-field fracture model



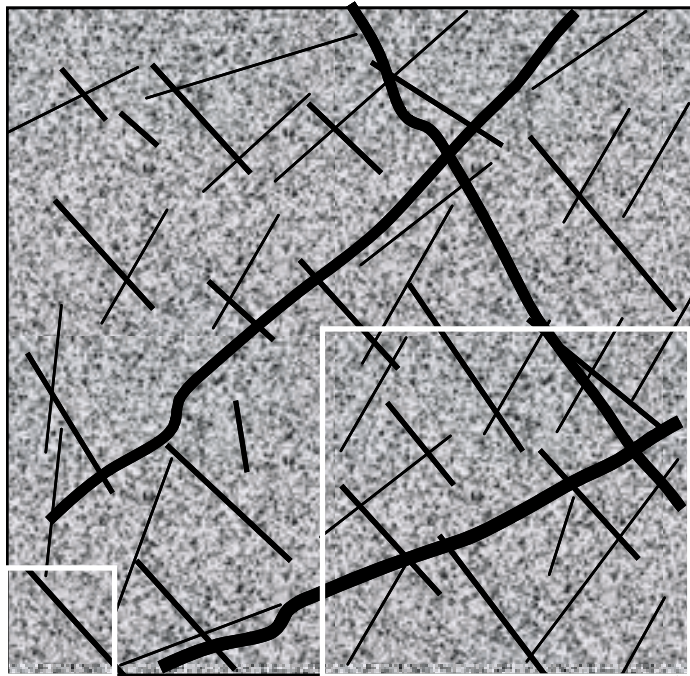
Seismic and hydraulic measurements

Compressional (circles) and shear wave (diamonds) velocities and permeabilities (squares) vs. depth for borehole 94001 (Alheid et al. 1999).



(blasted tunnel)

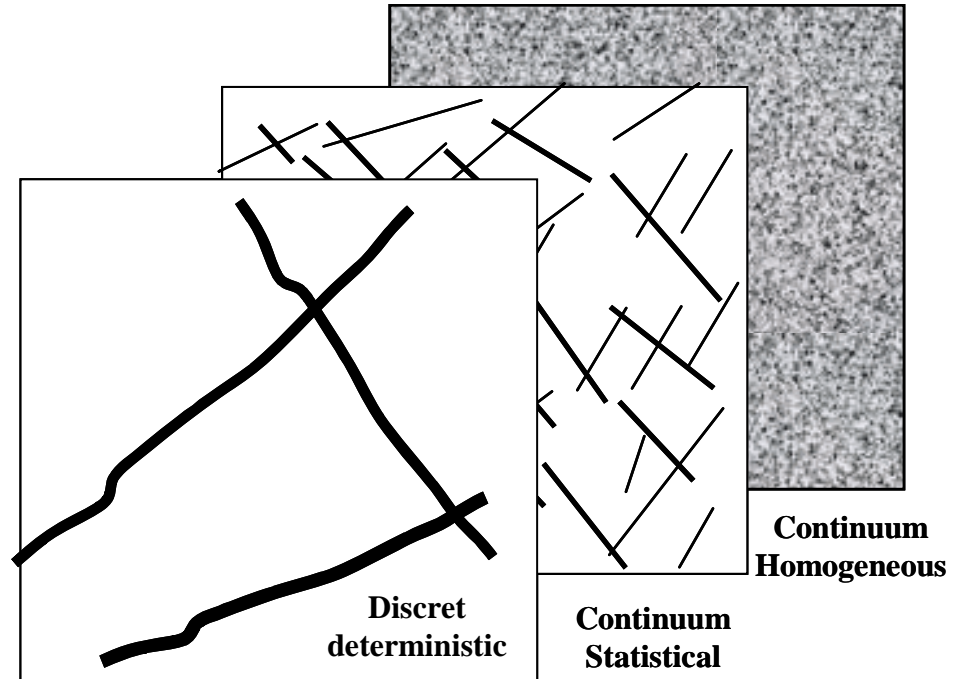
Principle of flow and transport mechanism in fractured rock



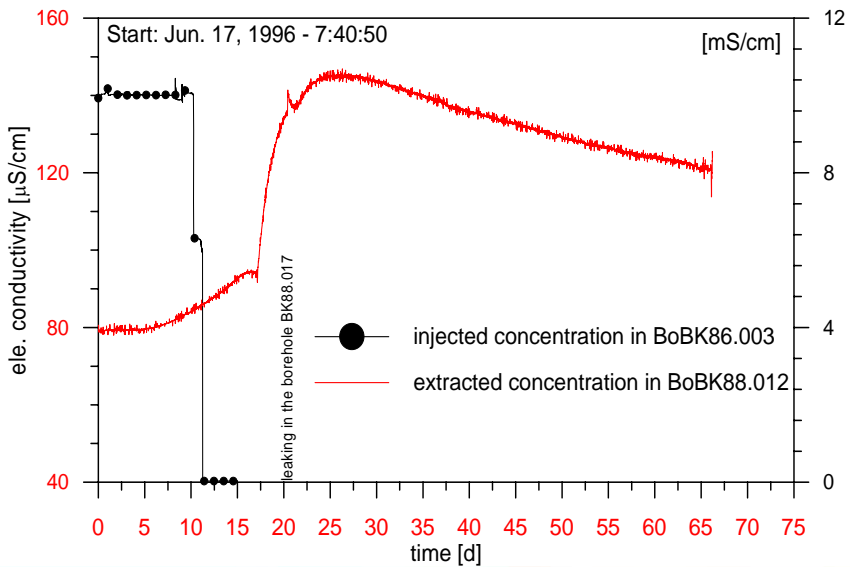
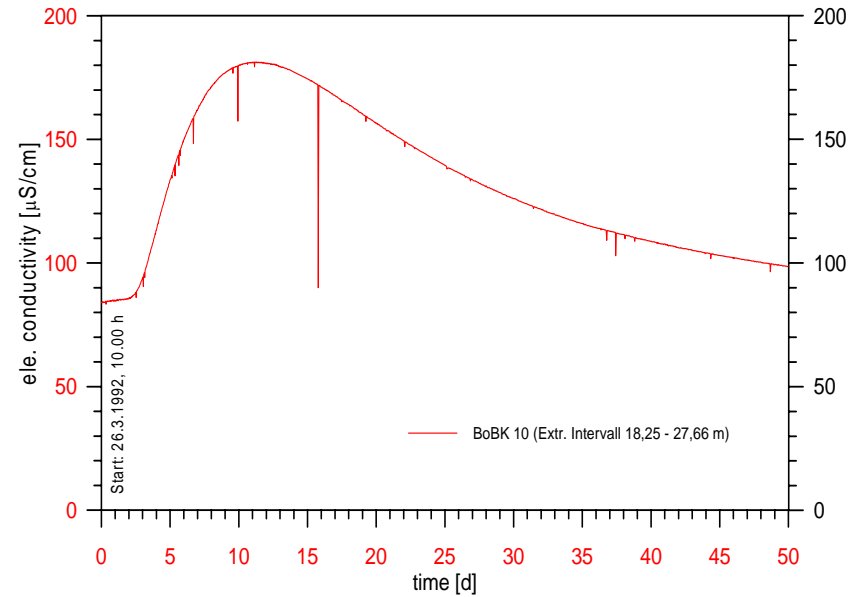
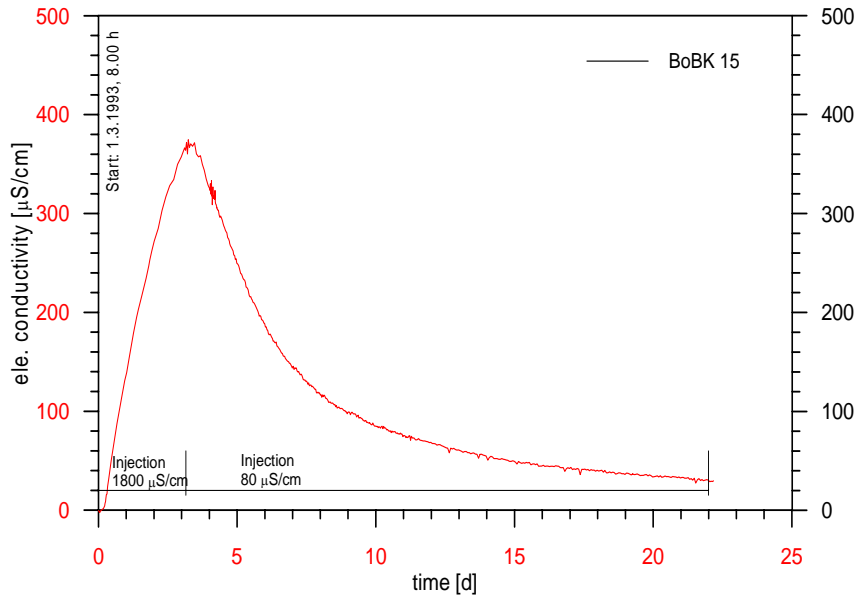
Large Scale
(> 100 m)
Coupled Fracture and Matrix model
Flow and Advection in Fracture System
Diffusion and Sorption in Matrix

Small Scale
(< 10 m)
Single Feature Model
Flow and Advection
in Fracture

Intermediate Scale
(< 50 m)
Fracture Network Model
Flow and Advection
in Fracture System



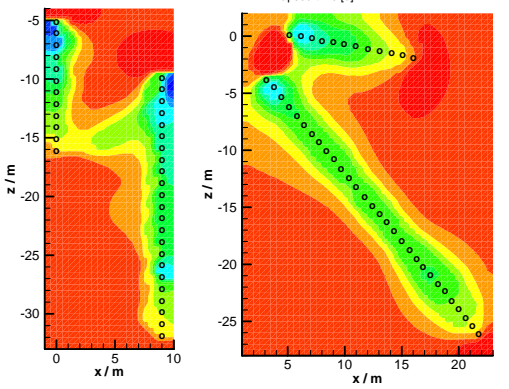
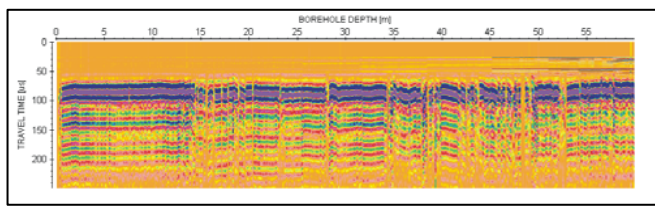
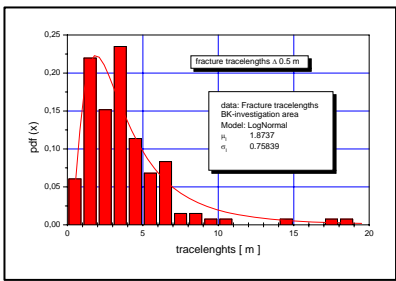
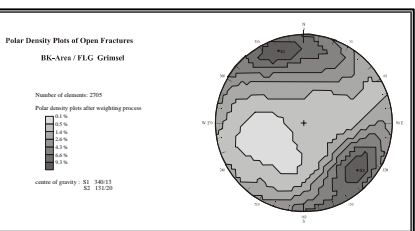
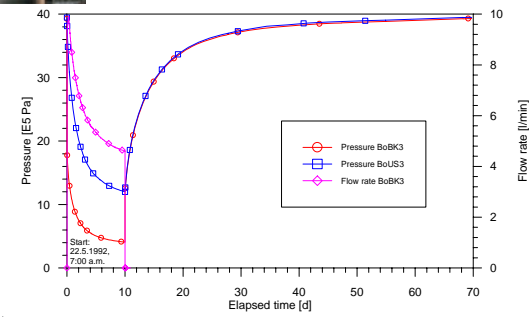
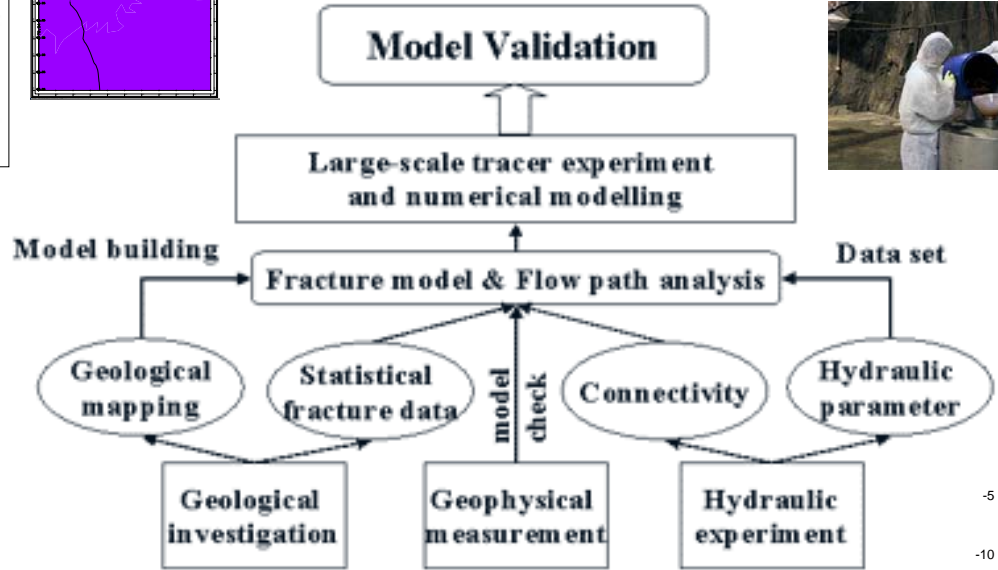
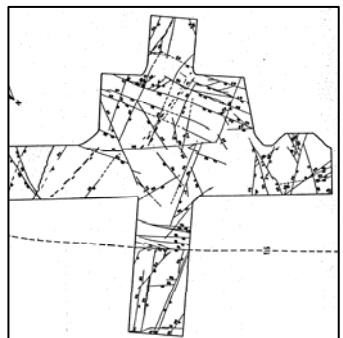
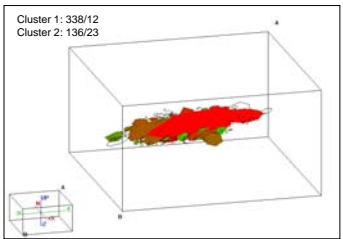
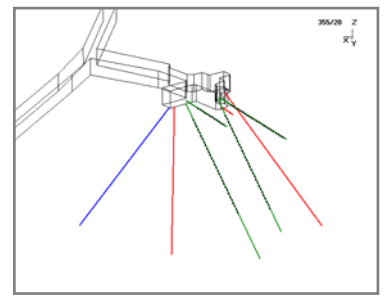
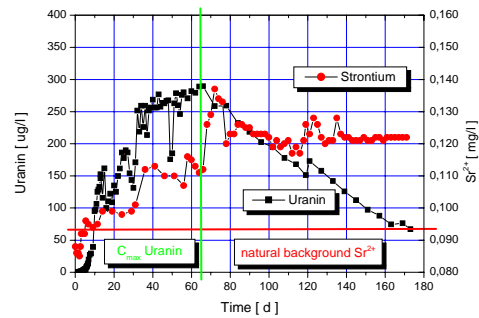
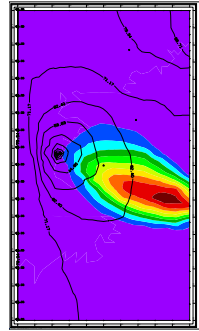
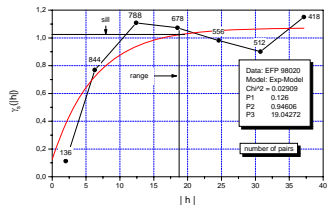
Scale dependence of solute transport in fractured rock



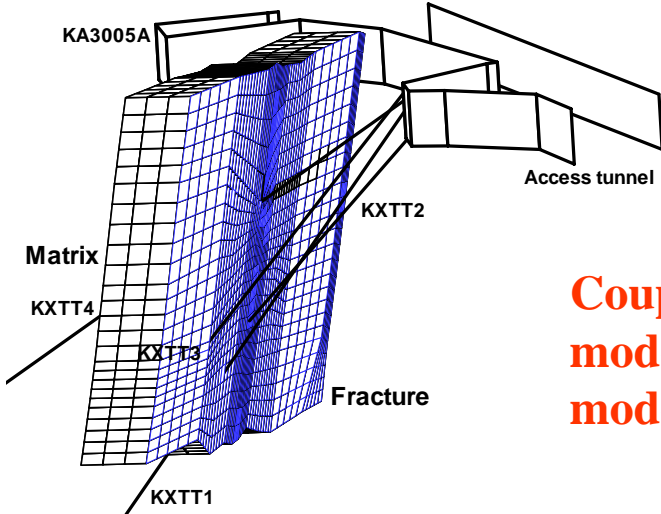
	$C_{max}/C_0(-)$	$t_{max} (d)$	$t_{5\%}(d)$	$t_{50\%}(d)$	$t_{95\%}(d)$
Small scale (< 10 m) (VE520)	0.25	3.5	1.4	5.1	18.4
Intermediate scale (< 70 m) (VE493)	0.018	11	5.8	19.4	49.6
Large scale (> 100 m) (VE800)	0.015	26.7	19.9	38.6	63

EFP - Effective Field Parameter

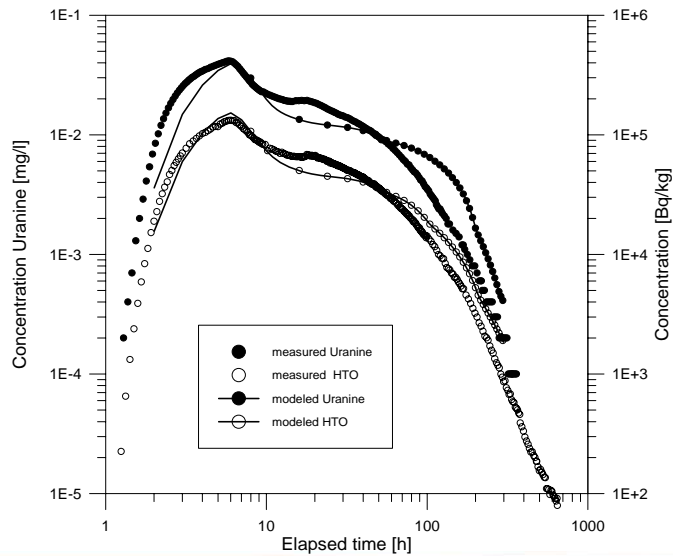
a combined modelling strategy considering deterministic and stochastic distribution of effective parameters



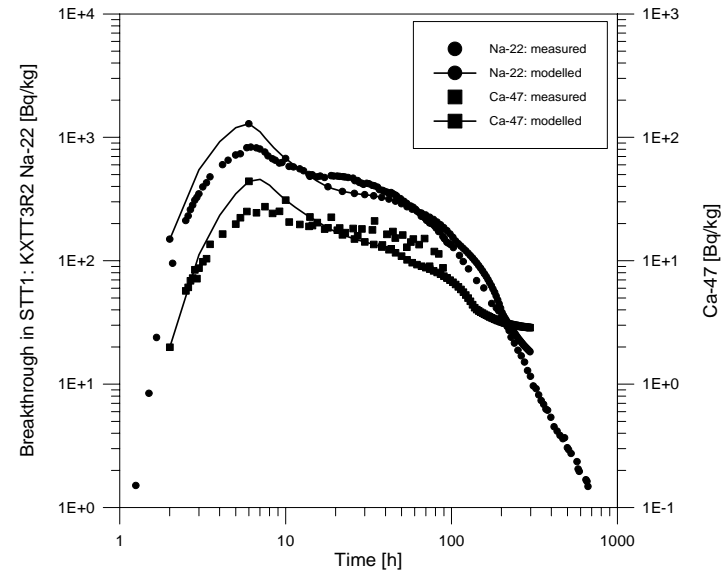
Numerical modelling of tracer transport in STT-1 Experiment TURE-1 / HRL Äspö (Sweden)



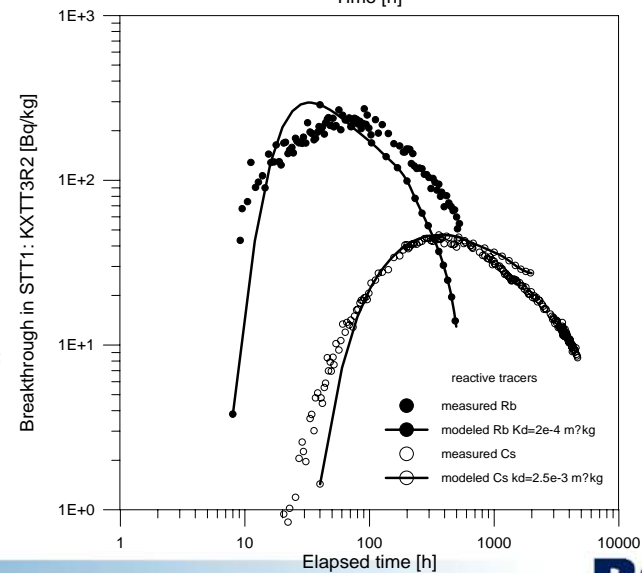
**Coupled 3D
model for numerical
modelling**



**Conservative
tracers:
Ur, HTO**

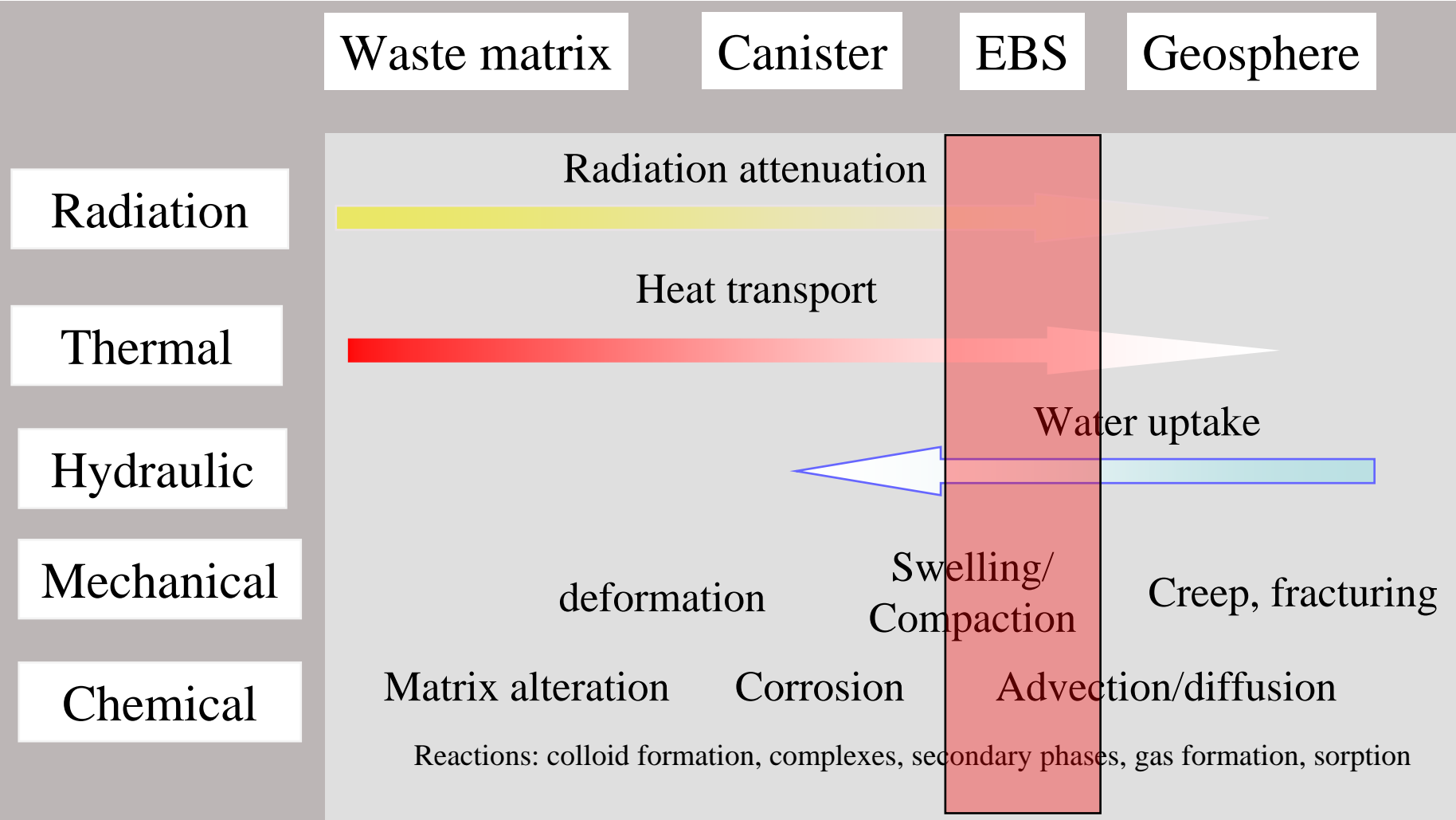


**Weak sorbing
tracers:
Na²², Ca¹⁴⁷**



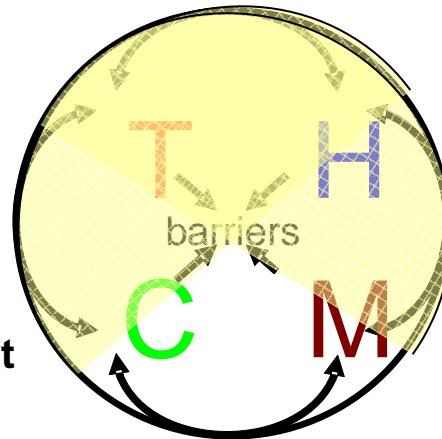
**Sorbing
tracers:
Rb⁸⁶, Cs¹³⁷**

Interacting near-field components and predominant processes



Simulation of coupled THMC processes

Heat transport
(conduction,
Advection)



Solute transport
Dispersion,
Diffusion,
Sorption,
decay und
chem. Chain reaction

(Equilibrium & Non-equilibrium reactions)

Ext. Chemical Simulators (PHREEQC, ChemApp...)

Groundwater flow
Gas flow
Multiphase flow
Unsaturated flow

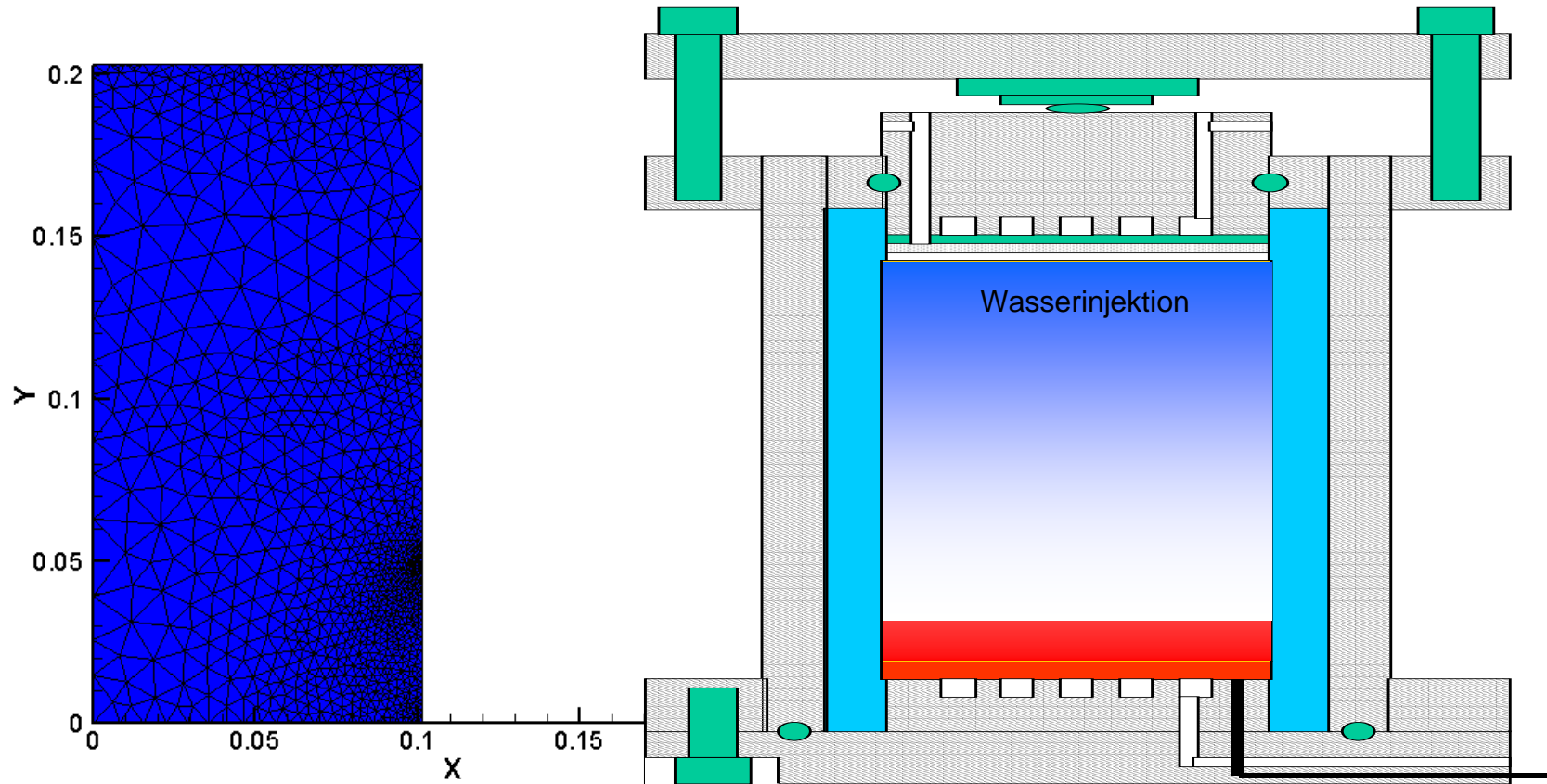
Deformation process
(elastic, plastic, creep)

Code GeoSys/RockFlow:

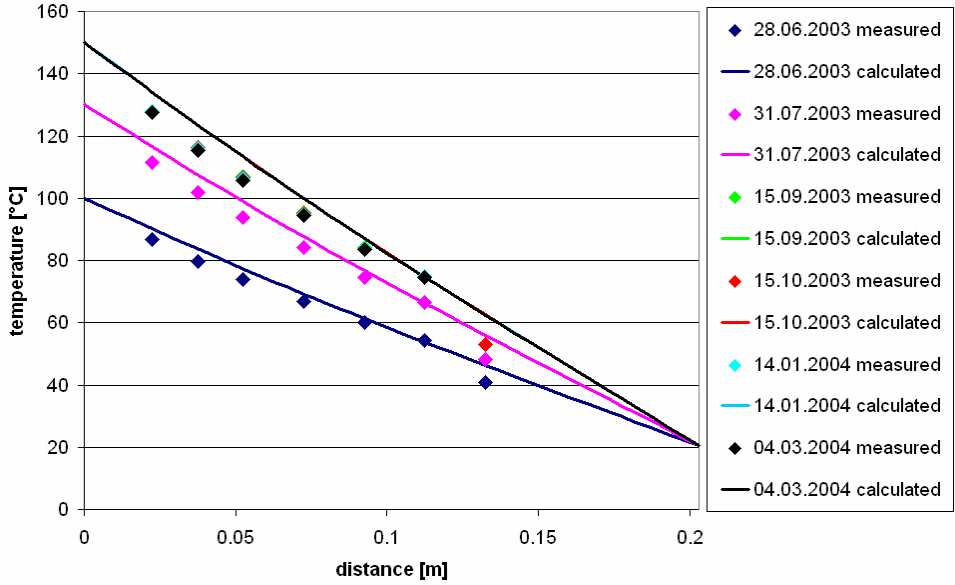
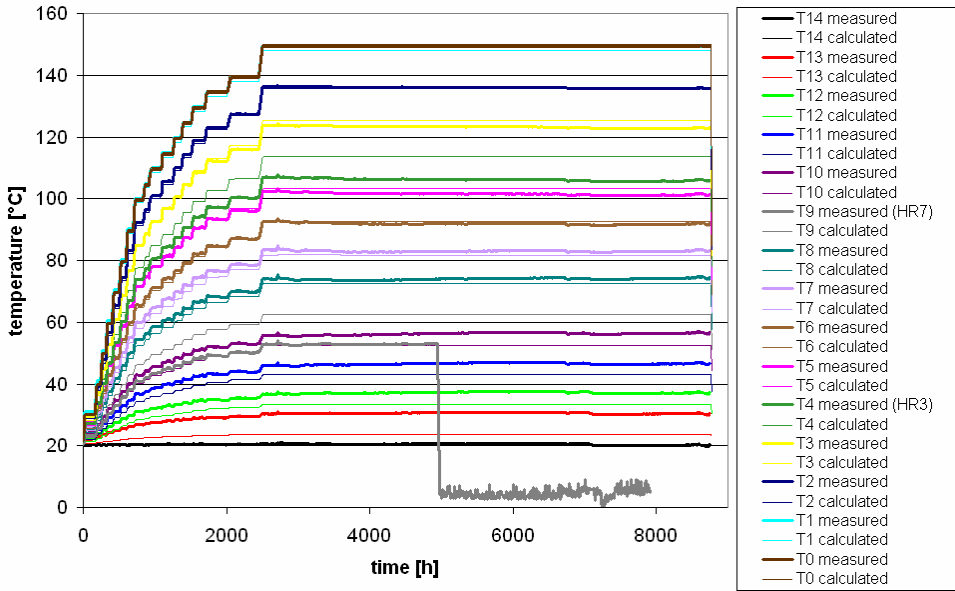
- *Object-Oriented implementation*
- *Partitioned method*
- *Different time stepping for different processes*
- *Sub-Domain deactivation techniques*
- *Parallelization*

Benchmarking THM

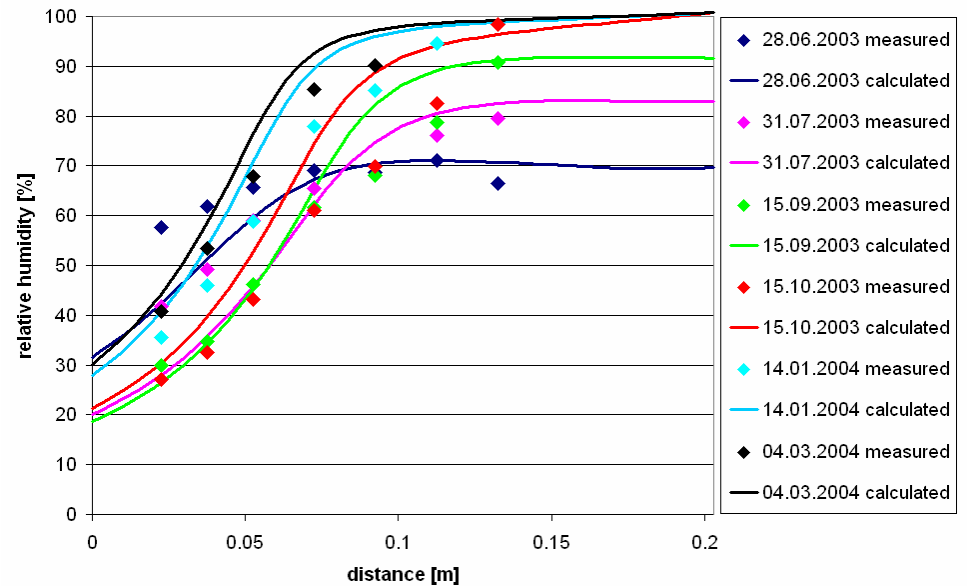
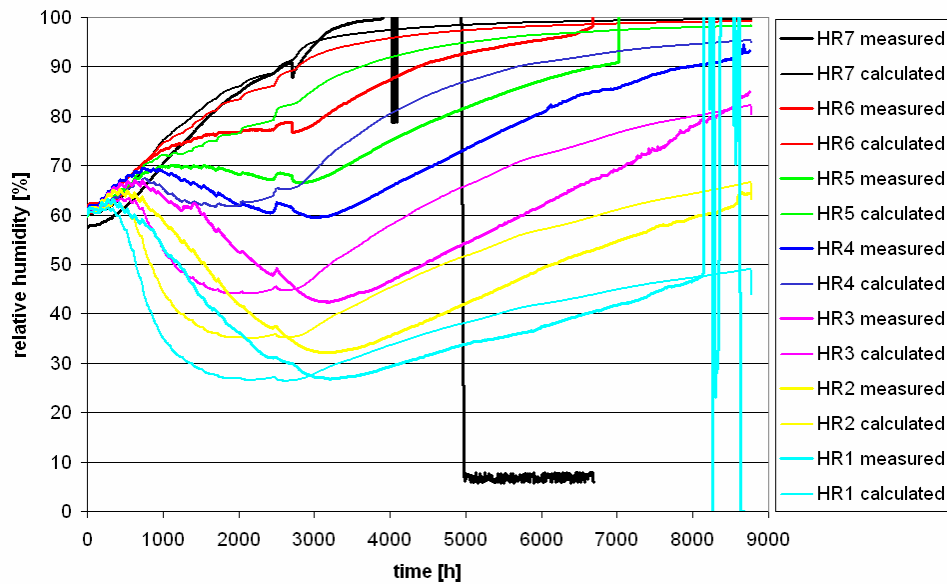
Laboratory experiments on bentonite-buffer



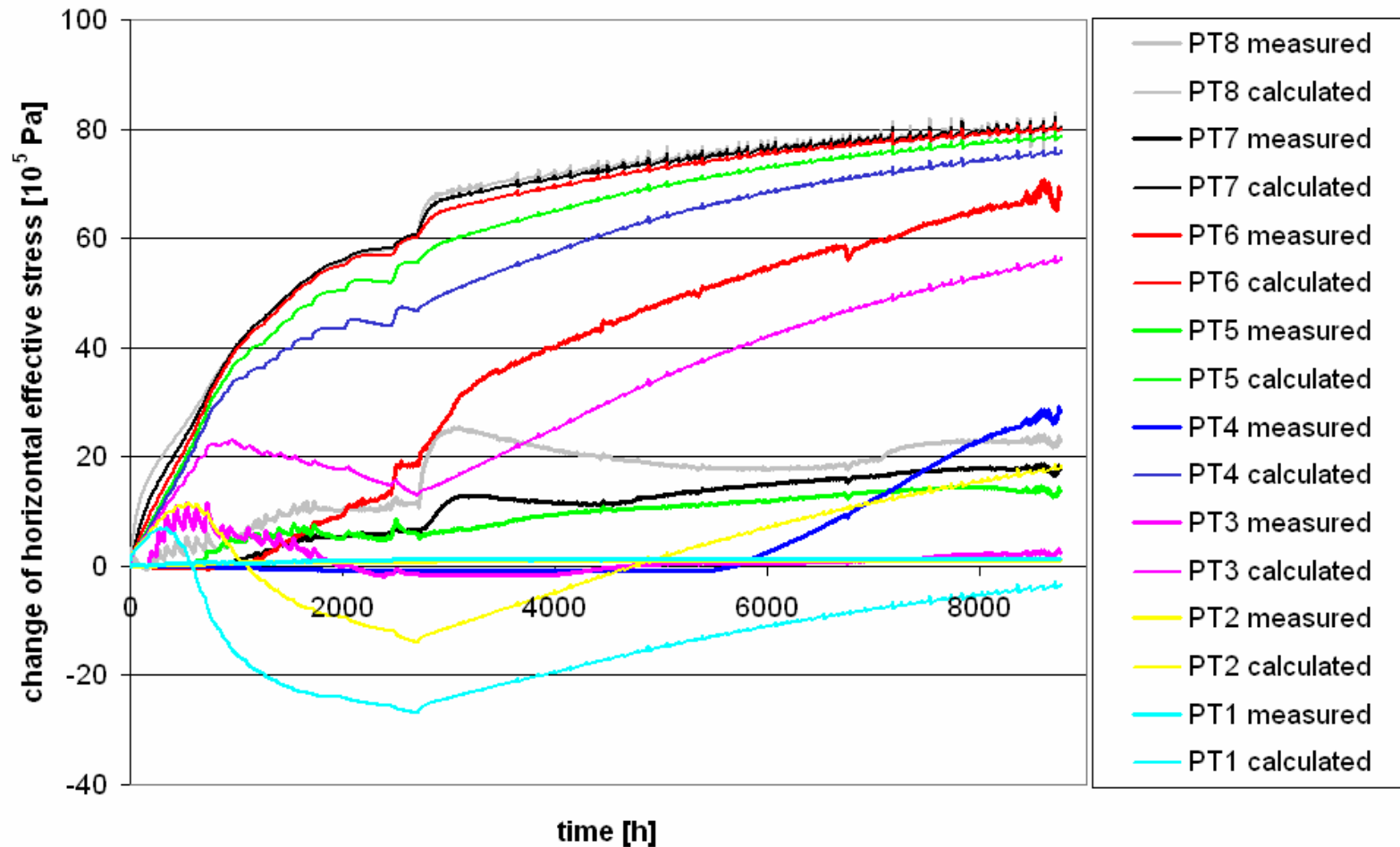
Results T: Temperature



Results H: Relative humidity



Results M: Change of horizontal effective stress - evolutions



Conclusions

- Successful interdisciplinary team work
- Test of investigation concept for large-scale flow and transport processes in fractured rock
- Near-field characterisation of possible potential flow path for transport process
- Heterogeneity of the fractured rock plays an important role, which may be simulated by fracture network model using stochastic generation of parameters based on the statistical evaluation of geological fracture data
- Long-term monitoring and modelling of the coupled THM(C) processes under natural conditions
- Validation of numerical code against laboratory and in situ experiments for ‘confidence building’
- Investigation of interaction between geological and geotechnical barrier systems

in situ **Hydro-Mechanical Characterisation of
Clay Formation
and Coupled HM Modelling**

Dr. SHAO, Hua

Federal Institute for Geosciences and Natural Resources (BGR)

Hanover, Germany

BGR Research Programs in Clay Formations

In situ measurements

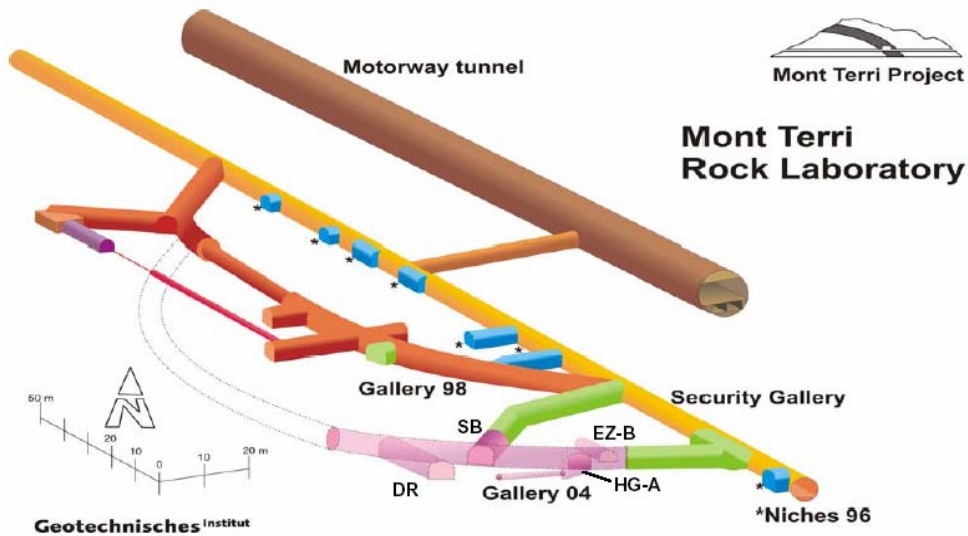
- **Permeability**
- *In situ* stress
- **Seismic**

Laboratory tests & Modelling

- *Rock properties*
- **Coupled HM processes**



(Schuster (BGR), 2005)

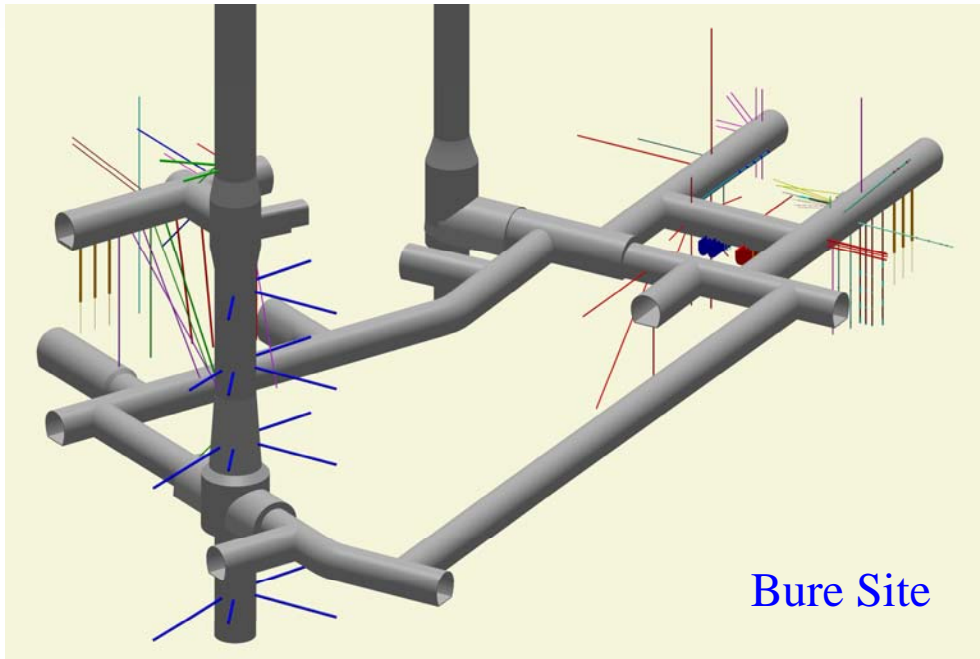


(GI, 2006)

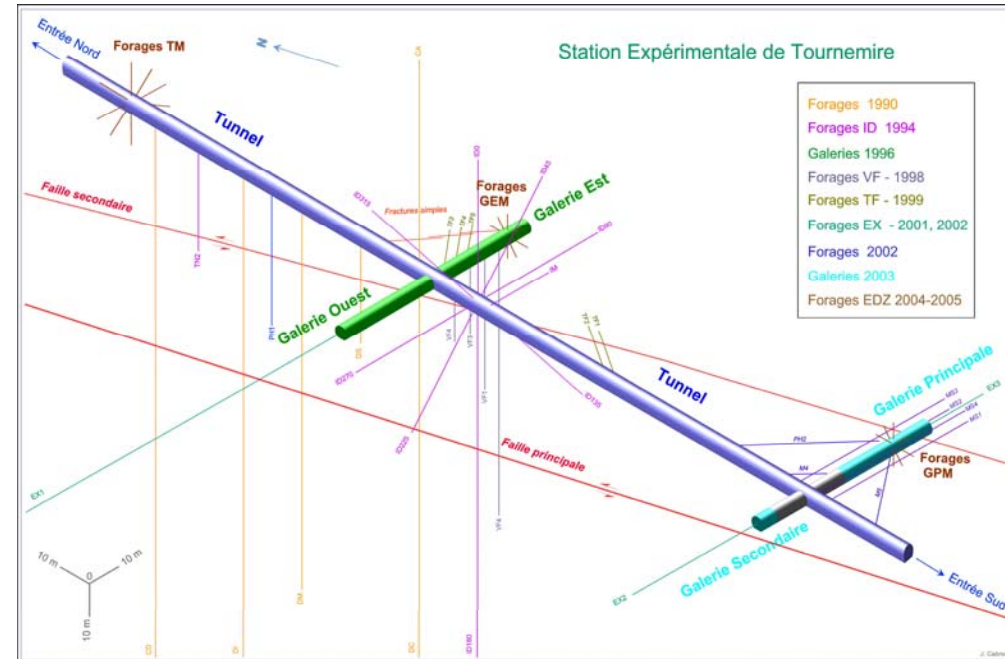
Test Sites

- Mont Terri (CH)
- Bure (F)
- Tournemire (F)

(IRSN, 2006)



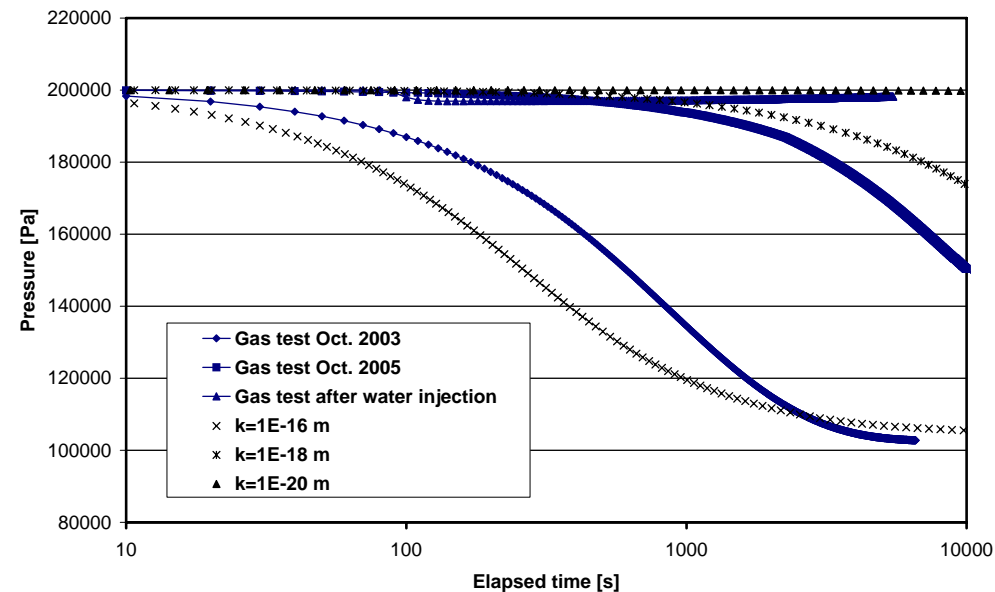
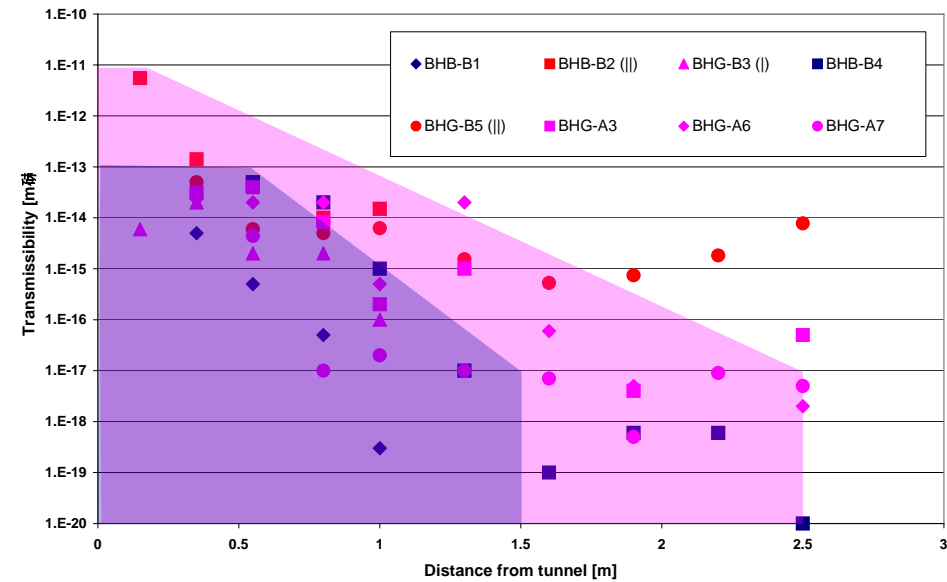
(ANDRA, 2006)



EDZ Permeability / Permeability Development



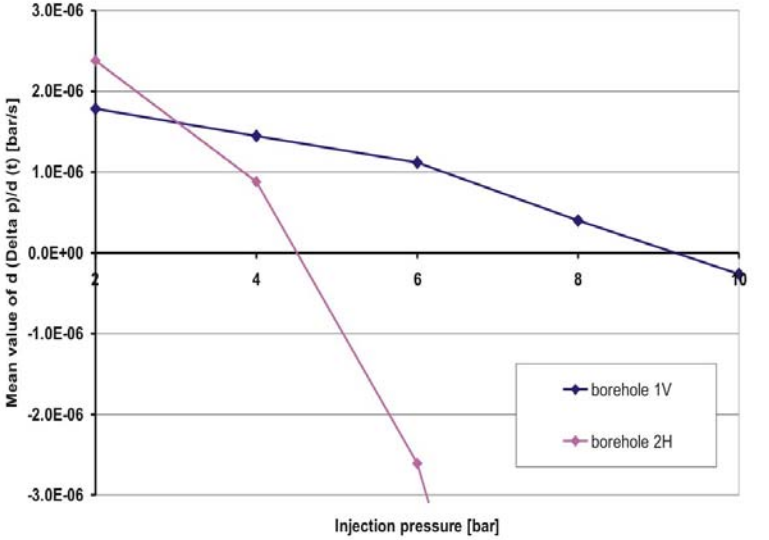
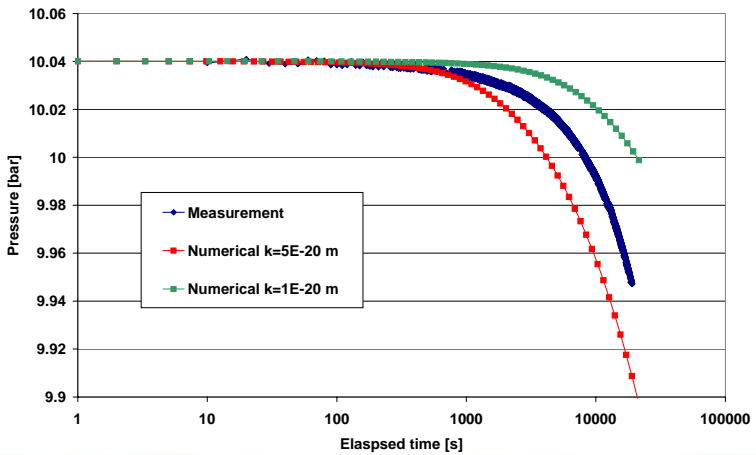
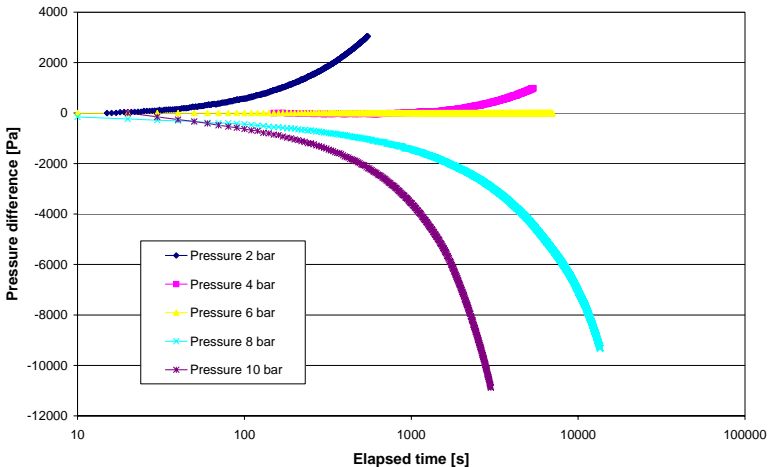
- Testing immediately after the drilling
- Mechanical double packer with 10 cm interval for testing (max. 2.5 m)
- High $k > 1.E-16 \text{ m}^2$: 1.5 m (\perp) and 2.5 m (\parallel)
- Instable borehole parallel to bedding
- Permeability decrease up to one order of magnitude after two years (temporary)
- Permeability decrease up to two orders of magnitude due to humidity (swelling)



Far-Field Gas Permeability / Gas Entry Pressure

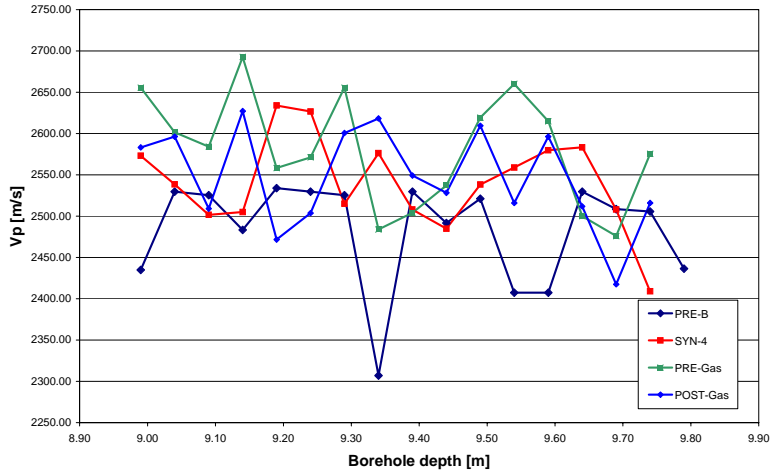
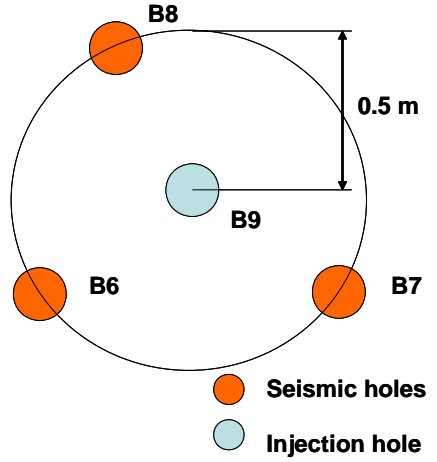
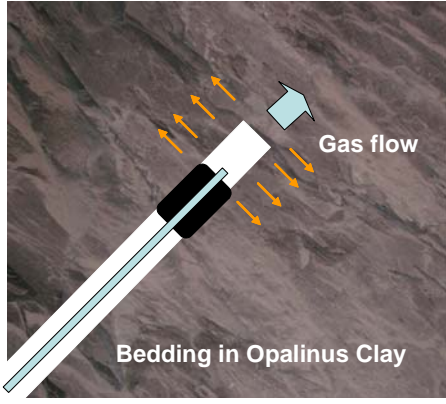


- Testing using a single packer (max. 20 m)
- Stepwise Increase of Gas Injection Pressure → Gas entry pressure (0.4 – 1.0 MPa)
- Evaluation of experiment using numerical two-phase-flow model taking capillary and pore water pressure into consideration
- Gas permeability $k < 5.E-20 \text{ m}^2$ (10 bar)

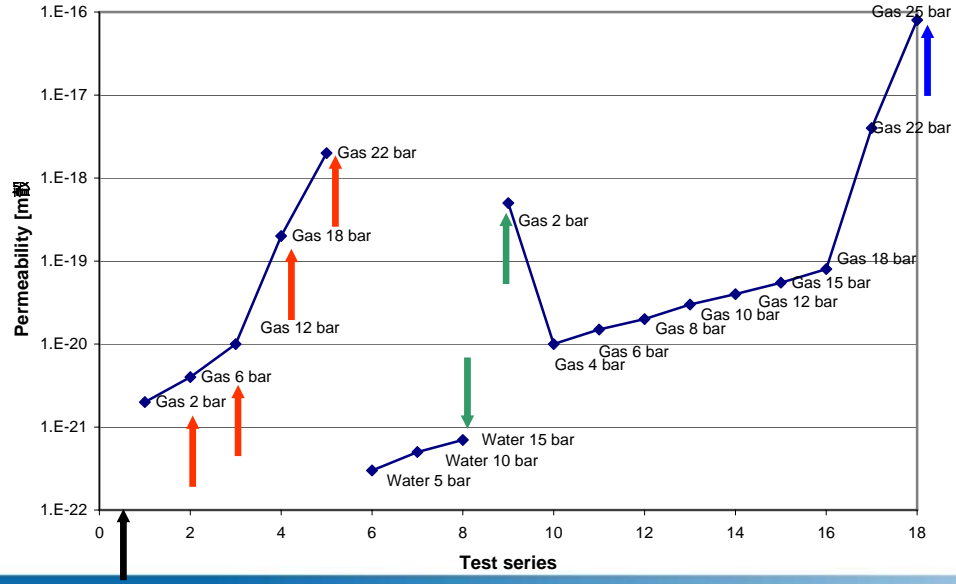


Dilatancy controlled gas flow and self-sealing capability

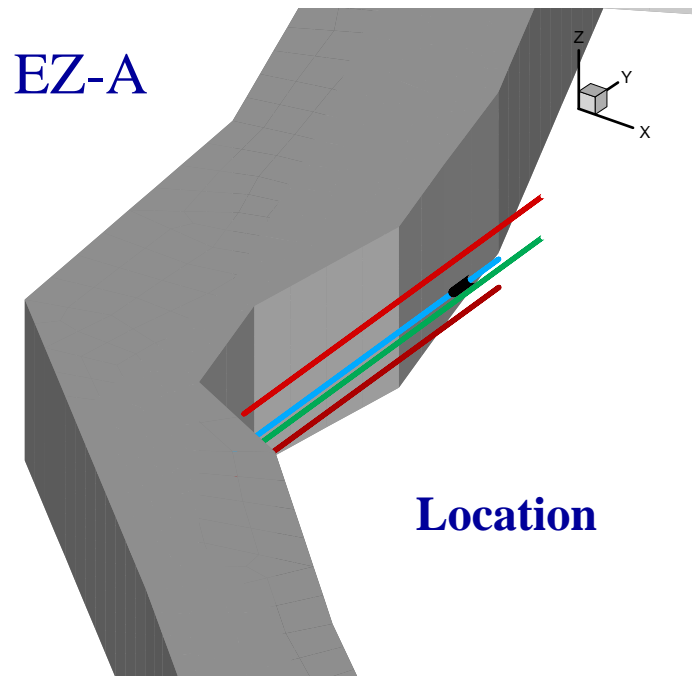
Concept



Test series

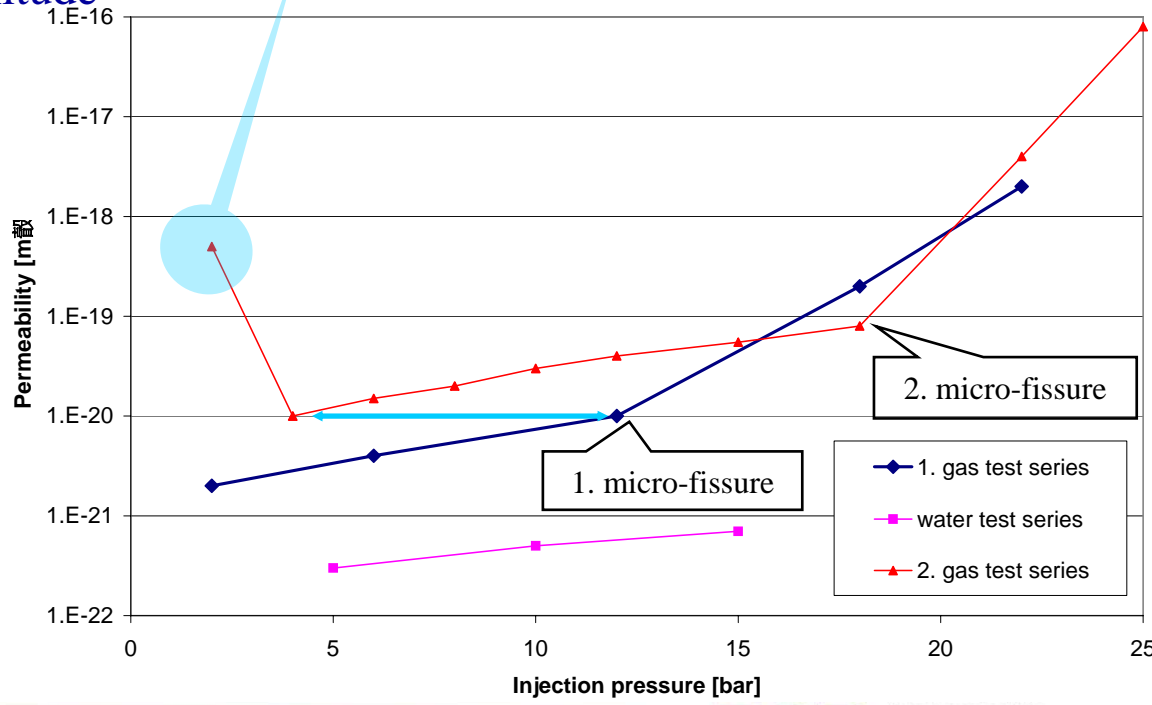
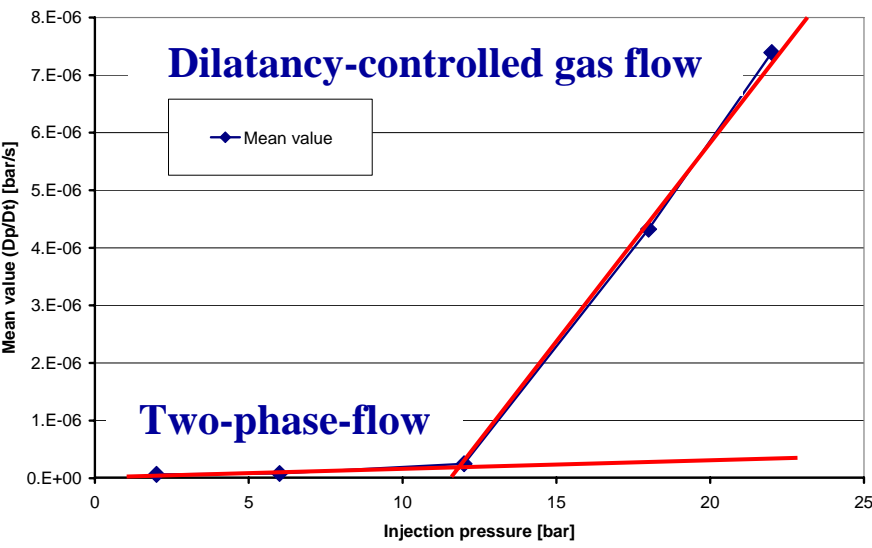
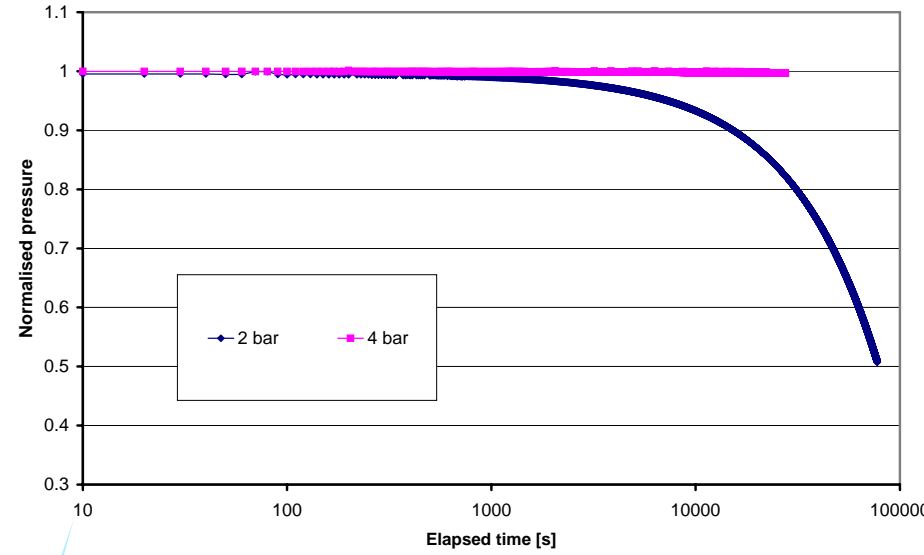


Seismic result

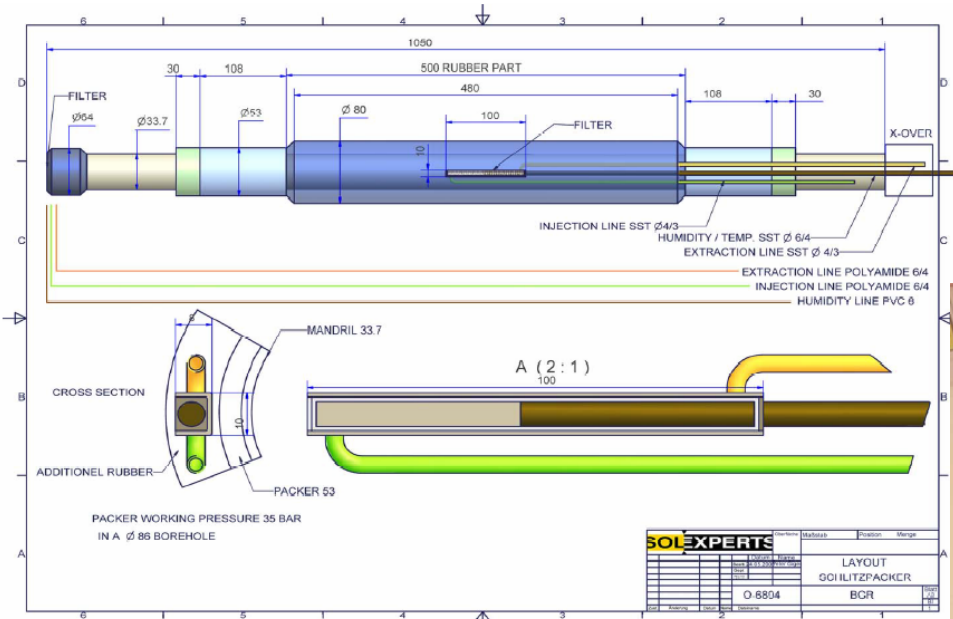


Semi-Permeable Membrane Function

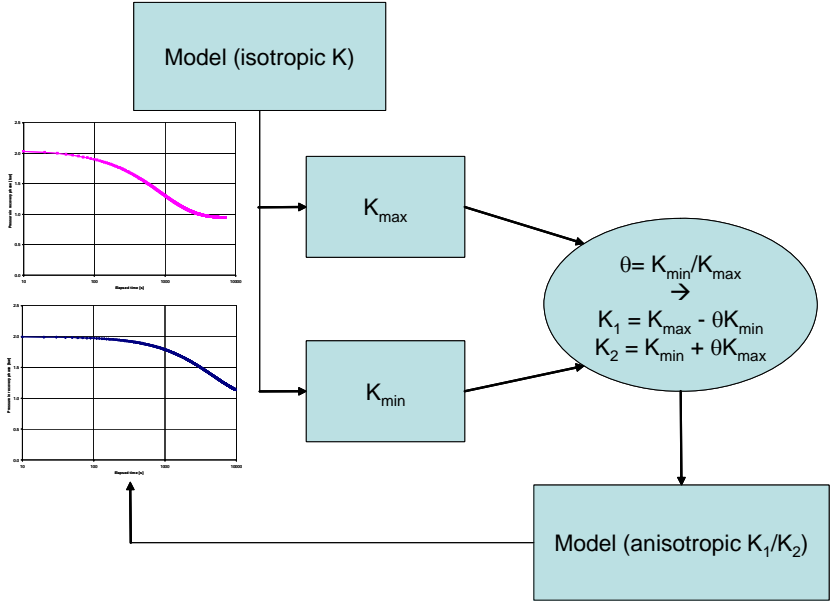
- Determination of two gas-flow-regimes (1.2 MPa)
- Linear relationship between permeability and injection pressure
- (Gas/Water) Pressure dependent permeability
- Sealing through swelling reduce the permeability (2 orders of magnitude)
- Permeability to water is 2 orders of magnitude lower than permeability to gas



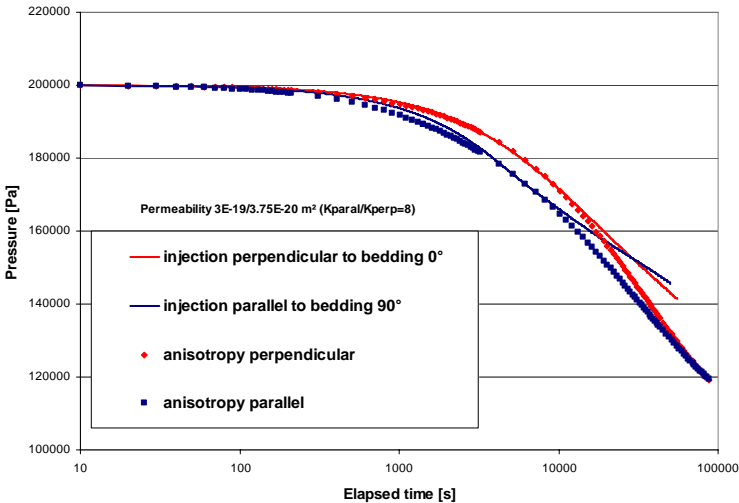
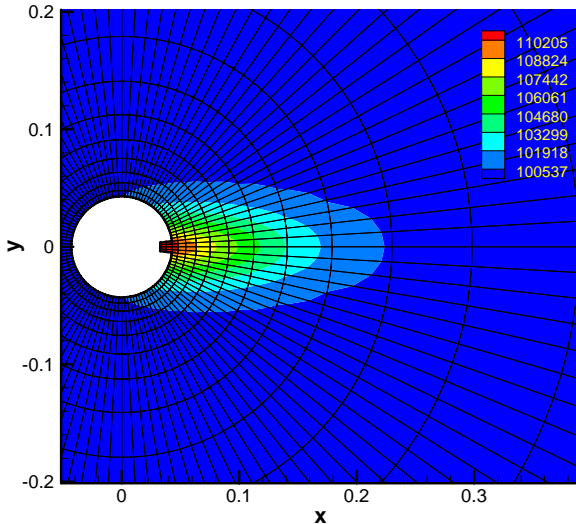
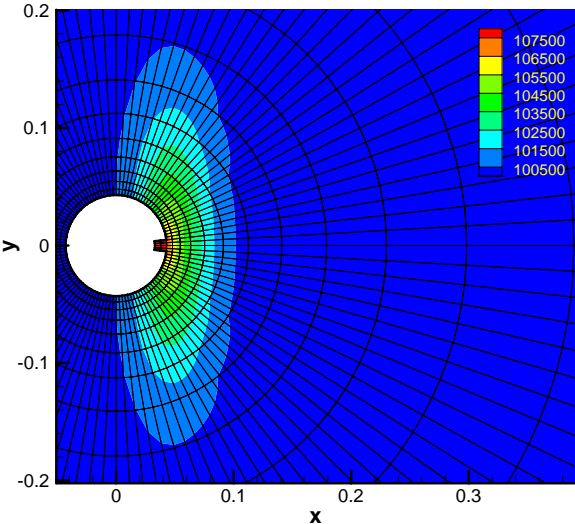
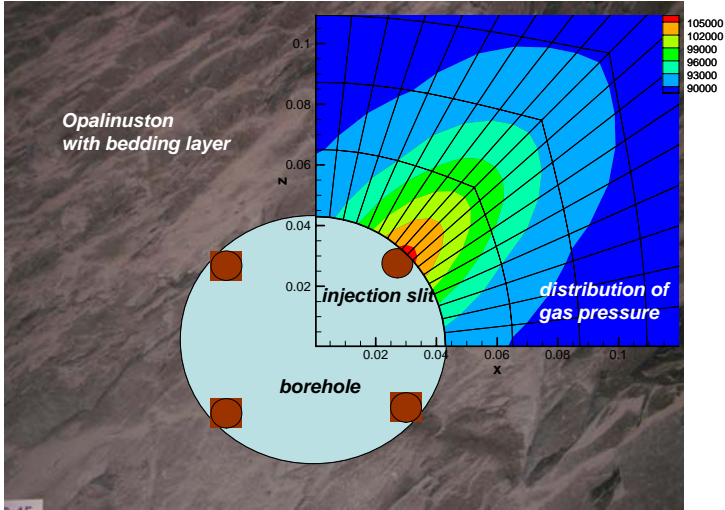
Determination of Hydraulic Anisotropy

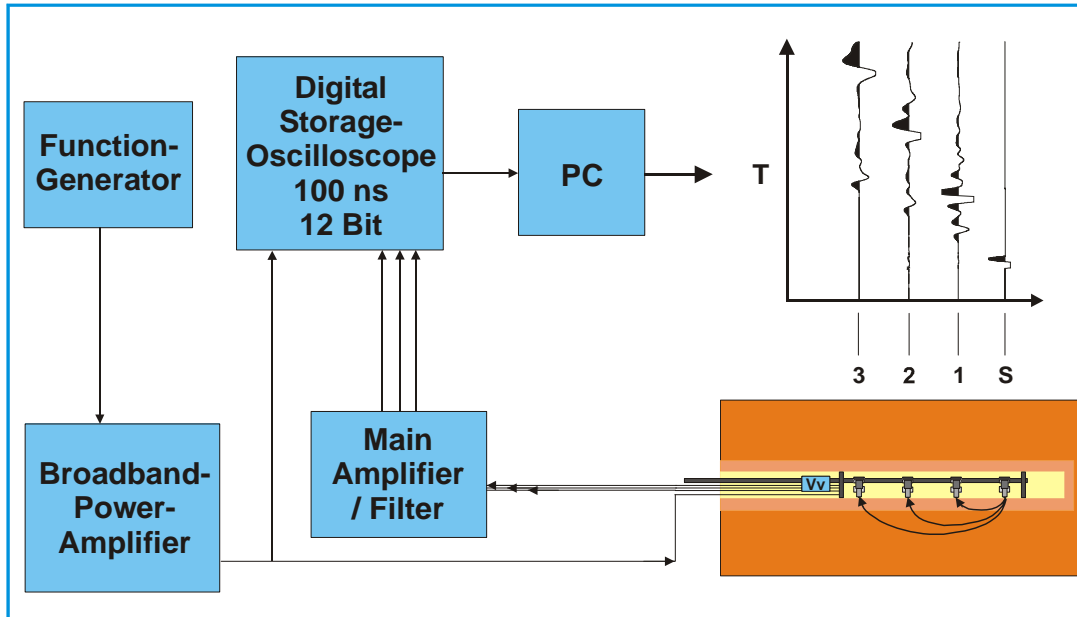


Numerical Evaluation



$K_{\parallel}/K_{\perp} = 8$

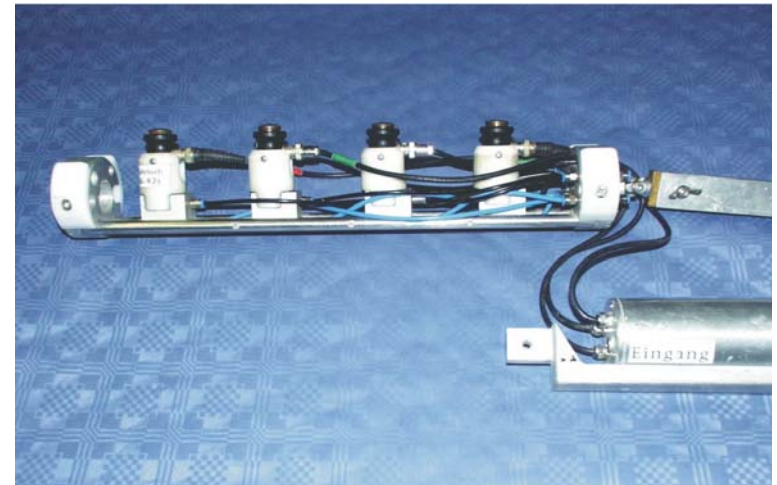




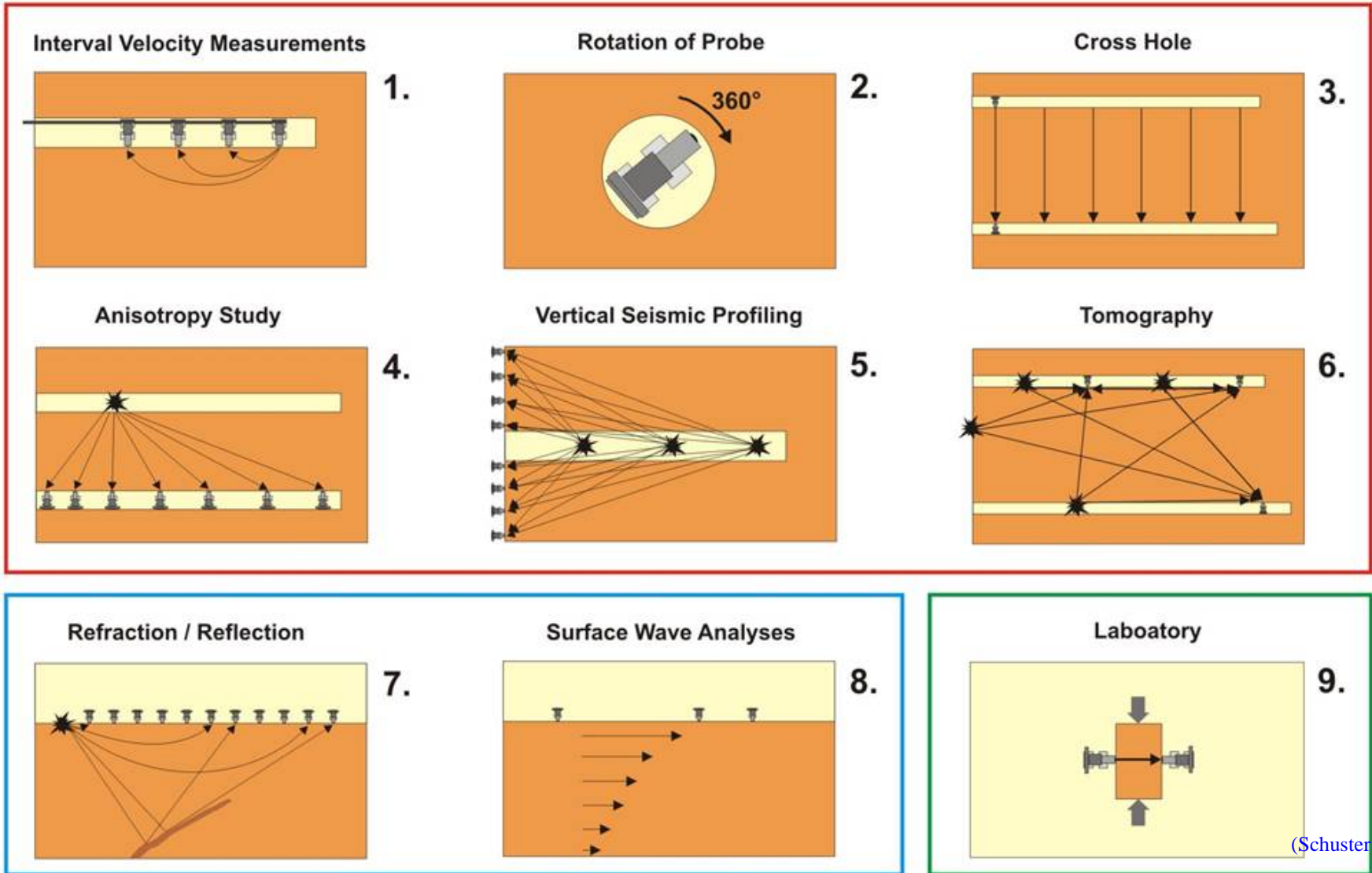
Mini-Sonic-Probe

- Crystalline rock: Grimsel, Äspö
- Salt rock: Morsleben, Gorleben
- Clay stone: Mont Terri, Bure

(Schuster (BGR), 2005)



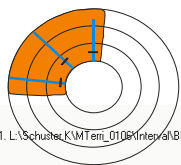
Applied seismic in situ methods



(Schuster (BGR), 2007)

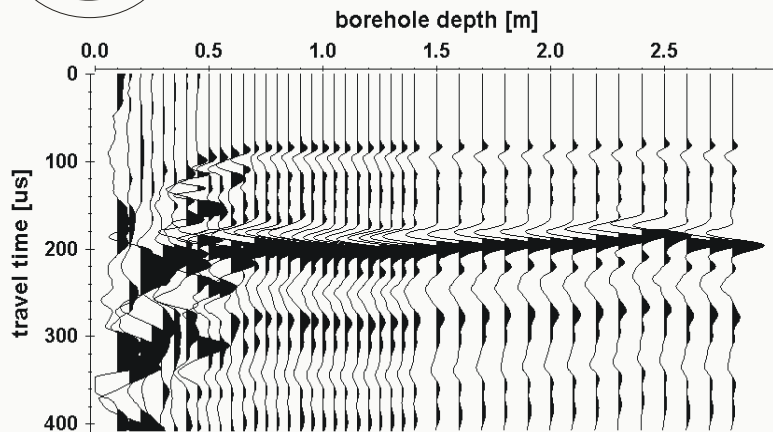
EDZ Characterisation

B 10

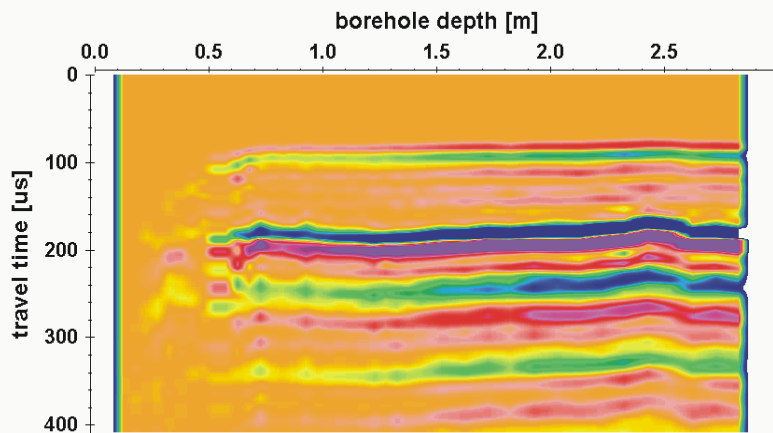


Borehole B10, 45° inclined

1. L:\Schuster.K\MTeri_0106\Interva\BEB10-00\PROCDATA\10_00_C2.01T / traces: 41 / samples: 5000



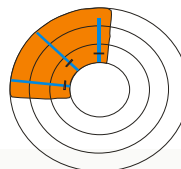
1. L:\Schuster.K\MTeri_0106\Interva\BEB10-00\PROCDATA\10_00_C2.20T / traces: 55 / samples: 5000



Amplitude
Negative 0 Positive

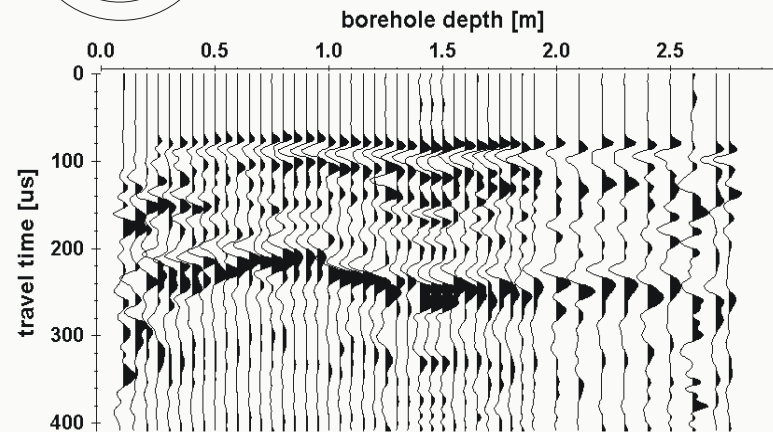
(Schuster (BGR), 2005)

B 9

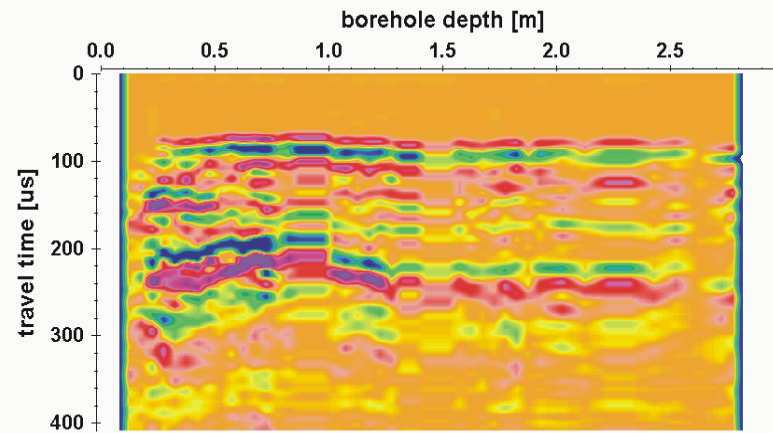


Borehole B9, 10° inclined

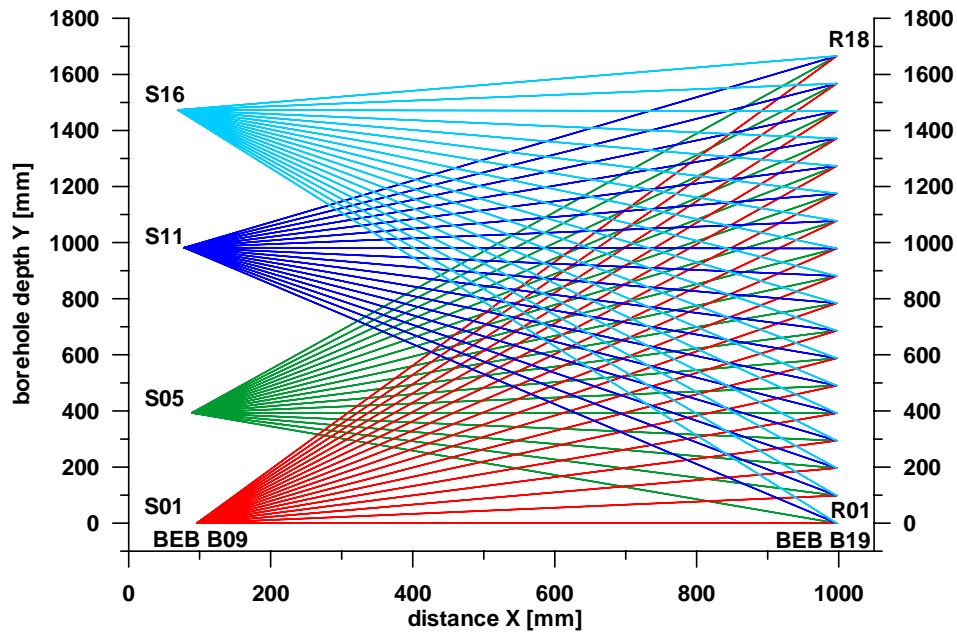
1. L:\Schuster.K\MTeri_0106\Interva\BEB09-00\PROCDATA\09_00_C2.20T / traces: 54 / samples: 6794



1. L:\Schuster.K\MTeri_0106\Interva\BEB09-00\PROCDATA\09_00_C2.20T / traces: 54 / samples: 6794

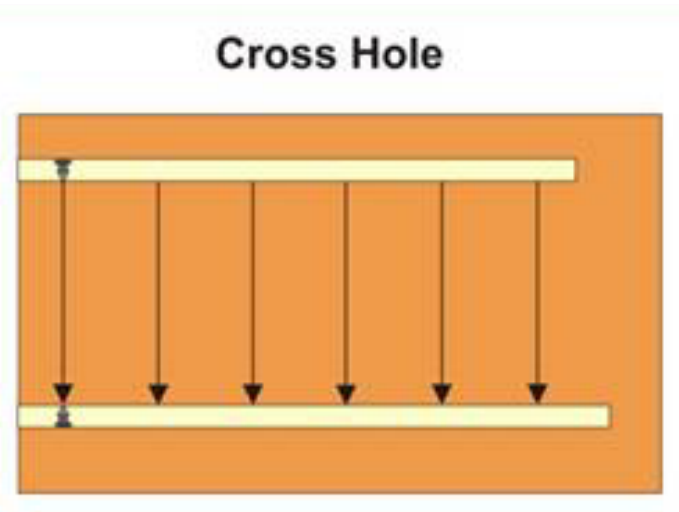
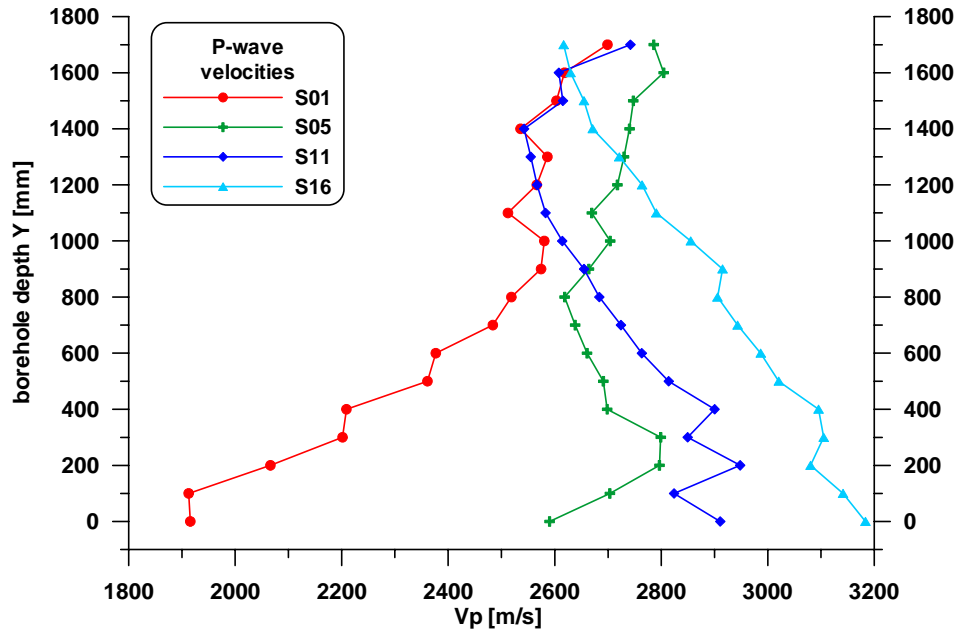


Amplitude
Negative 0 Positive



High resolution
cross hole measurements

between subhorizontal boreholes
distance: 1 m



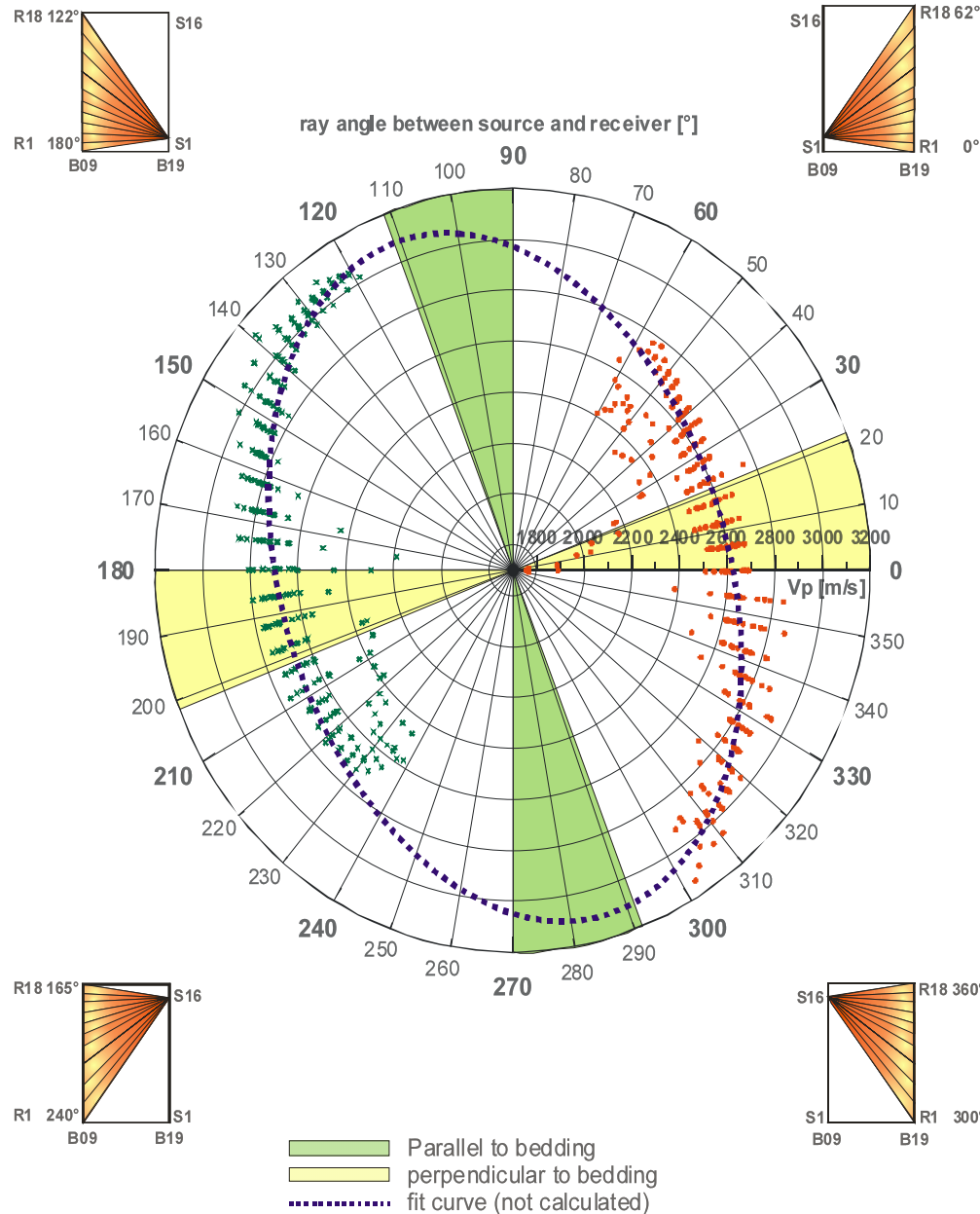
(Schuster (BGR), 2007)

Seismic Anisotropy

Result of cross hole measurements

EB-Niche

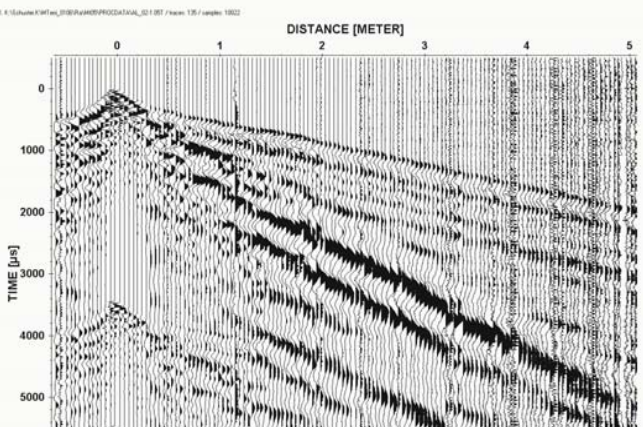
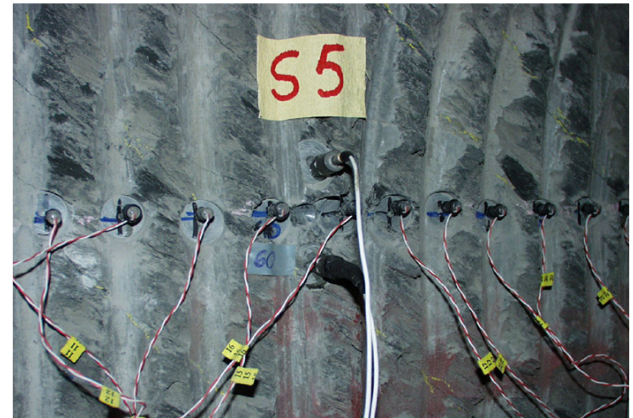
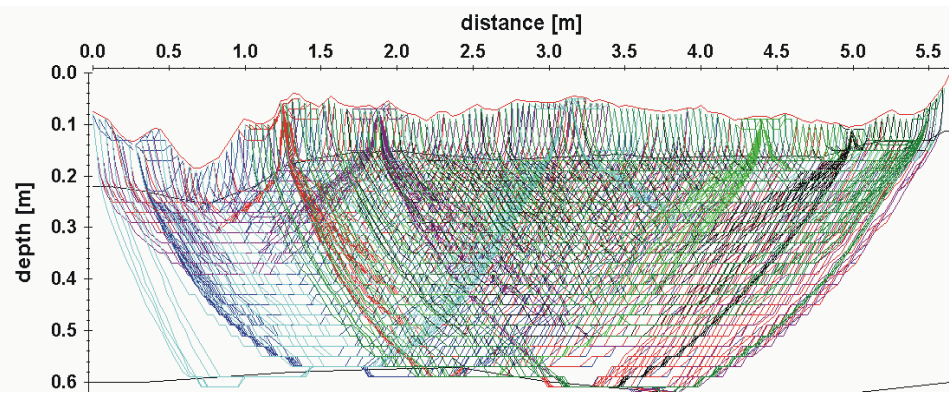
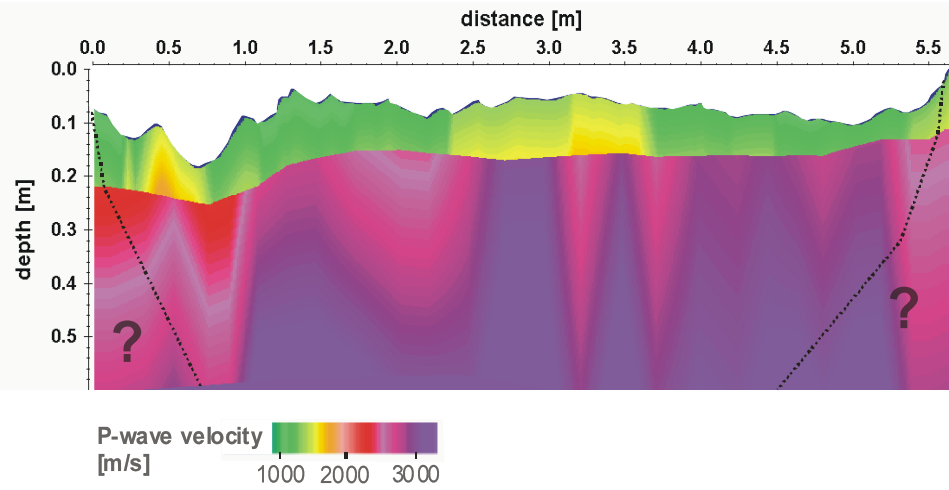
Total no. of rays: 576



(Schuster (BGR), 2007)

Seismic refraction measurements

traveltime inversion and iterative FD forward modelling



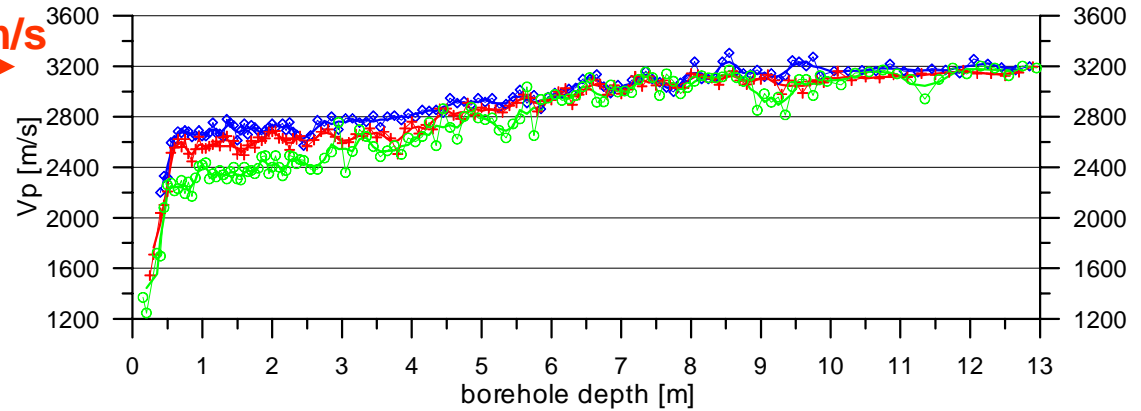
(Schuster (BGR), 2007)



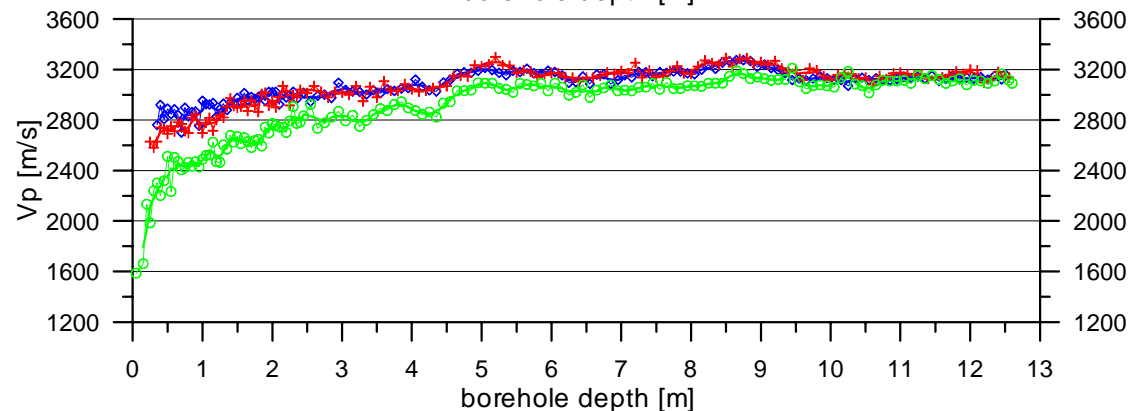
Results from shaft measurements

SUG1103
(GalPX, -490,8m level, NNW)

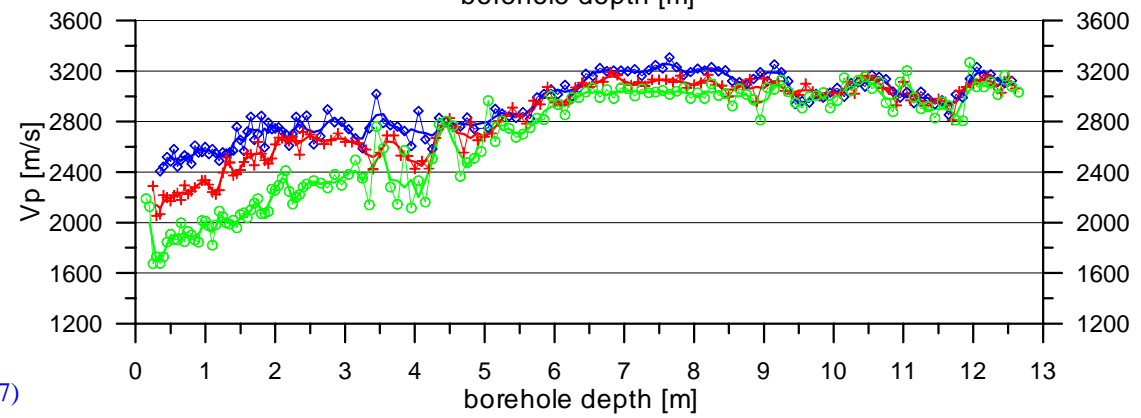
3200 m/s
→



PPA0035
(shaft PA, -480.3m level, F1, N320°E)



PPA0039
(shaft PA, -504m level, F1, N320° E)

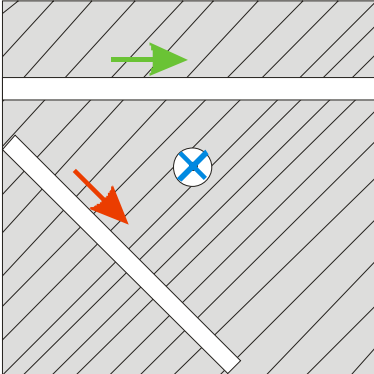
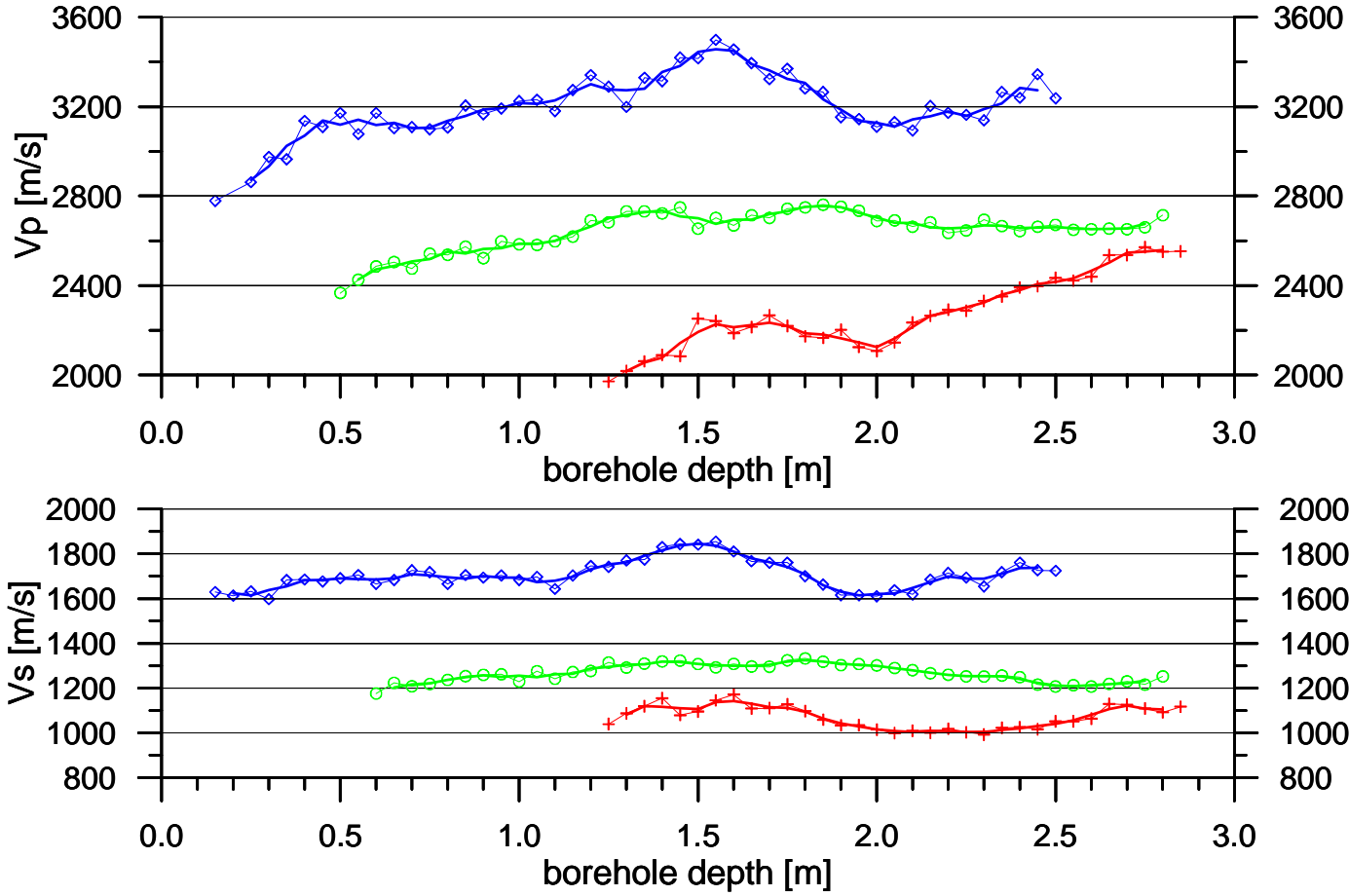


Horizontal distance „SUG – PPA“ : > 100 m
all boreholes sub-horizontal

circles: chan 1 crosses: chan 2 diamonds: chan 3
dz = 10 cm dz = 20 cm dz = 30 cm

(Schuster (BGR), 2007)

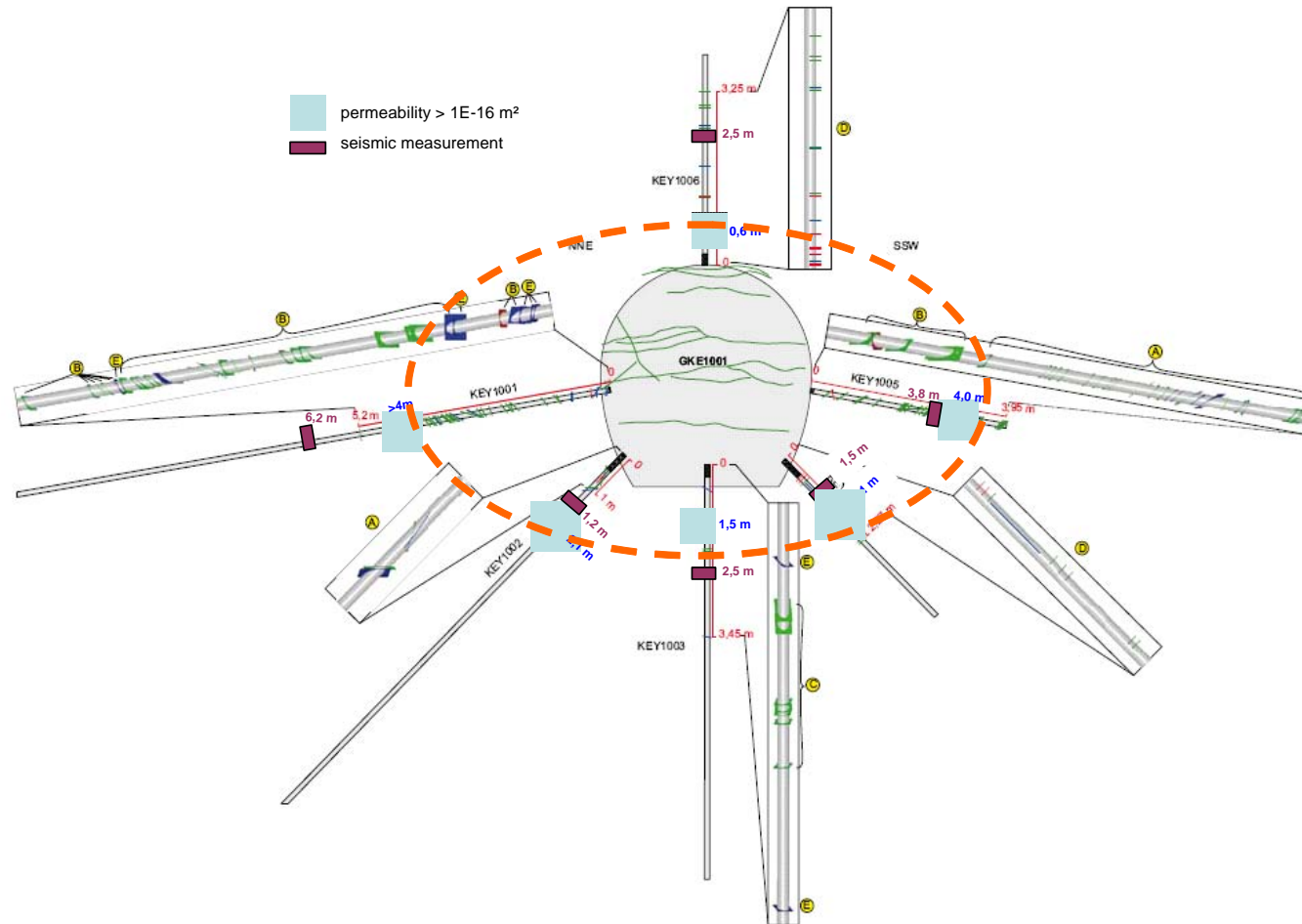
Derived parameters from seismic interval velocity measurements



Orientation to bedding:
 circles: B03 45°
 crosses: B13 perpendic.
 diamonds: B14 parallel

(Schuster (BGR), 2007)

Permeability Distribution - Comparison with Seismic Results and Geology



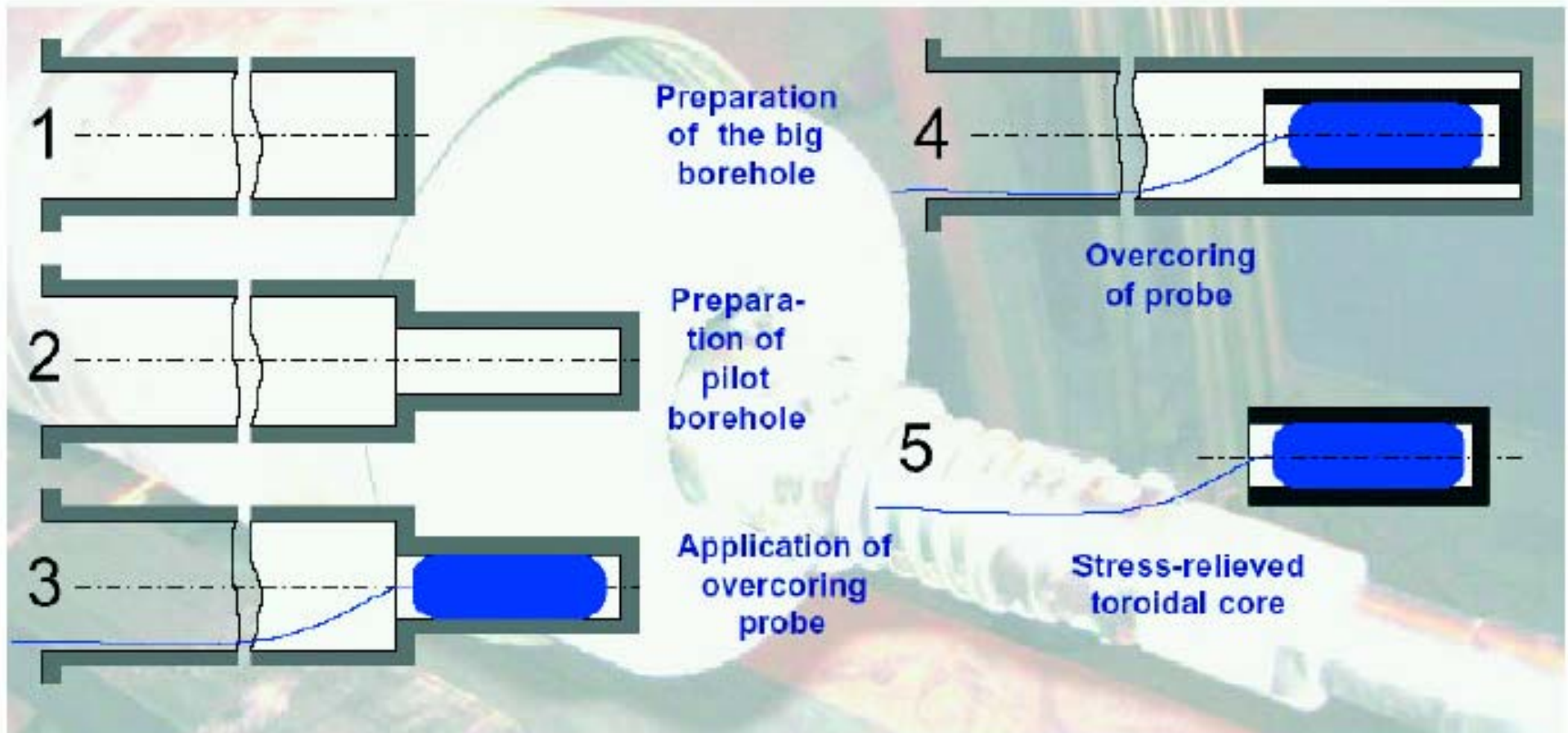
(BGR, 2005)

Initial Rock Stress Measurement



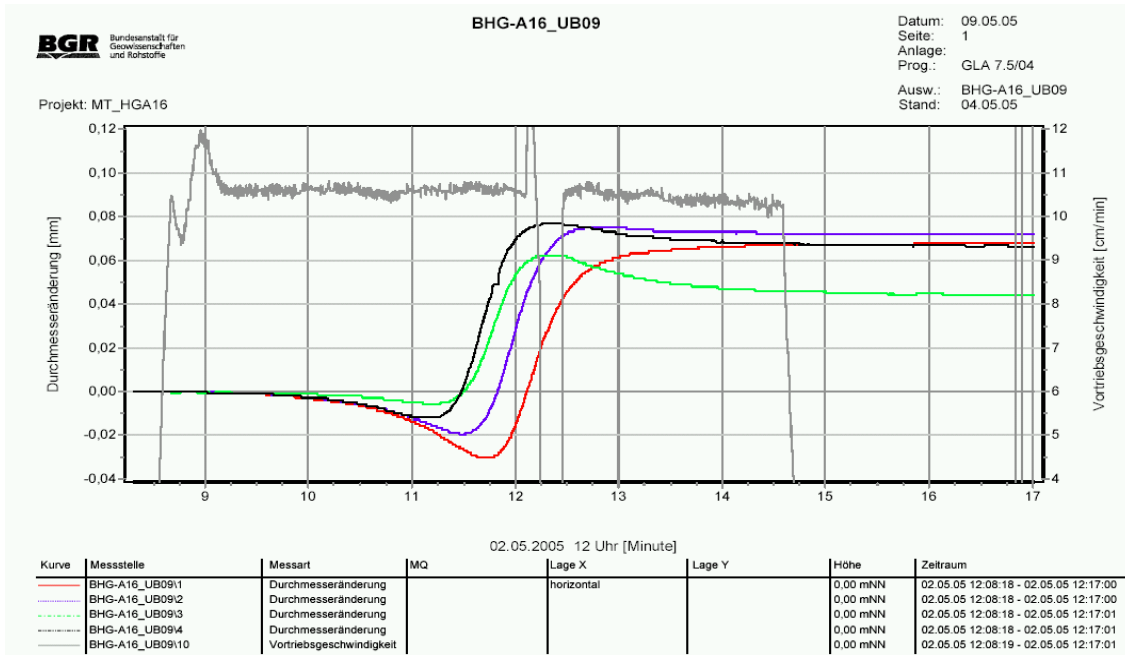
Installation of the overcoring drilling rod

BGR Overcoring Experiment



Principle of stress measurement with overcoring probe

in situ Stress Measurement (BGR Overcoring Experiment)



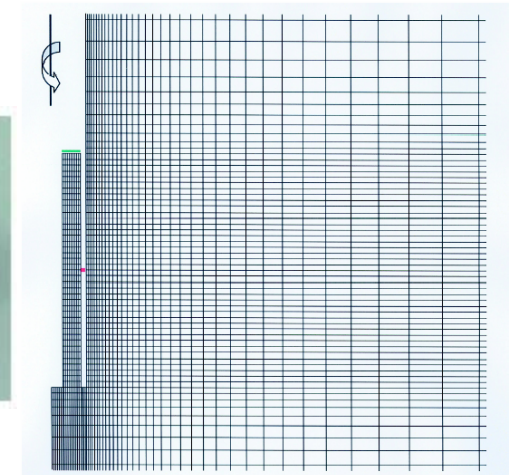
In situ test preparation

Model evaluation

Measurements



BGR 2D overcoring probe



Core-disking & Failure



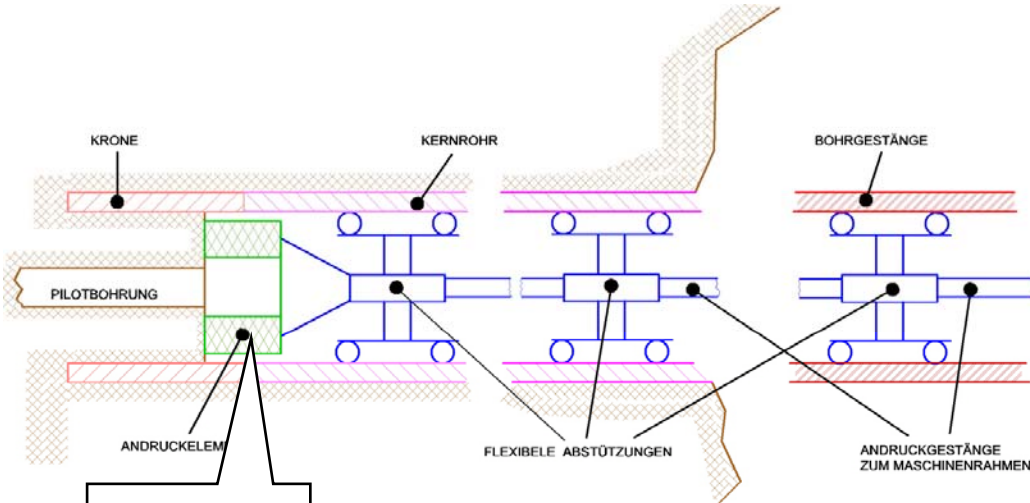
Breaking
& failure
(bedding,
operation
etc.)



Disking

- Overcoring tests in both boreholes were distinctly influenced by core-disking, failure and core losses (obviously caused by geological situation)
- Only 1 successful overcoring test (BIS-D3 – OC 03)

Techniques Improvement



Test	Interval		Remarks	Results
	from	to		
OC 01	5,22 m	5,72 m	core failure	not successful
OC 02	7,23 m	8,22 m	-/-	successful
OC 03	8,24 m	9,22 m	-/-	successful
OC 04	9,24 m	10,22 m	-/-	evaluation not possible
OC 05	10,34 m	11,22 m	-/-	limited evaluation possible
OC 06	11,54 m	12,42 m	-/-	successful
OC 07	12,42 m	13,40 m	-/-	successful
OC 08	13,74 m	14,45 m	-/-	successful
OC 09	14,47 m	15,07 m	-/-	successful

(Hoppe (BGR), 2005)

Comparison of Elasticity and in situ Stress

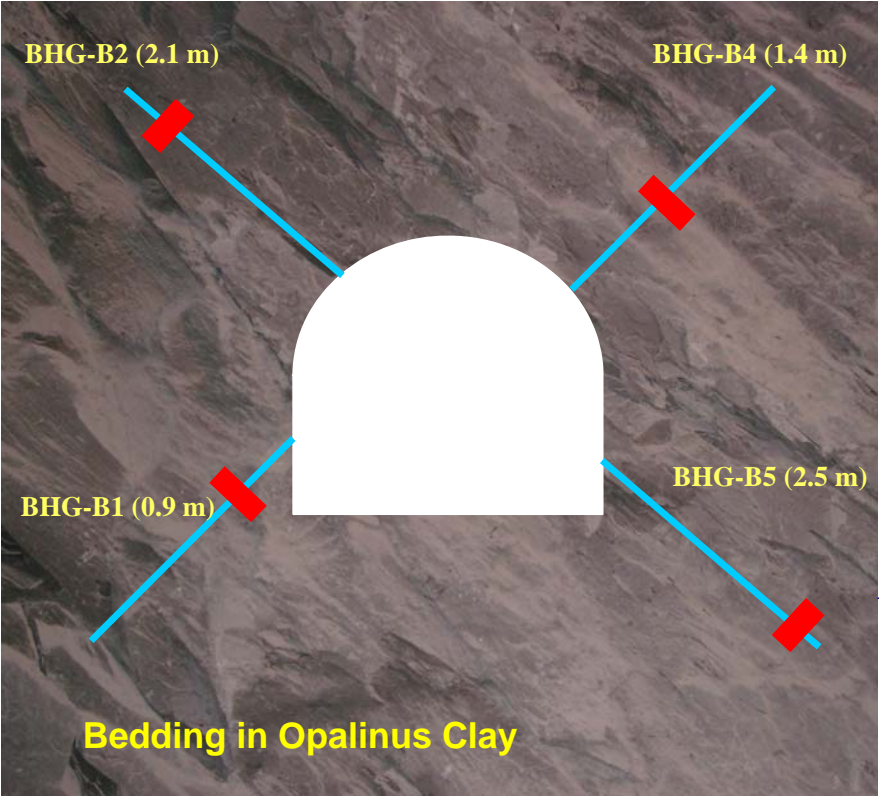
		E 1 [MPa]	E 2 [MPa]
IS-A	Undercoring	12.300	4.100
IS-B	Borehole-slotter	6.400 - 7.000	2.200 - 3.600
IS-C	Hydraulic fracturing	-/-	-/-
IS-D	Overcoring	4.600 - 10.800	1.000 - 2.200

		σ 1 [MPa]	σ 2 [MPa]	ω [°]
IS-A	Undercoring	6,5 - 8,0	0,6 - 1,1	90
IS-B	Borehole-slotter	2,0 - 5,7	0,1 - 0,4	45
IS-C	Hydraulic fracturing	7	3	90
IS-D	Overcoring	5,5 (2,5 ... 8,4)	2,6 (1,5 ... 4,4)	56 (44 ... 86)

(Heusermann (BGR))

Measurement and Observation (Mt Terri Site)

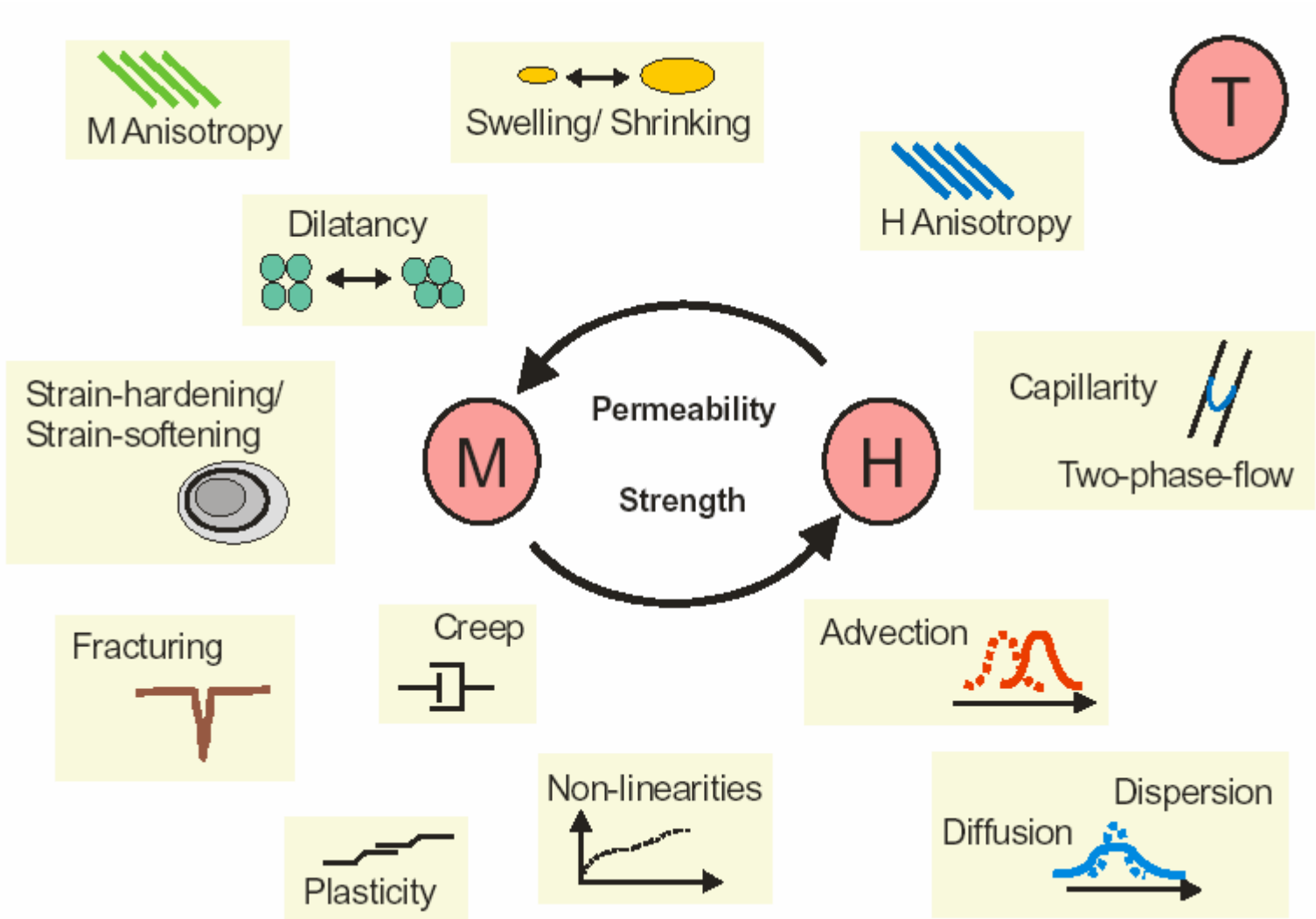
Low strength



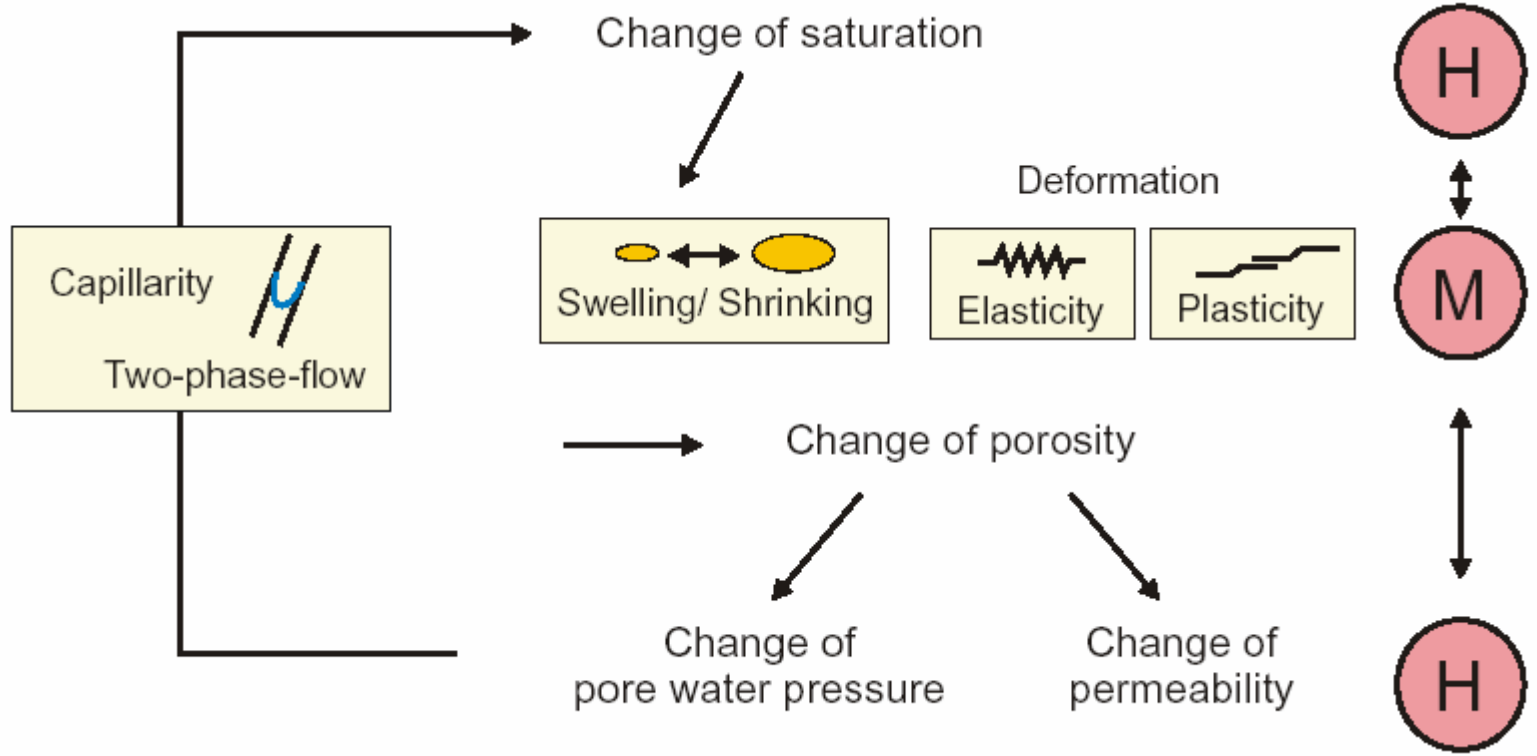
High permeability - ellipse -

Permeability > 1E-16 m²

Processes to be considered



Coupled Hydro-Mechanical Processes



Linear Swelling Model

$$\begin{aligned}\sigma_{\text{eff}}^s &= \mathbf{C} : \left(\varepsilon - \frac{1}{3} \varepsilon_{\text{vol},sw} \mathbf{1} \right) \\ &= \mathbf{C} : (\varepsilon - \mathbf{1} \beta_{sw} \Delta S_w)\end{aligned}$$

With:

$$\Delta S_w = S_w^* - S_w^0$$

Biot coefficient:

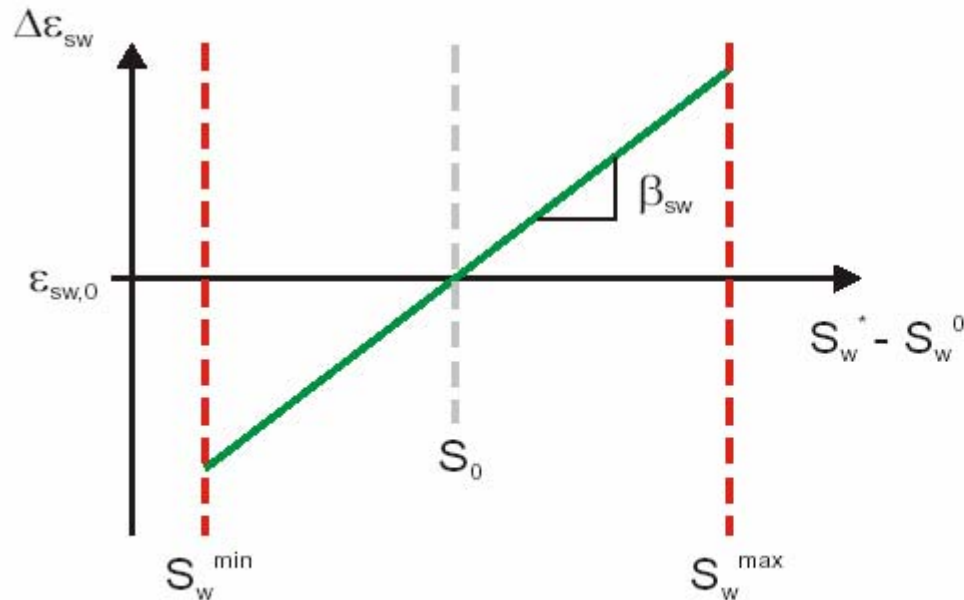
$$\alpha = 1.0$$

Volumetric swelling coefficient:

$$\beta_{sw}$$

Input parameters:

- Swelling coefficient β_{sw}
- Reference data $S_0, \varepsilon_{sw,0}$
- Swelling area S_{max}, S_{min}



Change of porosity

A change of porosity can result from swelling/shrinking or stress induced deformation.

- Deformation without swelling/shrinking

Volumetric strains influence the porosity:

$$n = n_0 + \epsilon_{vol}$$

- Deformation with swelling/shrinking

Volumetric strains influence the clay particles:

$$n = n_0 + \epsilon_{vol} - \epsilon_{vol,sw}$$

Model Mont Terri Near-field

- **Anisotropic Darcy flow**
- **Transverse isotropic elasticity**
- Richard's approximation (two-phase flow p_g)
- Linear **swelling function (saturation)**

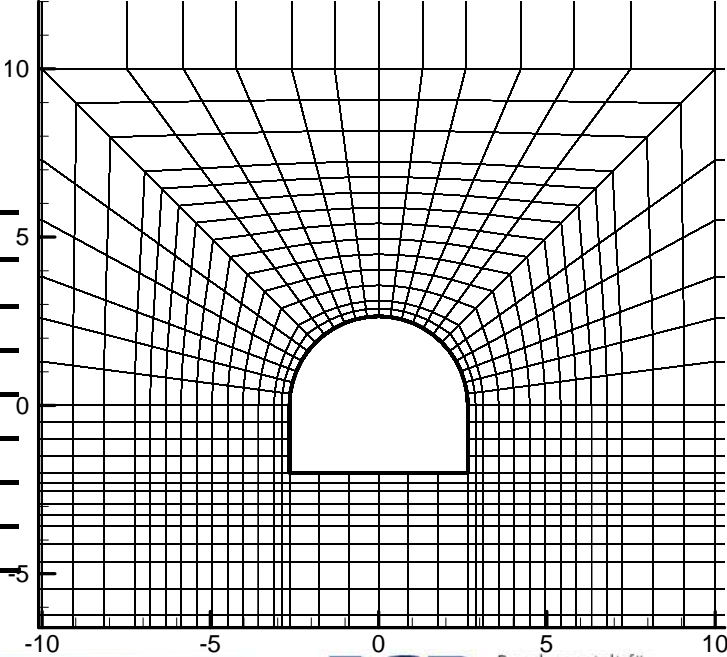
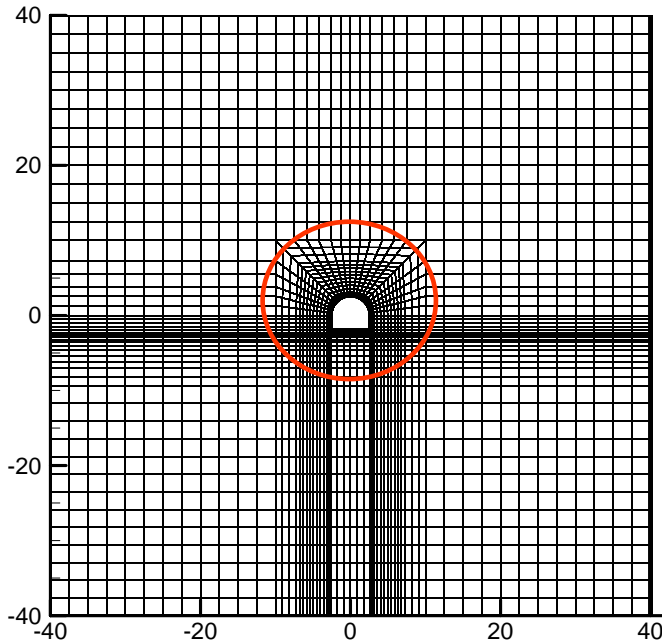
$$\varepsilon_{sw} = \beta_{sw} (S_w - S_w^0)$$

total_volumetric_strain (elastic + swelling)

- Change of porosity
- Change of permeability (Kozeny-Carman)

Basic parameter set

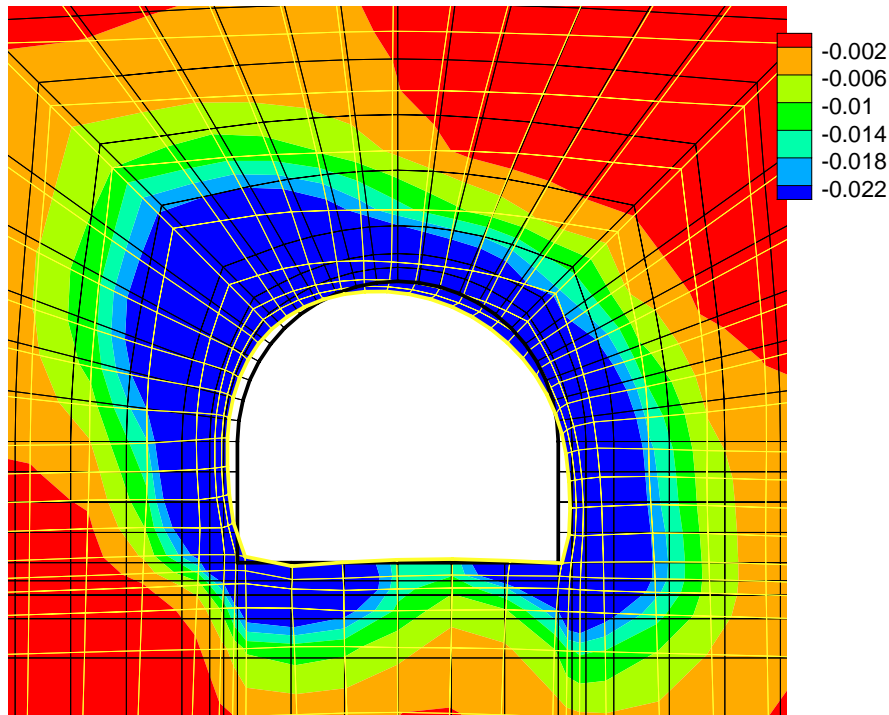
Parameter	Werte \perp	Werte \parallel	Einheit
Permeabilität	2×10^{-19}	10^{-18}	m ²
Porosität	0.16	0.16	-
E-Modulus	8	15	GPa
Poisson's Zahl	0.27	0.27	-
Quellkoeffizient	0.3	0.3	-
Feuchtigkeit im Tunnel	100 → 40	Abb. 7	%
Temperatur im Tunnel	15 → 7	Abb. 8	°C



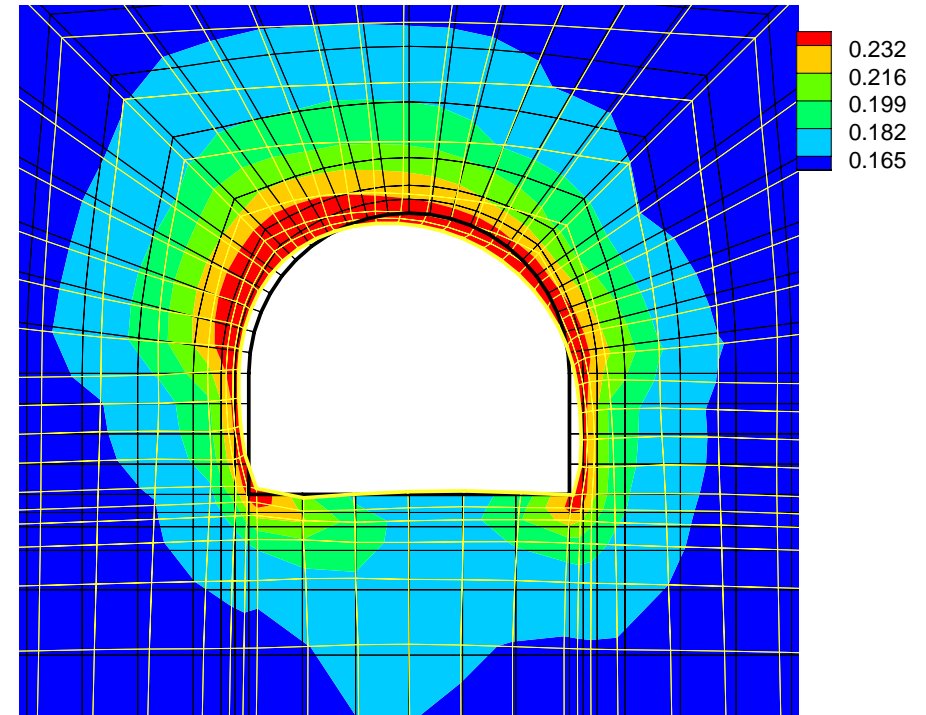
Coupled Hydro-Mechanical Modelling with Swelling Model

Swelling strain = 90% total_volumetric_strain

Strain + deformation

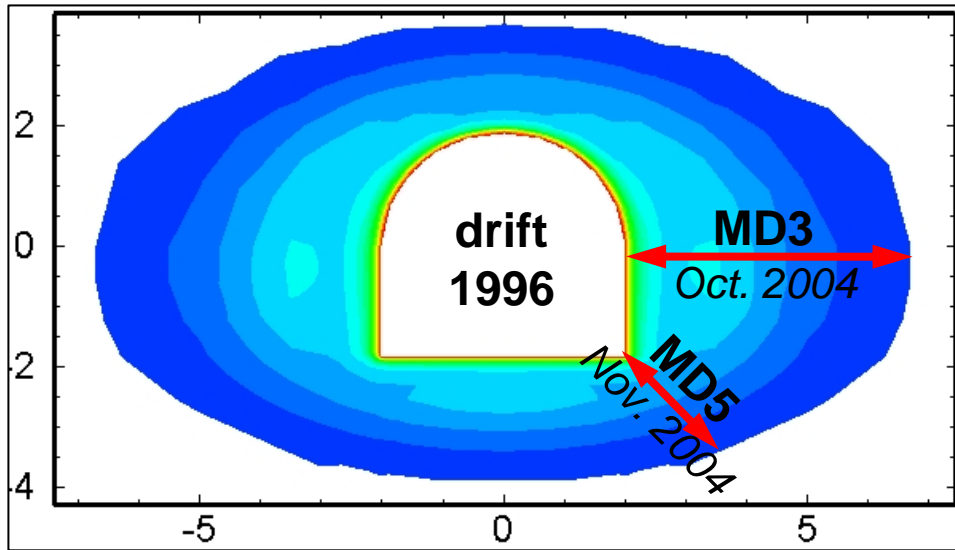


porosity



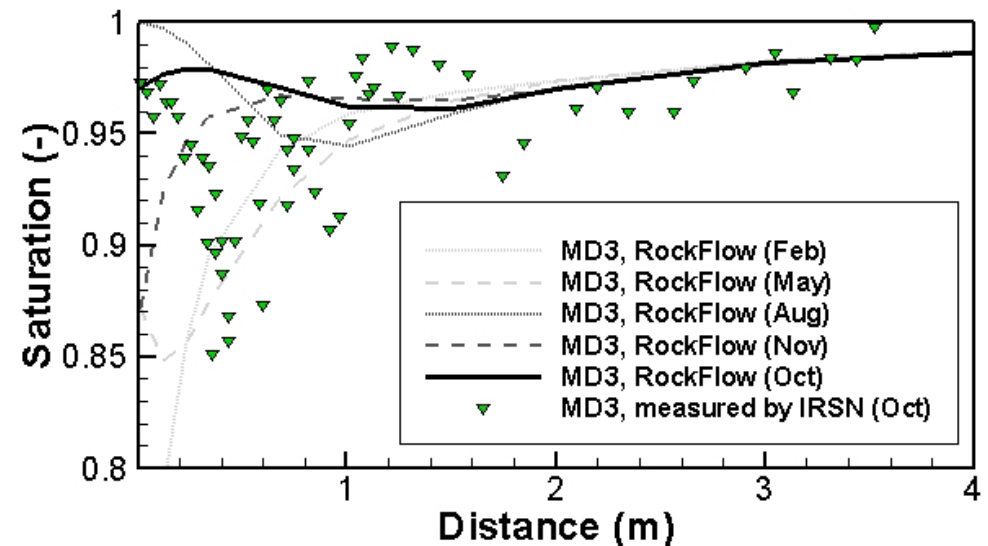
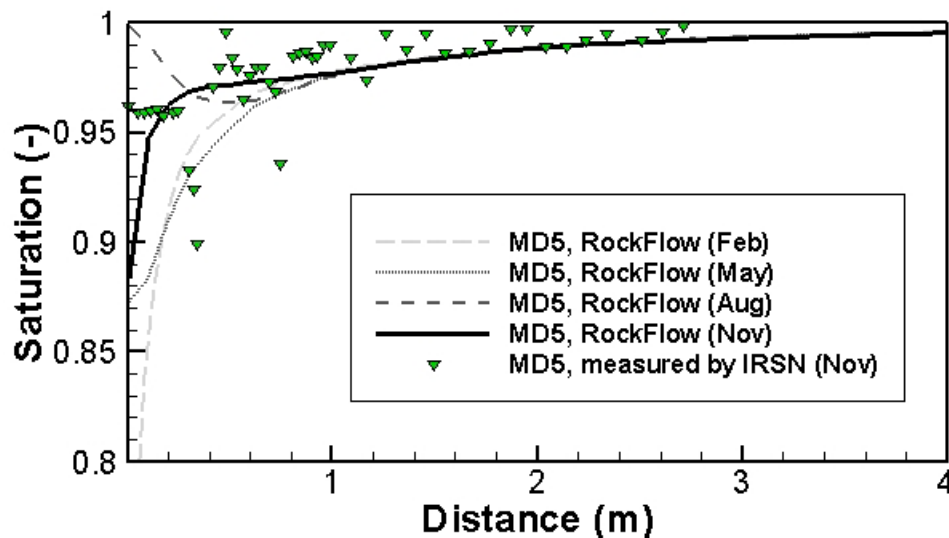
→ Current development: Strain induced anisotropic permeability

Desaturated Zone (Tournemire Site)

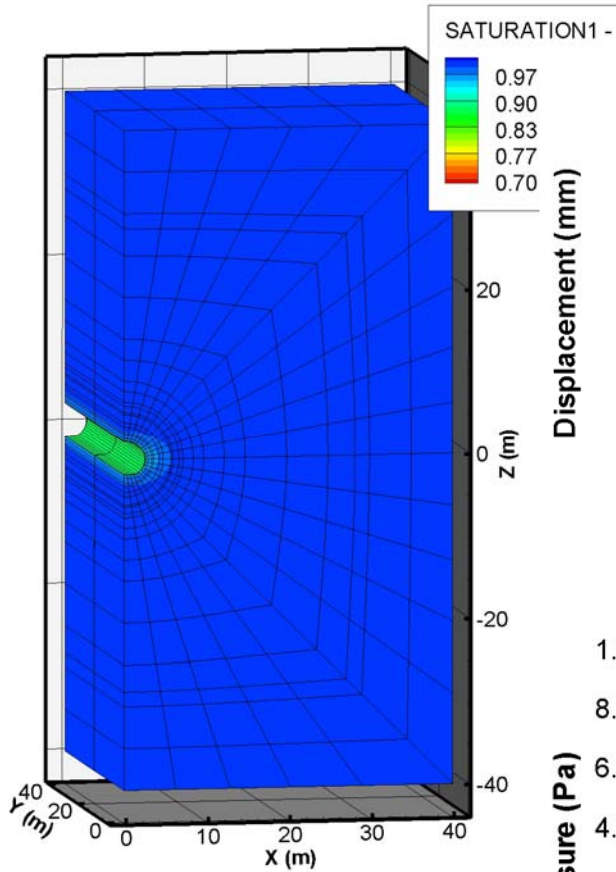


- Order of magnitude of the calculated results agrees with the measured data
- Anisotropic behavior can be simulated well

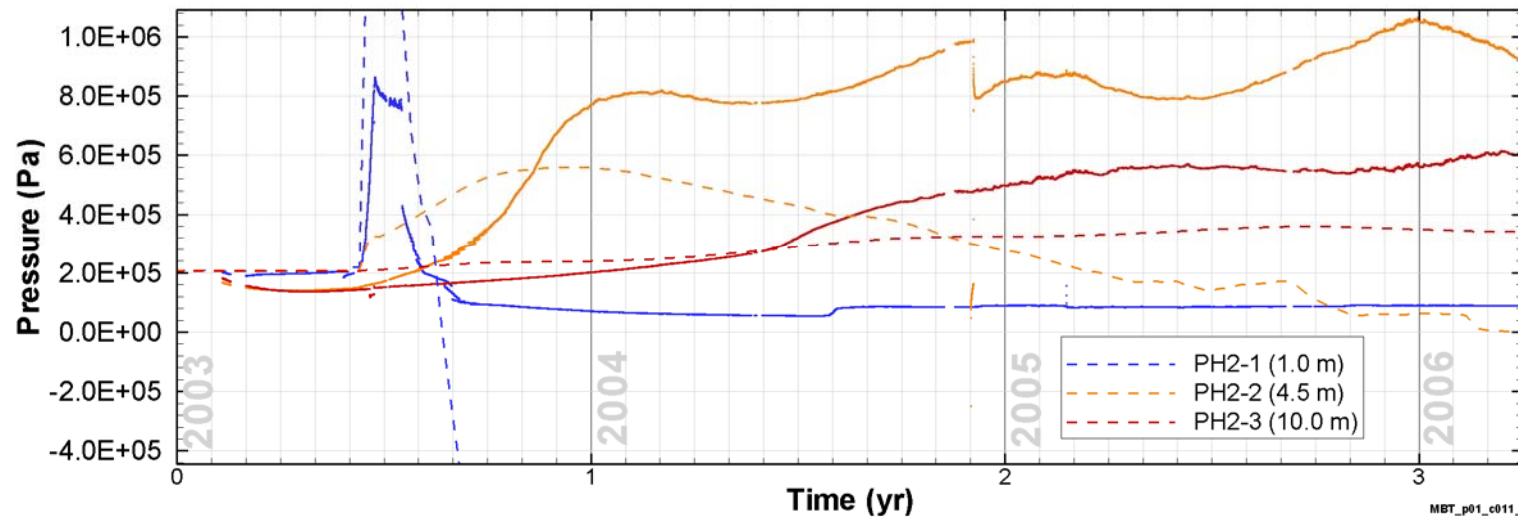
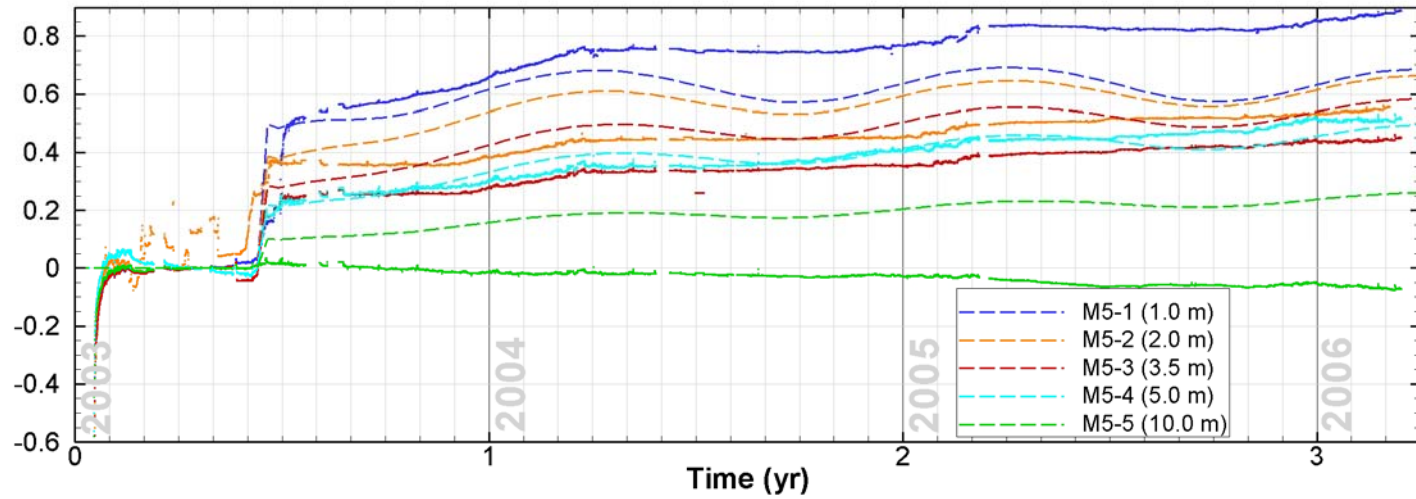
(IRSN/ISEB/BGR, 2006)



Mine-by experiment (Tournemire site)



(IRSN/ISEB/BGR, 2006)



MBT_p01_c011_91

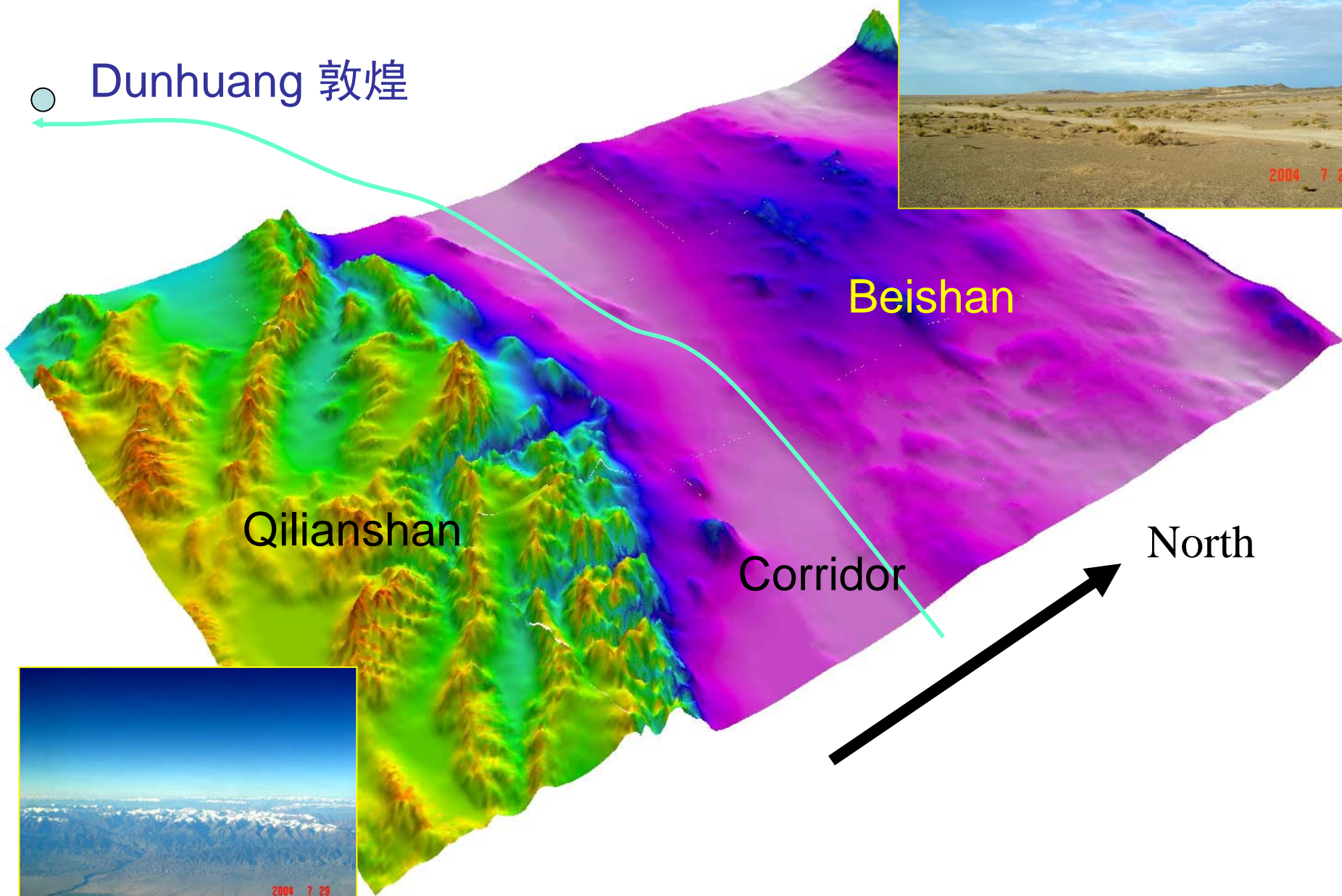
Geology of Beishan,

A Pre-selected Region for Disposal of High Level Radioactive Waste in China

CHEN Weiming (陈伟明)

Beijing Research Institute of Uranium Geology

Dunhuang 敦煌



Qilianshan

Beishan

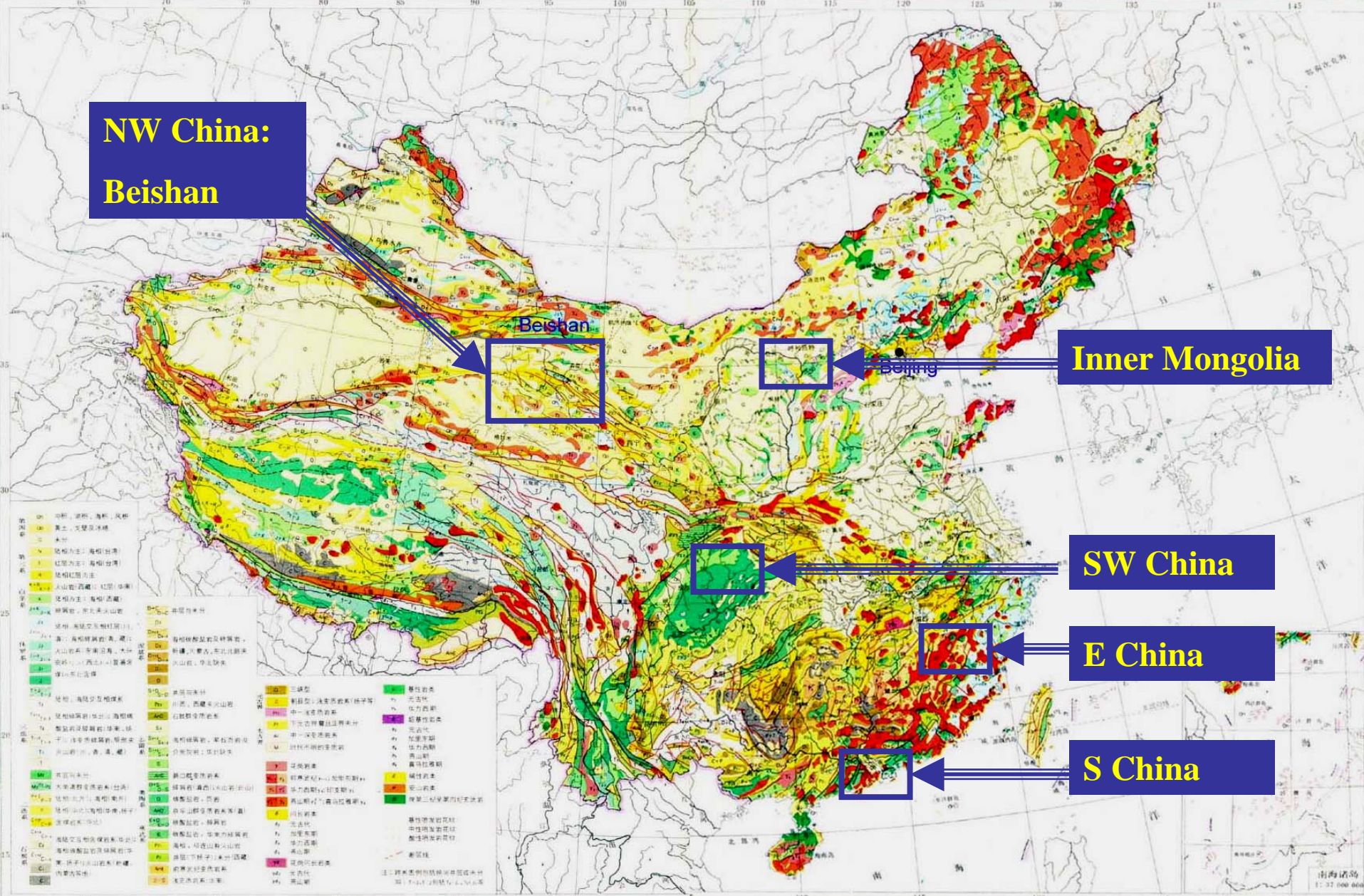
Corridor

North



3-D DEM of Beishan and Qilianshan

- Overview of Beishan (North Mt.)
- Major Activities 2000-2004
- Major Activities 2005-2006
- Summary and Coming Activities



5 Pre-selected regions for China's HLW repository 1986-1989
Efforts concentrated in Beishan area since 1990

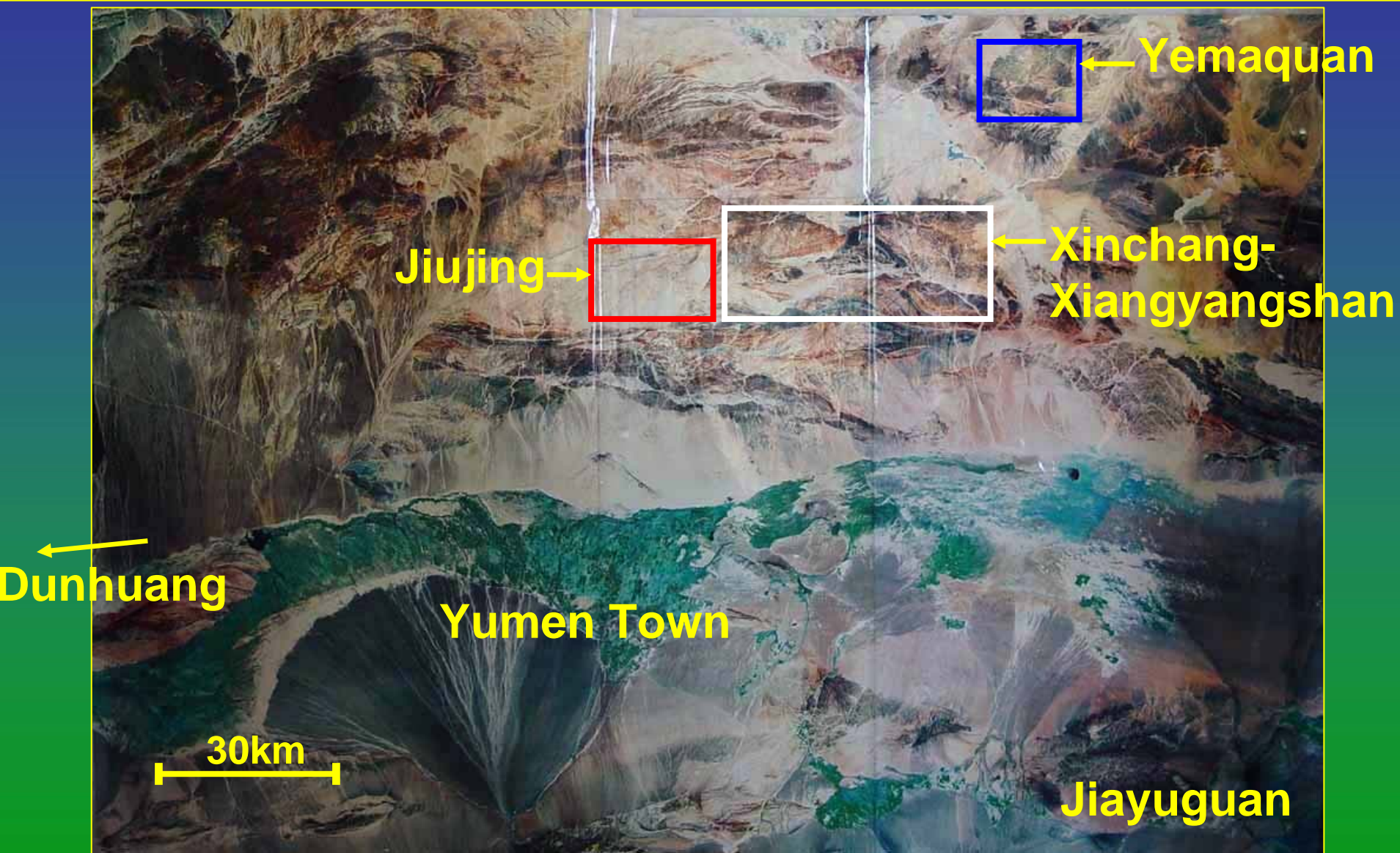


Beishan Region (1990-1999)

- in Gansu (甘肃) province, NW China
- the most potential area for China's repository
- gobi desert area
- low population density
- low precipitation : 60--80 mm/a
- high evaporation: 2900-3200 mm/a
- no economical prospect
- no important mineral resources
- convenient transportation
- stable crust, no earthquakes
- favourable hydrogeological conditions
- host rock: granite and diorite

1. Jiujing Area (granodiorite) 旧井
2. Xiangyangshan Area (diorite) 向阳山
3. Yemaquan Area (diorite) 野马泉
4. Xinchang Area (granite) 新场
5. Qianhongquan Area (granite) 前红泉
6. Yinmachang-beishan Area (granite) 饮马场北山
7. Xianshuijing Area (diorite) 咸水井
8. Baiyantou-shan-Heishantou Area (granite) 白圆头山-黑山头

Beishan Region





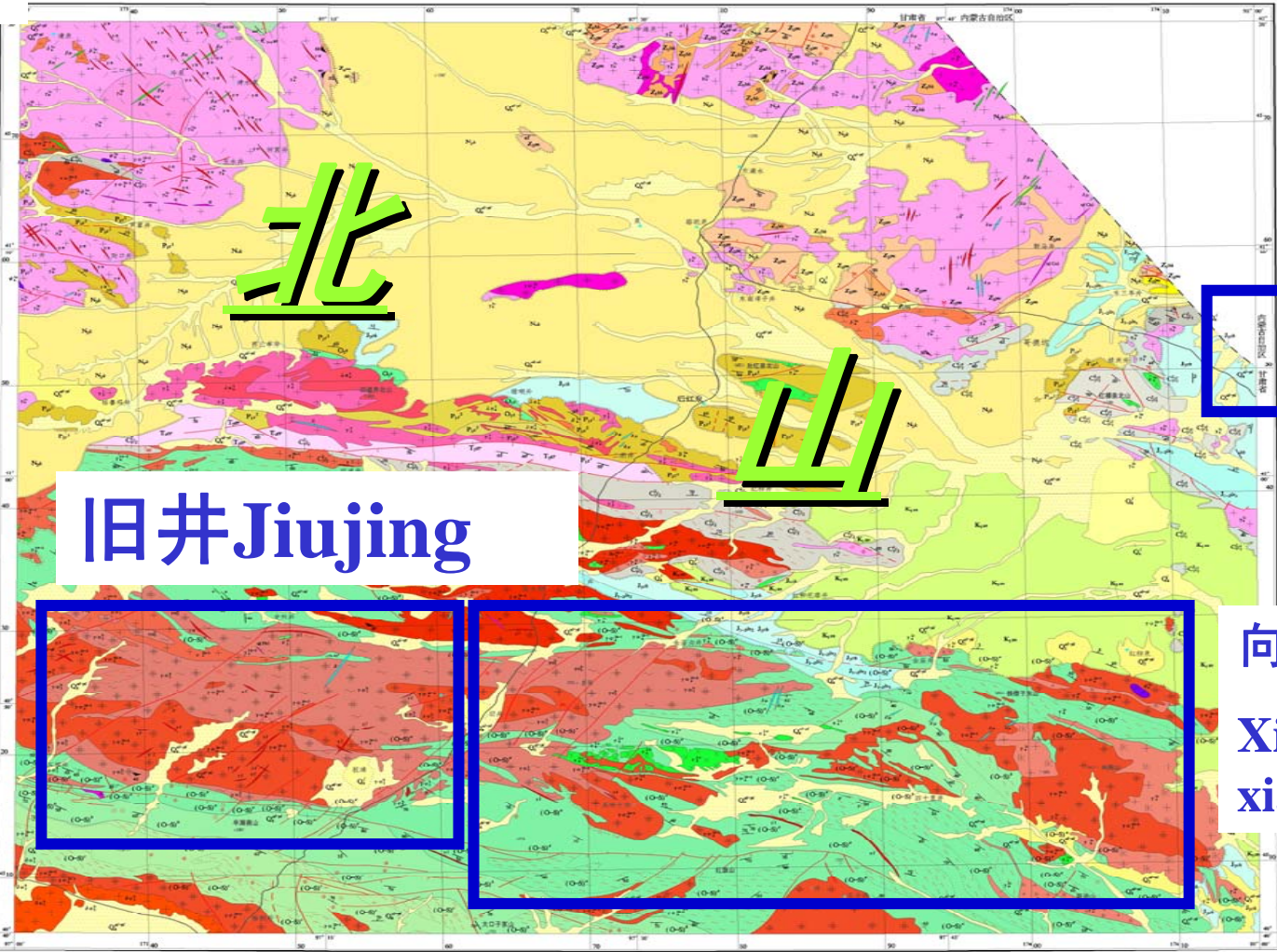
北

山

旧井 Jiujing

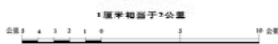
野马泉 yemaquan

**向阳山-新场
Xinchang-
xiangyangshan**



地质资料来源: 地质部甘肃省地质局第二区域地质测量队第二分队
1965-1967年测制, 1968年11月总队验收, 1969
年请地质部出版, 地质部五四二厂印刷。

1: 200000

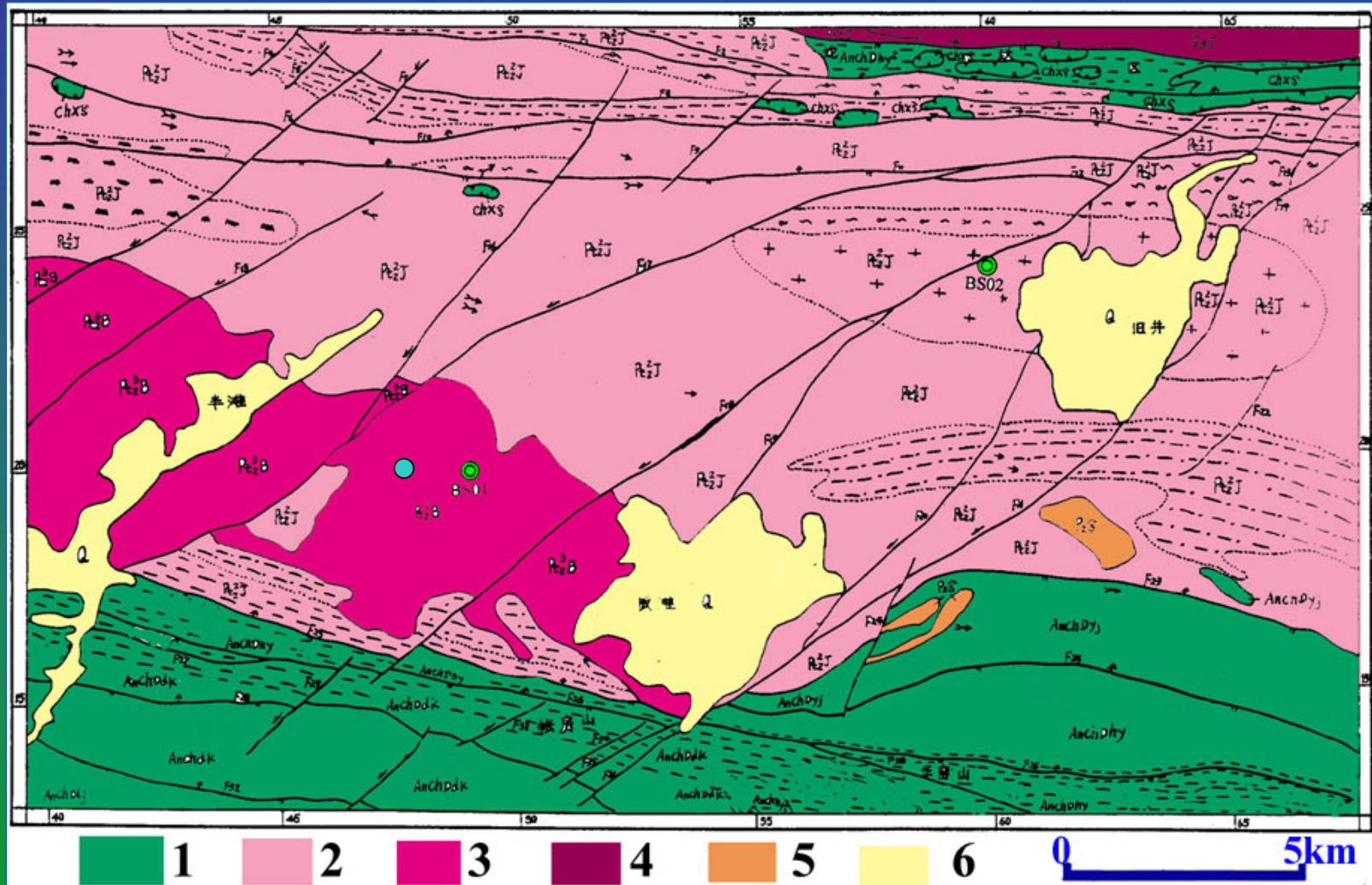


地形资料来源: 根据国家测绘总局1958年航测, 1959年成图出版的1:100000地形图。
1956年黄海高程系, 1954年北京坐标系。
等高线高程的等高距为40米。
附注: 图中甘肃省与内蒙古自治区之界线系根据国家测绘总局出版
1:50万五门镇幅草绘而成。

甘肃北山预选区3个重点预选地段对比

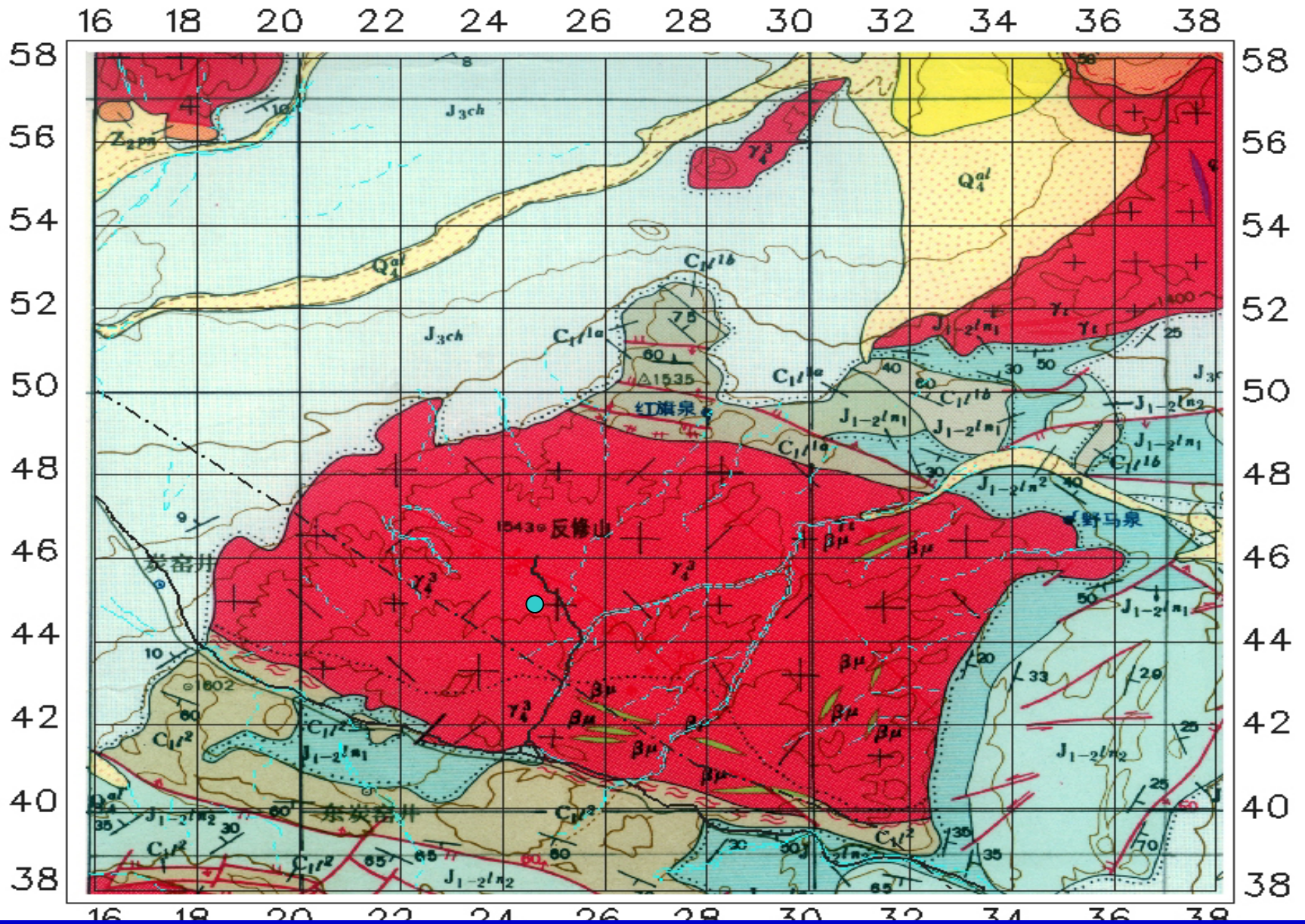
- **surface geological, hydrogeological and geophysical survey at Jiuqing Area and Yemaquan Area (1:50,000 scale)**
- **bore hole drilling for BS01, 02, 03, 04**
- **in situ tests in bore holes**
- **evaluation of deep geological environment and site suitability**

Geological Map of Jiujing Area



1-Metamorphic rock, 2~5-Variou granite unites, 6-Quarternary system

比例尺 1: 50000



Geological map of Yemaquan Area



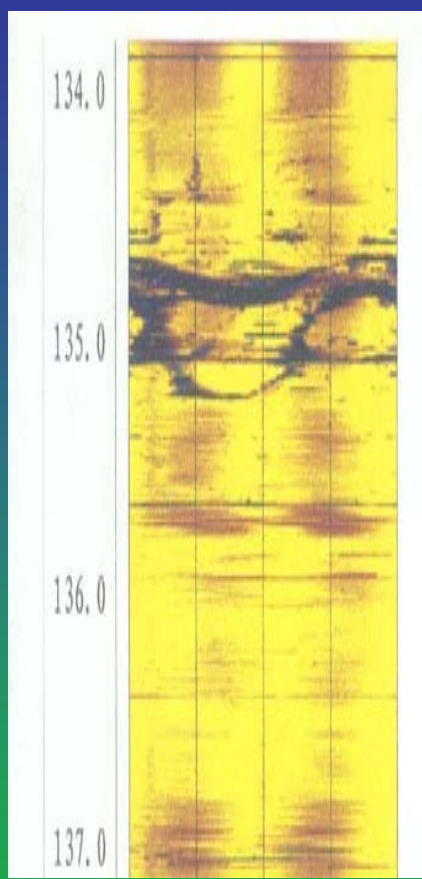
drilling sites at BS01, BS02, BS03, BS04 boreholes

- **Borehole optical camera**
- **Borehole acoustic televiewer**
- **Borehole hydrogeochemical logging**
- **Borehole radar survey**
- **Borehole geostress measurement**
- **Vertical seismic profile**



Vertical Joint

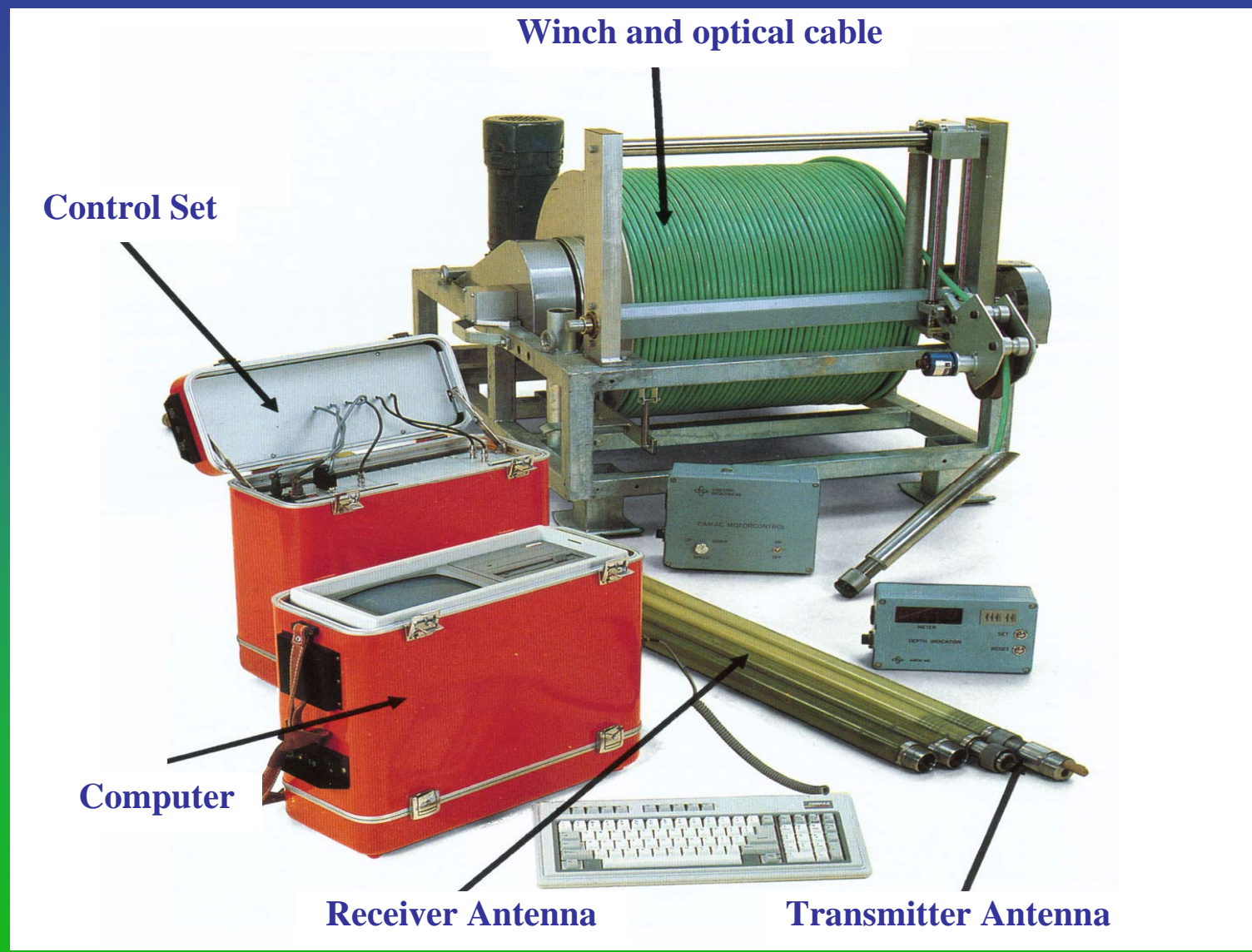




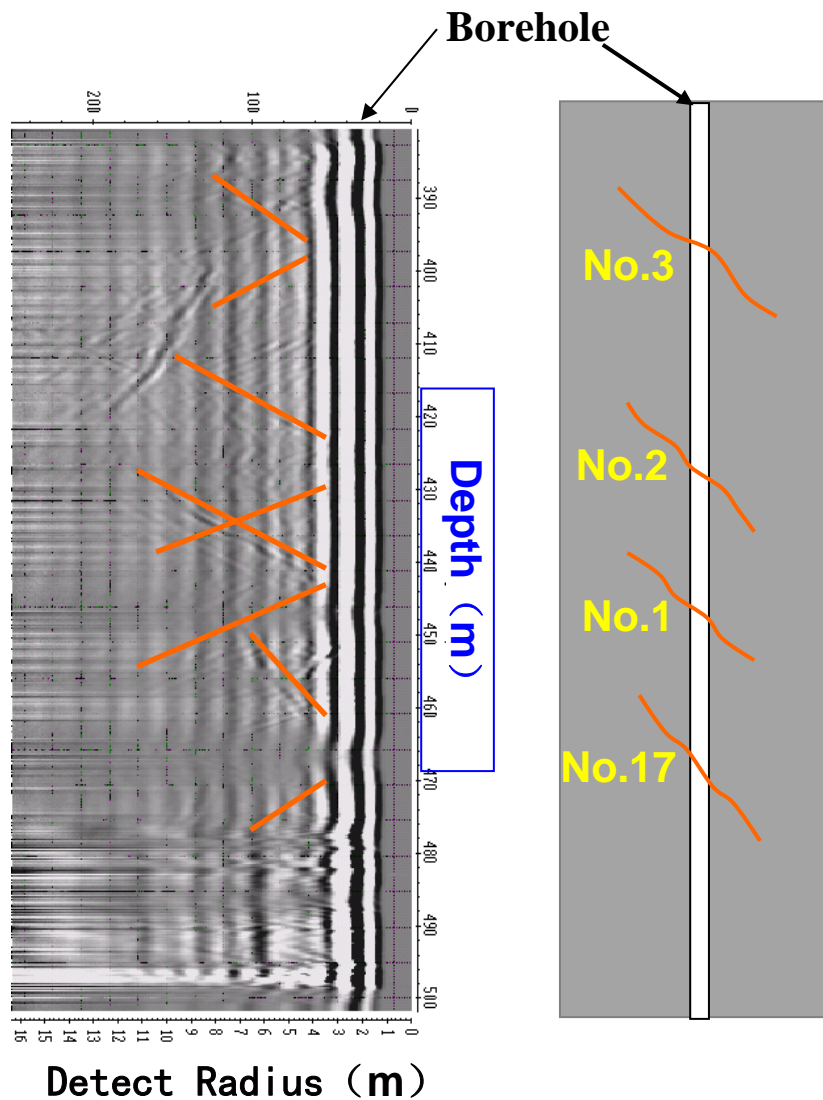
borehole televiewer survey

钻孔电视测量

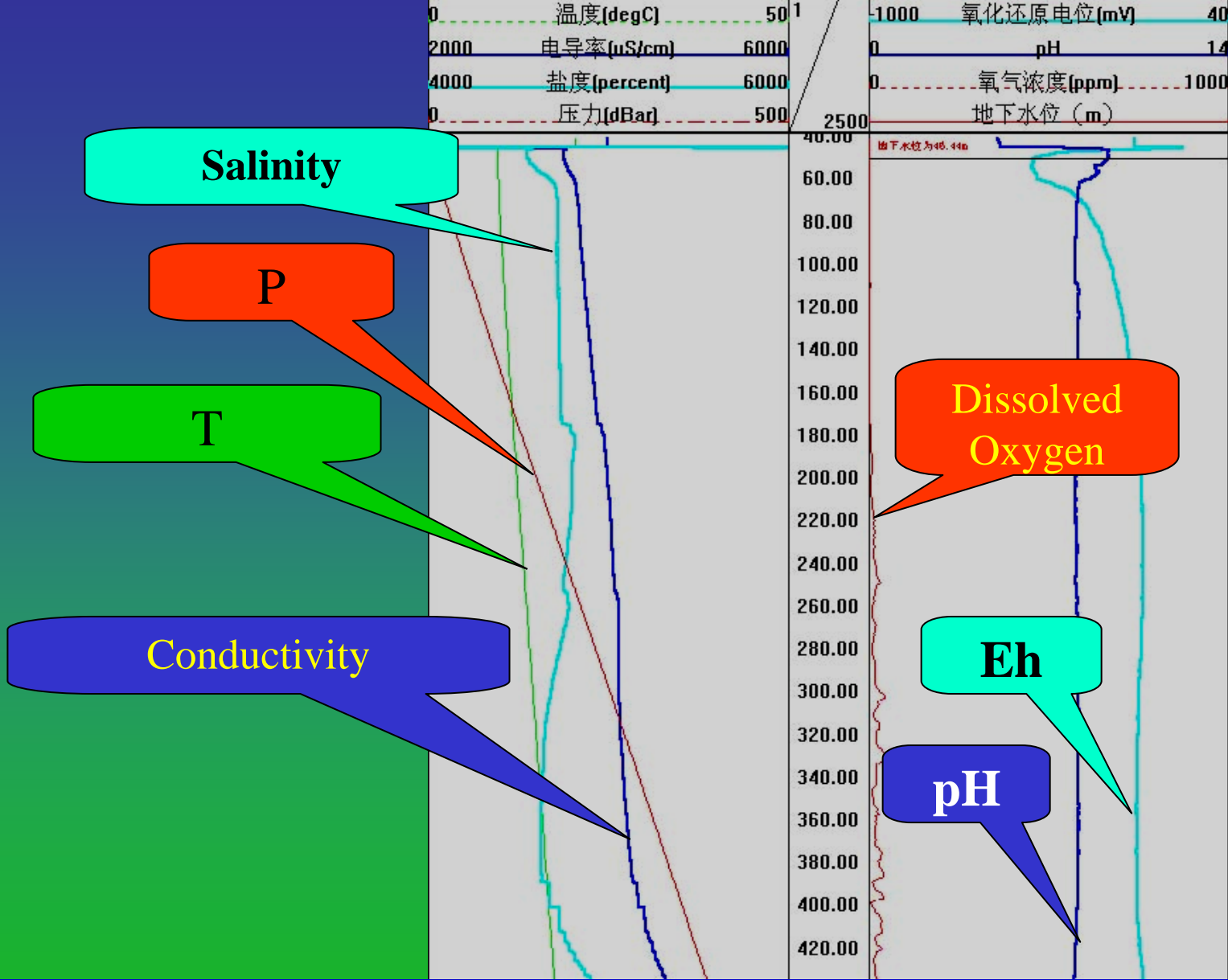
Borehole Radar



Radar Image (BS01:380~500m)



BS01孔综合水质测量曲线图



Borehole water quality logging in BS01

Double packer system



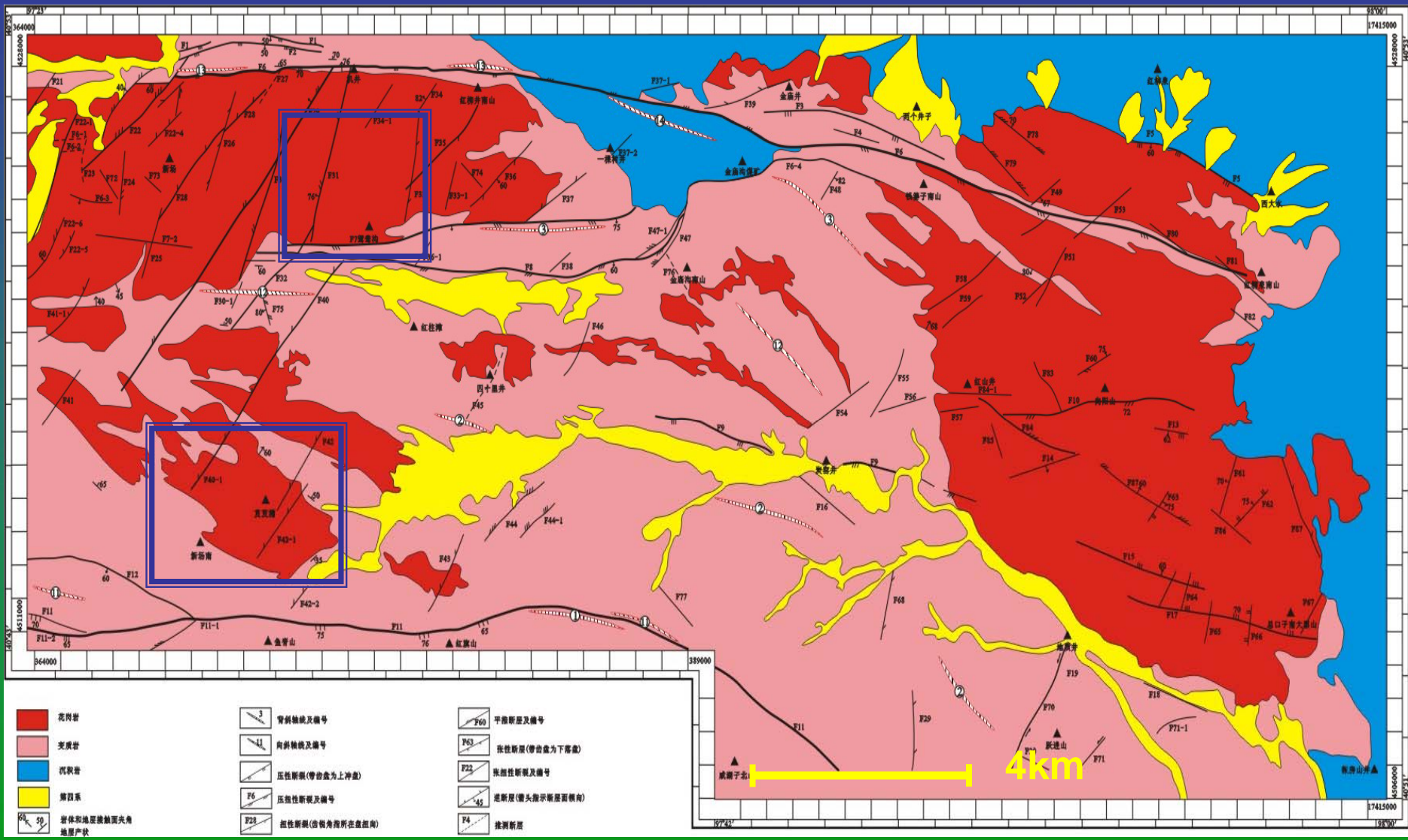
Stator of Moyno Pump



Rotor of Moyno Pump

Major Activities 2005-2006

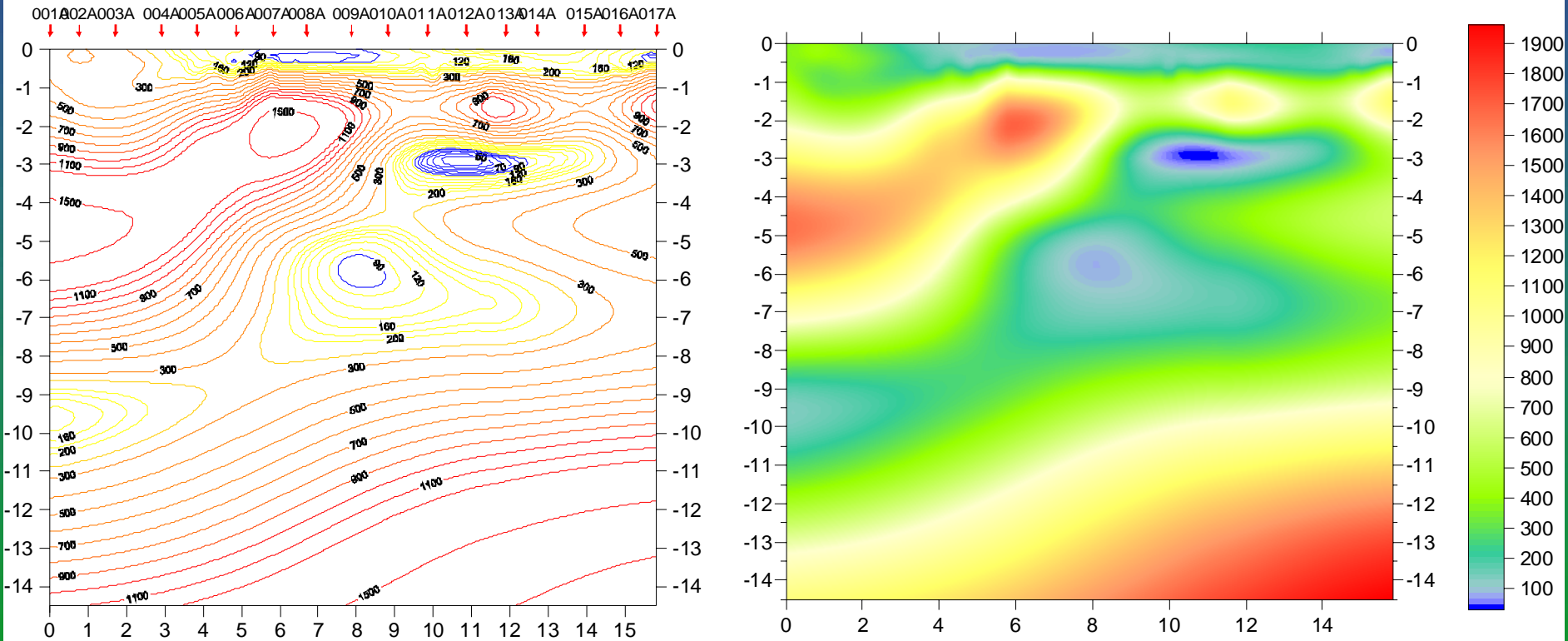
- **Surface geological, hydrogeological and geophysical survey at Xinchang-xiangyangshan Area (1:50,000 scale)**
- **Detailed surface geological survey at two potential sites (1:2000 scale)**



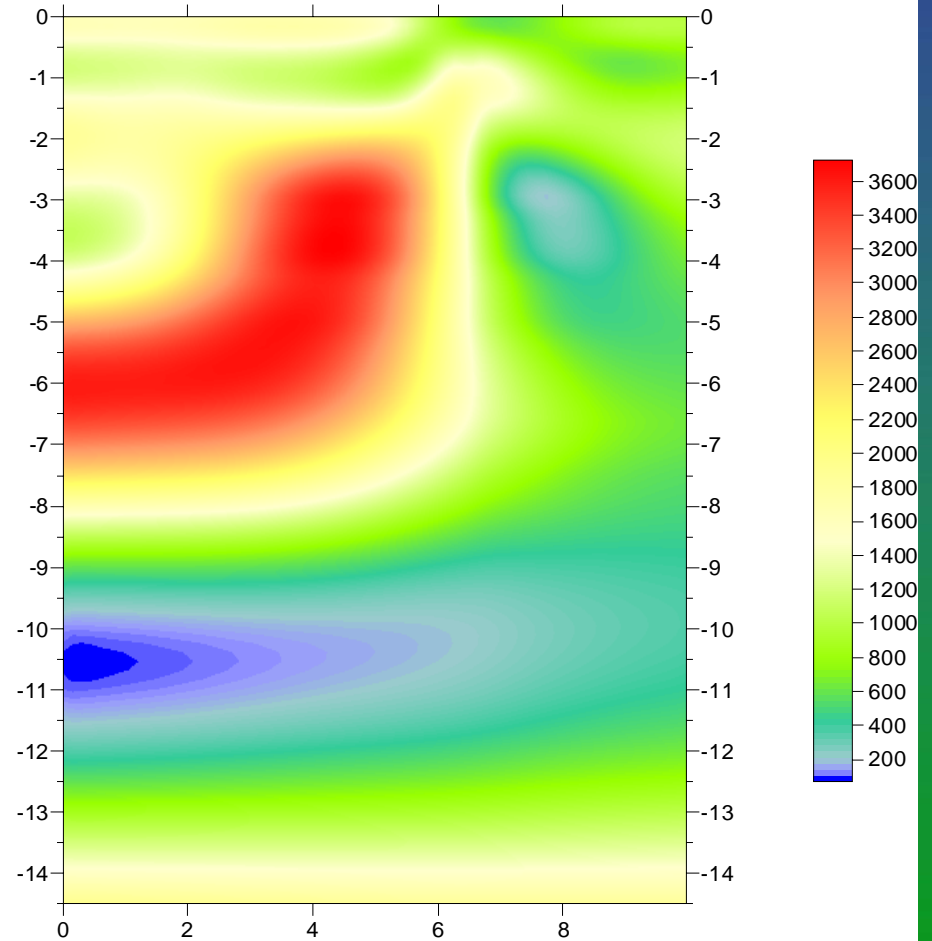
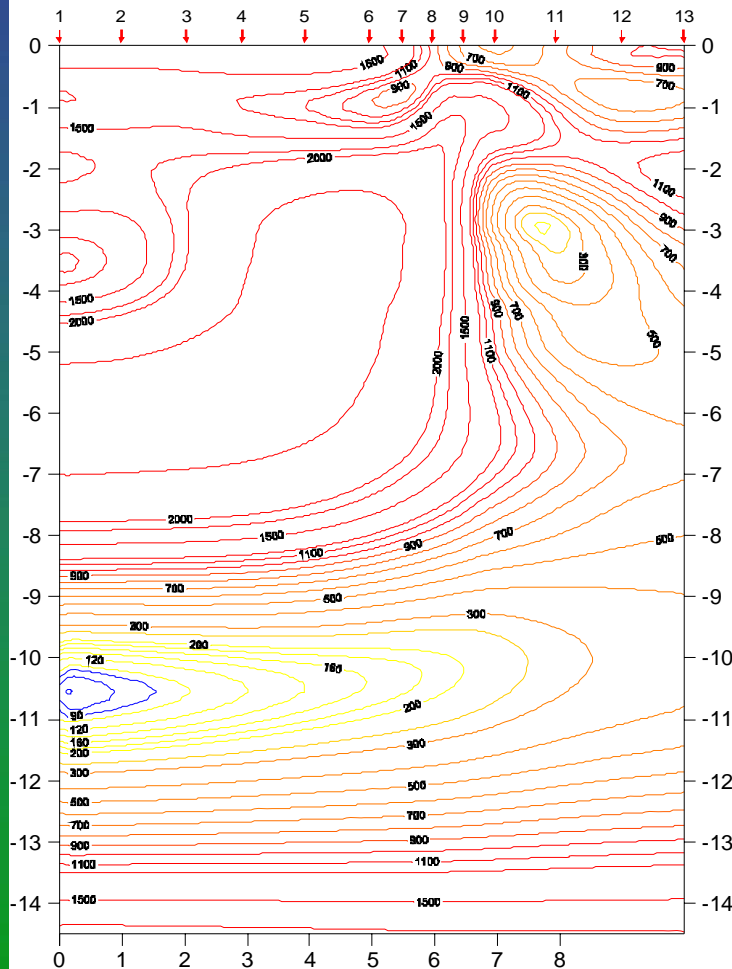
Major geophysical activities

- 1 Electromagnetic measurement : EH4**
- 2 High-resolution magnetic survey**
- 3 Magnetotelluric Survey: MT-1**

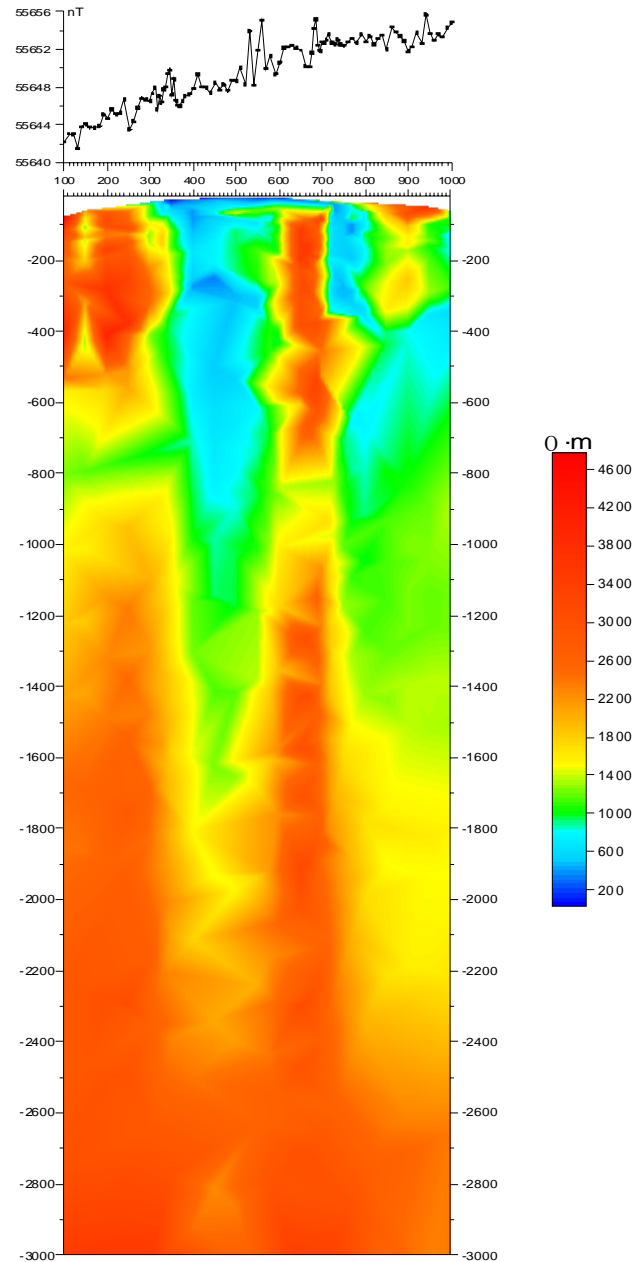
MT survey in Xiangshan Area



MT survey in Jijicao potential site



Magnetic and electromagnet section of fault



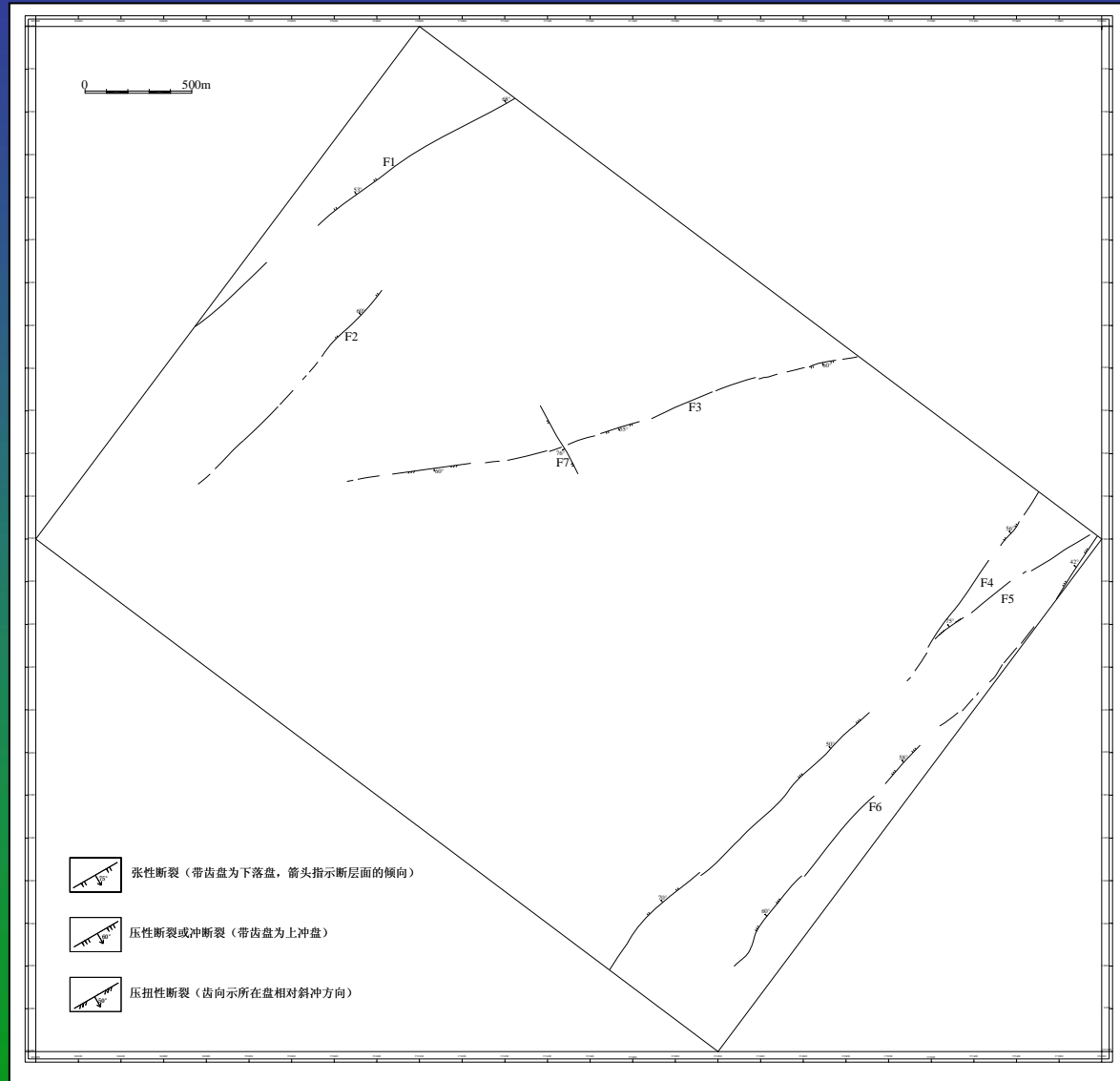
Antenna of EH4





Geological map of Jijican potential site

Fault map of Jijicao potential site



Fault



Outcrops of granite

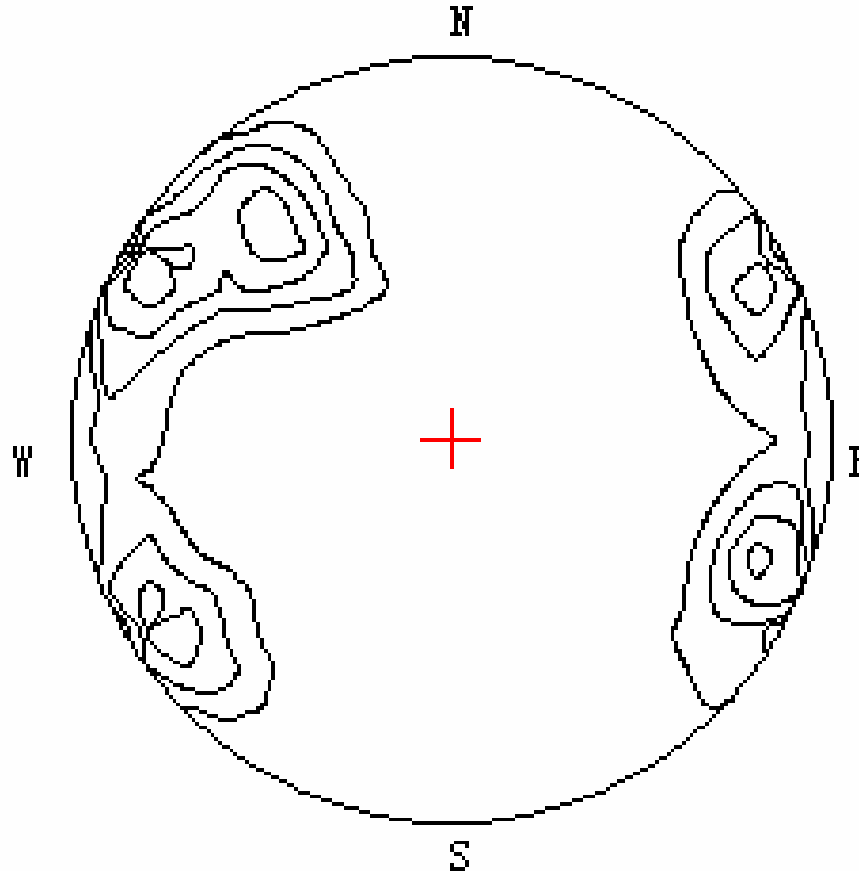


Joint pole diagram – 4 groups

THE DIAGRAM OF CONTOUR LINE

N= 8807

Date:2005-12-27



Max:3.80%

320.19/67.05

110.56/74.34

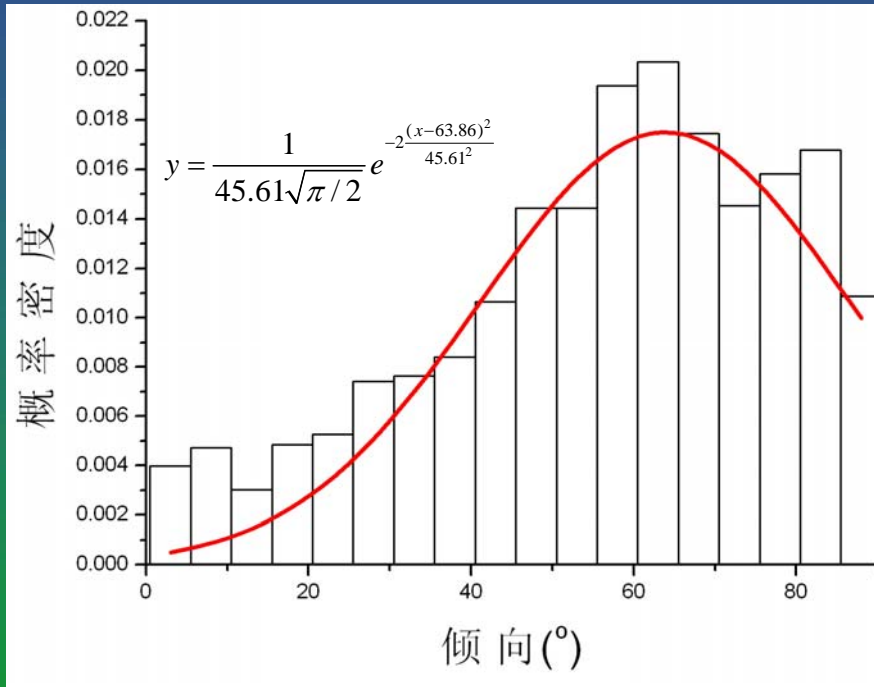
63.43/78.46

234.46/74.93

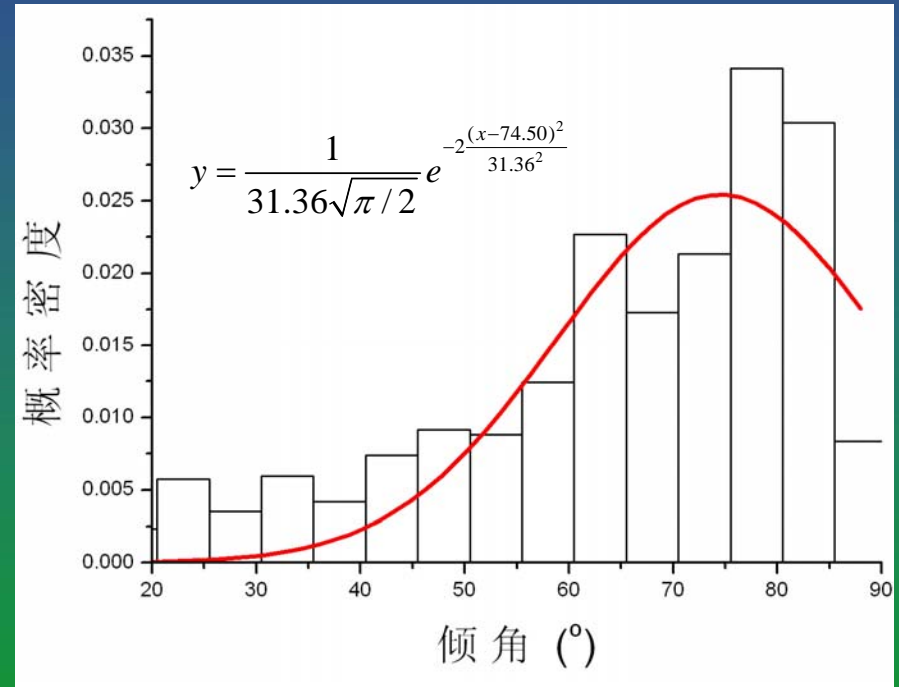
1.2% - 1.3% - 1.9% - 2.5% - 3.2% - 3.8%

Equal-area upper hemisphere projection

Probability Density



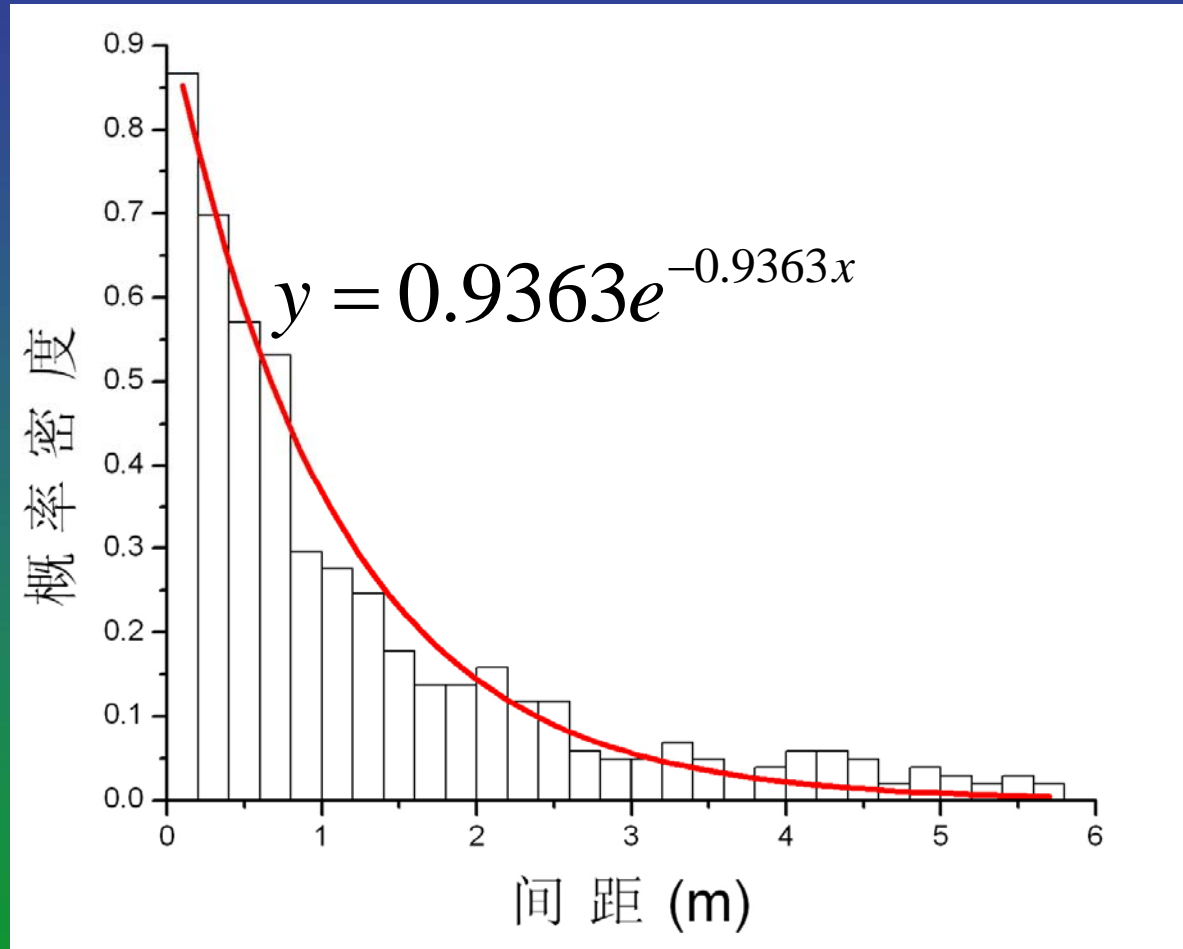
Dip direction



Dip Angle

Joint Spacing – Negative exponent

Probability
Density



Spacing

Summary

Region → Area → Potential site

1:200,000

1:50,000

1:2,000 & borehole

Beishan

3 areas

2 potential sites

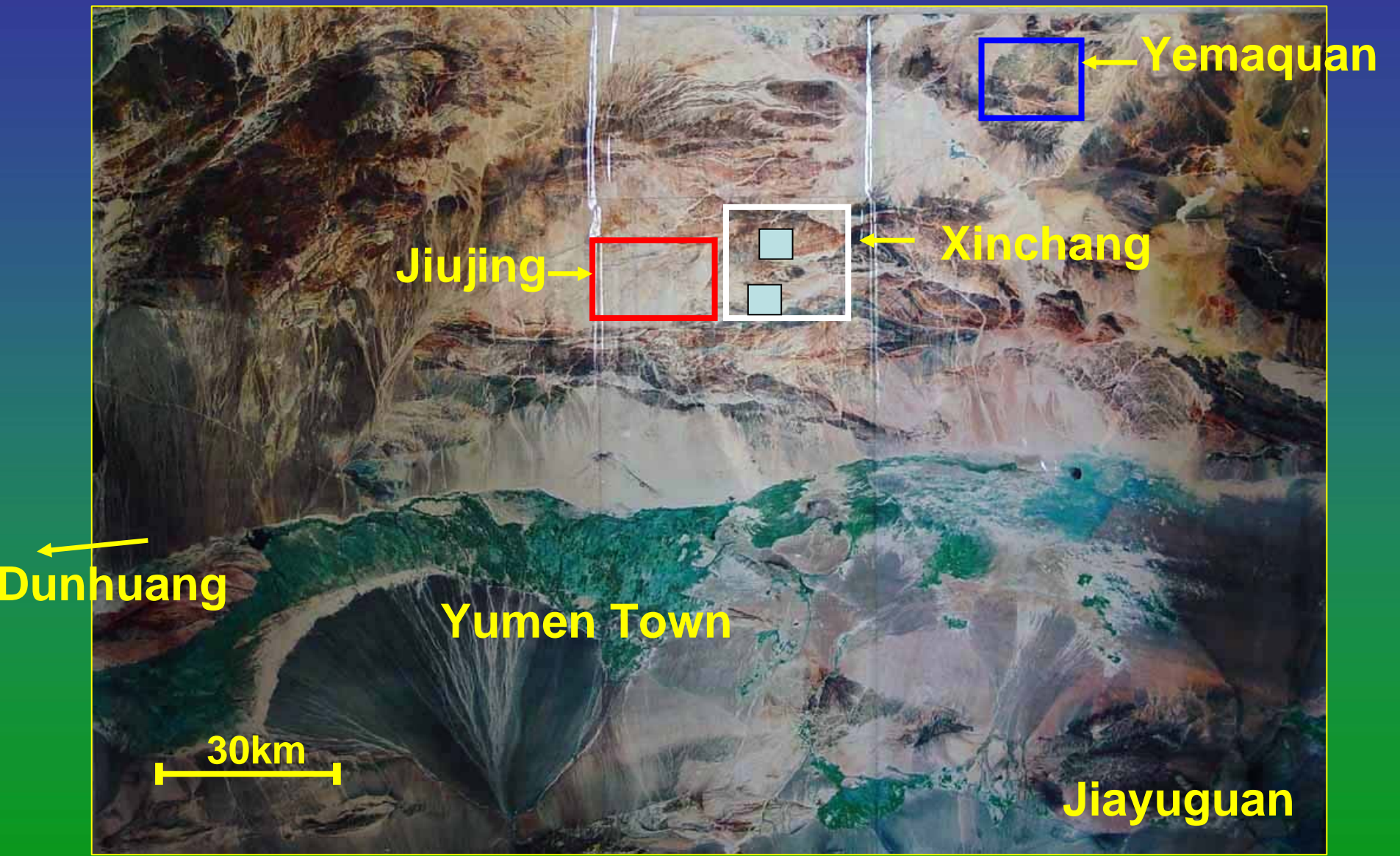
Next Objects

To compare these 3 areas

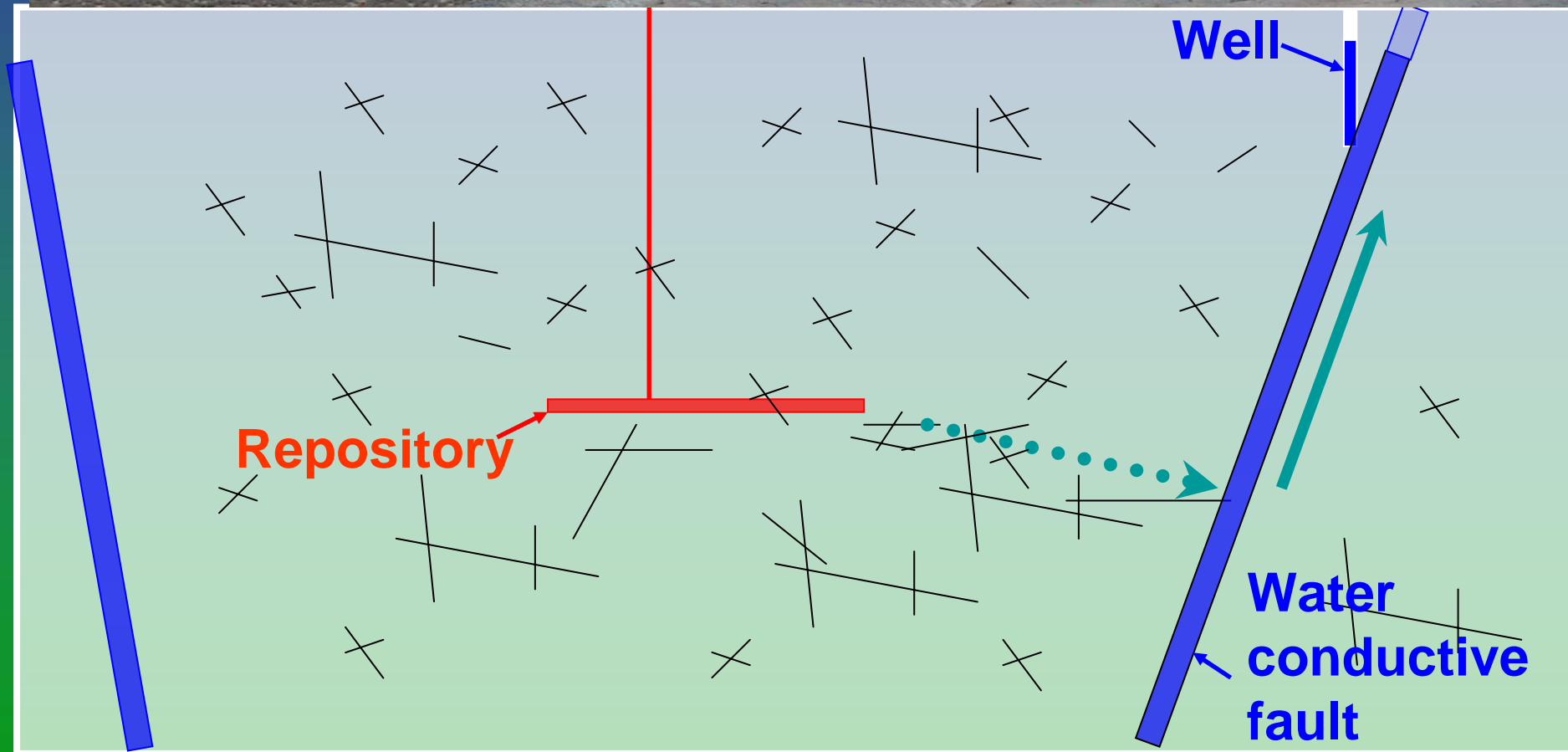
To select more potential sites

To build 3-D map of potential site

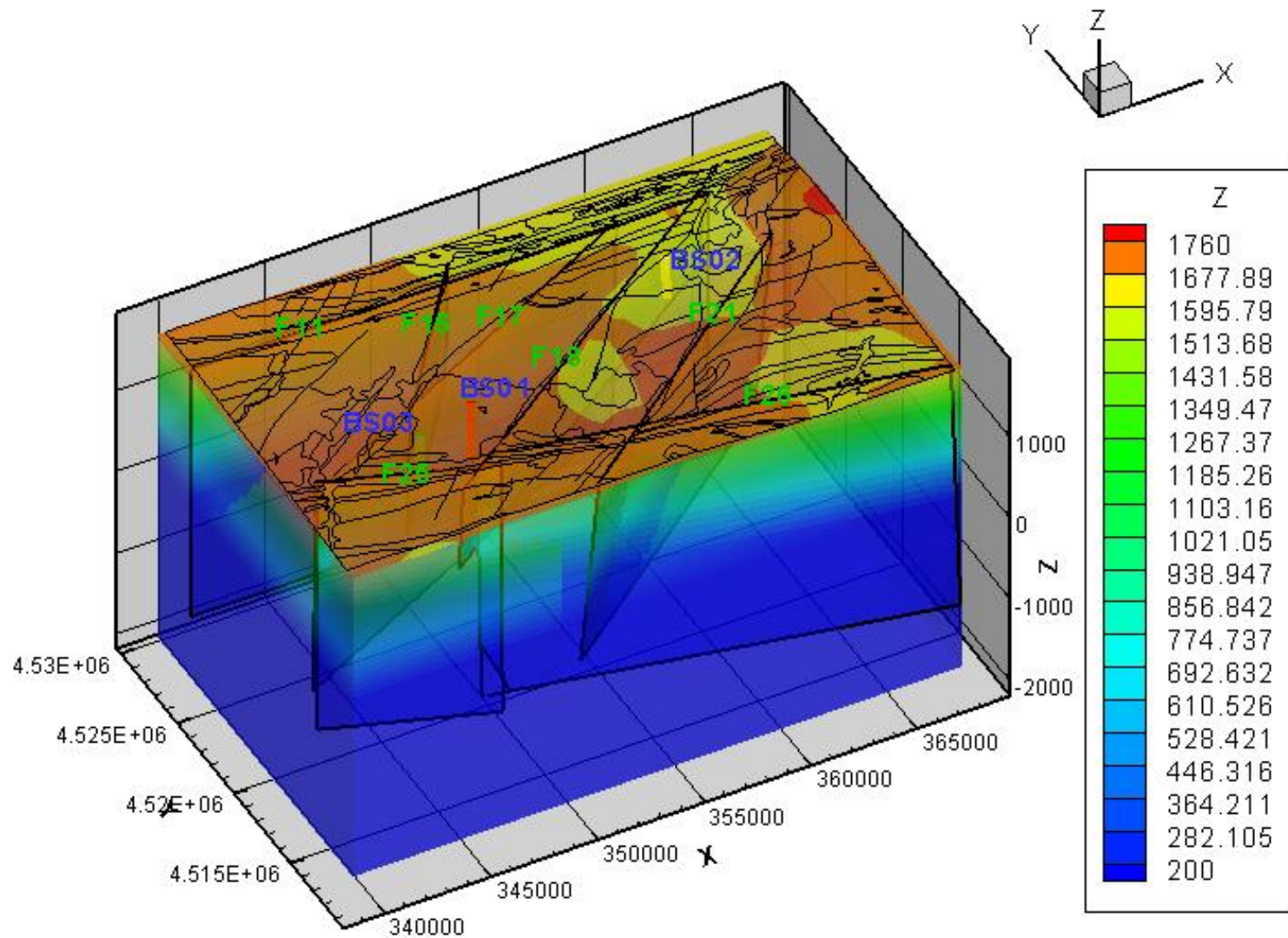
Beishan Region



Conceptual Model of Site



3D Geological Map



- 2 deep boreholes
- 8 shallow boreholes
- Which area is the best one?
- More surface survey, other area?



Geological Group



Picnic





**Experts from France, Switzerland dispatched by IAEA, Sep. 2003
So far, more than 60 foreign experts working or visiting at Beishan**



Beishan Holiday



Beishan Seasons



Welcome to Beishan



Hydrogeological Investigation of Beishan Area, Gansu province, China

GUO Yonghai

Beijing Research Institute of Uranium Geology

2007-05-28



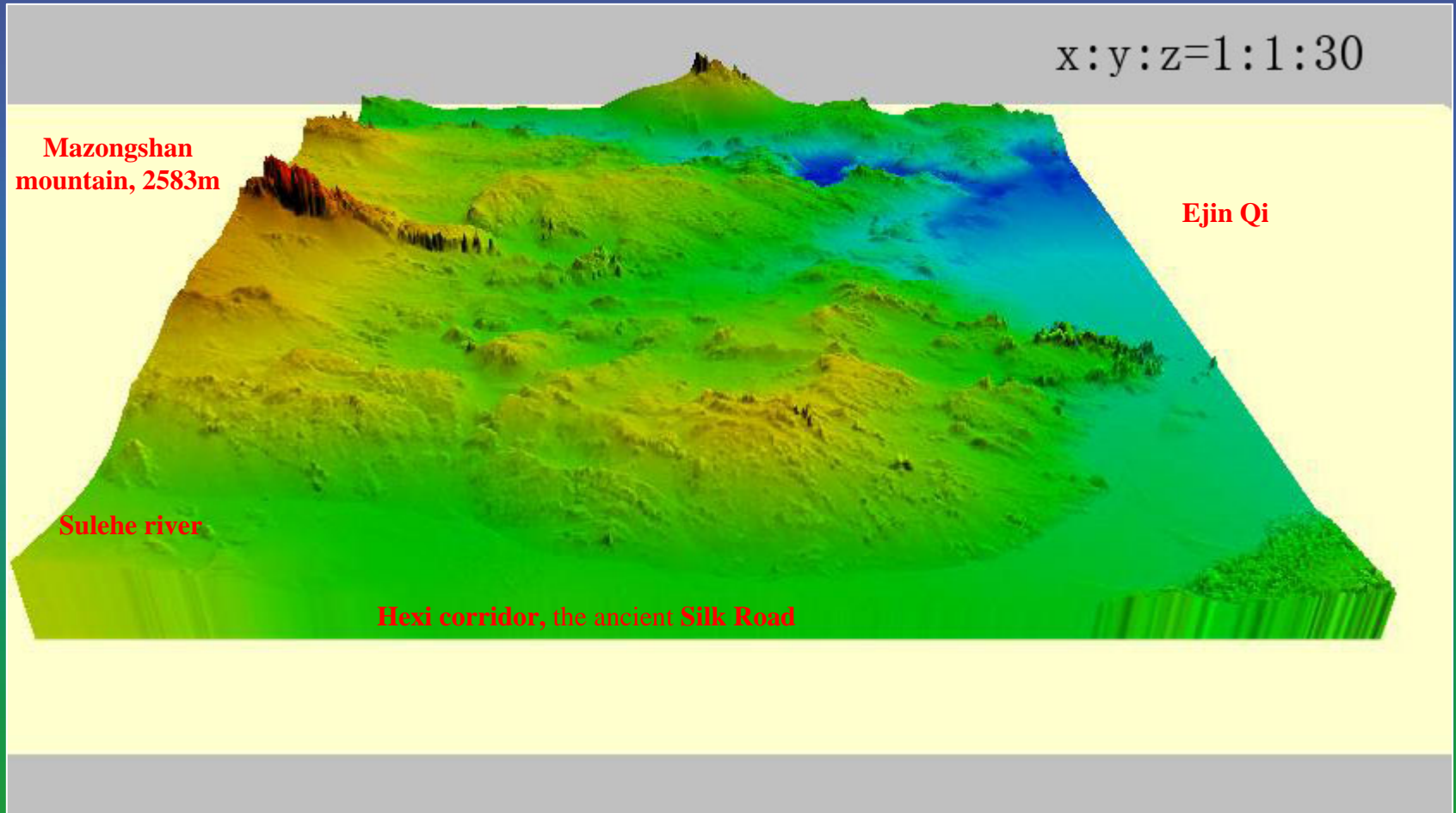
OUTLINE OF PRESENTATION

- **General Introduction**
- **Regional Hydrogeological Conditions**
- **Groundwater Chemistry**
- **Groundwater Isotopes**
- **Regional Groundwater Modeling**
- **Summary and Conclusions**

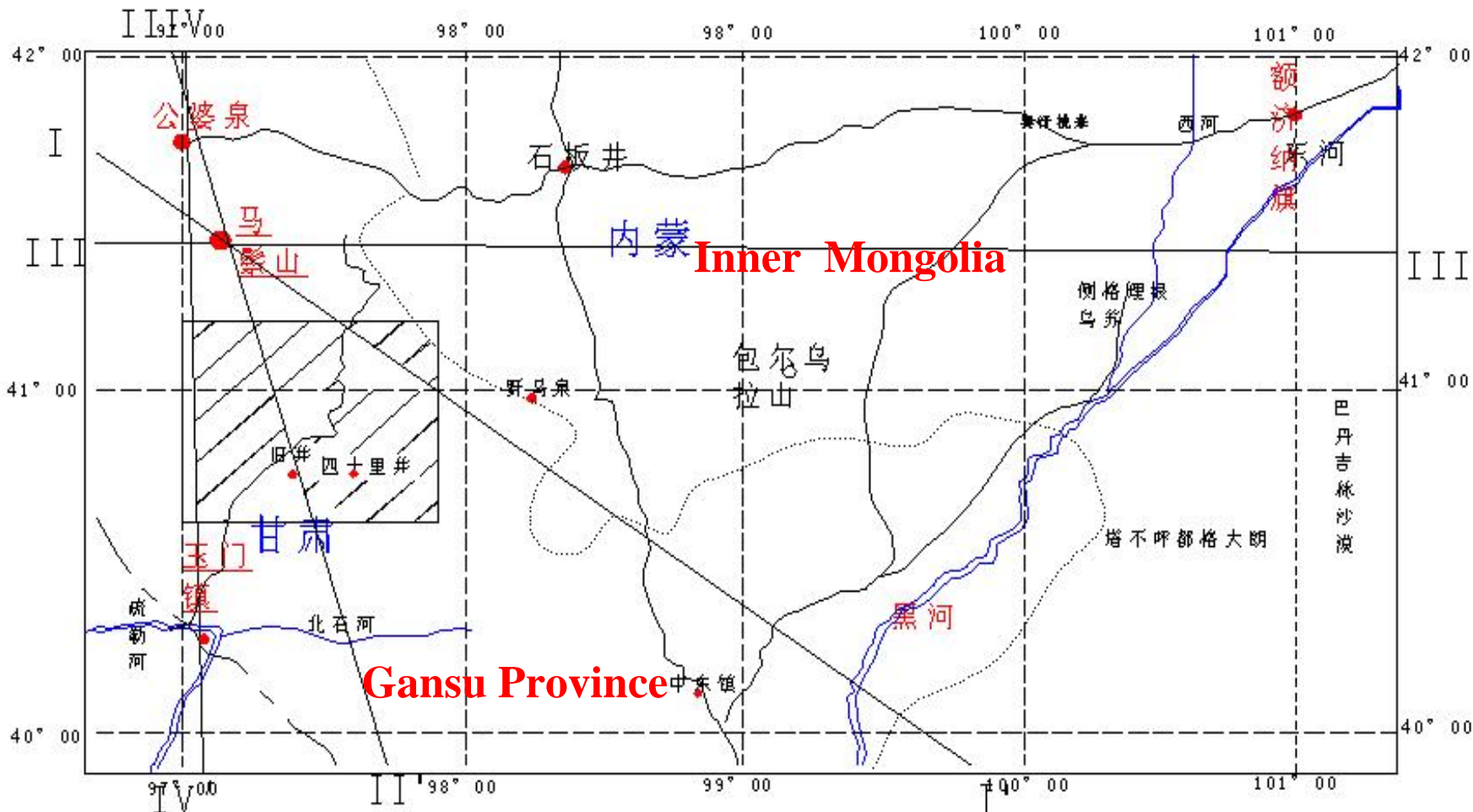


General Introduction

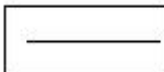
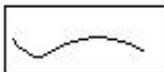



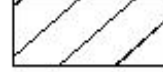
3 dimension view of the investigation area



北山地区地理位置示意图



图例

- 
剖面线
- 
普通公路
- 
河流
- 
城镇
- 
省界
- 
预选区位置

- belong to the rocky Gobi Desert region;
- geographic features are rocky uplands, Gobi, and sandy dunes;
- with dry climate , little precipitation (**40-120mm annually**), high evaporation (**>3000mm annually**);



2004 7 26

- few or no inhabitants;
- no industry and agriculture;
- no prospects of economic development;
- the granite is widely distributed.



2004 7 26



General Introduction

The hydrogeological investigation was started in 1995. The total investigated area is more than 80000km².

- **Stage 1:** 1995-2000, field investigation in Jiujing section;
- **Stage 2:** 2000-2002, field and borehole investigation in Jiujing section



General Introduction

The hydrogeological investigation was started in 1995. The total investigated area is about 80000km².

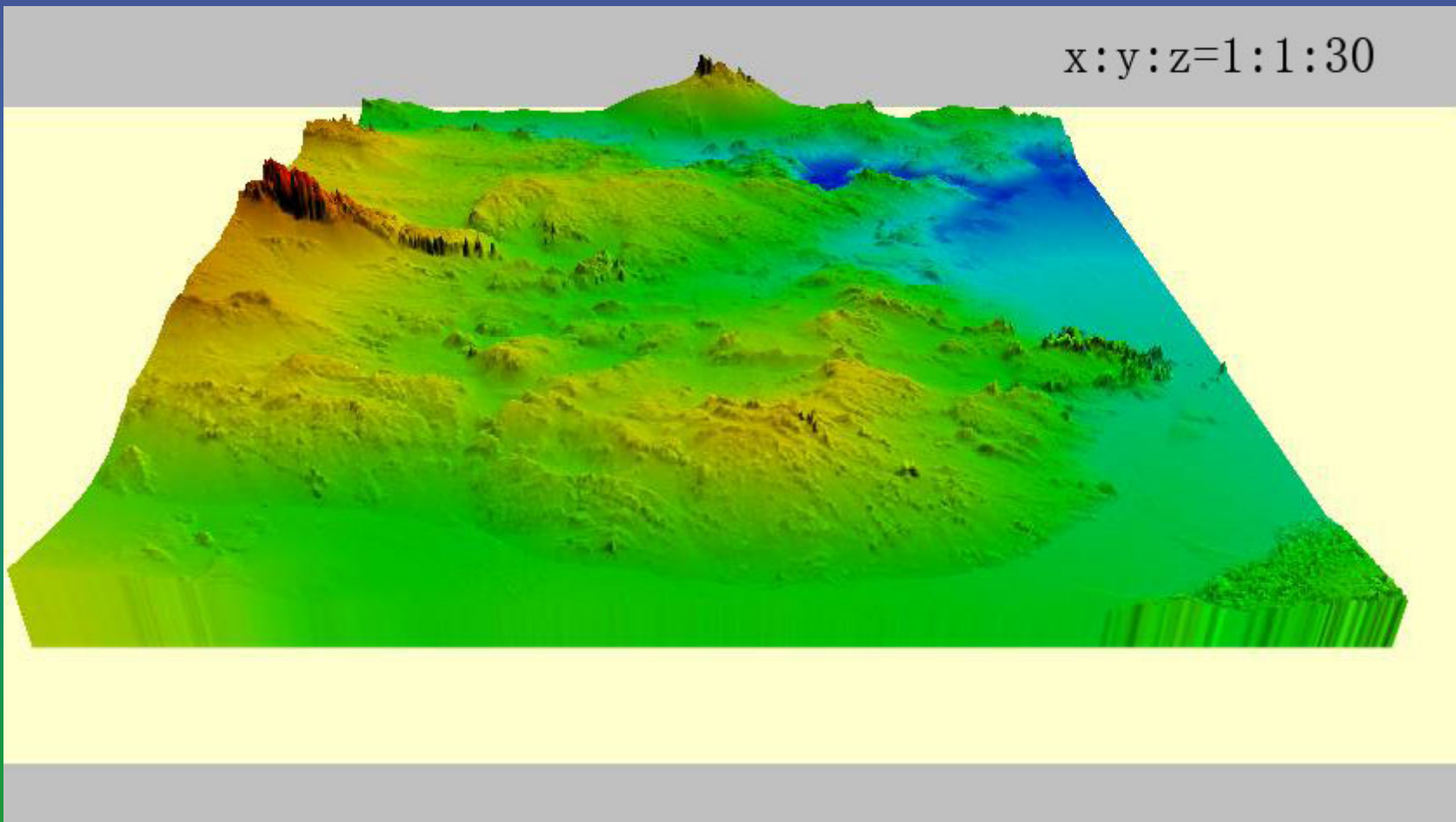
- **Stage 3:** 2002-2004, field and borehole investigation in Yemaquan section
- **Stage 4:** 2004-2007, field investigation in Xinchang and Xiangyangshan section and regional investigation and modeling.



Field hydrogeological investigation and results

研究区三维视图

$x:y:z=1:1:30$



Groundwater outcrops





Pumping test



Field hydrogeological investigation and results



Groundwater sampling





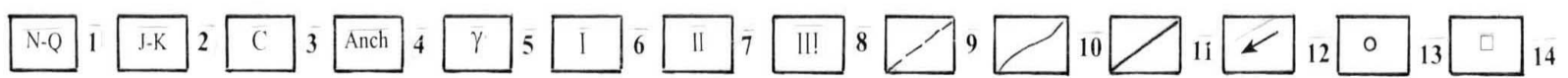
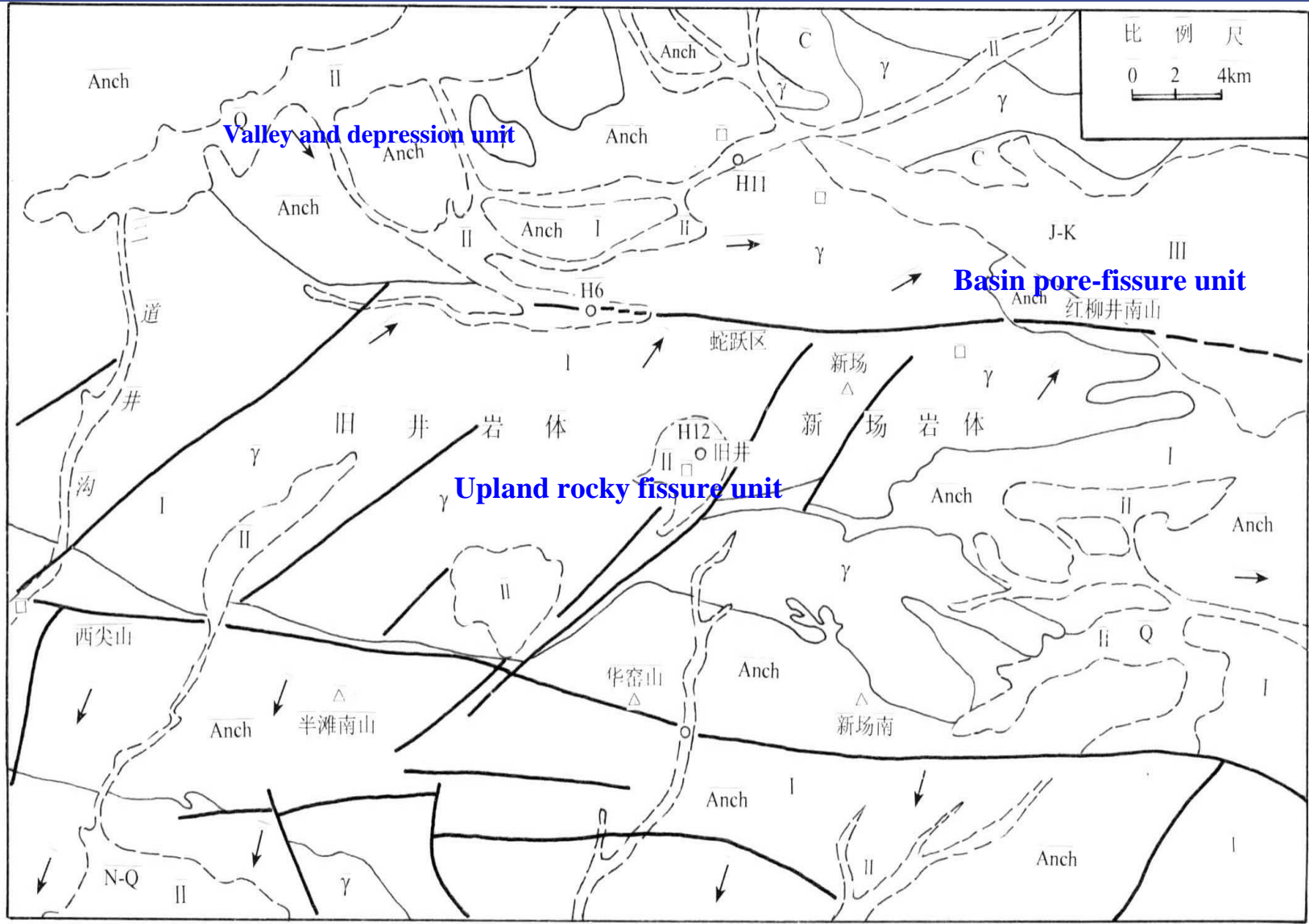
Regional hydrogeological conditions

Based on the topography, lithology, and geological structure, we grouped the Beishan groundwater system into three categories:

1. the upland rocky fissure unit,
2. the valley and depression pore-fissure unit and
3. the basin pore-fissure unit.



Figure 1 The hydrogeological map of the Jiujing area (1995-2002)





Hydrogeological map of Yemaquan area (2002-2004)

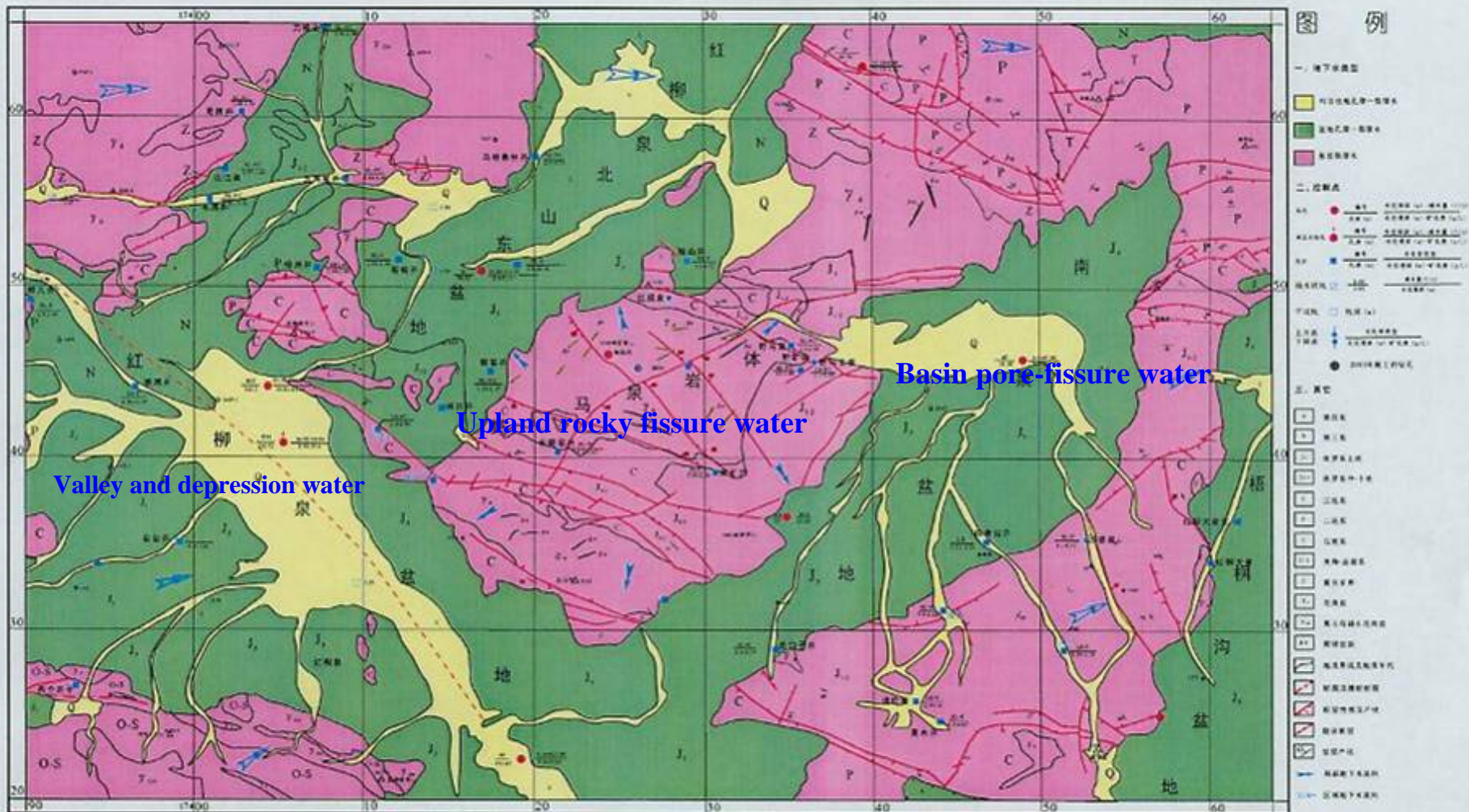
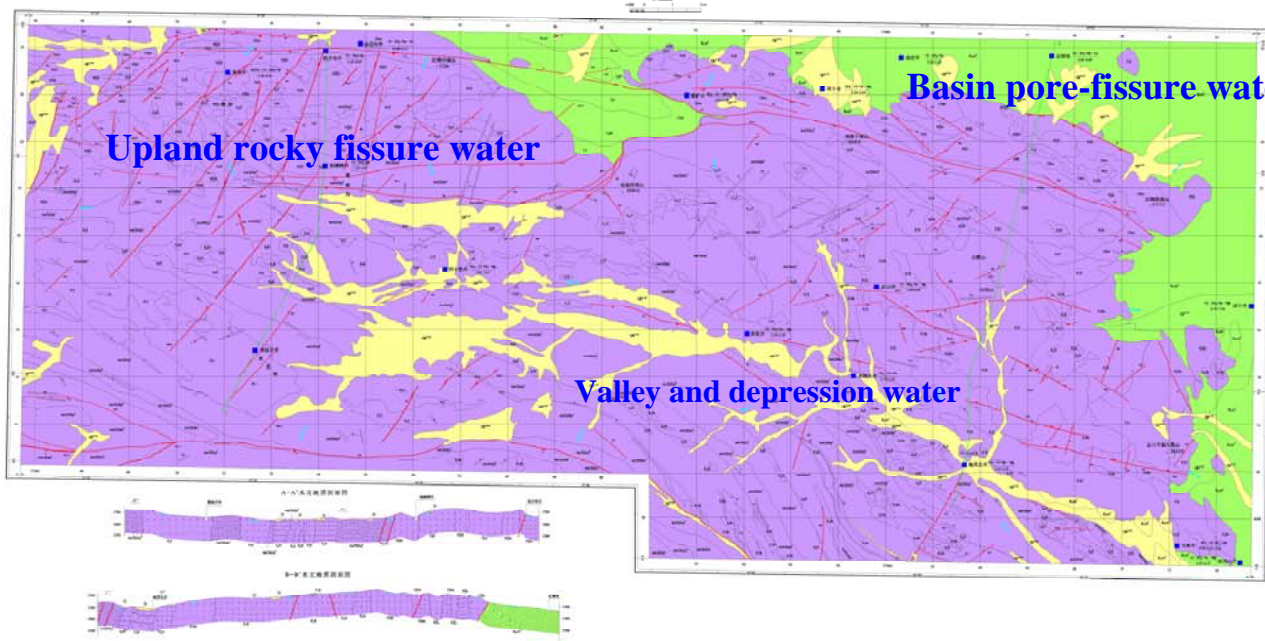


图1 甘肃北山预选区野马泉地段综合水文地质图



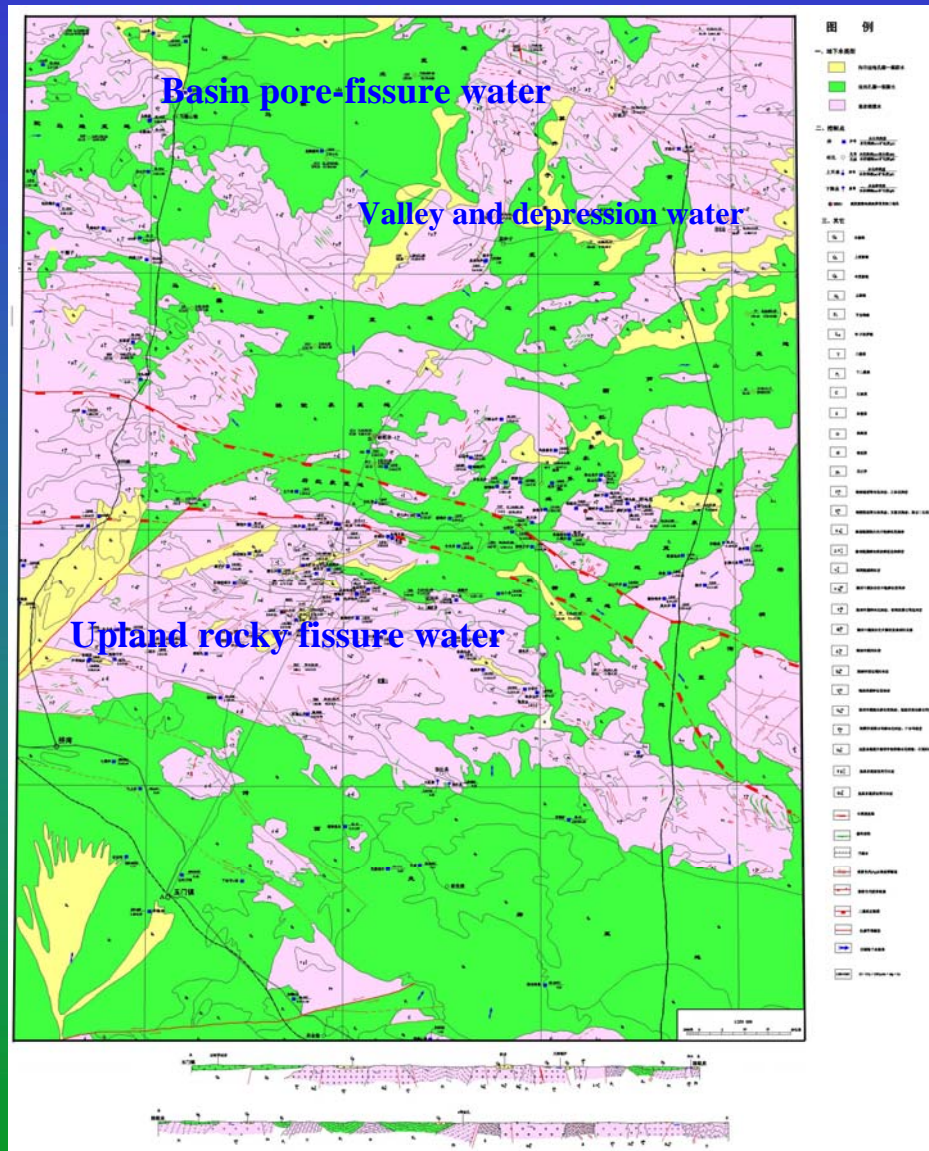
Hydrogeological map of Xinchang-Xiangyangshan area (2004-2007)

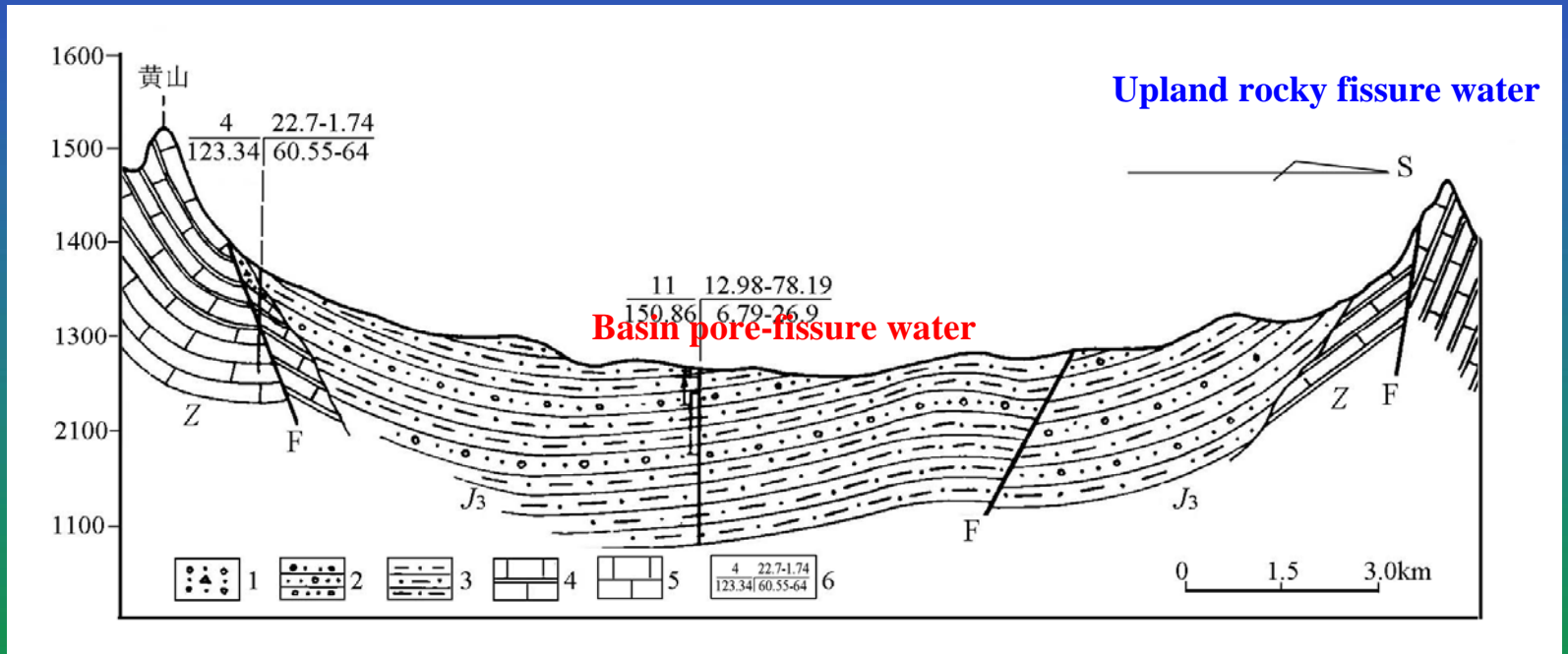
中国高放废物地质处置甘肃北山新场—向阳山地段水文地质图



图例

- 一、地下水资源
 - ① 第四系松散层孔隙水
 - ② 基岩裂隙水
 - ③ 裂隙水
- 二、地质点
 - ▲ 地质点
 - 水文地质点
 - 水文地质点
 - 水文地质点
- 三、其它
 - ① 断层
 - ② 裂隙
 - ③ 构造线
 - ④ 构造线
 - ⑤ 构造线
 - ⑥ 构造线
 - ⑦ 构造线
 - ⑧ 构造线
 - ⑨ 构造线
 - ⑩ 构造线
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Basin hydrogeological sectional drawing 盆地水文地质剖面图

Groundwater depth

Upland rocky fissure water: **> 40 m;**

Valley and depression water: **1 to 6m;**

Basin pore-fissure water: **<10m**

Variation of groundwater table in the past



The dead red- willows showing the drought of climate and drop of groundwater level in the past



Water-bearing features of different mediums

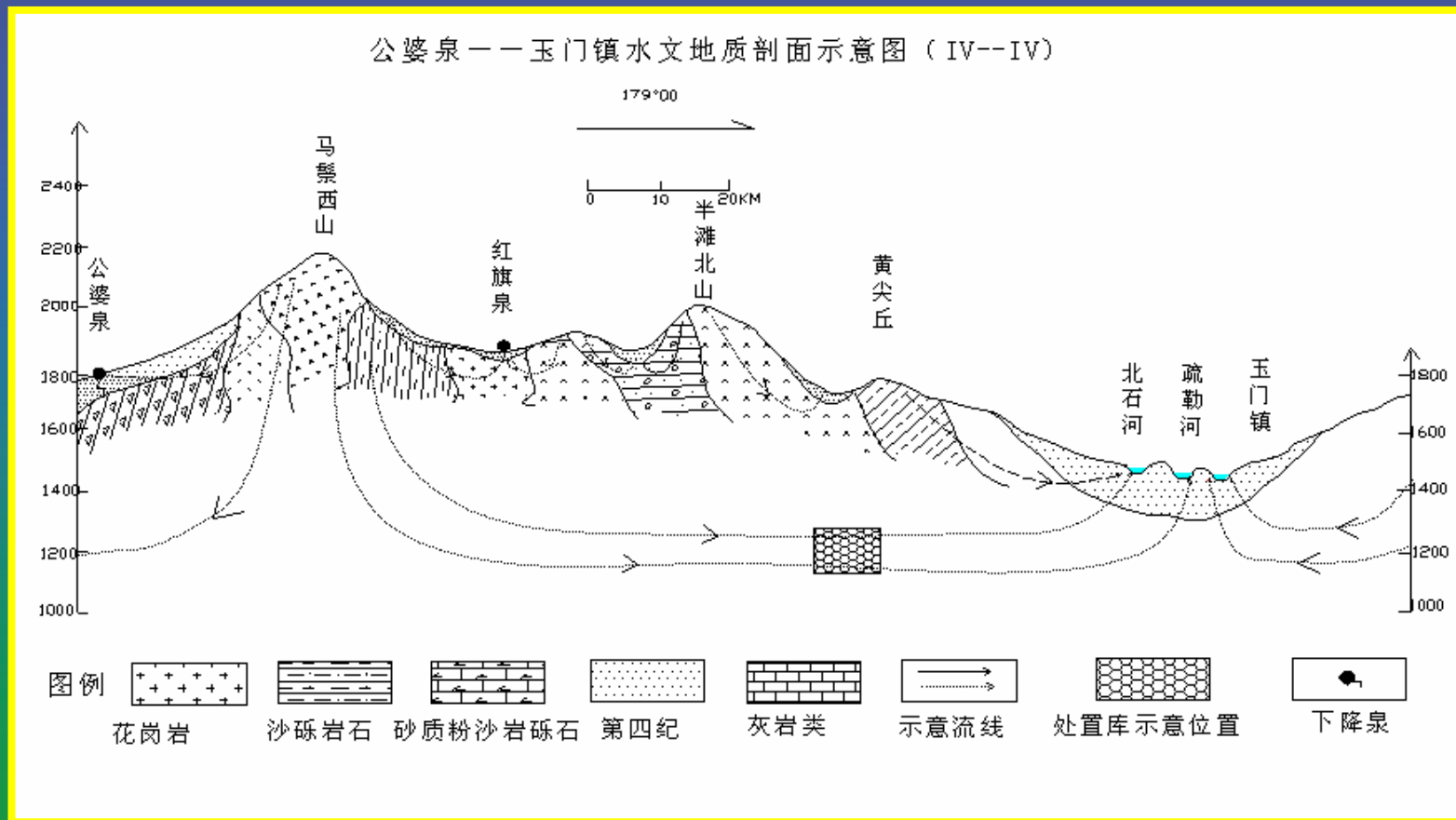
- **In general, granite is the better water-bearing medium in the area;**
- **Metamorphic rocks are the worse water-bearing medium;**



Water-bearing features of different medium

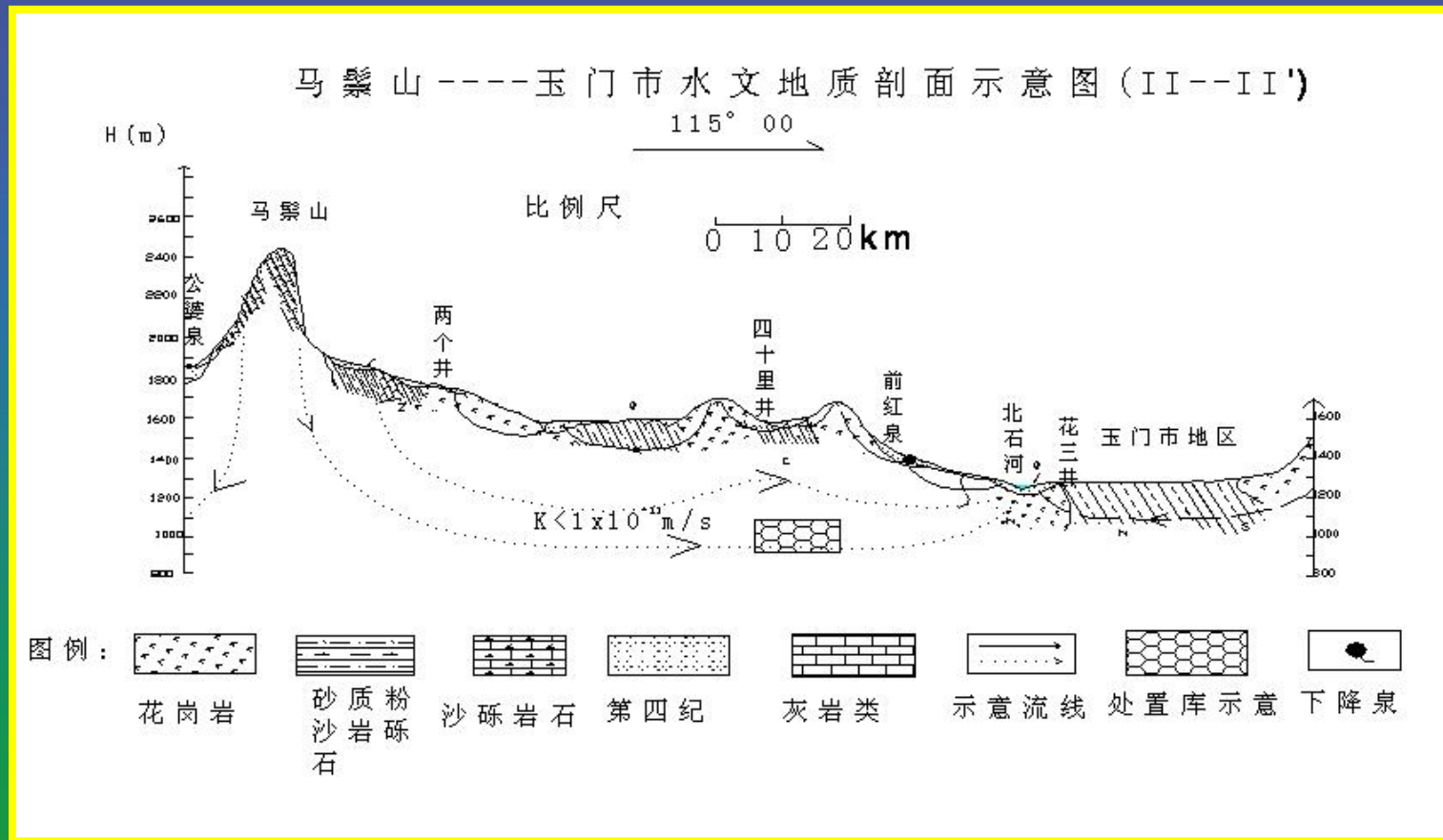
- **Sedimentary rocks and the fault zone without fillings of gouge are the best water-bearing medium.**

Regional groundwater flow sketch sectional drawing



Profile from Mazongshan to Sulehe river

Regional Groundwater Flow Sketch Sectional Drawing



Profile from Mazongshan to Yumen city

4 boreholes have been drilled in Jiujing and Yemaquan sections (2000-2004)

- **Water sampling for isotope and chemical component analysis.**
- **Pumping and injection tests for getting hydrogeological parameters.**
- **Long term monitoring for getting groundwater dynamic features.**



Groundwater Chemistry

Table 6 The content distribution of major ions in Beishan groundwater(mg/L)

Ions	Mean content	Range of content
Na (main cation)	631.00	37.2~4010.4
K	58.66	7.0~465.6
Ca	154.88	29.9~561.1
Mg	42.45	3.9~173.8
HCO ₃	201.64	68.9~637.0
Cl (main anion)	645.39	38.6~3694.2
SO ₄ (main anion)	750.98	67.7~4025.0

Water chemical type: Cl-Na, Cl . SO₄
-Na, SO₄ . Cl-Na;

TDS: mostly >2g/L to 5g/L, the
highest one can reach 80g/L;

pH value: mostly >7.5 to 9



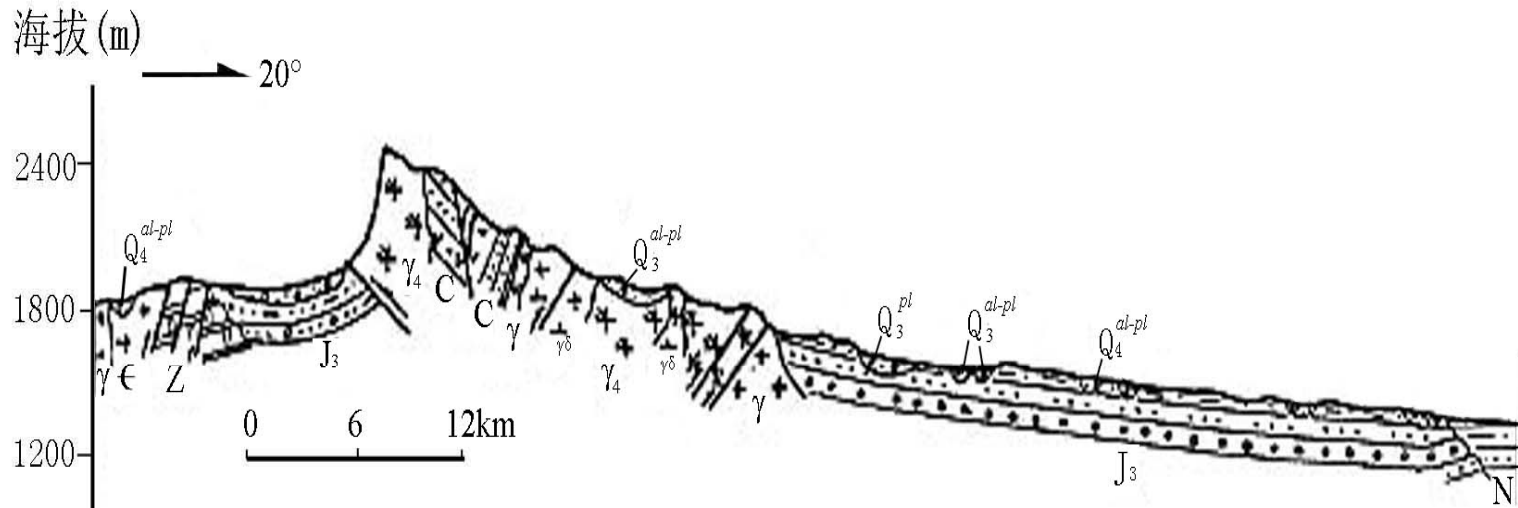
Groundwater chemical data in study area (mg/L)

Sample No.	取样位置	水温℃	pH	TDS	化学类型
W01-00-07	金庙沟	13.0	7.8	1238.0	Cl SO ₄ -Na
S02-00-07	后红泉	11.6	7.8	5129.3	Cl SO ₄ -Na
W03-00-07	咸水井	11.6	6.8	5013.2	Cl SO ₄ -Na
S03--00-09	二道井泉	12.0	7.7	1157.2	Cl -NaCa
W05-00-07	梧桐井	12.6	7.6	773.4	Cl SO ₄ -Na
W08-00-07	旧井（南）	7.5	8.0	4012.6	Cl SO ₄ -Na
W11--00-07	十月井（北）	13.1	8.0	4265.2	Cl SO ₄ -Na
W12-00-07	月亮湾	10.0	7.2	2620.2	Cl SO ₄ -NaCa
S04-00-07	骆驼泉	10.0	7.3	1851.0	SO ₄ Cl -NaCa
W16--00-09	花三井	14	7.8	722.3	SO ₄ -NaCa
W17-00-09	花二井	14	7.9	1195.0	SO ₄ -MgNa
W20-00-09	地质井（2）	17.4	8.3	911.7	Cl -NaCa
W19--00-09	地质井（1）	15.3	7.9	1166.5	Cl -NaCa
W21-00-09	羊角井（1）	15.8	7.7	835.6	Cl -CaNa
W22--00-09	羊角井（2）	14.1	7.8	1051.9	Cl SO ₄ -NaCa
W 24-00-09	草爬子	17.2	6.7	1887.8	Cl -NaCa
W28-00-09	英格尔雄井	12	7.6	5365.5	Cl -NaCa
W29-00-09	旧井（北）	7.6	8.1	3919.3	Cl SO ₄ -Na
S05-00-09	小泉	12.5	7.0	742.1	SO ₄ HCO ₃ - MgNa



Groundwater chemical data in study area (mg/L)

Sample No.	取样位置	K ⁺	Na ⁺	Ca ²⁺	Mg ²⁺	Cl ⁻	HCO ₃ ⁻	SO ₄ ²⁻	SiO ₂
W01-00-07	金庙沟		339.0	78.0	20.4	369.0	221.4	302.9	8.7
S02-00-07	后红泉	9.3	1677.0	117.5	60.0	1873.6	197.8	1269.9	2.9
W03-00-07	咸水井	29.5	1313.0	363.0	70.7	1764.1	209.9	1357.6	3.3
S03--00-09	二道井泉	36.5	187.2	157.6	37.8	465.8	145.7	215.2	--
W05-00-07	梧桐井	20.7	150.6	85.8	20.5	196.0	139.6	230.8	14.4
W08-00-07	旧井（南）	5.48	1075.5	322.4	40.4	1470.1	250.9	948.1	12.3
W11--00-07	十月井（北）	18.4	1185.8	253.8	46.1	1420.0	279.7	1185.1	13.7
W12-00-07	月亮湾	20.9	602.4	217.4	44.8	522.9	233.0	1097.8	7.9
S04-00-07	骆驼泉	10.5	430.3	157.0	25.3	415.1	274.3	652.4	21.8
W16--00-09	花三井	12.0	128.0	56.2	29.0	85.0	79.3	366.8	14.5
W17-00-09	花二井	3.07	150.2	89.9	96.3	247.9	93.3	541.4	15.1
W20-00-09	地质井（2）	7.47	180.6	95.3	26.7	390.4	83.2	158.1	--
W19--00-09	地质井（1）	20.0	223.9	130.1	36.7	515.7	145.6	162.5	--
W21-00-09	羊角井（1）	24.8	114.9	126.4	35.6	381.9	99.9	114.2	--
W22--00-09	羊角井（2）	12.7	216.1	93.5	36.7	462.2	87.4	175.7	--
W 24-00-09	草爬子	24.0	366.1	230.9	44.4	964.5	105.0	188.8	--
W28-00-09	英格尔雄井	40.6	1286.5	505.8	164.4	3278.6	58.3	87.8	--
W26-00-09	炭窑井	13.0	208.6	58.6	33.3	332.1	149.8	188.8	--
W29-00-09	旧井（北）	23.2	531.2	643.8	55.84	734.1	192.6	1802.6	18.0
S05-00-09	小泉	37.5	112.4	36.8	64.7	108.2	270.7	259.5	15.1



水化学类型	$\text{SO}_4^{2-}-\text{Cl}^--\text{Na}^+$		$\text{Cl}^- - \text{SO}_4^{2-} - \text{HCO}_3^- - \text{Na}^+$		$\text{SO}_4^{2+}-\text{Cl}^- - \text{Na}^+$		$\text{Cl}^- - \text{SO}_4^{2-} - \text{Na}^+$	
矿化度	1-2g/l		<1g/l		1-2g/l		2-5g/l	>5g/l
地貌单元	丘陵	山前倾斜平原	低	中	山	山间平原	低山	山前倾斜平原
							波	状
							平	原

The main influence factors of groundwater chemistry

- Landform
- Precipitation
- Water level
- Evaporation (fundamental factor)



Summary of groundwater chemistry

- **High TDS**

from 0.4 to 12.0 g/L, and the highest TDS can reach 80 g/L

- **Slightly alkaline**

The pH values are mainly from 7.2 to 8.8

- **Low solubility**

Most of waters are oversaturated with calcite, dolomite and clay minerals

- **Water chemical types**

- Sodium chloride sulphate
- Sodium sulphate chloride

- **The main influence factors of groundwater chemistry**

- Landform
- Precipitation
- Water level
- Evaporation (fundamental factor)

^{18}O : -7.0‰ to -11‰;

^2H : -53‰ to -66.5‰;

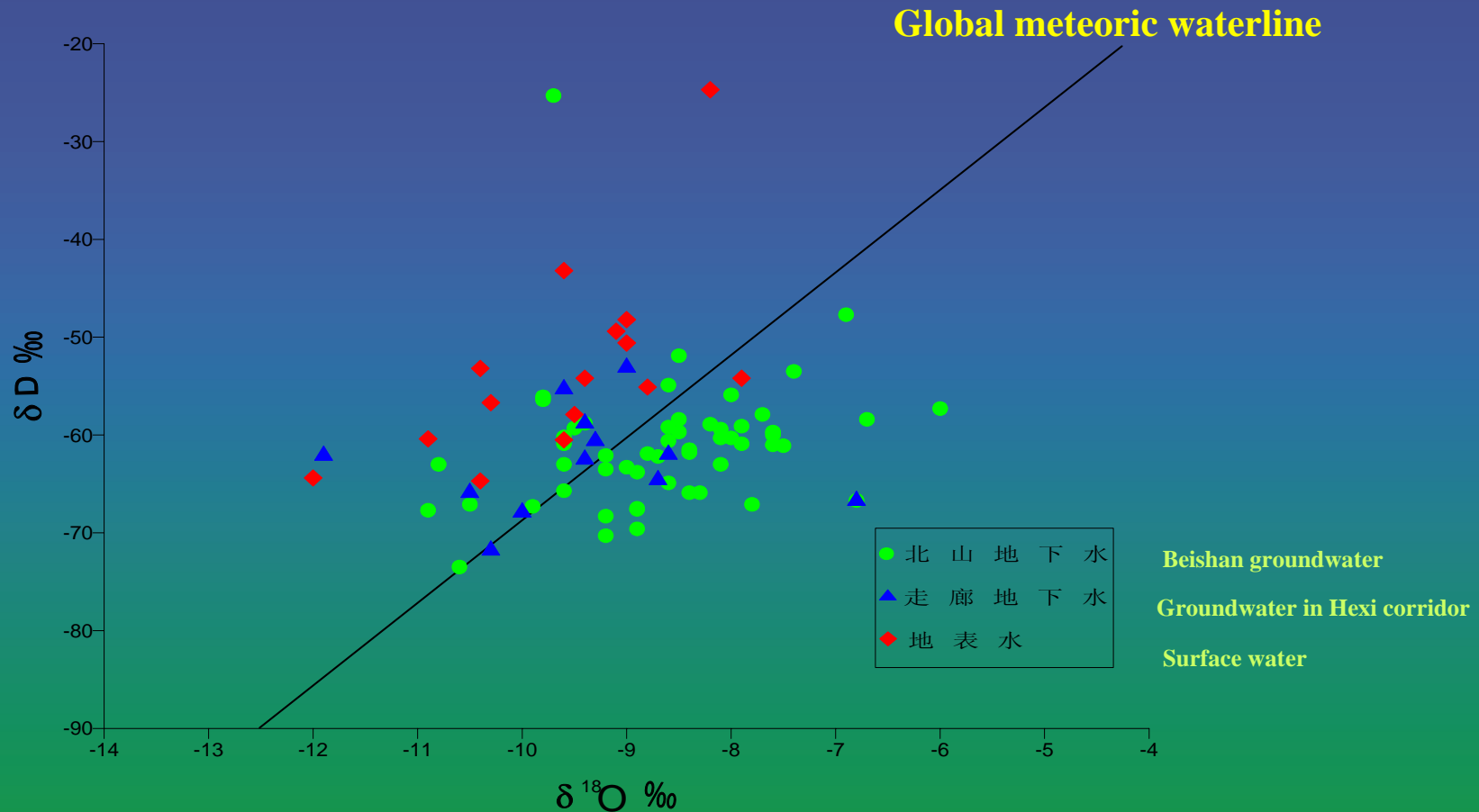
^3H : 5.08 TU to 38.5 TU.



Groundwater Isotopes

Groundwater hydrogen and oxygen isotope

Sample No.	Location	$\delta^{18}\text{O}$ (‰)	δD (‰)	tritium(TU)
W05-00-07	梧桐井	-9.3	-59	59.54
W05-00-07	旧井(南)	-8.7	-56	34.1
W29-00-09	旧井(北)	-10.4	-67	33.24
W30-00-09	十月井(南)	-7.6	-56	37.27
W11-00-07	十月井(北)	-7.7	-54	31.10
W12-00-07	月亮湾	-9.2	-62	6.77
S02-00-07	后红泉	-9.1	-66	0.94
S04-00-07	骆驼泉	-9.6	-63	40.26
W03-00-07	咸水井	-8.2	-54	14.48
W01-00-07	金庙沟	-9.0	-58	12.34
W24-00-09	草爬子	-7.4	-63	24.44
W19-00-09	地质井(1)	-8.9	-65	41.61
W20-00-09	地质井(2)	-8.6	-70	35.78
W16-00-09	花三井	-10.7	-73	10.34
W17-00-09	花二井	-10.2	-74	36.53
W21-00-09	羊角井(1)	-8.0	-69	61.55
W22-00-09	羊角井(2)	-8.2	-70	69.80
W28-00-09	英格尔雄井	-6.9	-70	17.68
S03-00-09	二道井泉	-8.8	-61	48.20
W26-00-09	炭窑井	-8.4	-59	45.62
S05-00-09	小泉	-10.0	-66	36.61
R01-00-07	雨水	-8.3	-66	64.38



Plot of ^{18}O vs. ^2H in groundwater in Beishan Area



Groundwater flow modeling

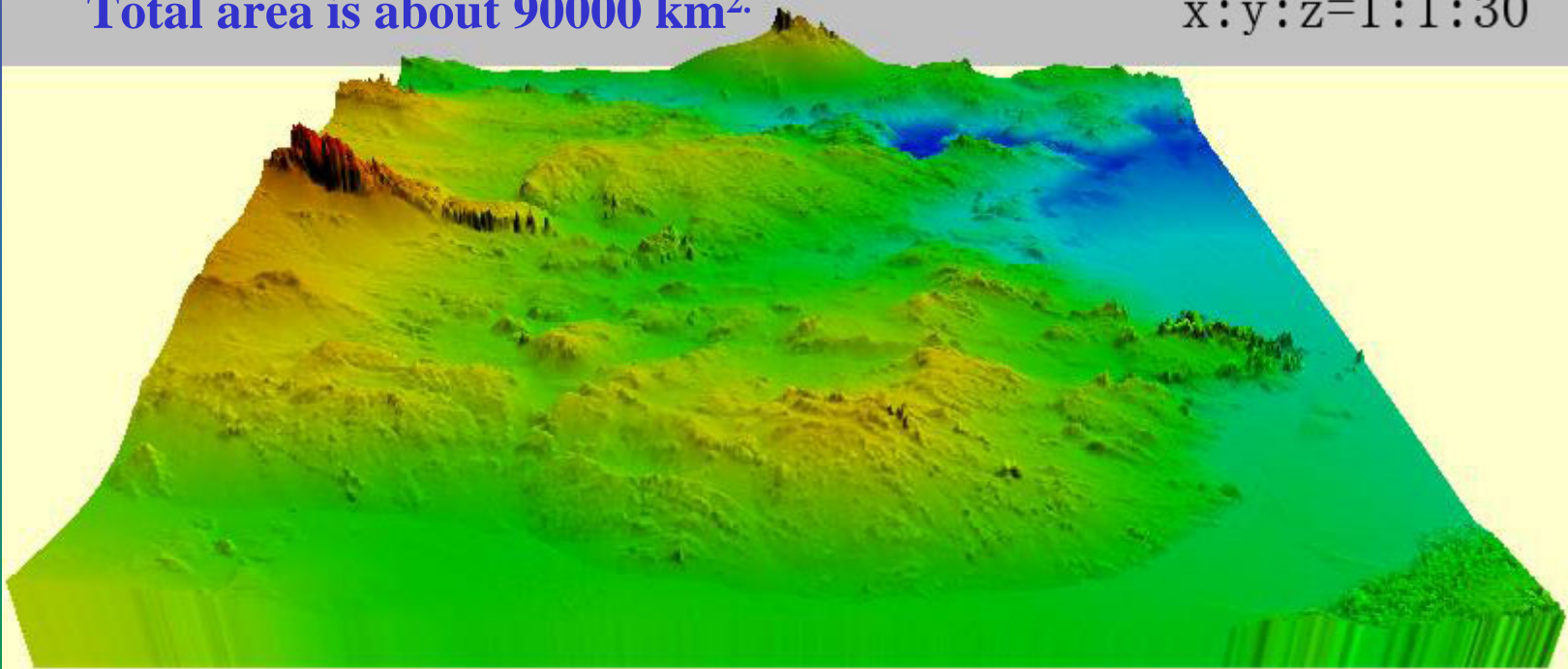
From 2005 to this year, a cooperated project of groundwater flow modeling was carried out by our group and Institute of Geology and Geophysics, Academy of Sciences . The project was completed mainly by Dr. Guomin Li.



Groundwater flow modeling

Total area is about 90000 km².

x:y:z=1:1:30



3 dimension view of the study area



Regional Groundwater Flow Modelling

Define the boundary conditions

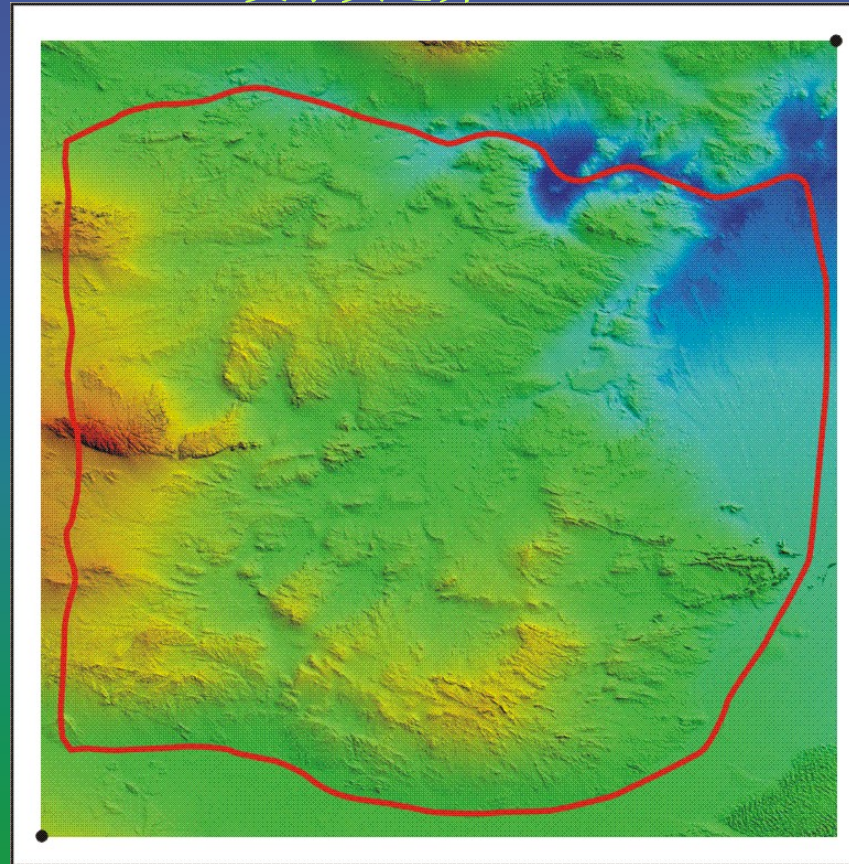
water divide,
zero flux
boundary

零通量边界

Water level boundary

一类水头边界

North



Heihe River,
water level
boundary

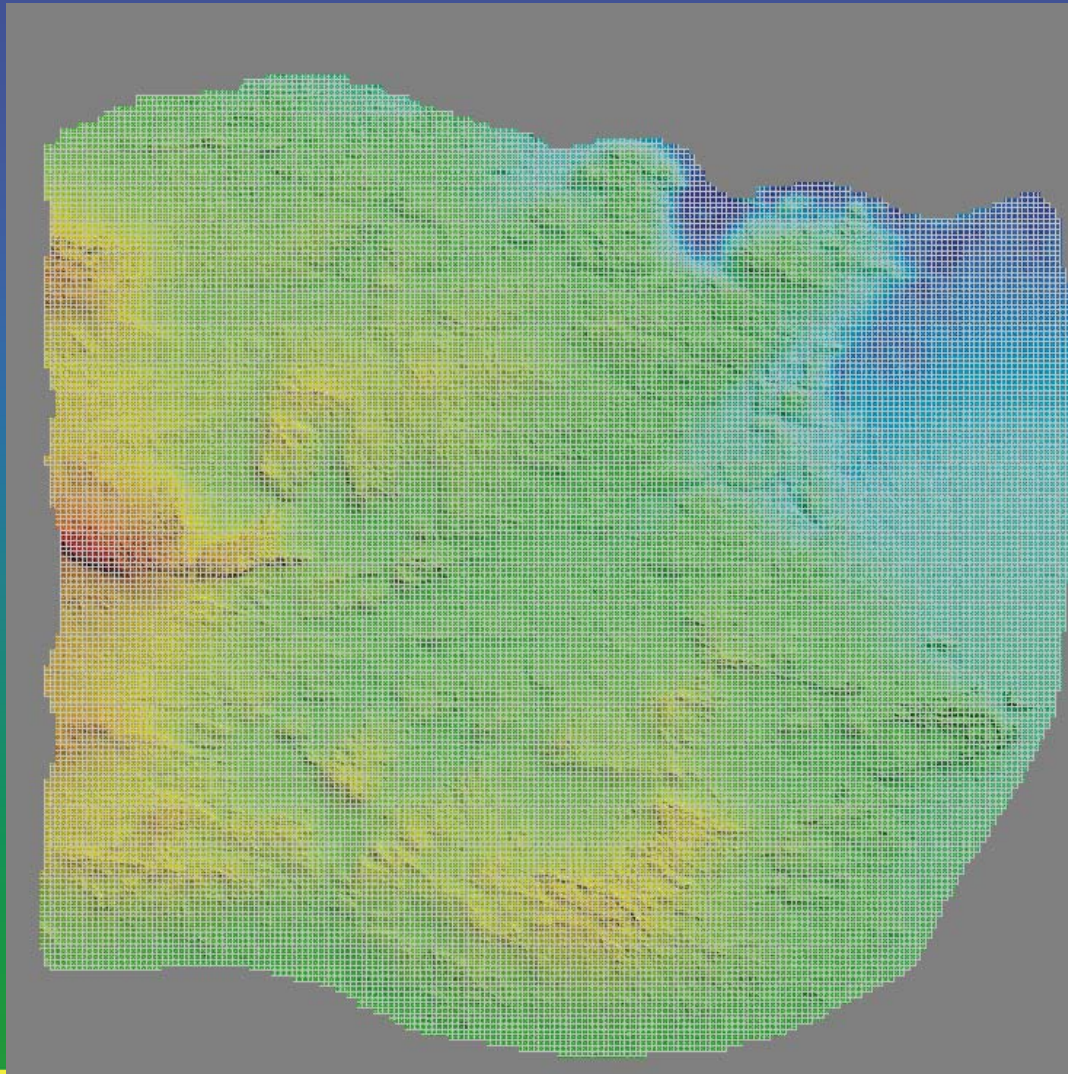
一类水头边界

Hexi corridor, and Sulehe river

Water level boundary 一类水头边界



Defining the grid



Rows: 200

Columns: 200

**Finite difference
method**

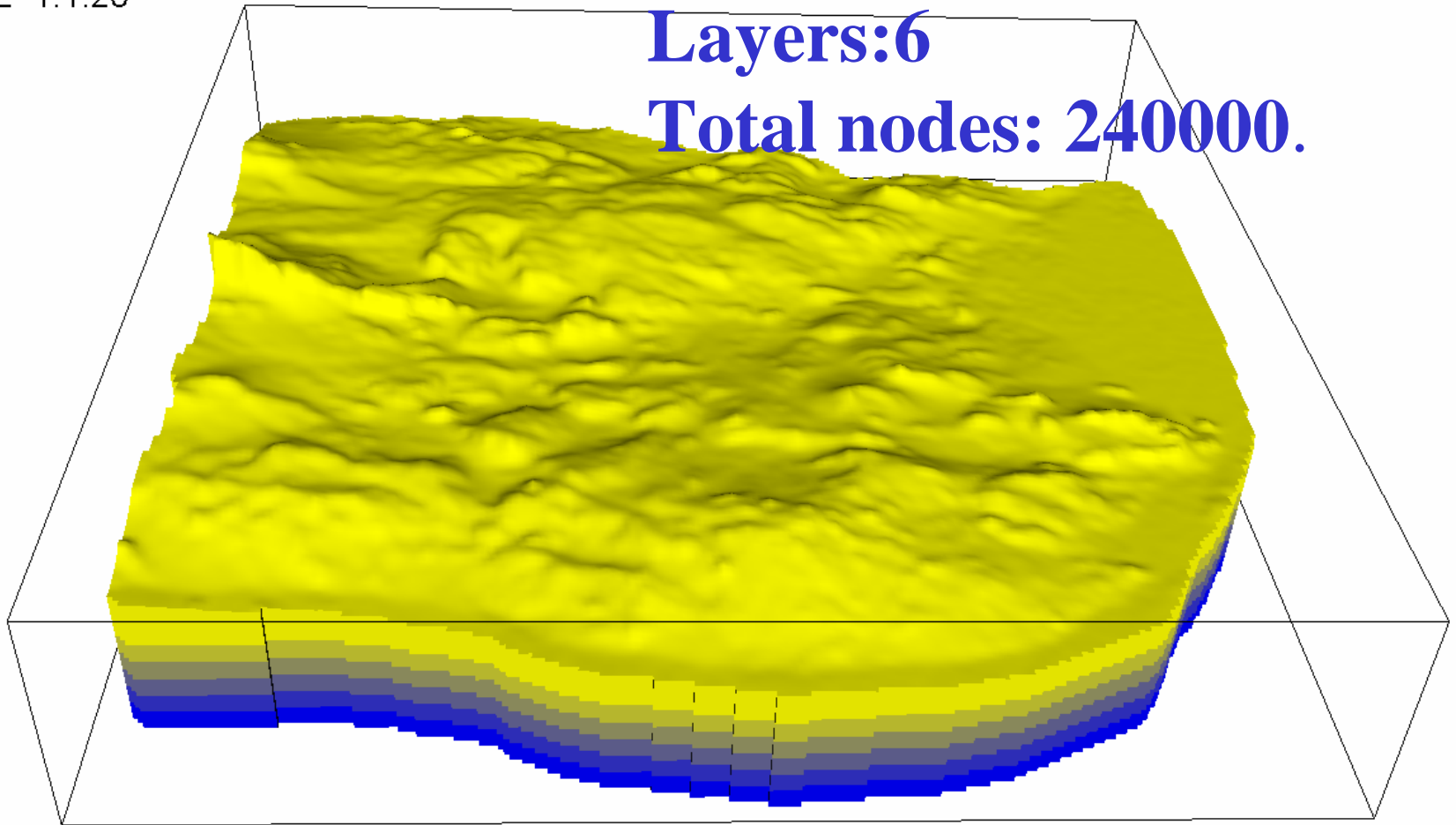


Regional Groundwater flow modelling

X:Y:Z=1:1:20

Layers:6

Total nodes: 240000.





Regional Groundwater Flow Modelling

Input Hydrogeological Parameters

- **Rainfall:**
 - West part :80mm/y;
 - Middle part : 65mm/y;
 - East part:50mm/y.

- **Evaporation:**
 - West part : 2800mm/y
 - Middle part : 3100mm/y。
 - East part: 3500mm/y,



Input Hydrogeological Parameters

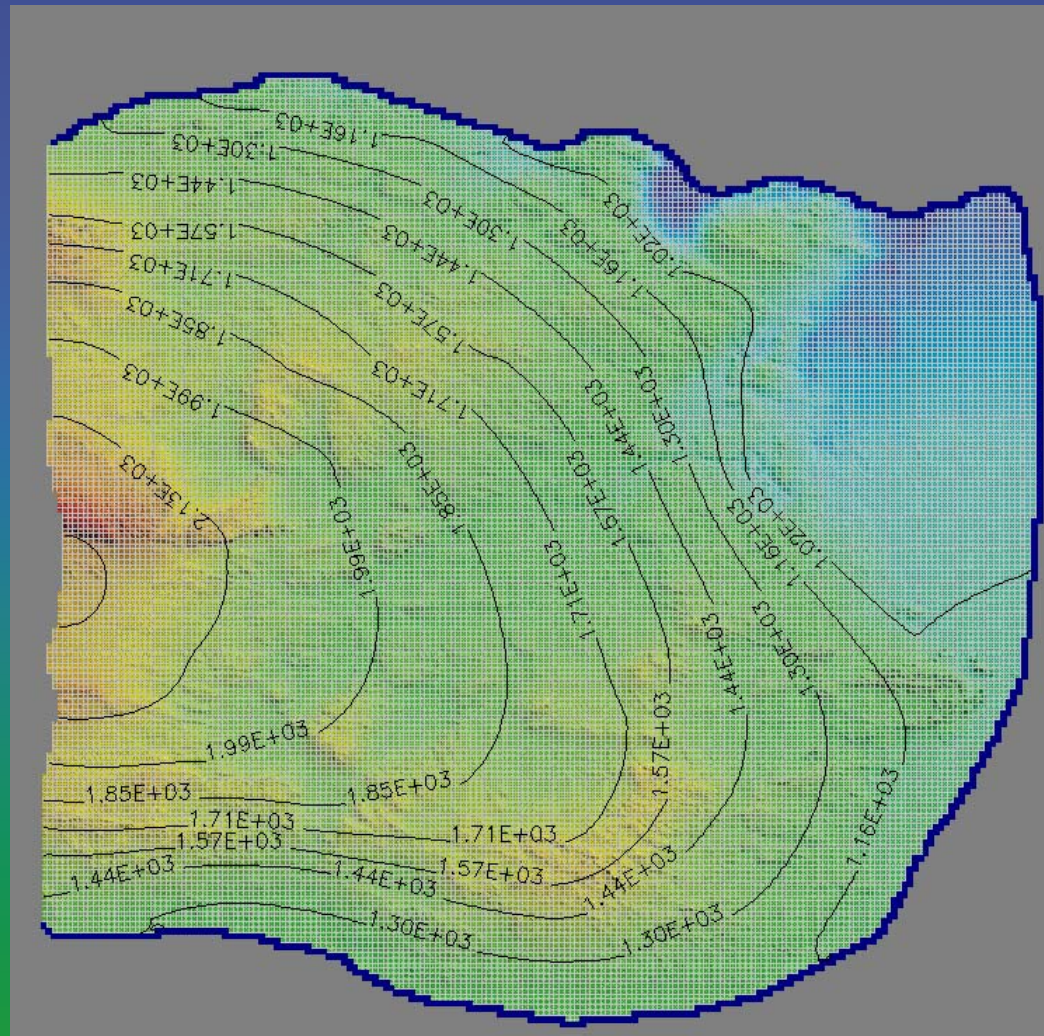
- **Permeability coefficient:** (almost have no real data). Design different schemes:
 - scheme 1: 10^{-6} m/s
 - scheme 2: 10^{-7} m/s
 - scheme 3: 10^{-8} m/s
 - scheme 4: 10^{-9} m/s



Regional Groundwater Flow Modelling

**Groundwater flow field
modeling result:
Scheme 4:**

Permeability
coefficient:
 10^{-9}m/s





Regional Groundwater Flow Modelling

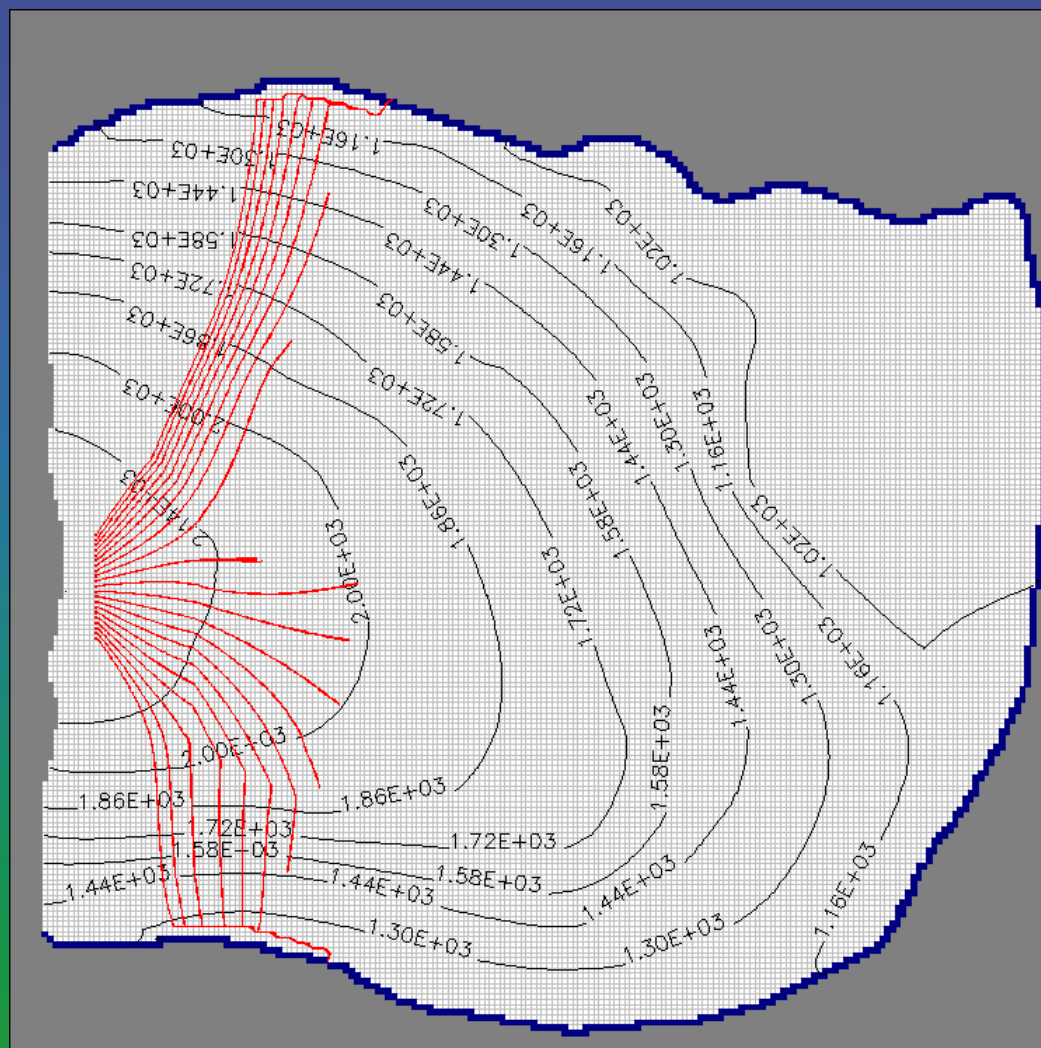
Groundwater pathline
modeling result:

Scheme 4

Permeability
coefficient:

10^{-9} m/s

Red line shows the particle
travel track in 1 million years.





Summary of the presentation

- Groundwater system in Beishan area can be classified into three units:(1) upland rocky fracture unit; (2) valley and depression pore-fracture unit; and (3) basin pore-fracture unite, in which the upland rocky unit is the principal hydrogeological unit in the area.



Summary of the presentation

- Water content is mainly depend on lithology, topography, fracture and fault. In general, water content of magmatic rocks is much more than that of metamorphic rocks.



Summary of the presentation

- Chemically, groundwater in Beishan area is characterized by high TDS.



Summary of the presentation

- Isotope study shown both shallow groundwater and deep groundwater are of meteoric origin.



Summary of the presentation

- **Groundwater modeling was done initially and the result could provide valuable reference for site selection and evaluation.**

- Regional hydrogeological investigation
 - regional circulation;
- More shallow borehole drilling
 - site groundwater flow field;
- More deep borehole drilling
 - site deep hydrogeological environment;
- Hydrogeological test
 - hydrogeological parameters.
- Groundwater modeling continually
 - provide support for site evaluation

radioactive waste is a major problem facing many countries worldwide.

It is our dream to make a wonderful future in this field.

Let us cooperate and work together on it to protect our beautiful global village.

Thank you



HYDRAULIC TESTS IN BSO3

SU Rui

- • **INTRODUCTION**
- **HYDRAULIC TEST
TECHNIQUE WITH DOUBLE
PACKERS**
- **DATA INTERPRETATION OF
TESTS**
- **Summaries**

OBJECTIVES

- To establish the approaches and techniques
- To take groundwater samples
- To obtain the hydraulic parameters

Basic information of BS03

- Geometry: 500m, 95mm, vertical
- Host rock: Porphyritic monzonitic granite
- Aquifer features: heterogeneity, anisotropy, fractured-rock aquifer
- Water level below the ground: ~60m
- Drilling was finished in 2003

HYDRAULIC TEST TECHNOLOGY WITH DOUBLE PACKERS

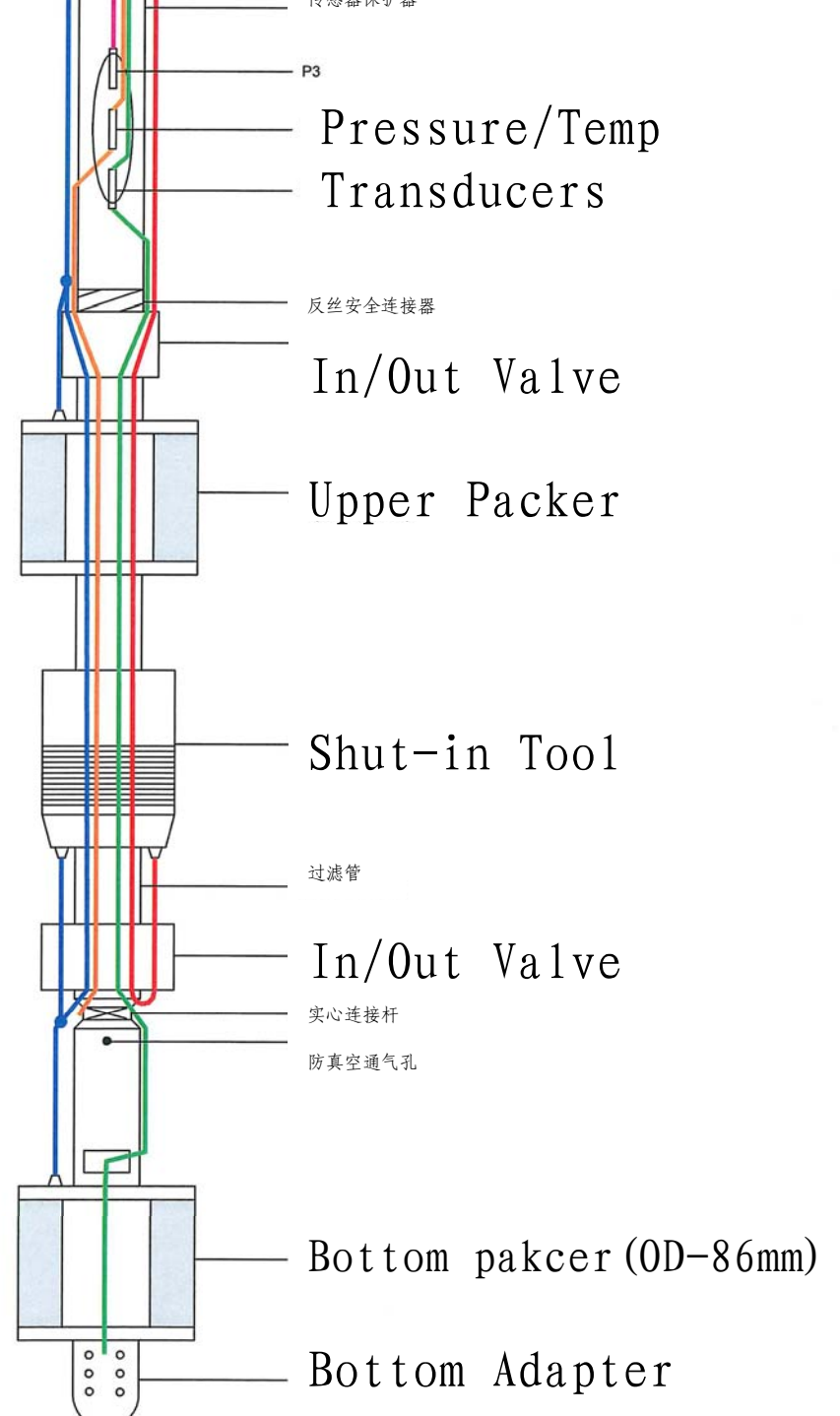
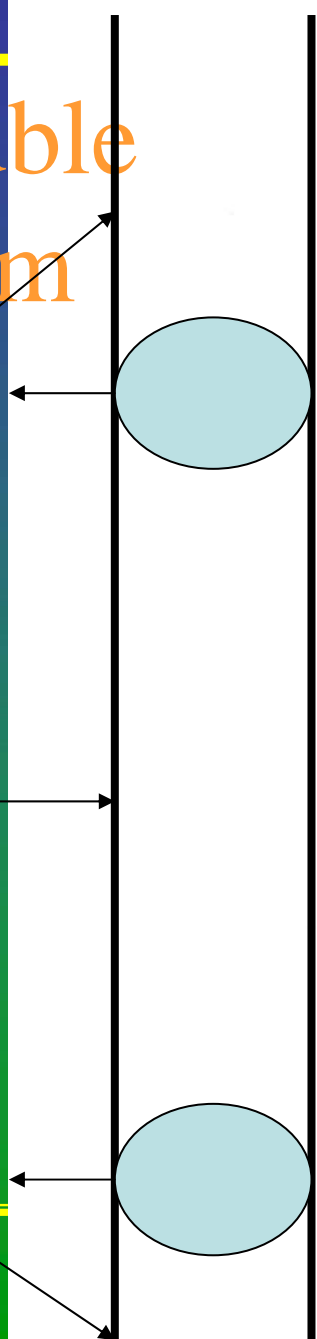
- Equipments
- Test design
- Preparation for test
- Implementation of test in situ
- Data interpretation

Layout of double packer system

Upper Interval

Test interval

Bottom Interval





Double Packer



Shut-in Tool

主要设备

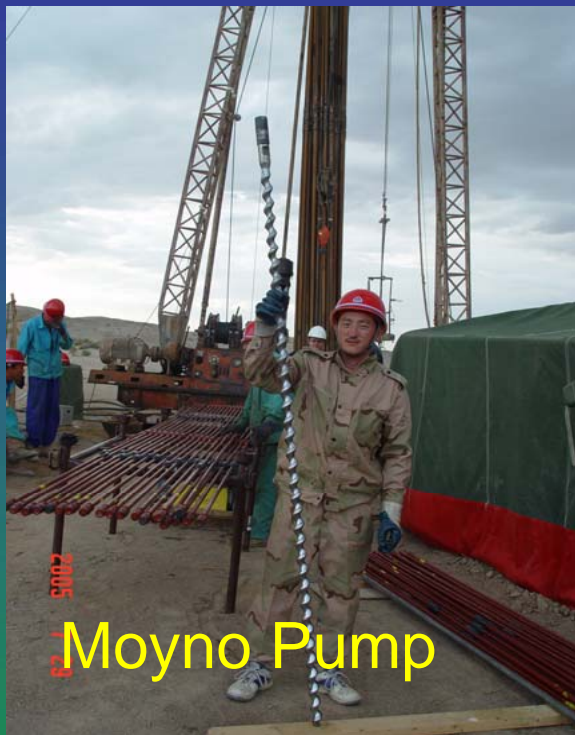


Pressure Transducer



Calibration tool

主要设备





Magnetic Flow meter



Data acquisitions system

表 2-2 BS03 钻孔水文地质试验设计

试验 编号	上栓塞下 封隔点 (m)	下栓塞上 封隔点 (m)	试验段 长度 (m)	试验 目的	试验 方法	备 注
1	144.23	157	12.77	W、T/K、H、G	S、C、R	
2	126.25	139.02	12.77	T/K、H	S、P、I	
3	95.26	108.03	12.77	T/K、H	S、P、I	
4	108.26	121.03	12.77	T/K、H	S、P、I	
5	160	172.77	12.77	T/K、H	S、P、I	
6	172.77	185.54	12.77	T/K、H	S、P、SS	
7	182.26	195.03	12.77	T/K、H	S、P、I	
8	196	208.77	12.77	T/K、H	S、P、I	
9	208.51	238.51	30.00	W、T/K、H、G	S、C、R	
10	238.26	253.47	15.21	T/K、H	S、P、I	
11	253.26	268.47	15.21	T/K、H	S、P、I	
12	268.26	283.47	15.21	T/K、H	S、P、I	
13	283.26	298.47	15.21	T/K、H	S、P、I	
14	298.53	313.735	15.21	T/K、H	S、P、I	
15	313.26	328.26	15.21	T/K、H	S、P、I	
16	328.26	343.465	15.21	T/K、H	S、P、I	
17	430.51	445.72	15.21	W、T/K、H、G	S、C、R	
18	473.51	488.72	15.21	W、T/K、H、G	S、C、R	
19	343.51	358.72	15.21	T/K、H	S、P、I	
20	358.51	373.72	15.21	T/K、H	S、P、I	
21	373.51	388.72	15.21	T/K、H	S、P、I	
22	391.51	406.72	15.21	T/K、H	S、P、I	
23	406.51	421.72	15.21	T/K、H	S、P、I	
24	416.79	432	15.21	T/K、H	S、P、I	
25	448.01	463.22	15.21	T/K、H	S、P、I	
26	458.26	473.47	15.21	T/K、H	S、P、I	



Installation

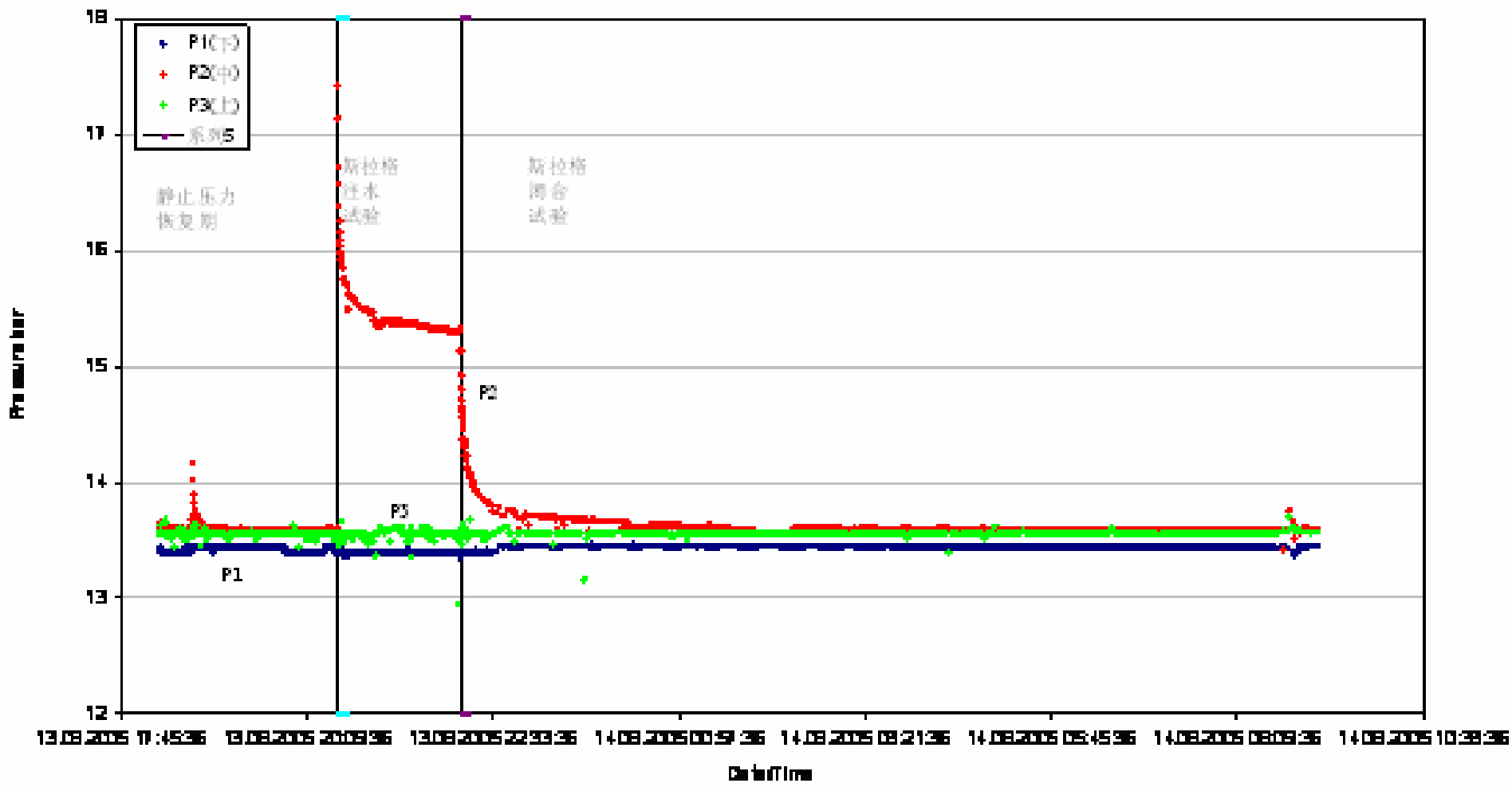


Installation

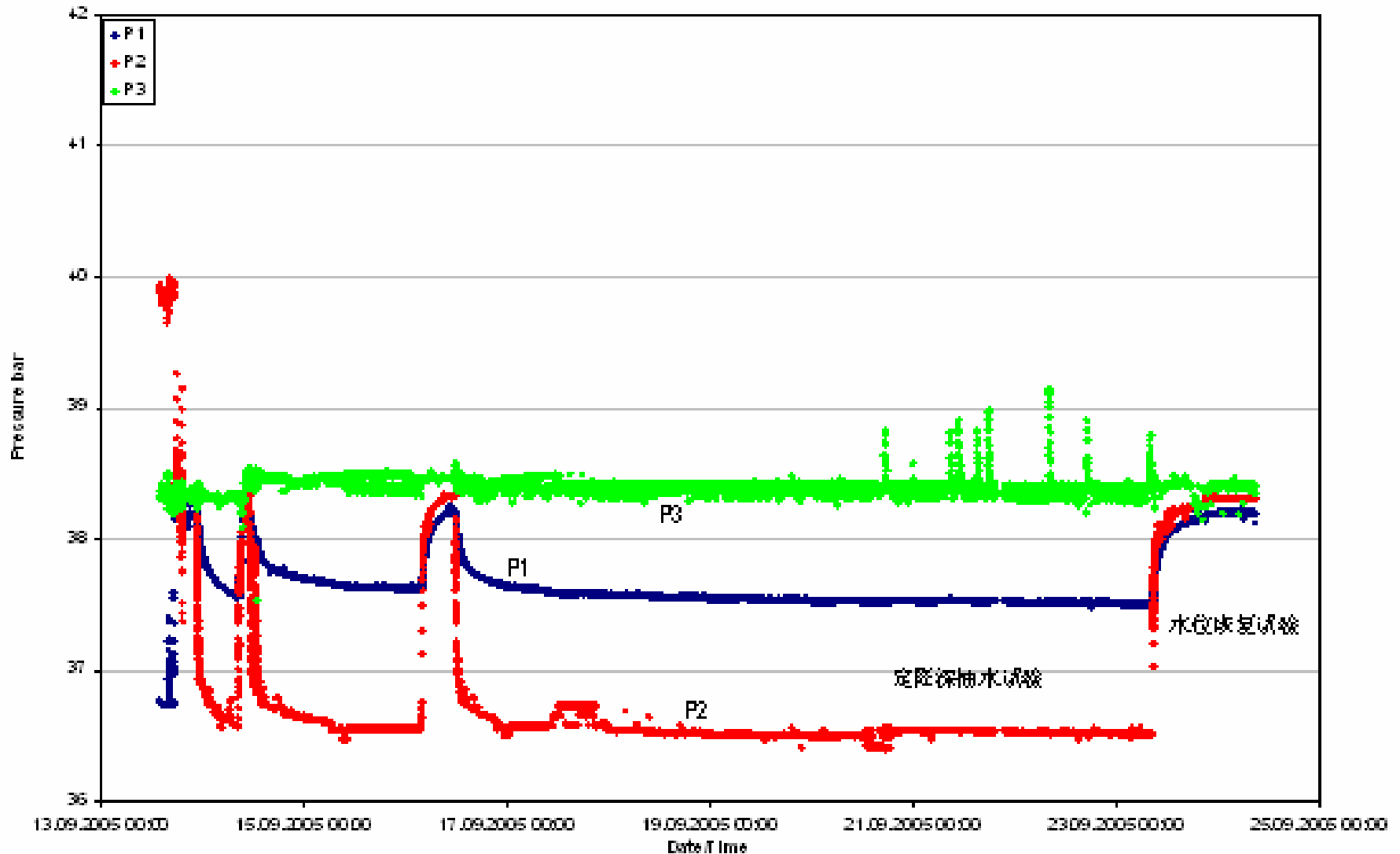




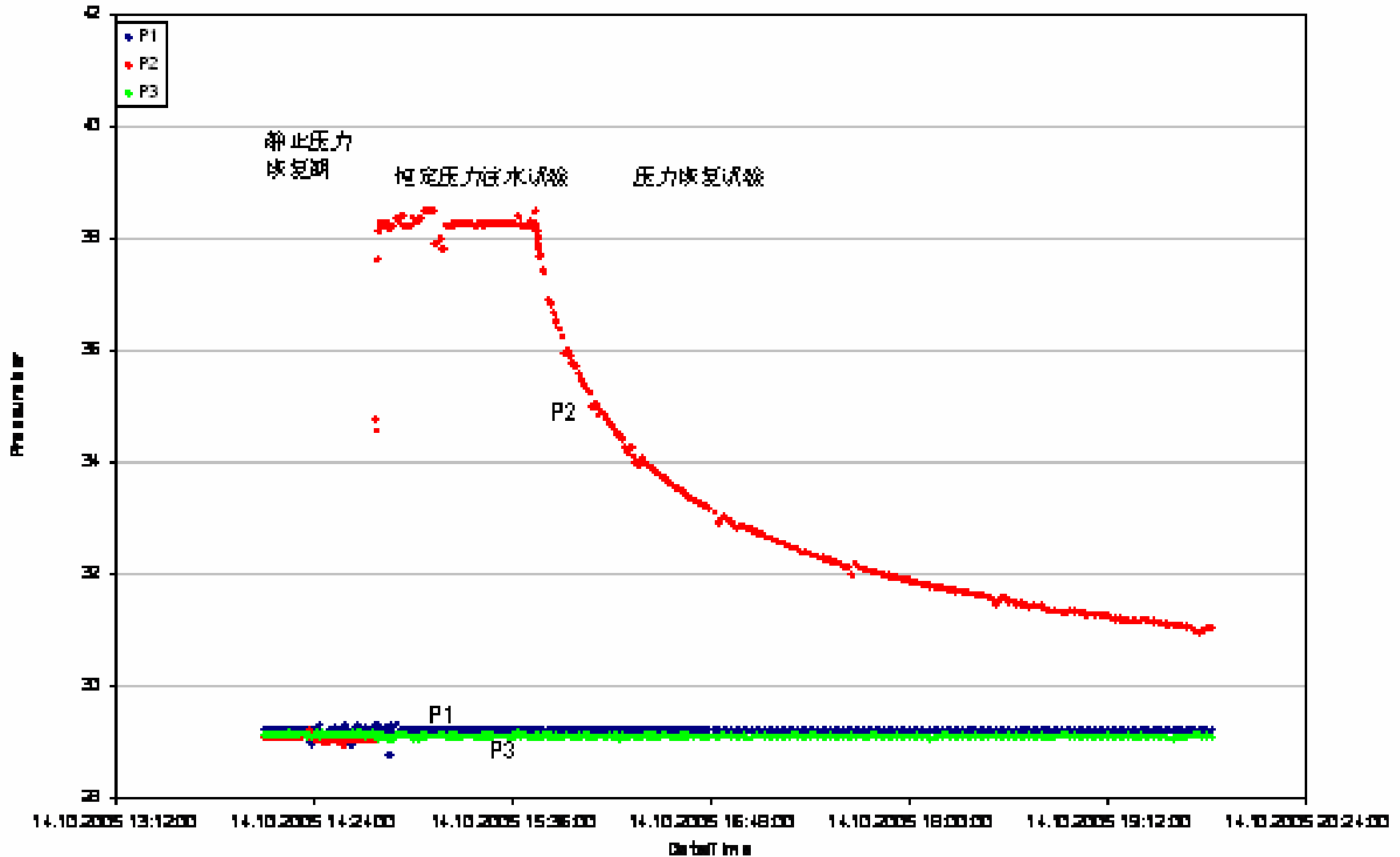
Data Response Curve—Shut-in Slug T.



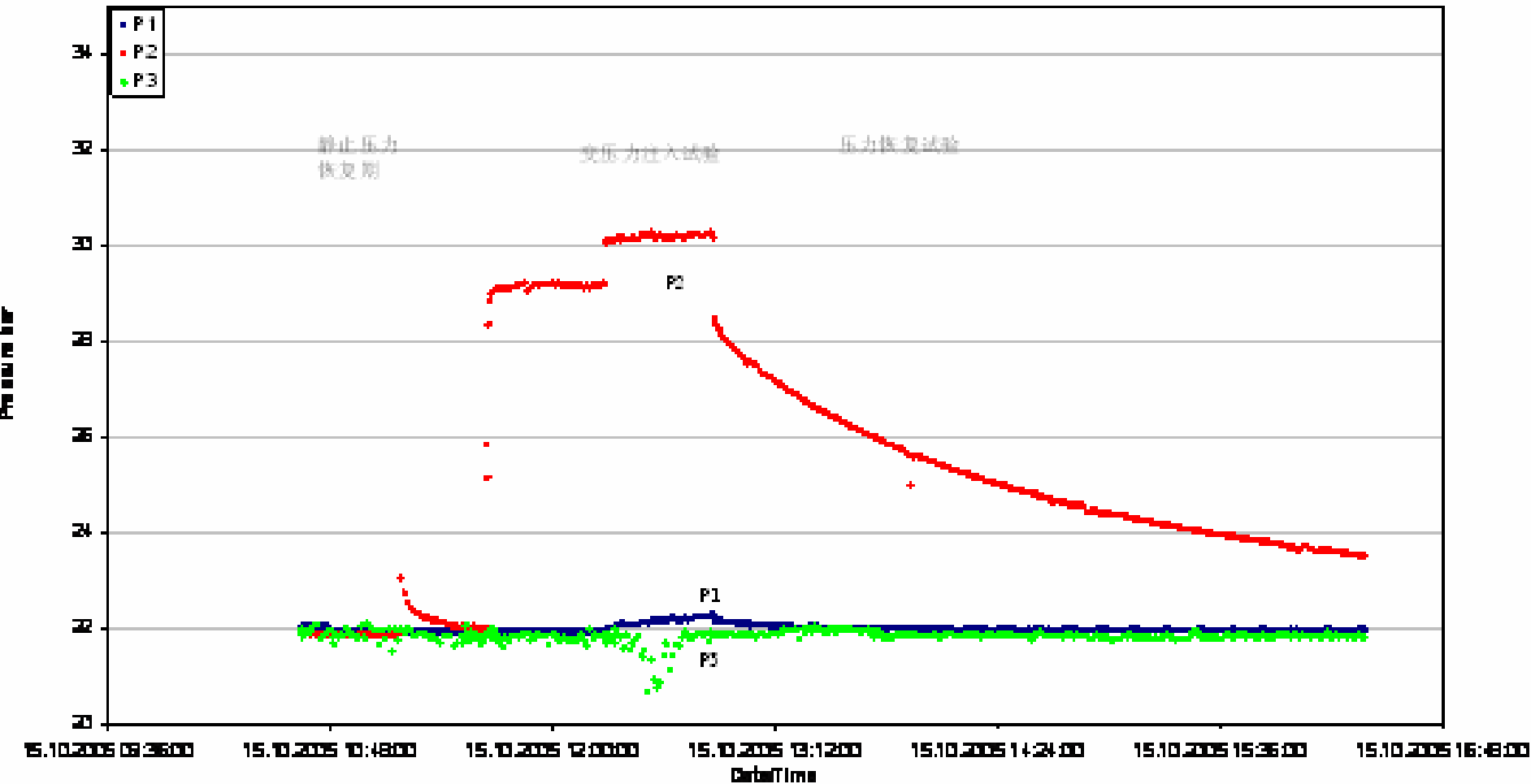
Data Response Curve—Pumping T.

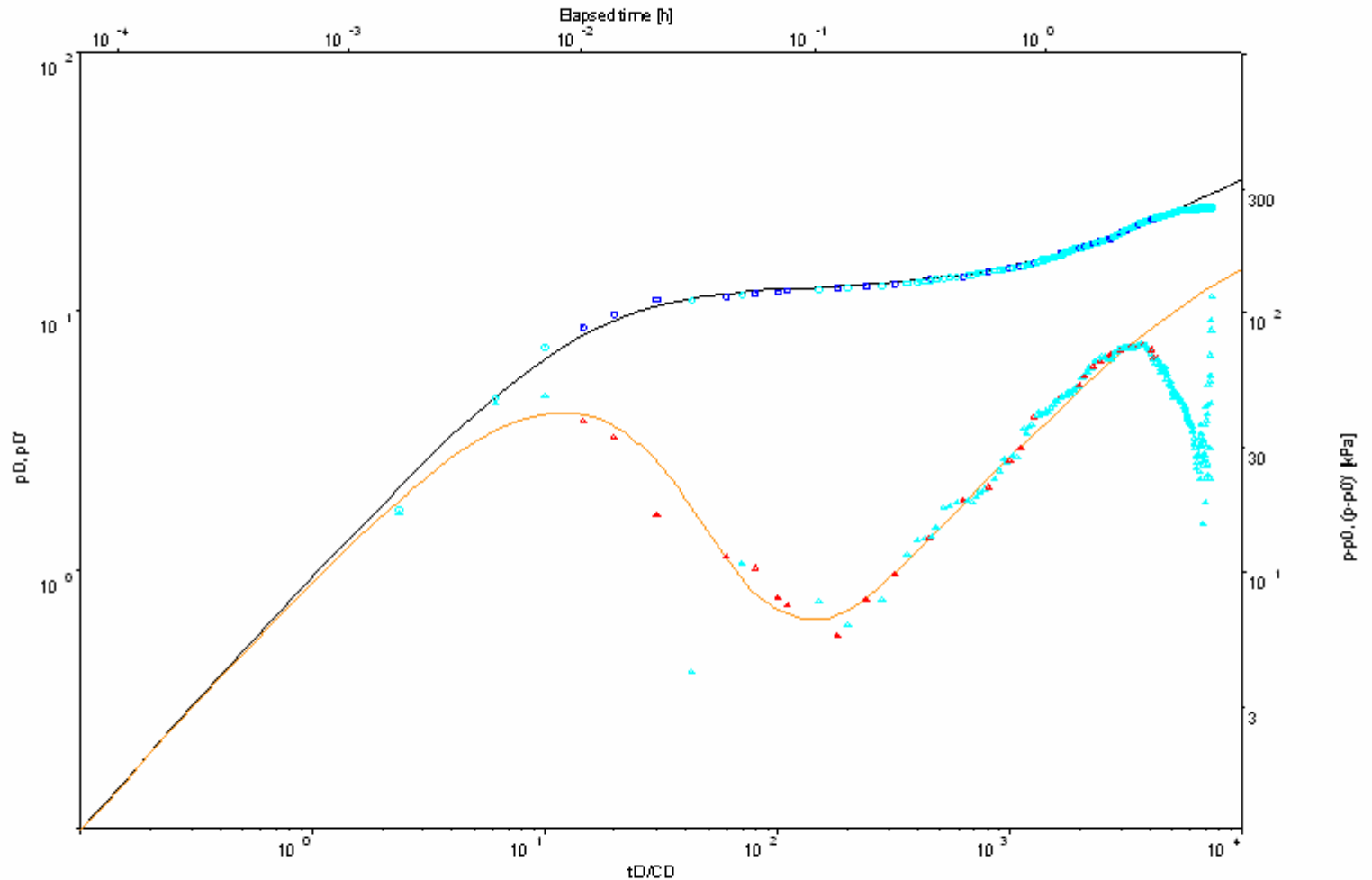


Data Res. Curve—Water Injection T.



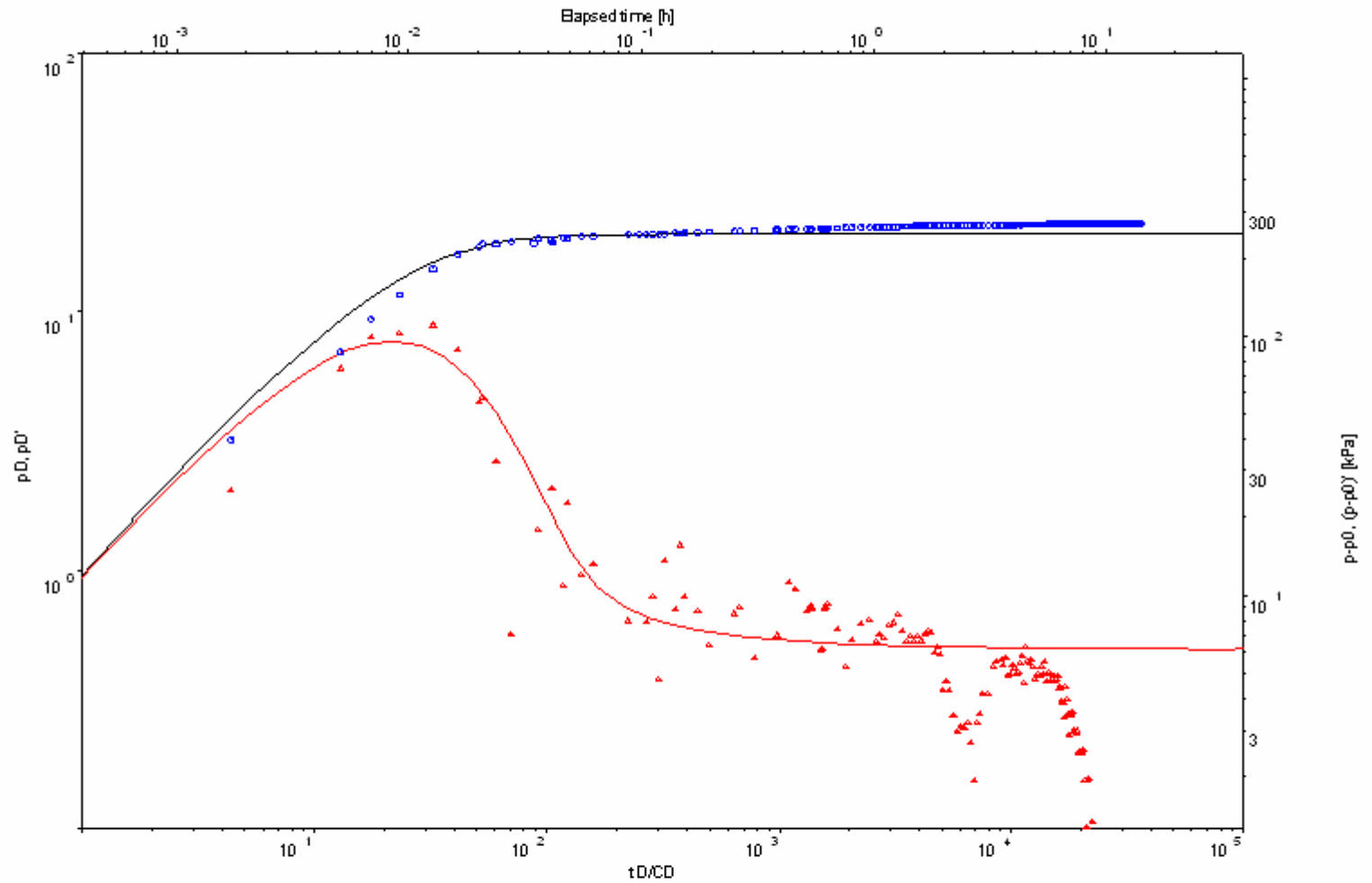
Data Response Curve—Variable Head T.





FLOW MODEL : Two shell composite
 BOUNDARY CONDITIONS: Constant rate
 WELL TYPE : Source
 SUPERPOSITION TYPE: No superposition
 PLOT TYPE : Log-log

T	3.46E-05	m ² /s
S	1.88E-10	-
C	5.54E-08	m ³ /Pa
n1	2.00E+00	-
n2	2.00E+00	-
rD1	3.53E+05	-
brw	2.25E+01	-

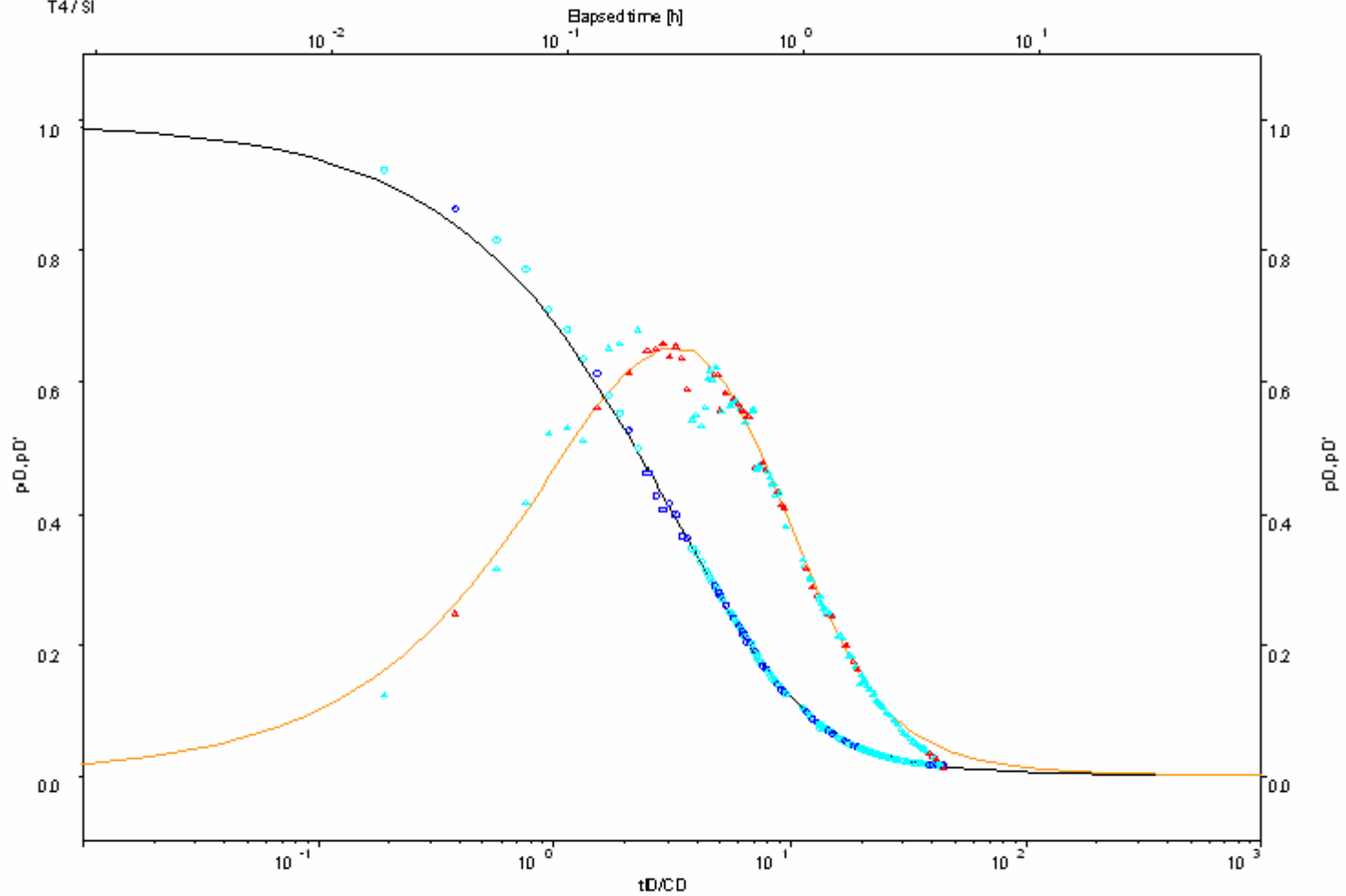


FLOW MODEL : Homogeneous
 BOUNDARY CONDITIONS: Constant rate
 WELL TYPE : Source
 SUPERPOSITION TYPE : Build-up TC
 PLOT TYPE : Log-log

C=	2.55E-08	m ³ /Pa
T=	2.83E-05	m ² /s
S=	1.73E-17	-
s=	0.00E+00	-
n=	2.00E+00	-

Beishan
T4 / S1

Flow Dim Version 2.14b
(c) Golder Associates

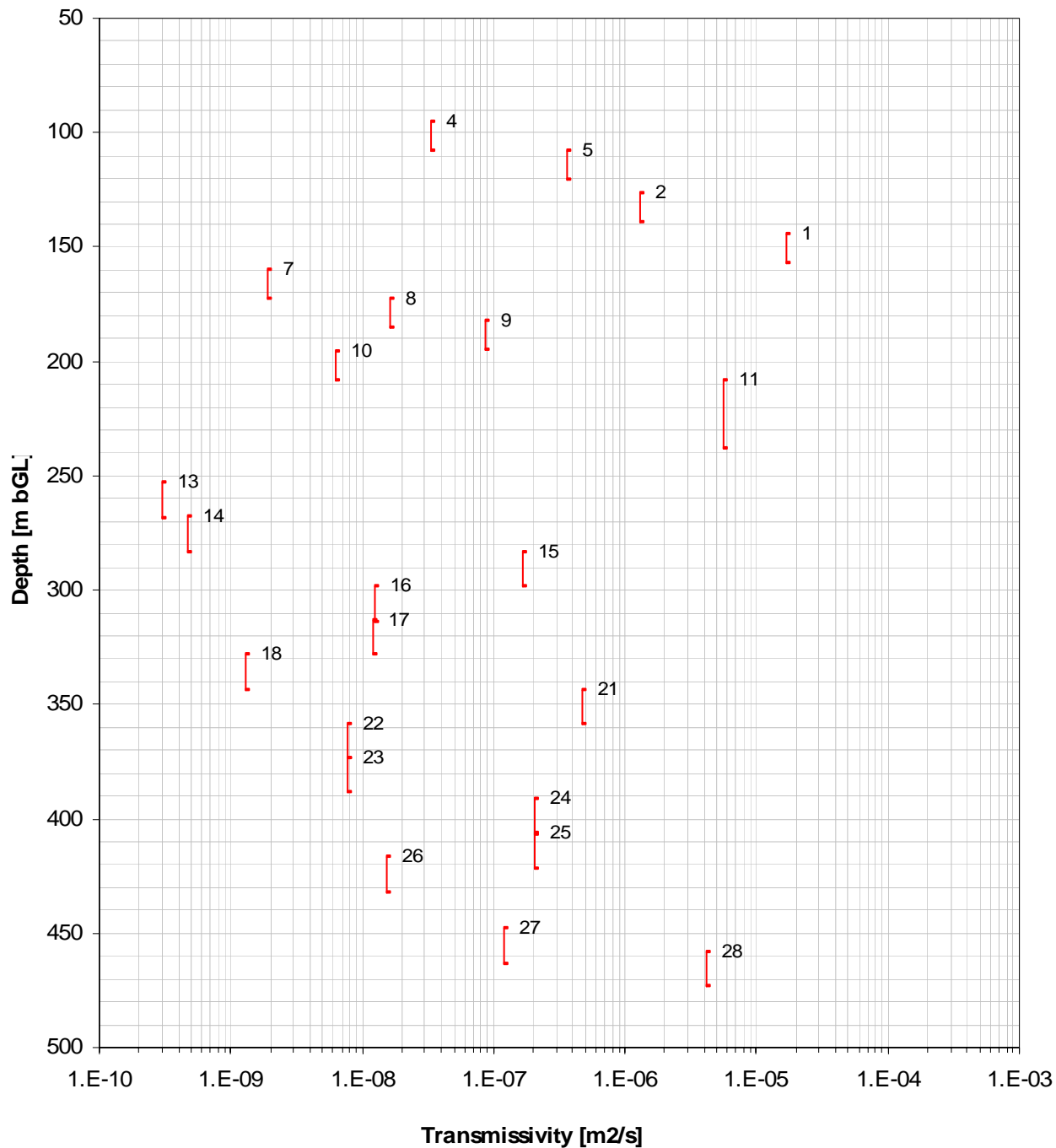


FLOW MODEL : Two shell composite
BOUNDARY CONDITIONS: Slug/pulse
WELL TYPE : Source
SUPERPOSITION TYPE: No superposition
PLOT TYPE : RameyA

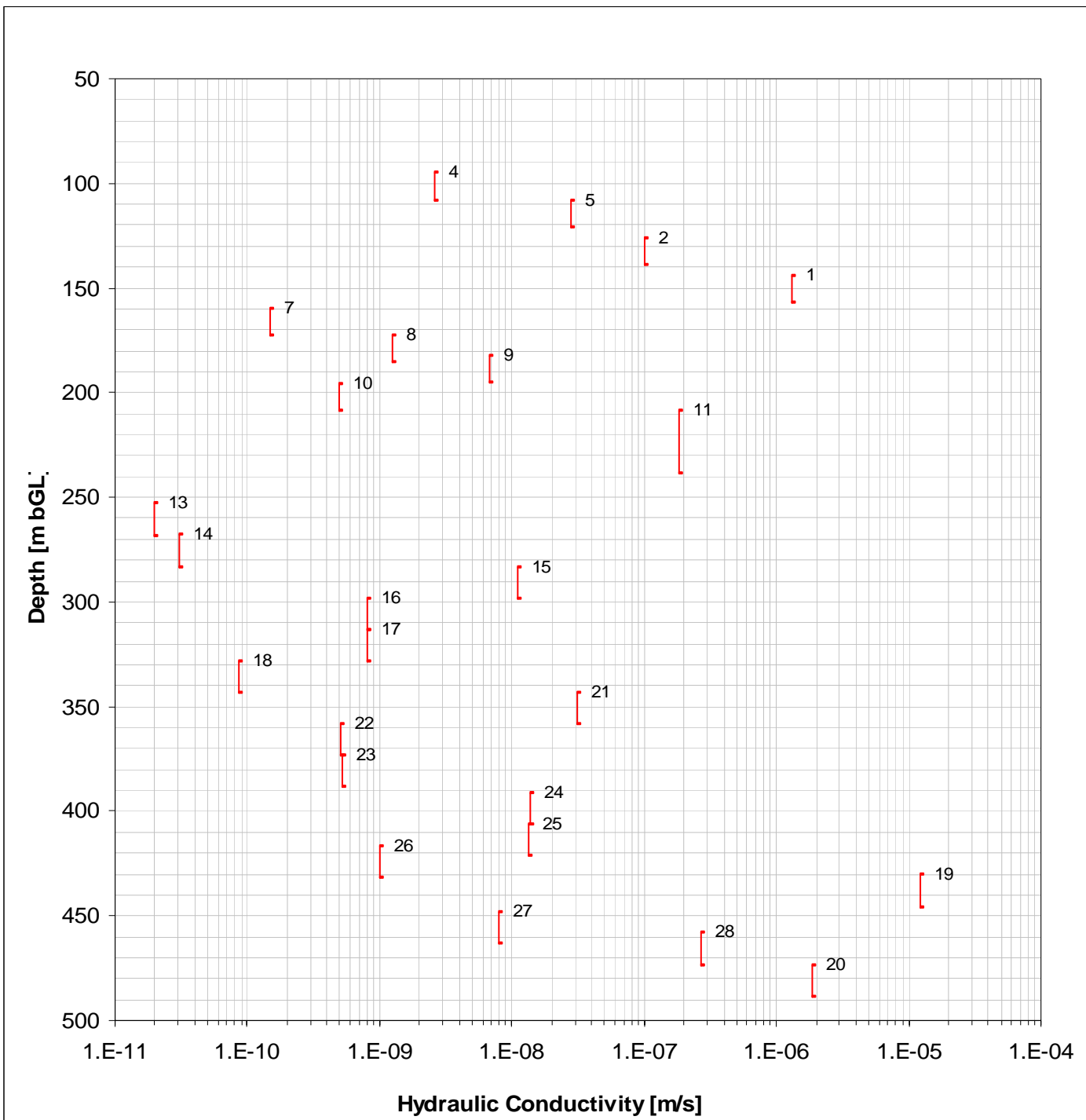
T	9.93E-07	m2/s
S	1.30E-02	-
C	2.00E-07	m3/Pa
n1	2.00E+00	-
n2	2.00E+00	-
rD1	2.50E+03	-
brw	1.50E-01	-

- Drilling campaign: 2003-9
- Test campaign: 2005-7-26~10-16
- Range of depth: 95m-489m
- Test intervals: 12.77m, 15.21m, 30m
- Test approaches: Slug test; Shut-in slug test; Pulse test; Constant discharge/Withdrawal test; Water injection test and recovery test.
- Water sampling: 144m-156.77m、208m-238m、430.51m-445.72m

95m-489m, Transmissivity Profile in BS03



95m-489m, Hydraulic Conductivity Profile in BS03





China-Germany Workshop on Management of Radioactive Waste 2007

THANK YOU FOR
YOUR ATTENTION



Chinese-German Workshop on Radioactive Waste Disposal

Radioactive Waste Disposal in Various Host Rock Formations –
Geomechanical Aspects (**Selected Applications**)

O. Czaikowski

Sino-German Science Center, Beijing
May 28-31, 2007

Contents

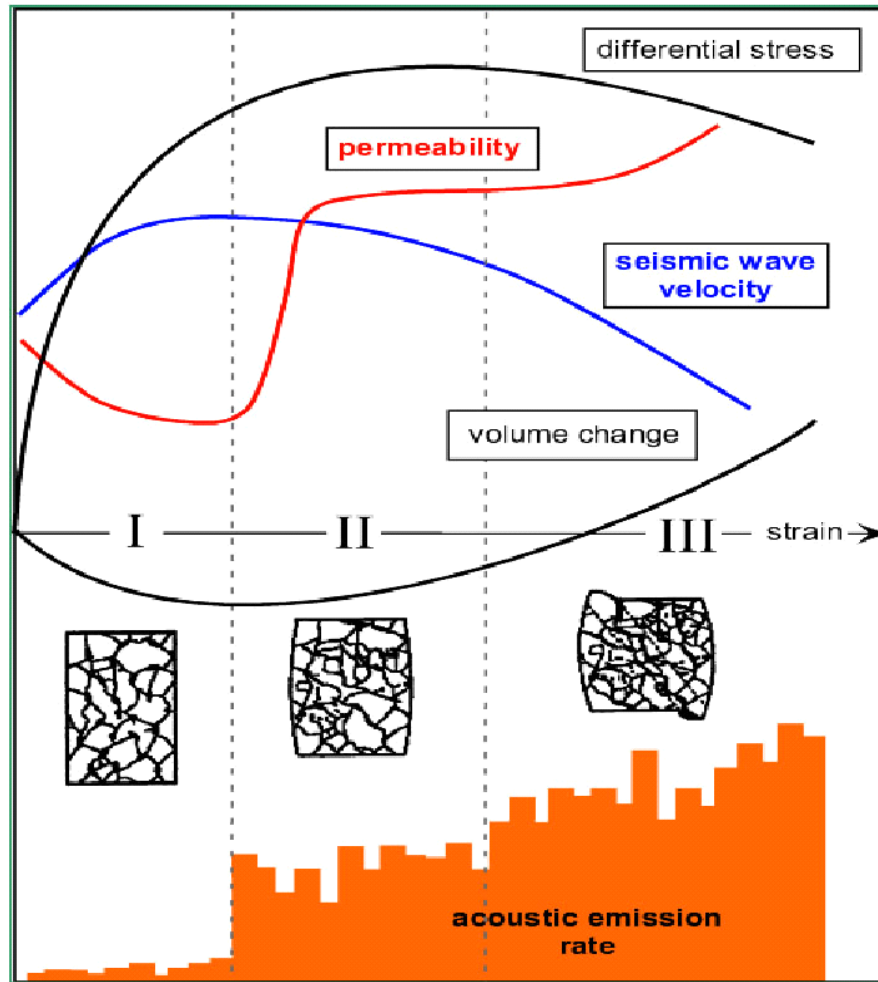
- Demonstration of Safety / General Aspects
- Waste Properties
- Site Selection
- Physico-chemical Modelling / Coupled Processes
- Thermo-Mechanical – Hydraulic Aspects
- **Some Aspects with respect to change of mechanical / hydraulic properties**
 - Nearfield processes/EDZ
 - Damage process – rock salt
 - Damage process – claystone
 - Recreation of damage/Rehealing – rock salt
 - Damage process – granite
lab investigations
 - Some preliminary calculations with respect to static stability /
EDZ evolution - granite
- The Best Repository
- Conclusions



- Some Aspects with respect to change of mechanical / hydraulic properties
 - *Nearfield processes/EDZ*
 - *Damage process – rock salt*
 - *Damage process – claystone* → presentation
O. Czaikowski
 - *Recreation of damage/Rehealing – rock salt*
 - *Pressure-forced infiltration of fluids (liquids, gas) in primarily impermeable or nearly impermeable rock formations*
 - *Damage process - granite*



Change of Material properties with respect to fabric damage



Change of properties is used for monitoring and determination of dilatancy / damage

I - compaction

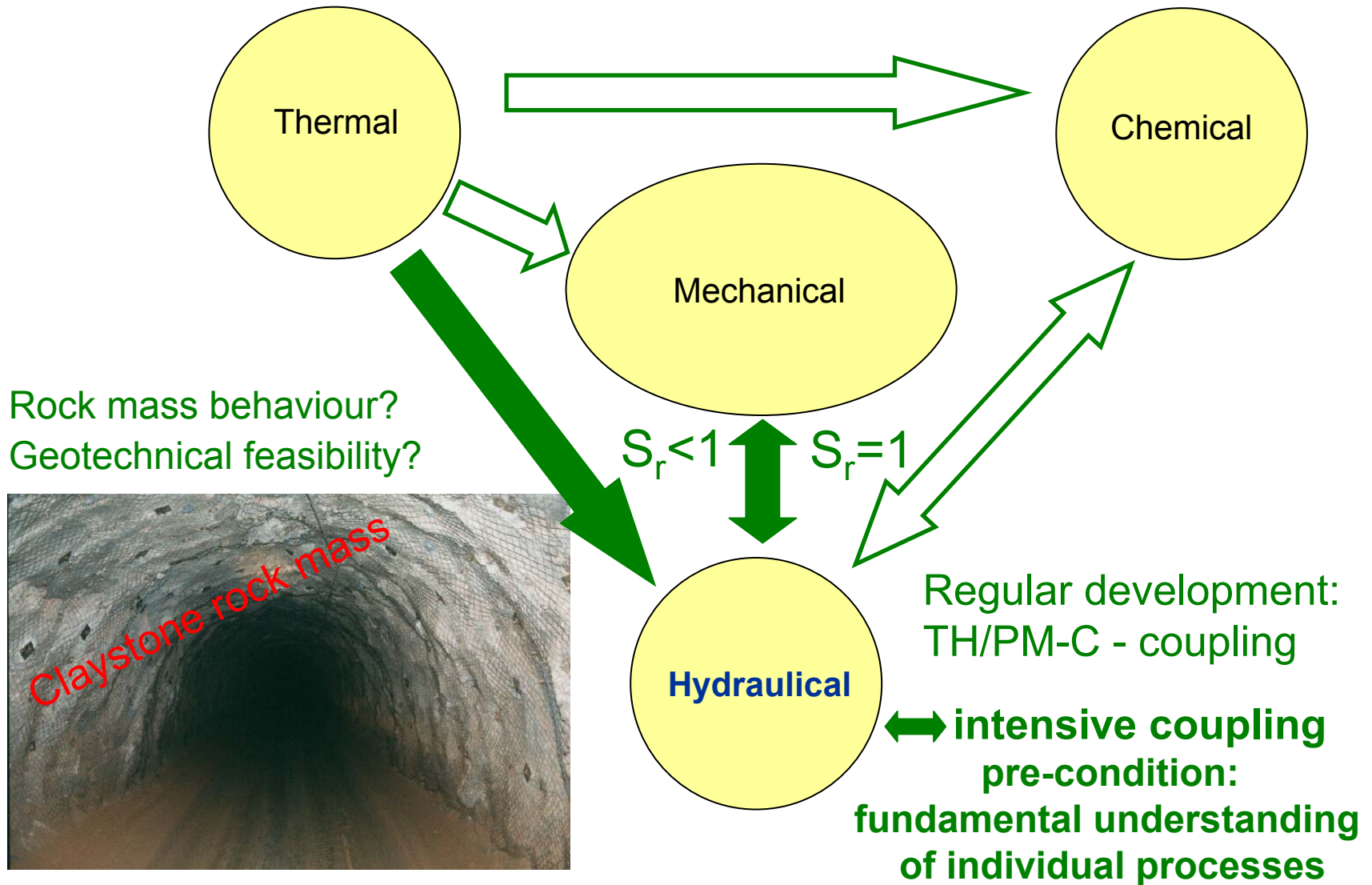
II - damage (micro)

III - rupture (macro)

BGR (2001)



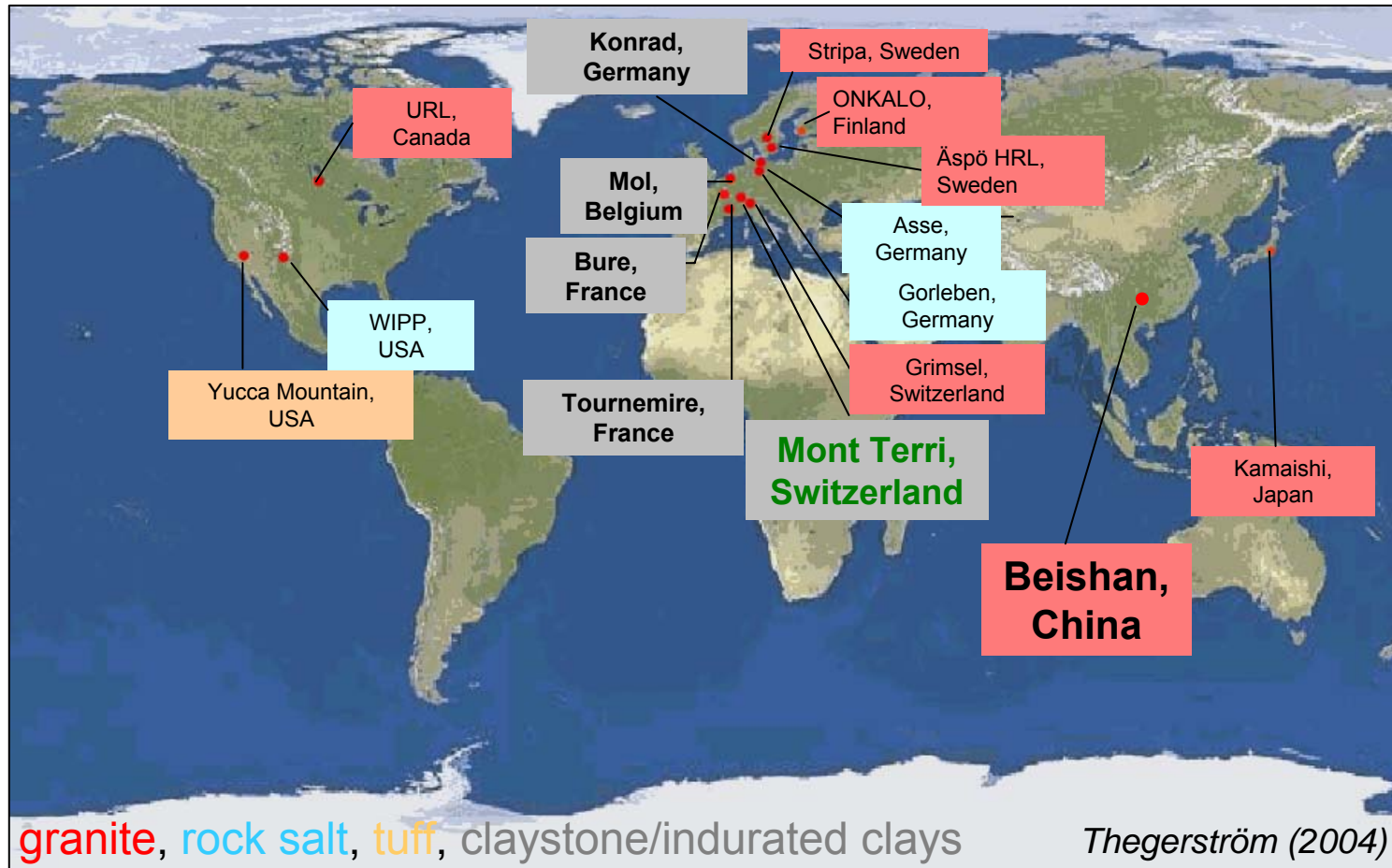
Change of Material properties with respect to saturation degree / pore water pressure



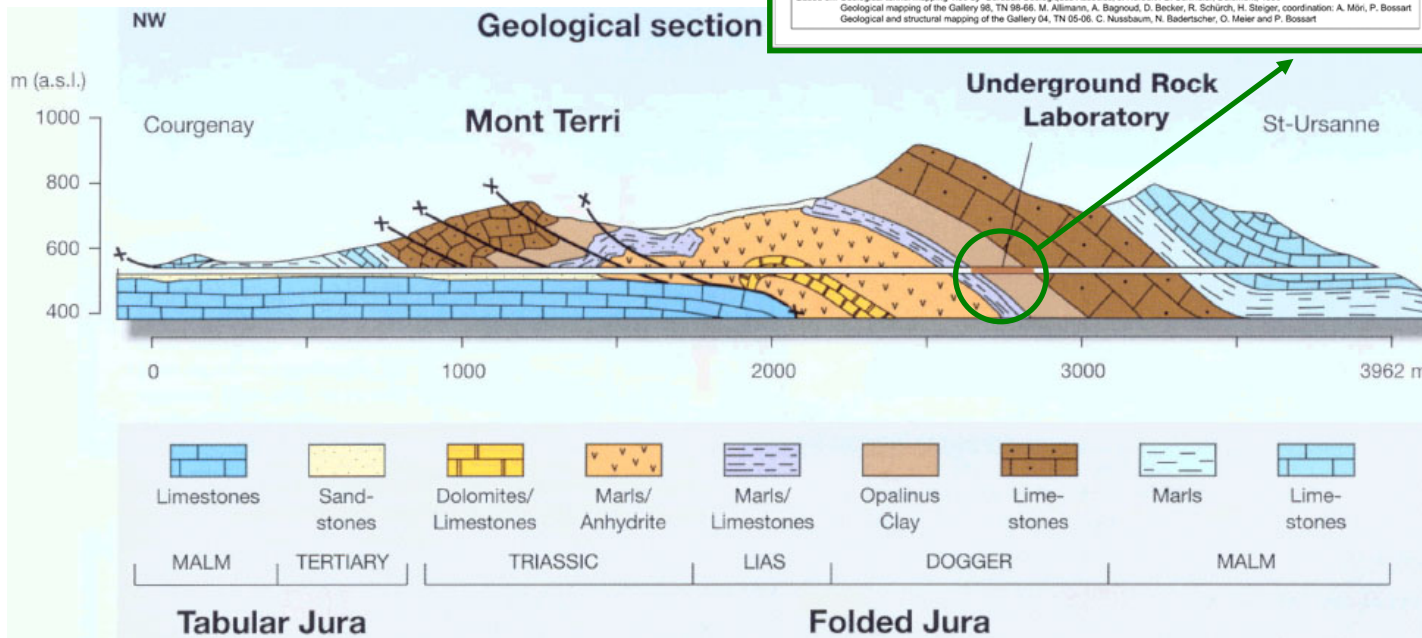
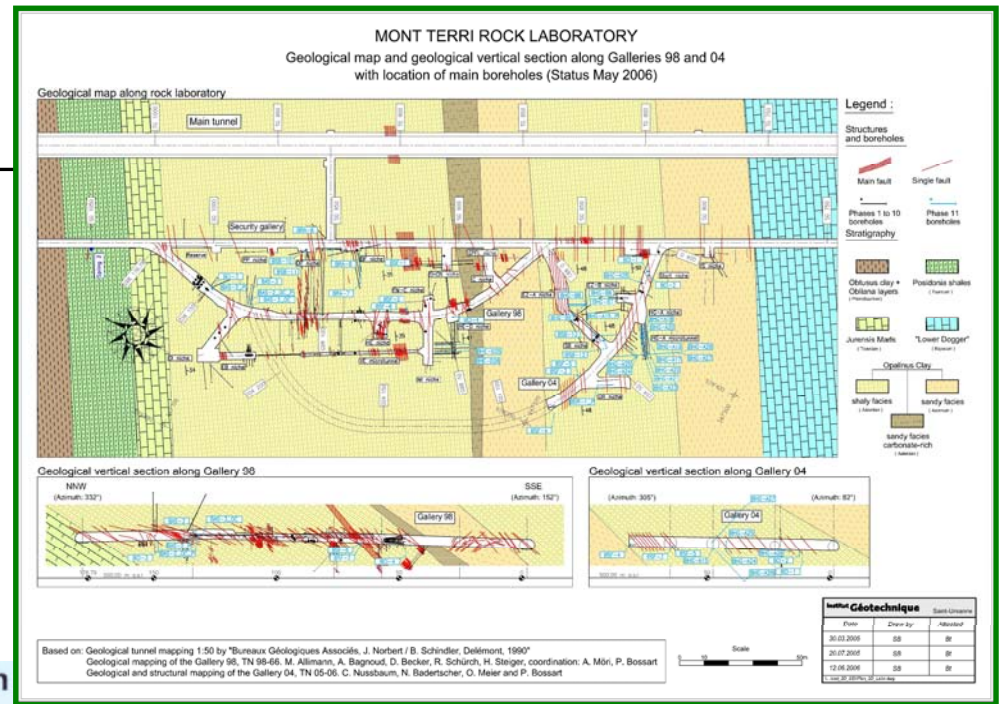
laboratory investigation on international claystone samples



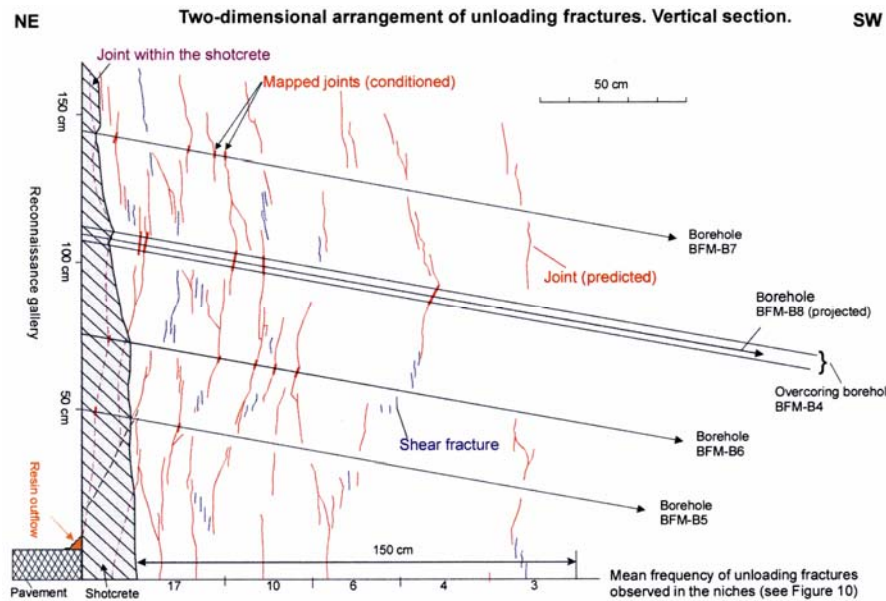
International scientific state of the art in claystone / indurated clays



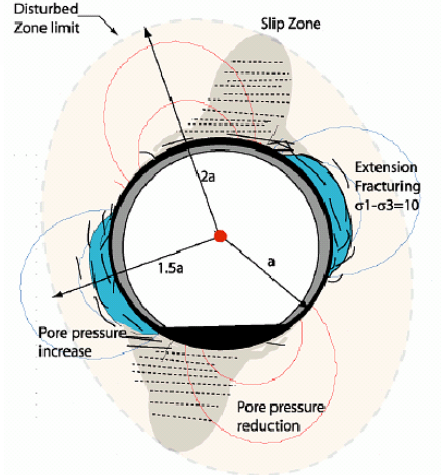
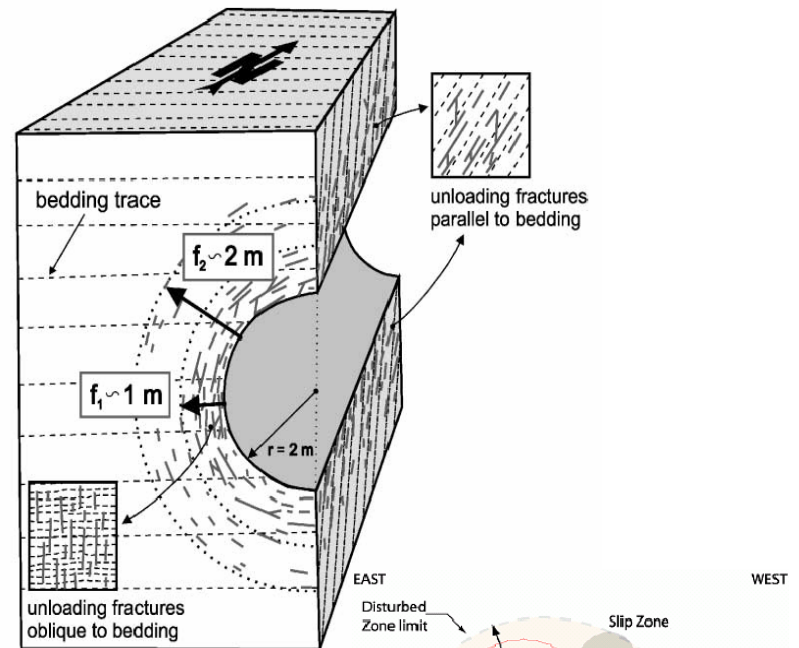
Mont Terri Site



EDZ and coupled processes



Arrangement of investigated and interpolated macro fractures, *Thury & Bossart (1999)*



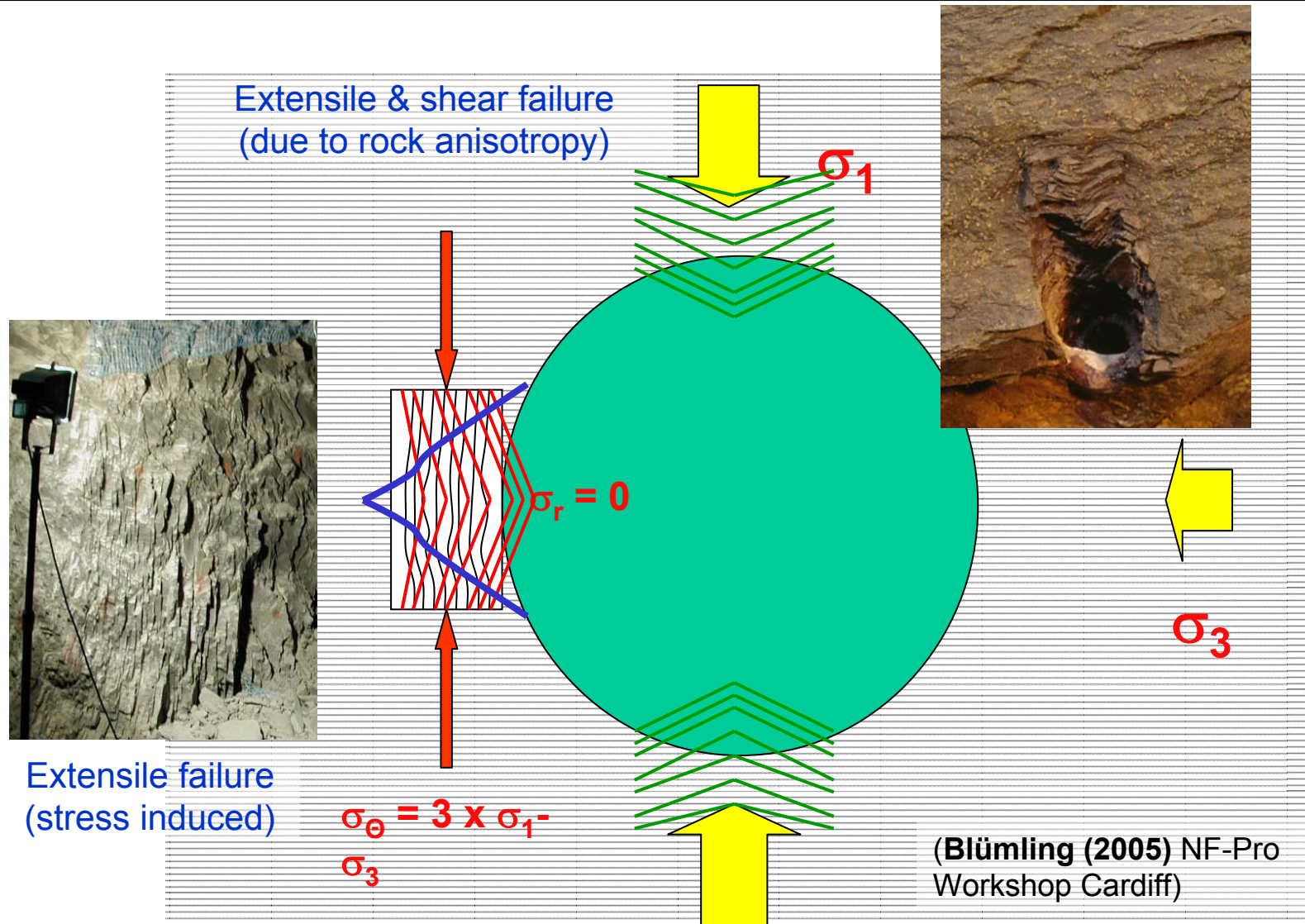
Conceptual model of the EDZ, *NAGRA NTB 02-02 und NTB 02-03 (2002)*



Contour destrengthening behind shotcrete liner



Failure process mainly dominated by bedding plane orientation



In Situ



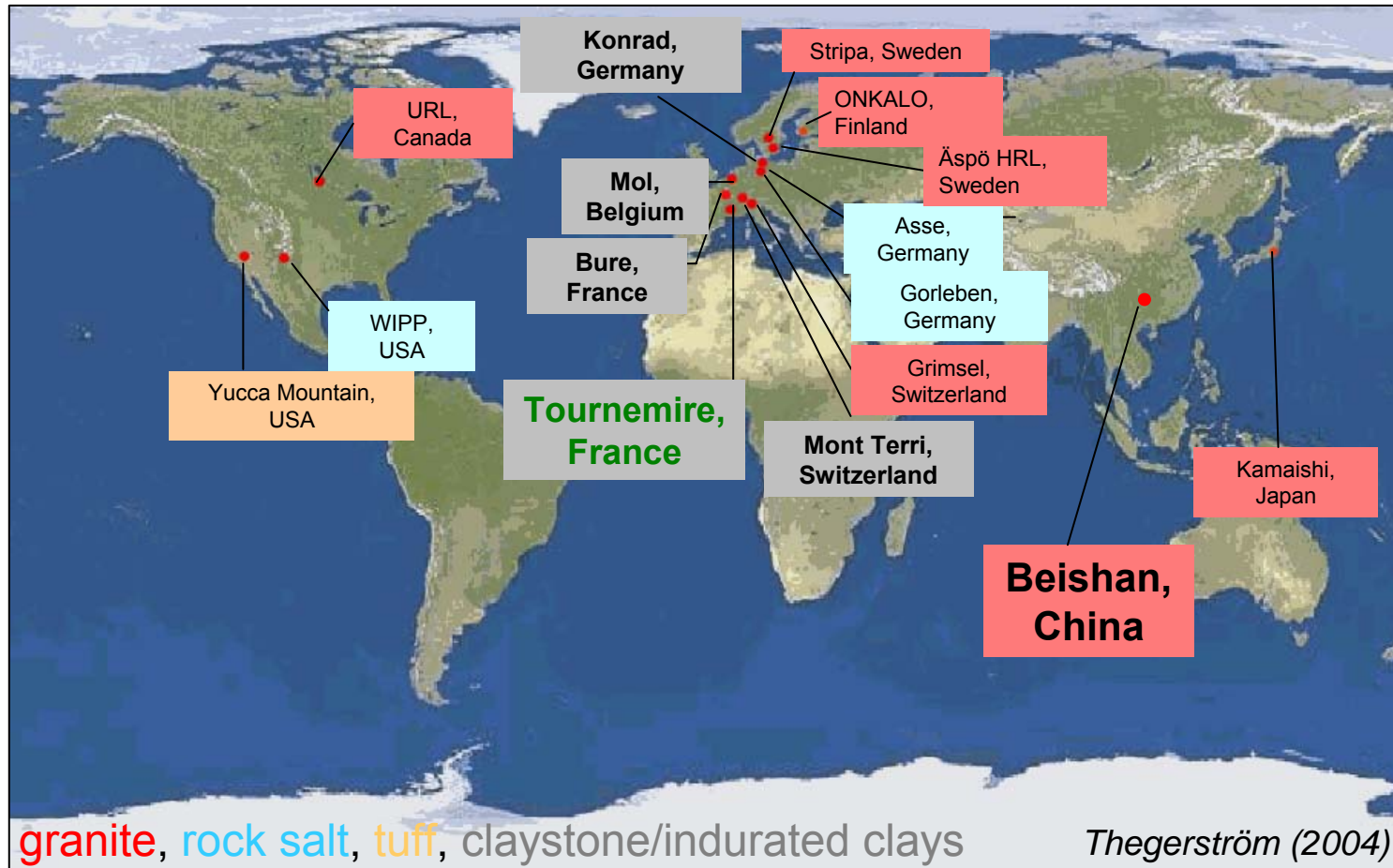
Bedding plane failure



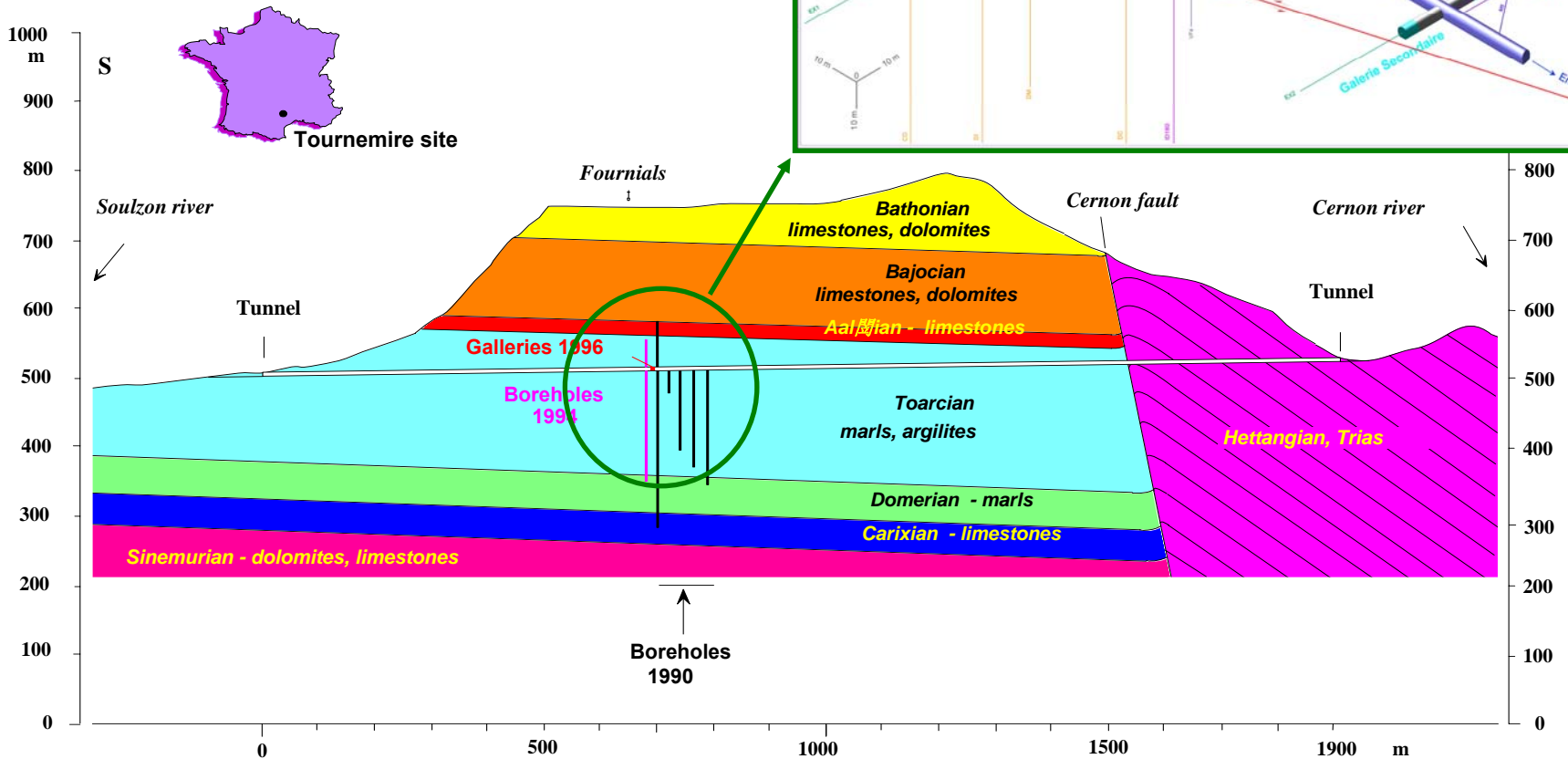
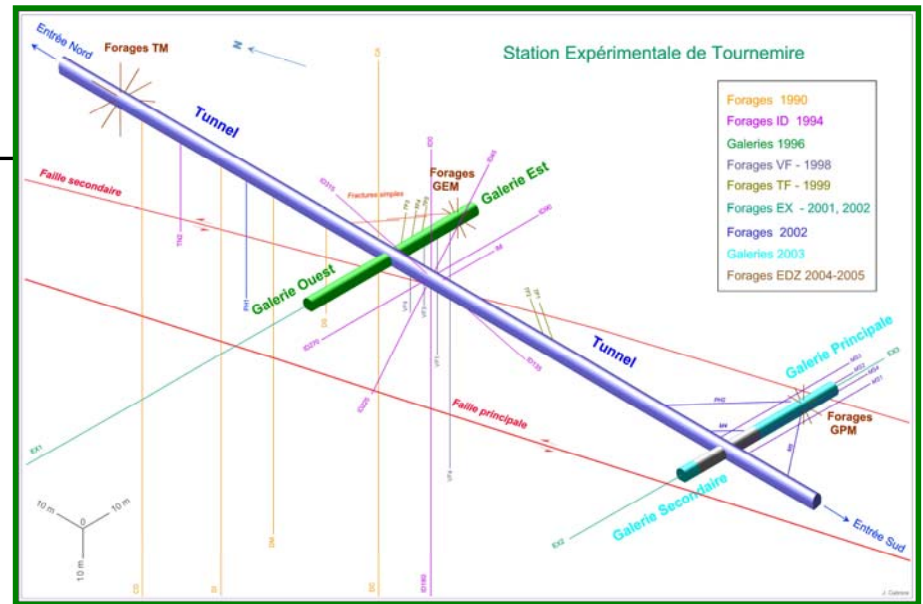
Matrix induced contour failure



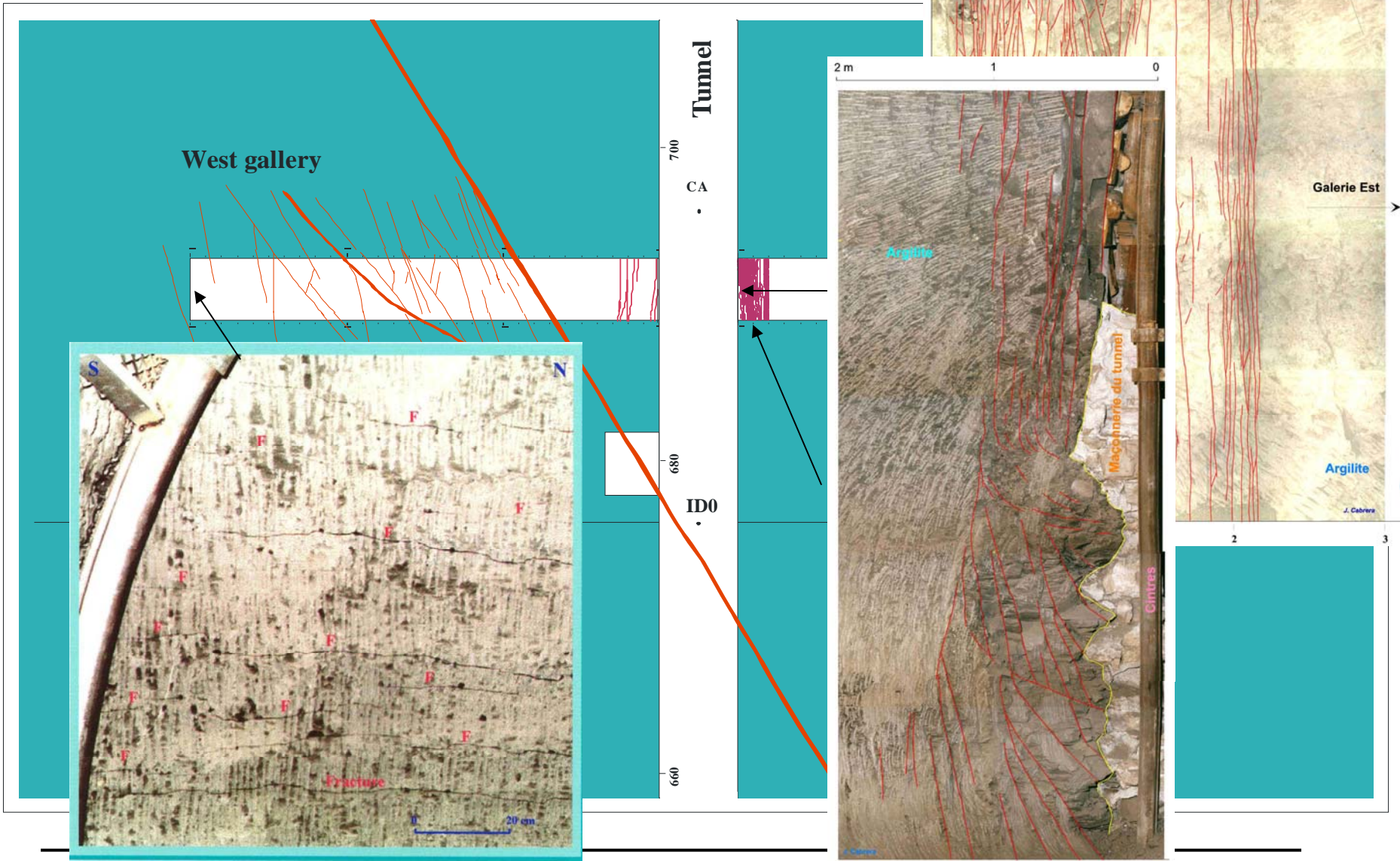
Tournemire site



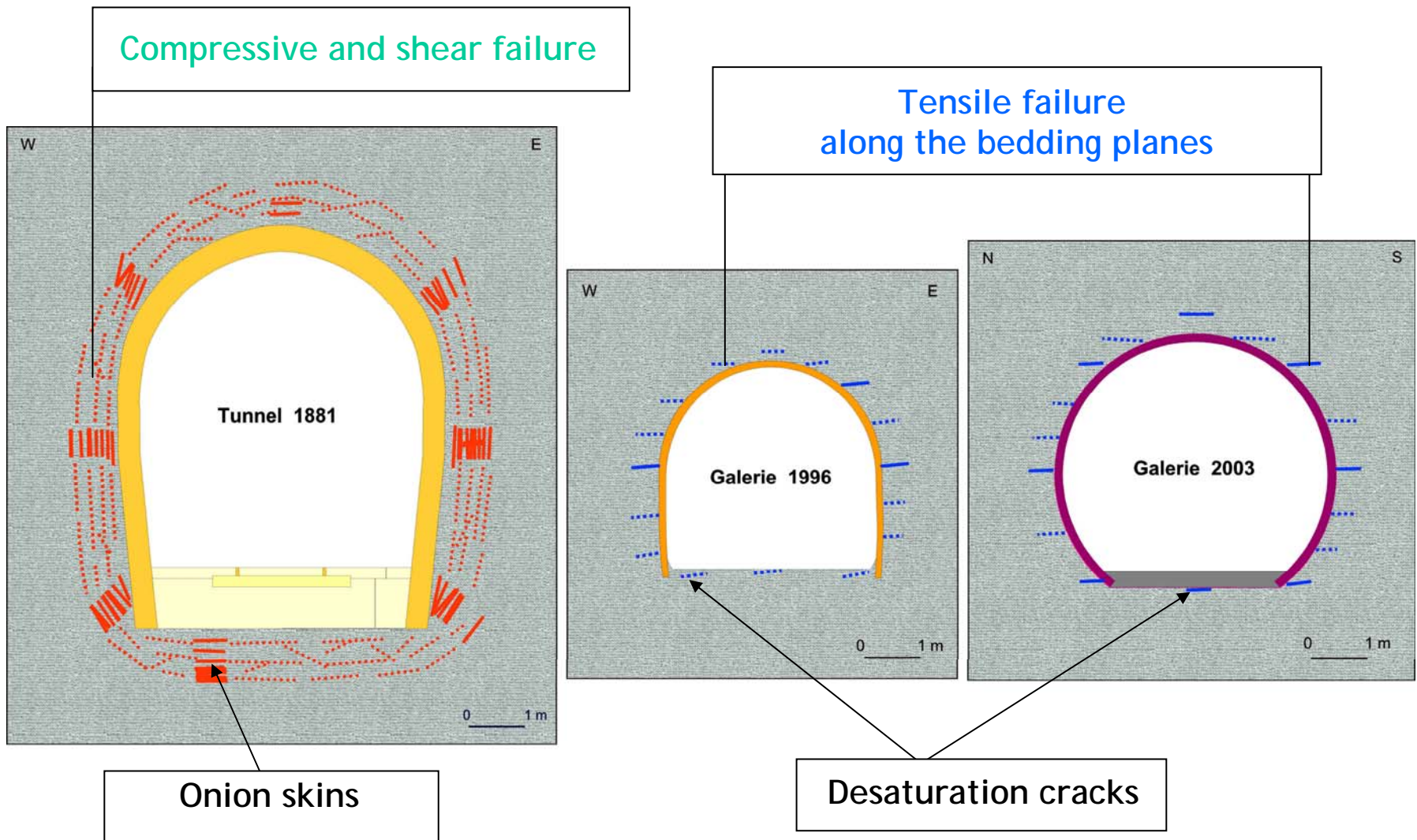
Tournemire site



In Situ Observations, *Rejeb (2006)*

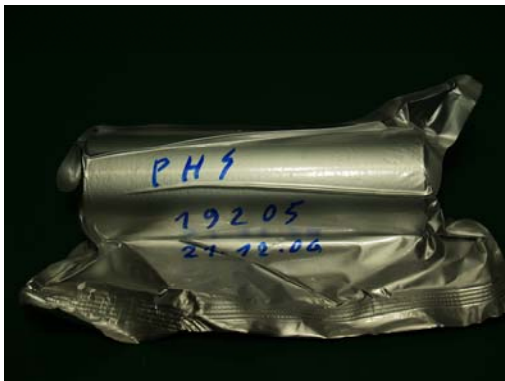
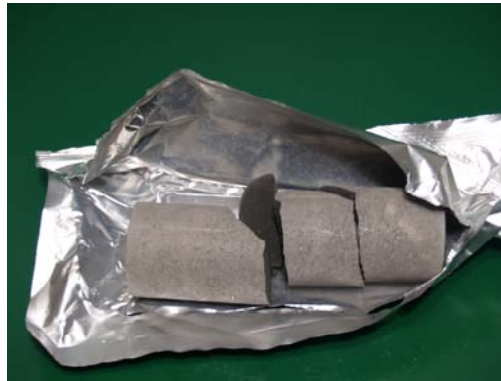


EDZ - Deferred failure around the three openings, *Rejeb (2006)*

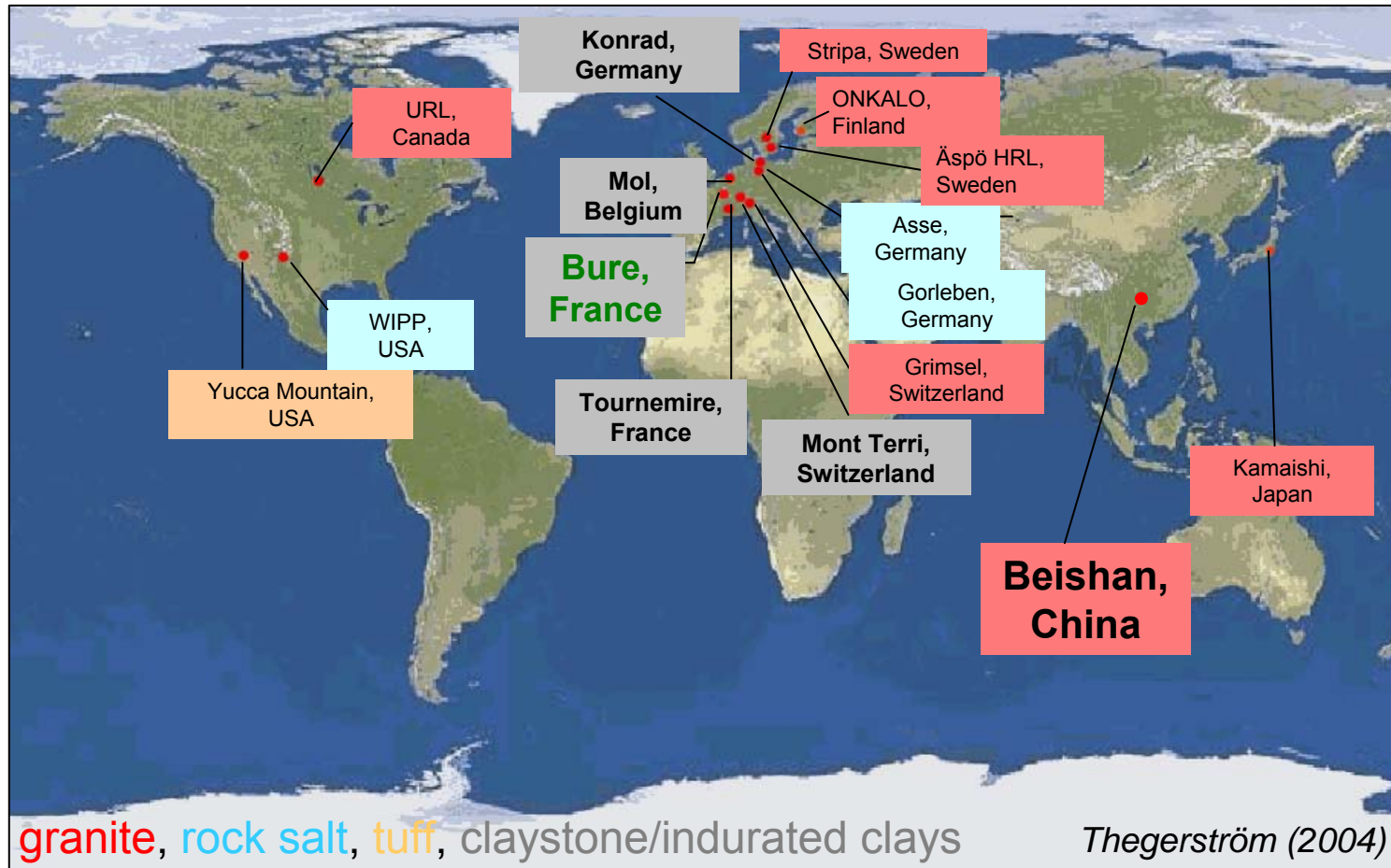


test program

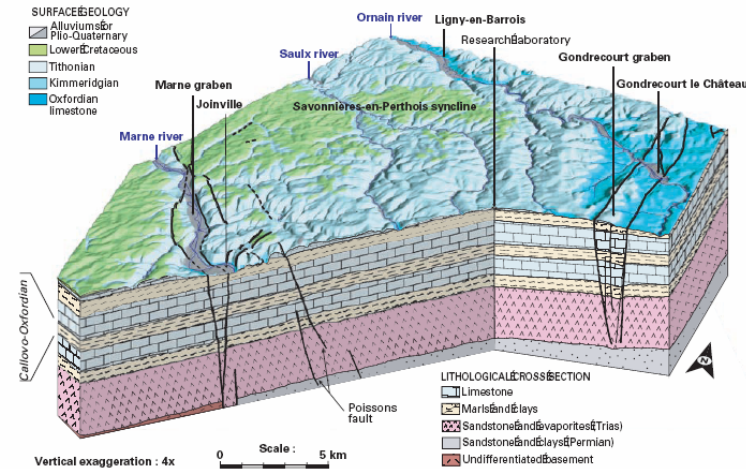
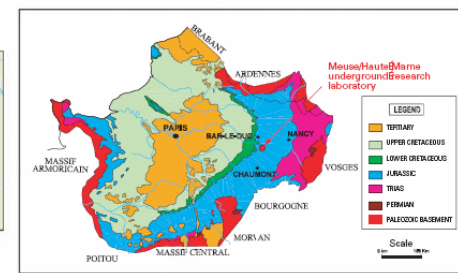
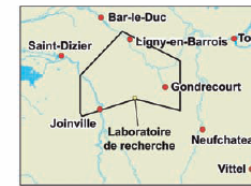
- Unfortunately most of the delivered samples were broken according to bedding plane orientation (PH4-MGM-16931 / PH4-MGM-19050).



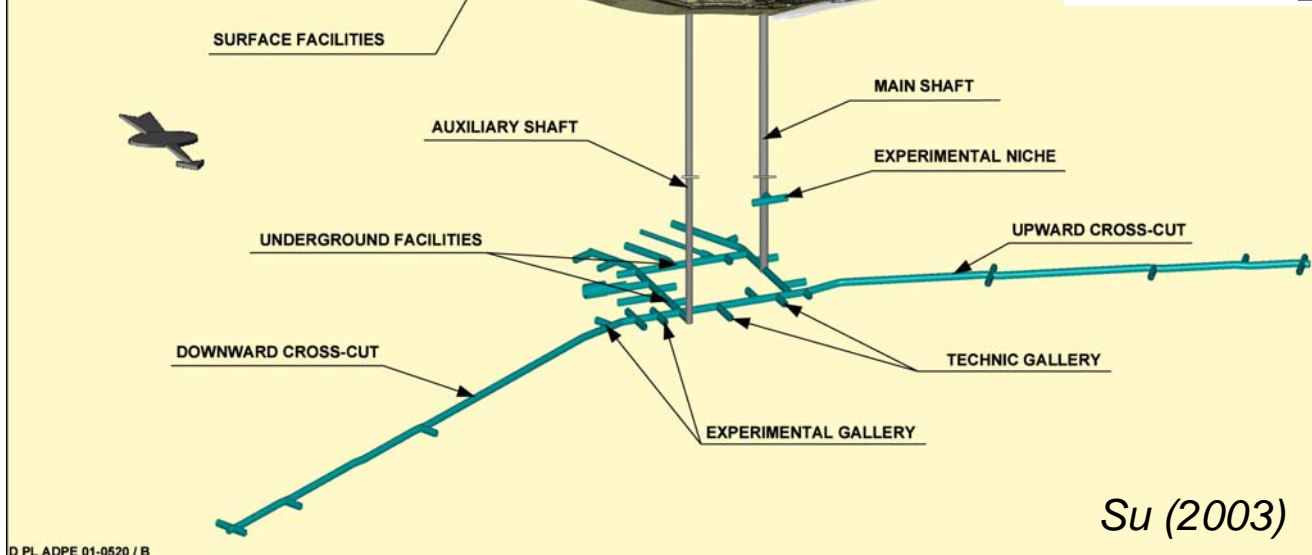
Bure site



Bure site



SURFACE FACILITIES



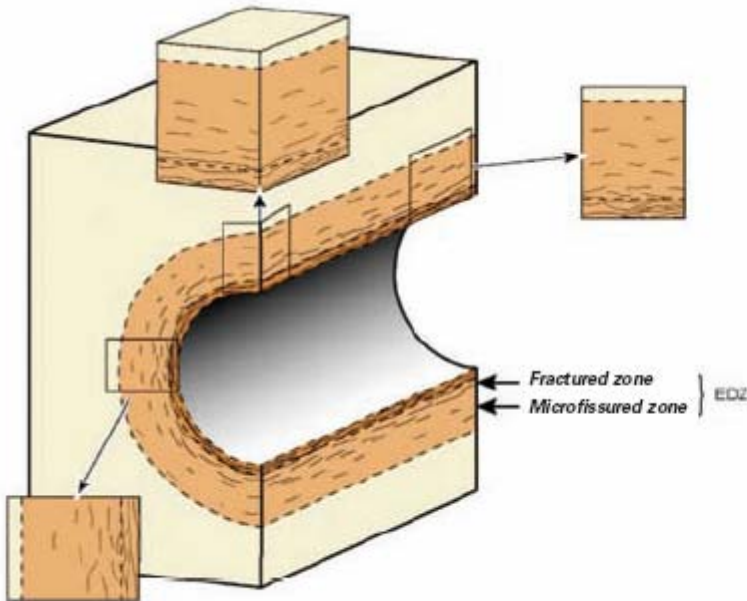
Su (2003)

D PL ADPE 01-0520 / B

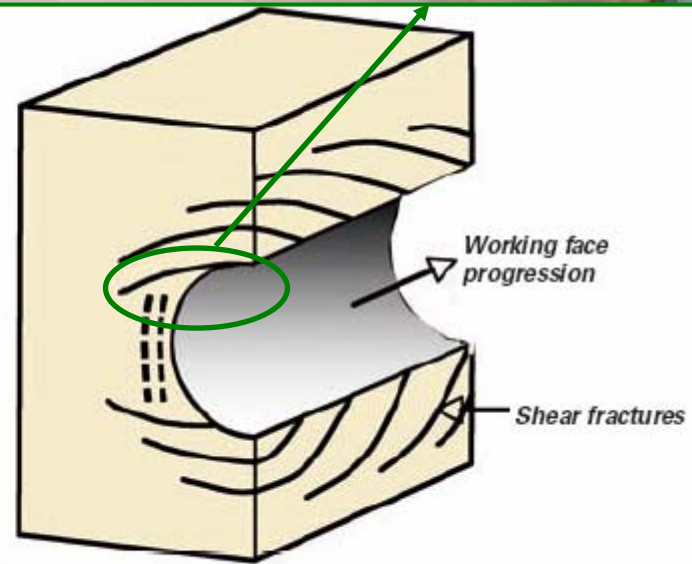
Dossier 2005



In Situ



*Current conceptual model of EDZ
(associated to wall deconfinement)*



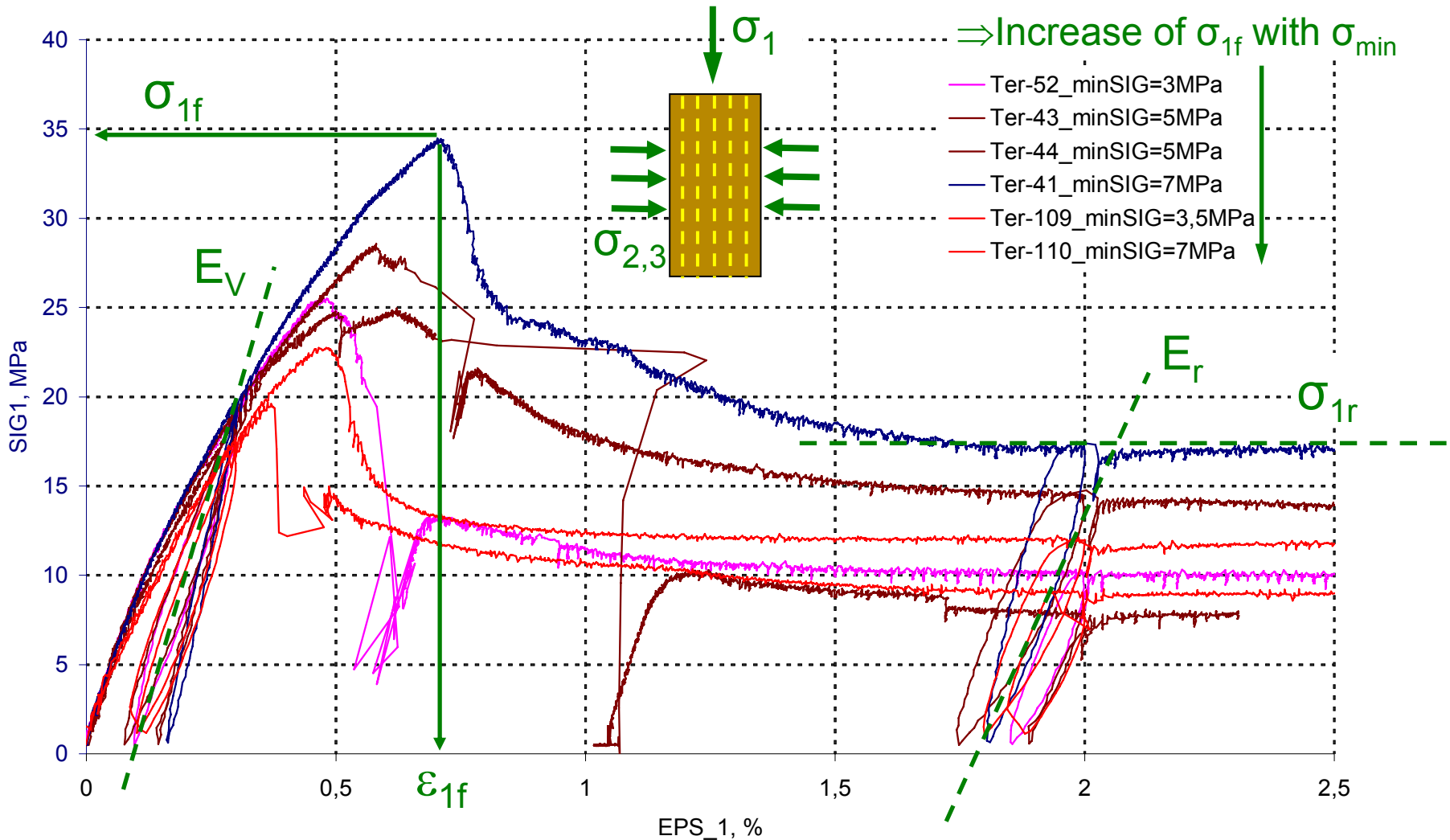
*Conceptual model of shear fractures as observed
in the Meuse/Haute-Marne Laboratory*



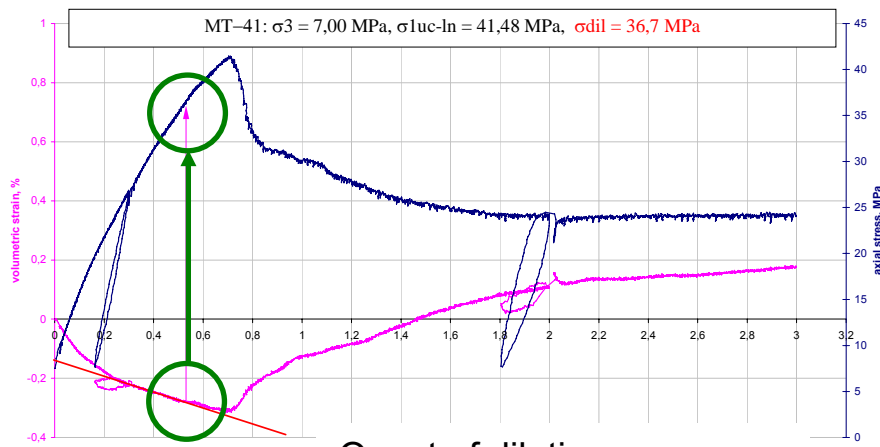
Selected laboratory investigation on international claystone samples



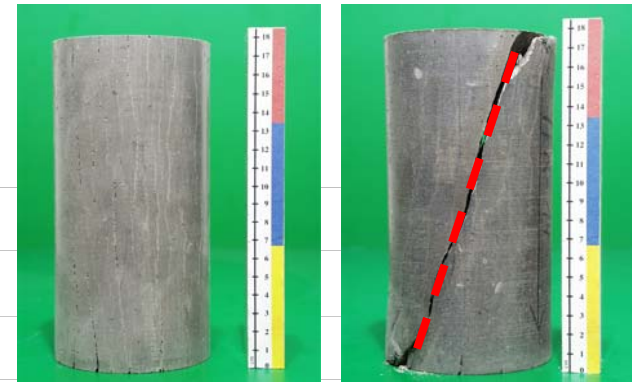
Determination of deformation and failure material behaviour



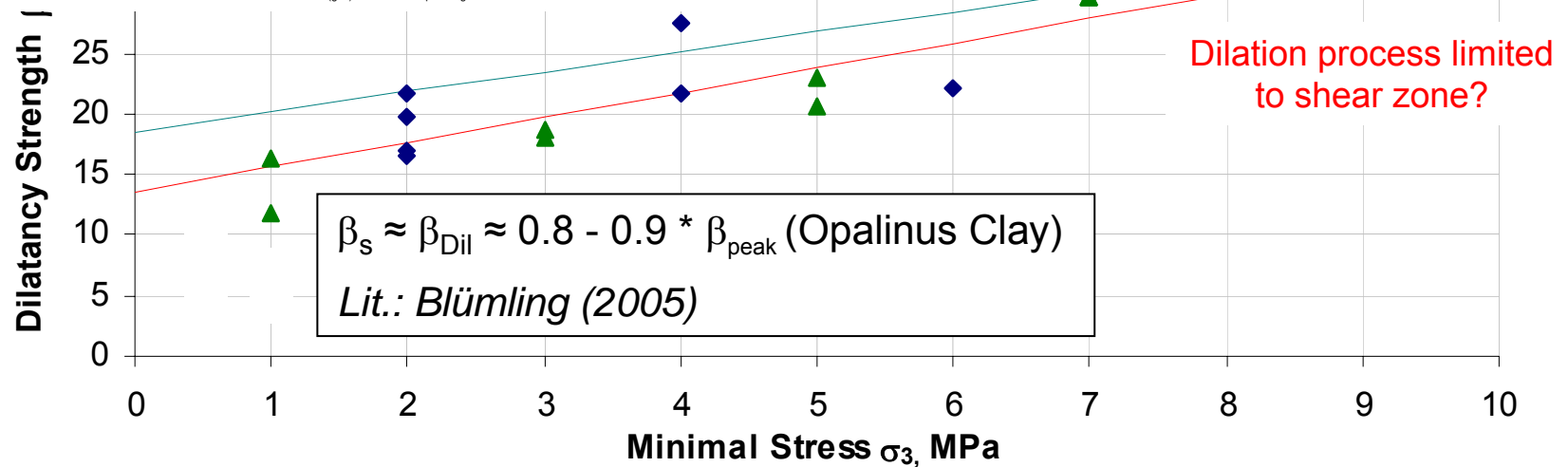
Determination of damage induced deformation behaviour



P-Sample Mont Terri (pre- and post-testing)



Onset of dilation processes



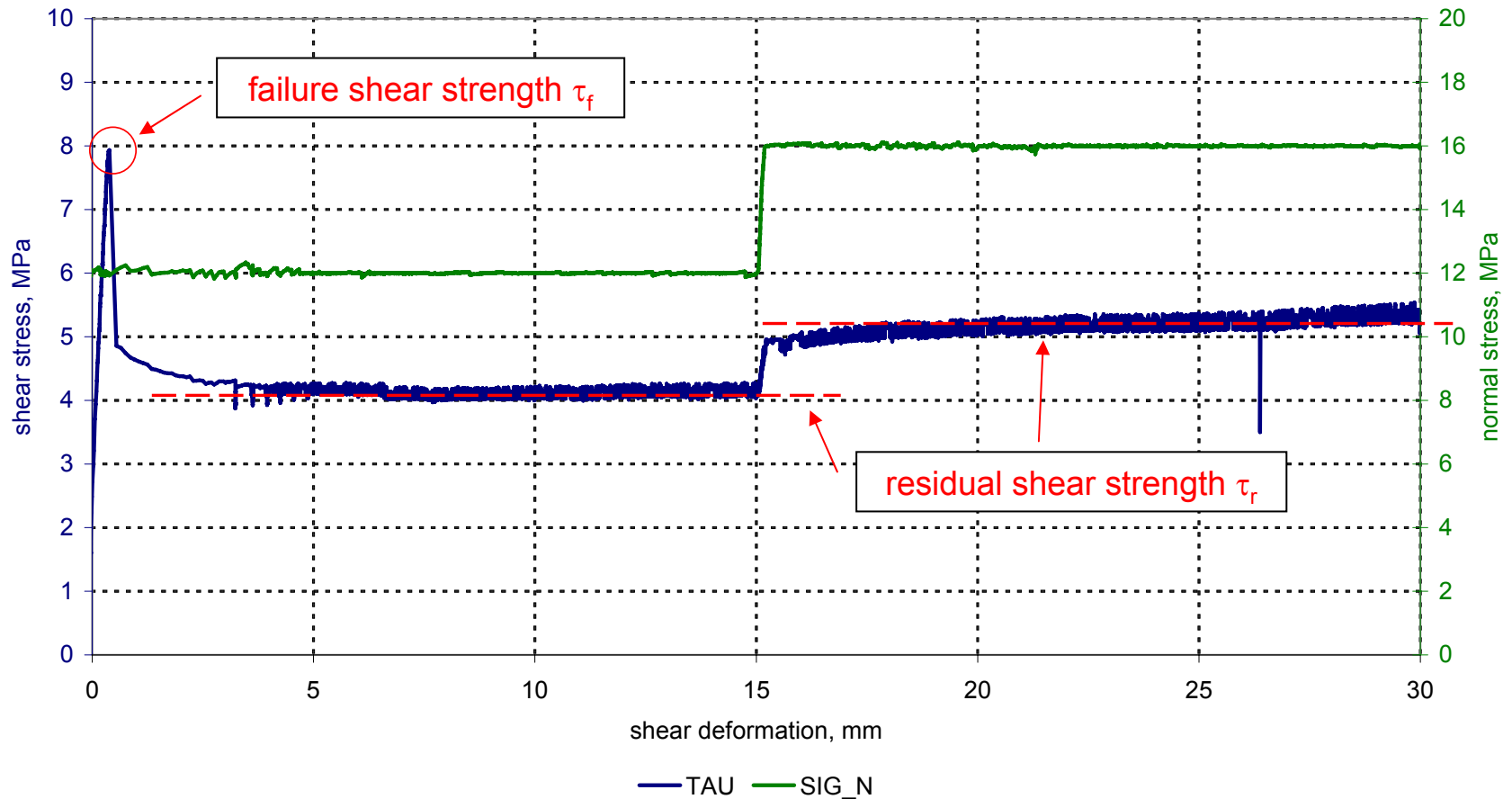
◆ BLT7 (//) ▲ BLT9 (//) — Regression (//-dilatancy) — Regression (//-failure)

DST-tests (Direct-Shear-Test)



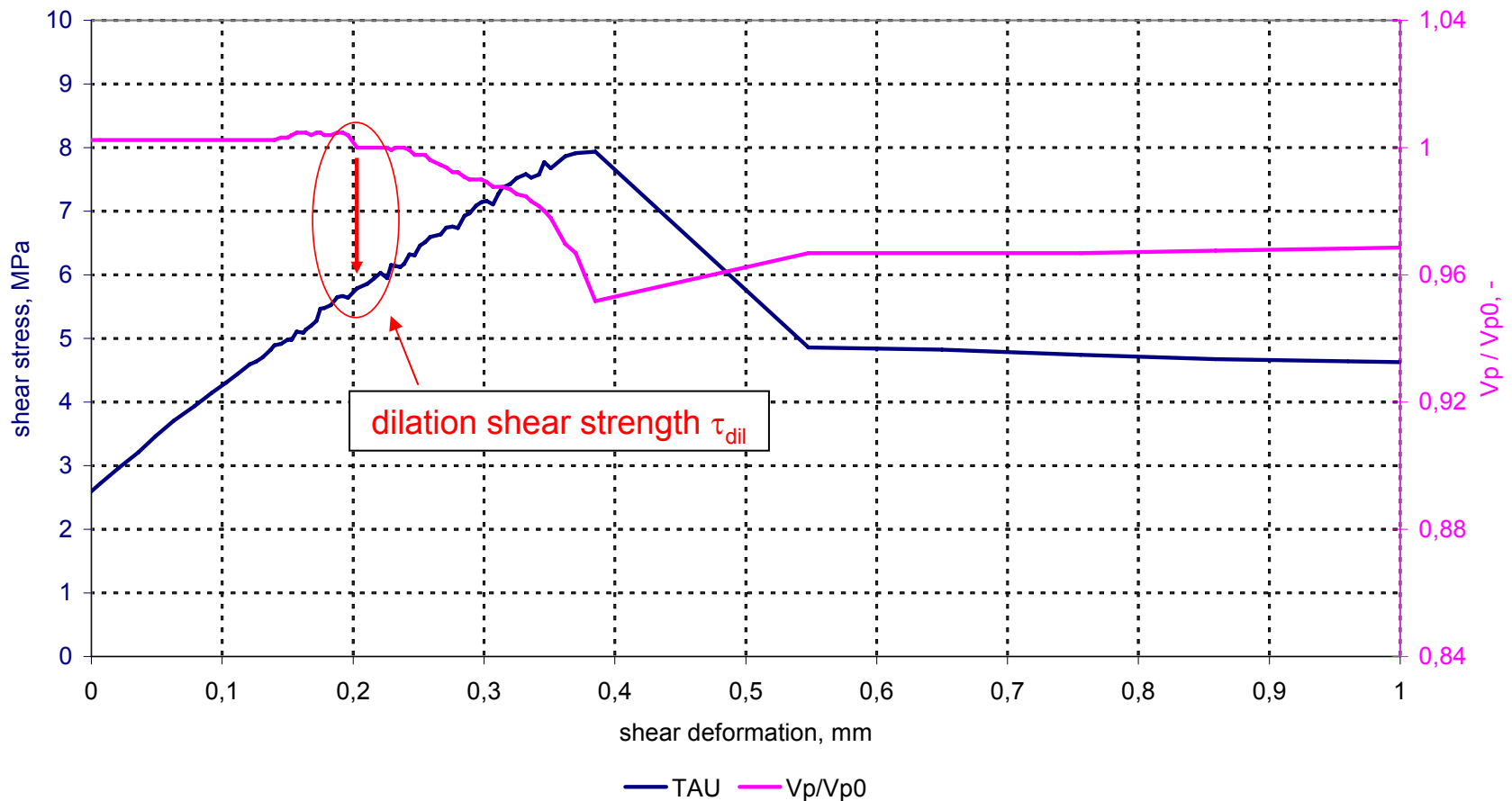
test results

- Definition of failure shear strength and residual shear strength for sample Tou-4.12



test results

- Determination of dilation strength on the basis of ultrasonic travel times

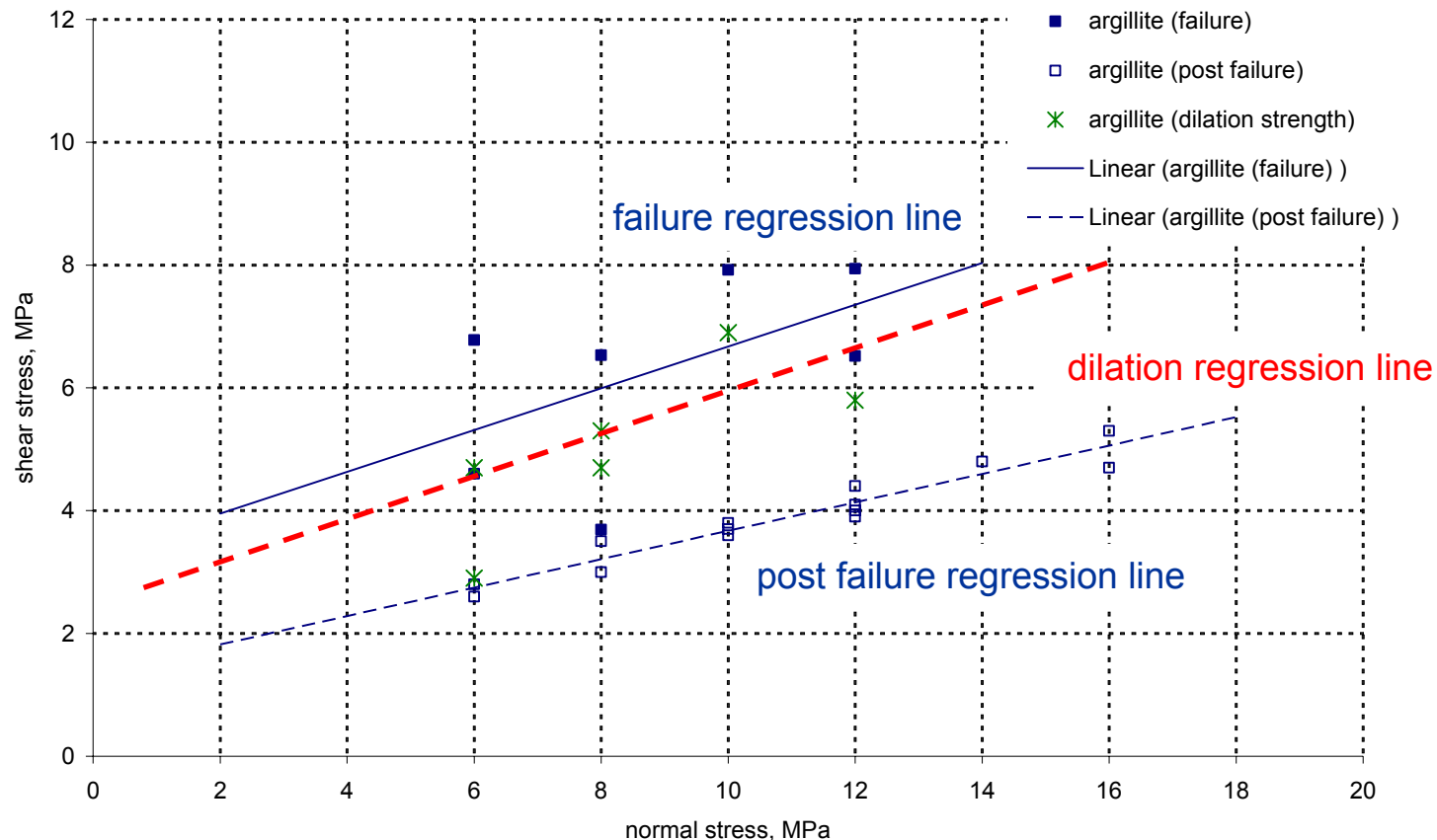


Determination of material model parameters

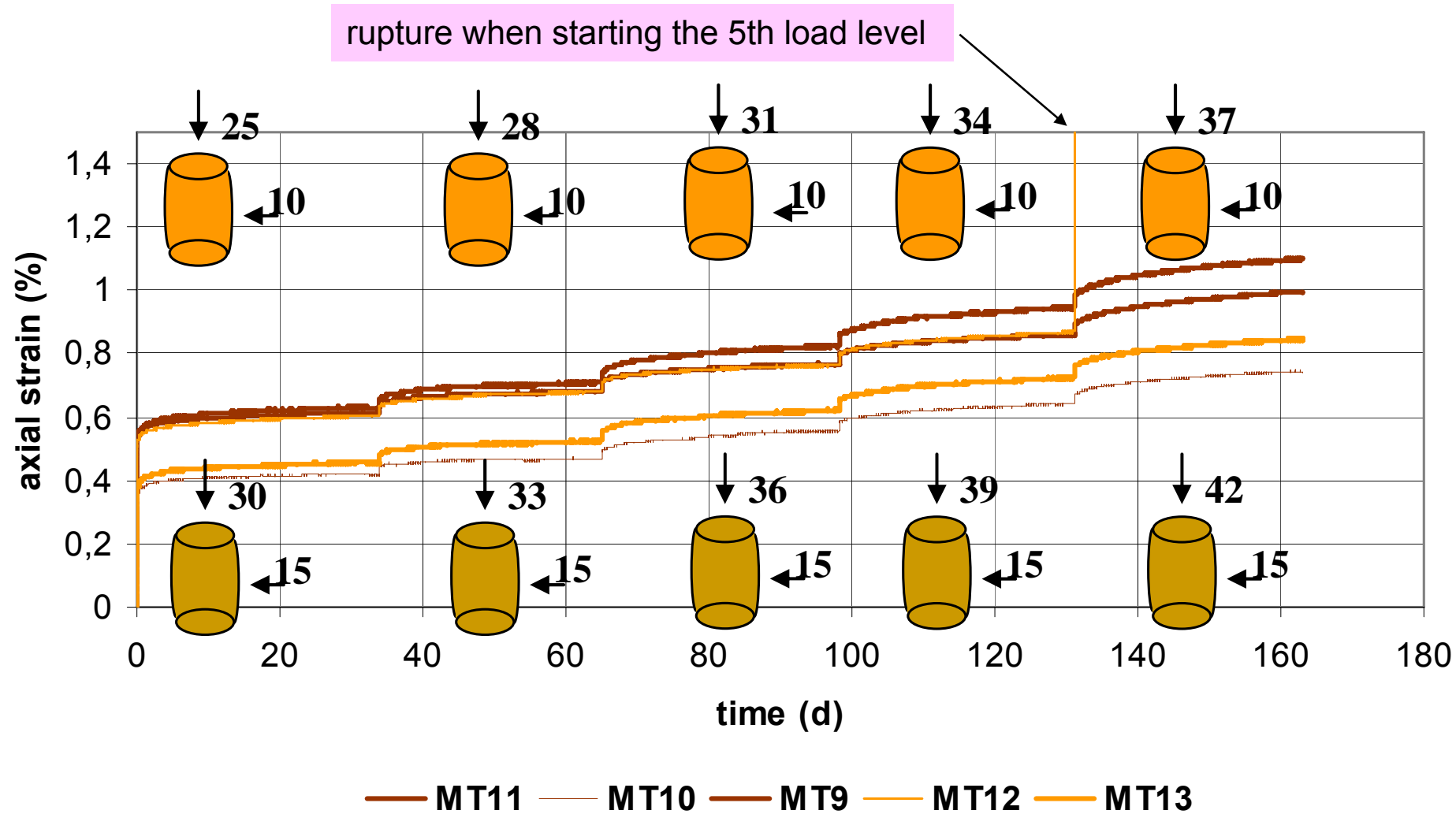
- Shear strength, residual strength, dilation strength for Tournemire PH4 **argillite**

Shear strength: $c = 3,27 \text{ MPa}$; $\varphi = 18,8^\circ$

Residual shear strength: $c = 1,36 \text{ MPa}$; $\varphi = 13,0^\circ$

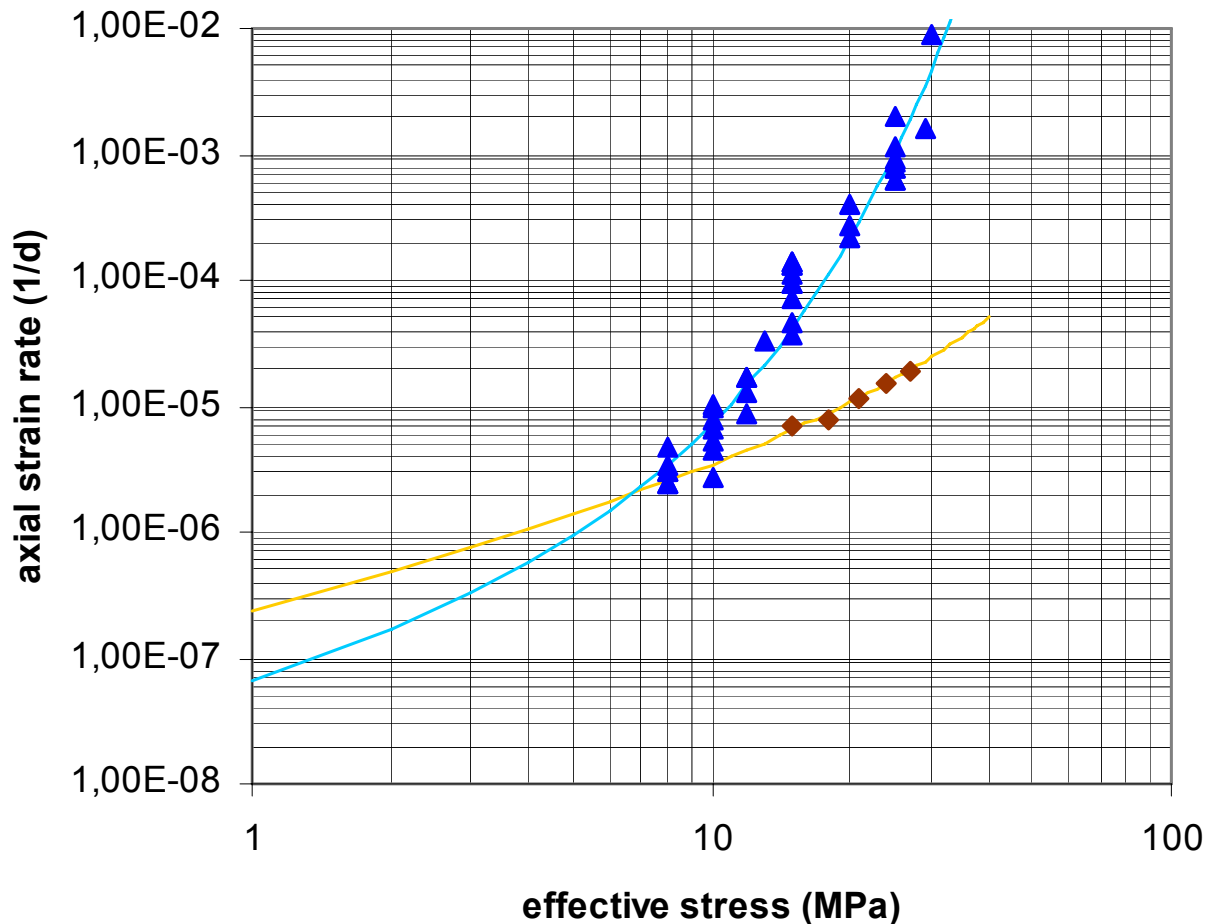


Triaxial creep tests (5 load levels)



NF-Pro Deliverable 4.4.5

Determination of time-depending material parameters



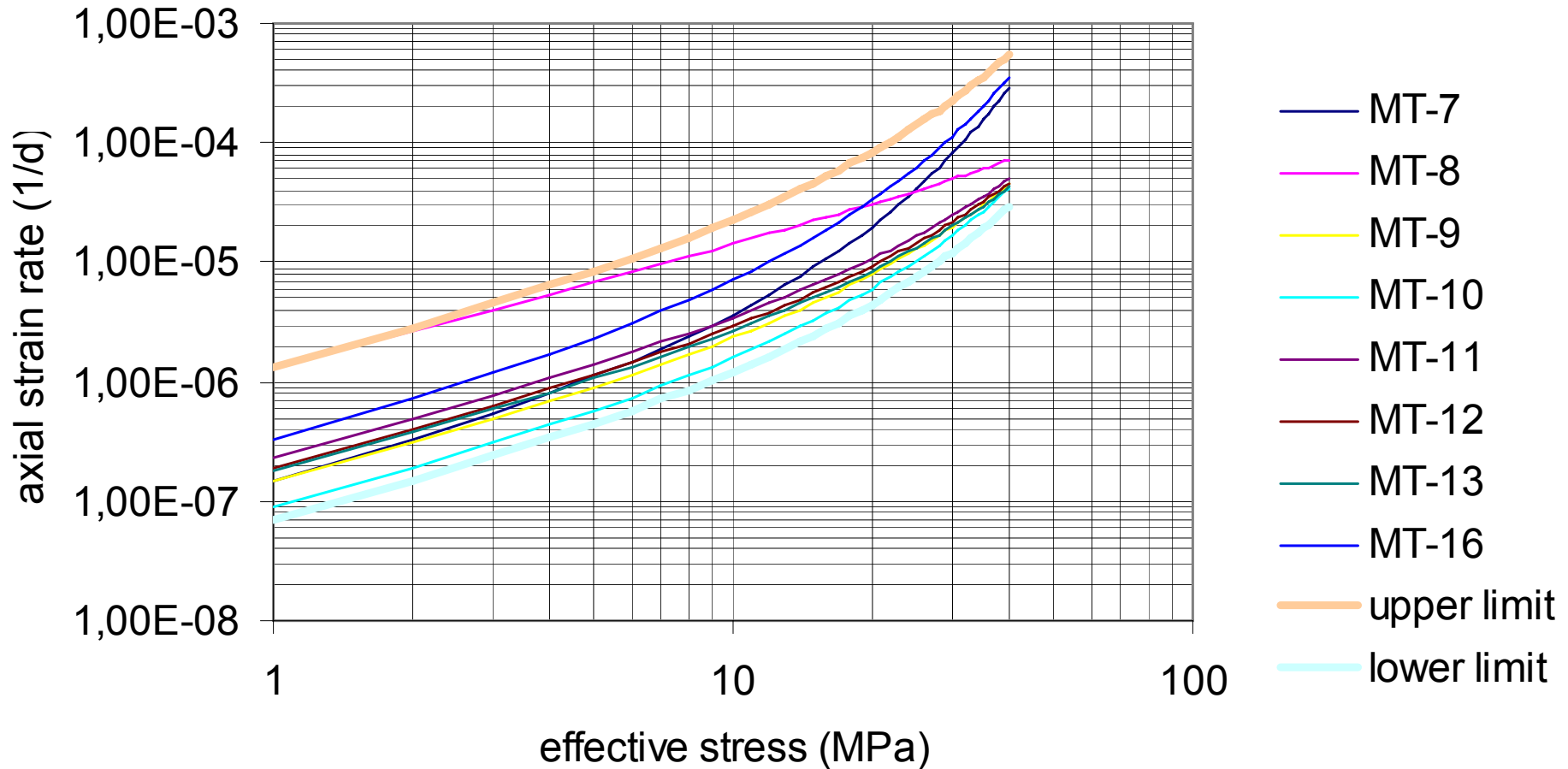
Parameter determination
only feasible for one
sample
↓
limited scatter band

- ◆ measured data for claystone
- regression for claystone
- ▲ measured data rock for salt
- regression for rock salt

NF-Pro Deliverable 4.4.5



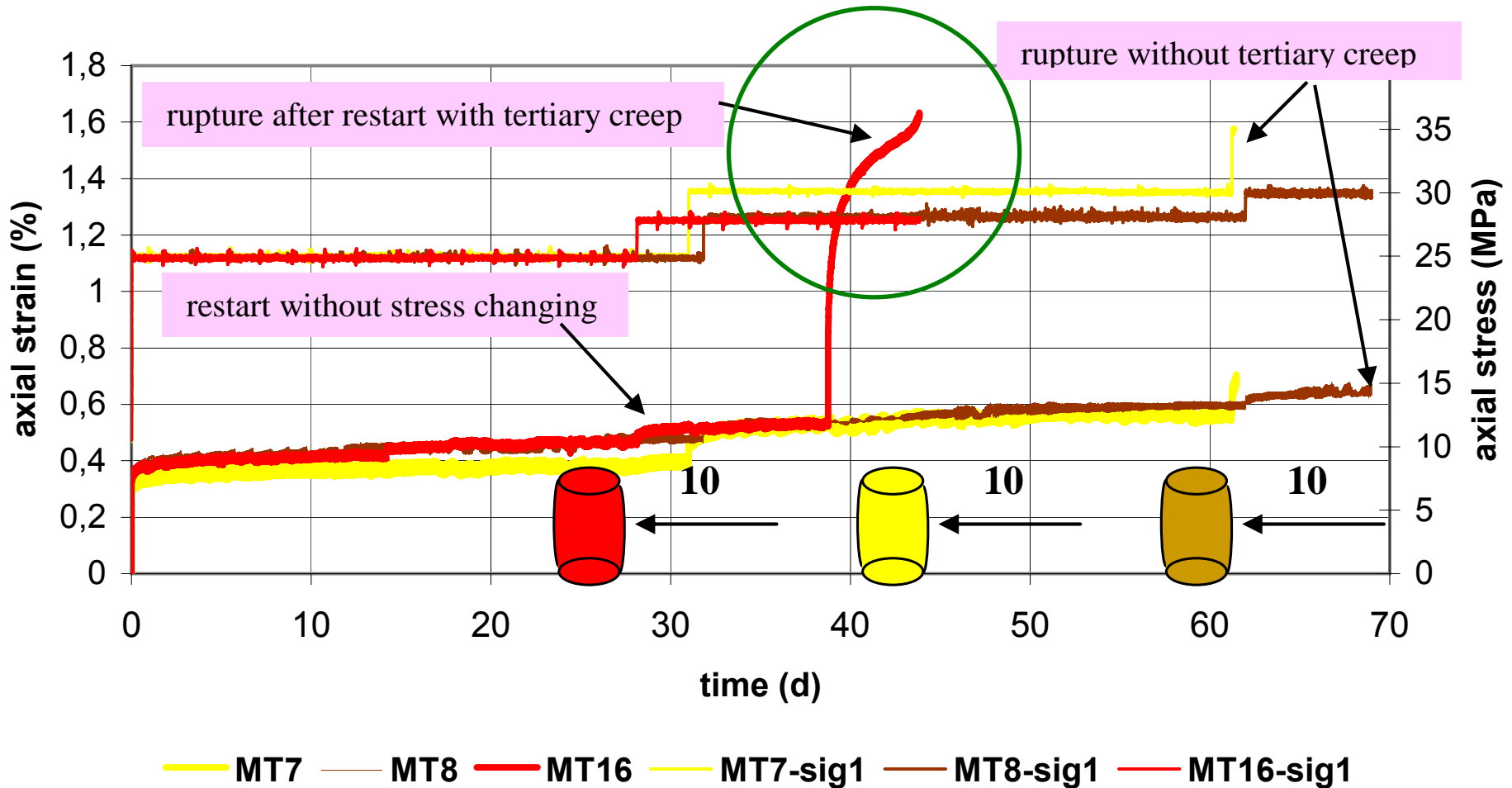
Stationary creep behaviour (limited scatter band)



NF-Pro Deliverable 4.4.5



Damage induced creep behaviour

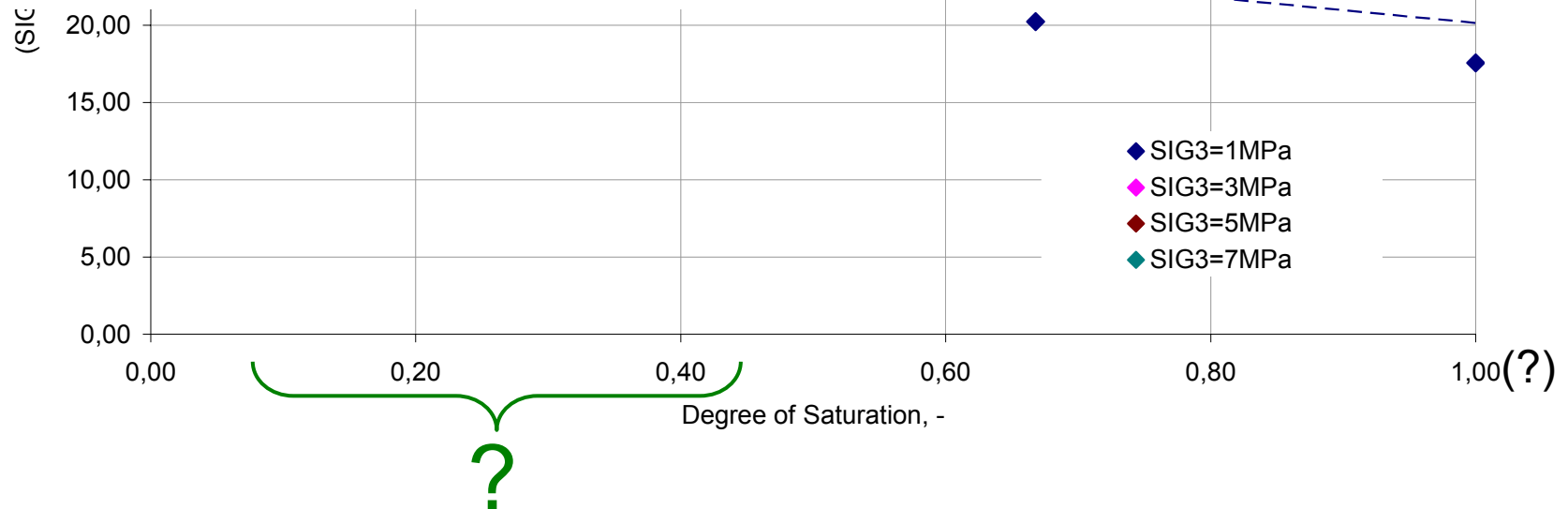
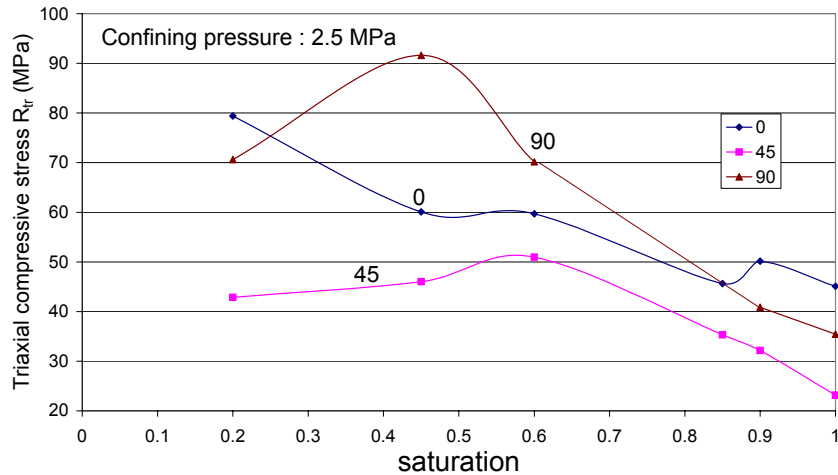


NF-Pro Deliverable 4.4.5

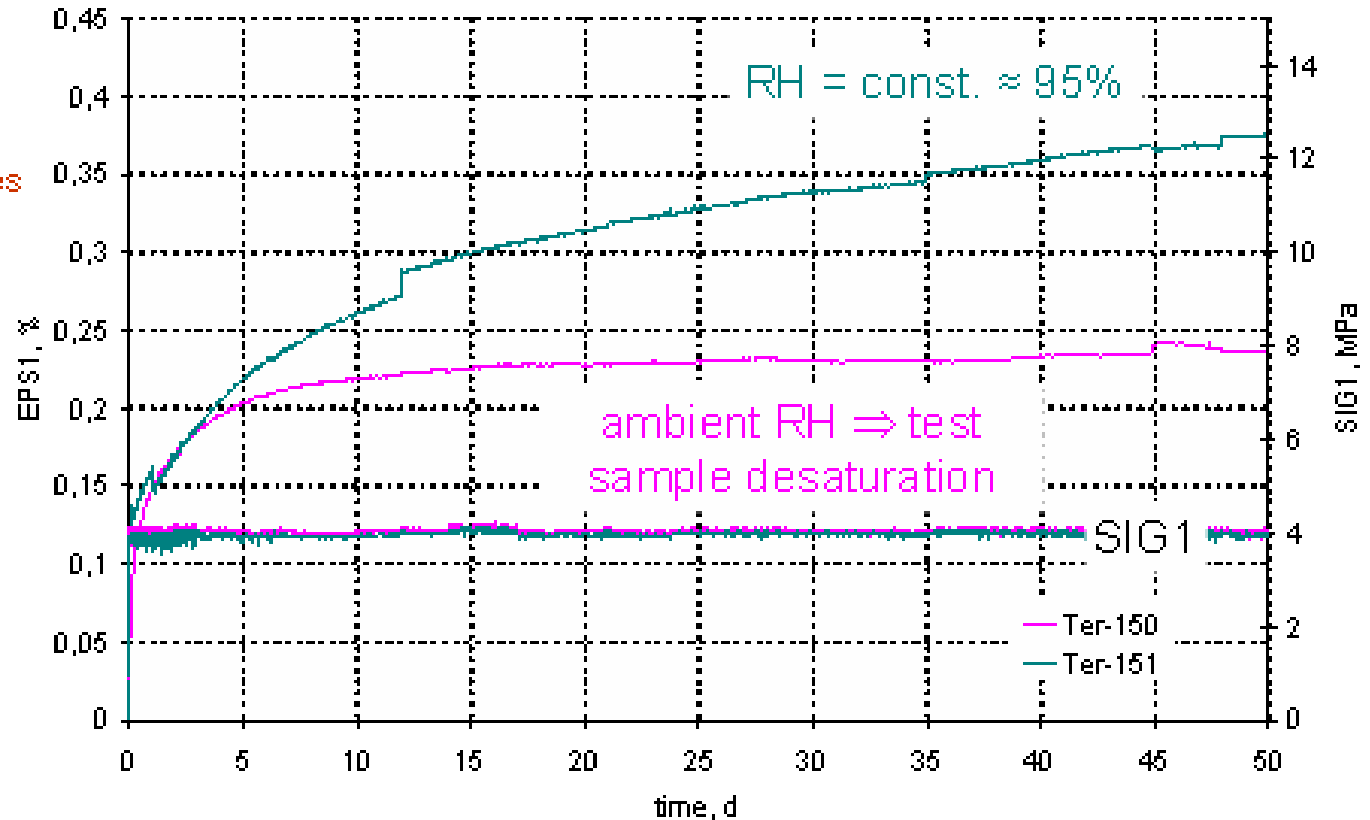
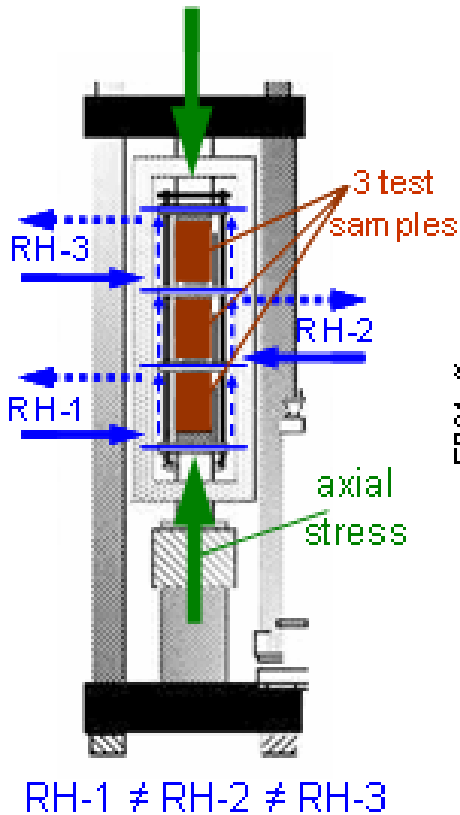


Short-term investigation for $S_r < 1,0$

Triaxial compressive stress, *Vales et al. (2002)*



Long-term investigation for $S_r < 1,0$



- Uniaxial creep test with different relative humidity (RH) to determine the long-term deformation behaviour depending on desaturation effects for Mont Terri samples

General Outcome

- Minor deformation capacity ($\bar{\varepsilon}_1 < 1\%$)
- Marginal stress depending stationary creep rate
- No significant transient creep phase detectable after increasing deviatoric stress
- A change in the parameter determination procedure is recommended as follows:
 - (a) performing tests with more than one load level (multi load level tests)
 - (b) determination of creep parameters separately for each sample
 - (c) determination of (average) mean material parameters from sample-related separately determined parameters.
 - (d) The sample size should be enlarged, h:d ratio should be 2.5:1 or 3:1
 - (e) High accuracy displacement transducers with optimised measurement range are recommended



Material behaviour depending on storage conditions



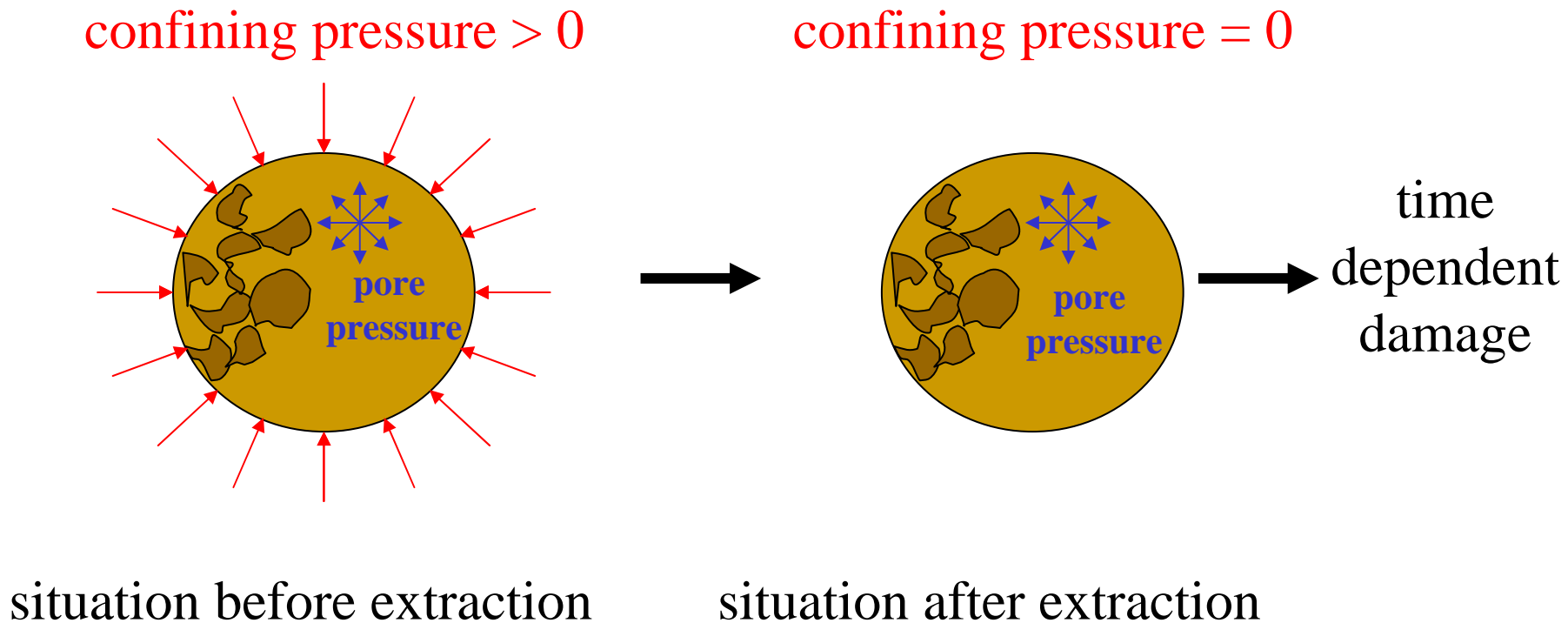
Plastic bag sealed
and stored claystone sample
(6 weeks storage time)



Ageing cracks in plastic bag
sealed and stored claystone
sample (6 months storage time)

Schematic overview on effects in rock mass

Pore pressure induced tensile stress after core extraction



Phenomenological identifications dependent on the storage time

- **increase in shear strength** of the rock (increase of the effective stress because of the **reduced pore water pressure or desaturation** (build-up of a water potential, suction),
- **increasing damage** to (or destruction of) the rock structure resulting from the **pressure difference** now active, i.e. the difference between the pore water pressure and the ambient pressure that has now been reduced to the atmospheric pressure, as well as
- **increasing damage** to the rock structure by further **desaturation** which leads to the formation of **contraction cracks** (shrinkage, enlarged suction).



Photographic view of the storage containers



plastic bag sealed and stored claystone sample

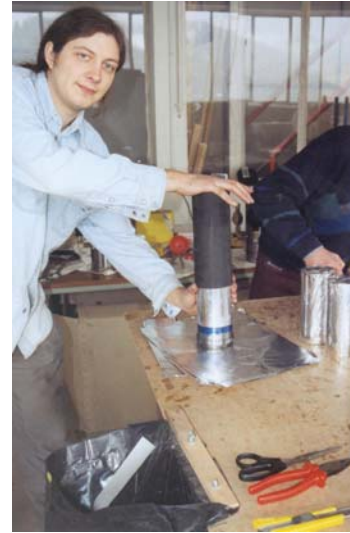


claystone sample stored in **TUC container**

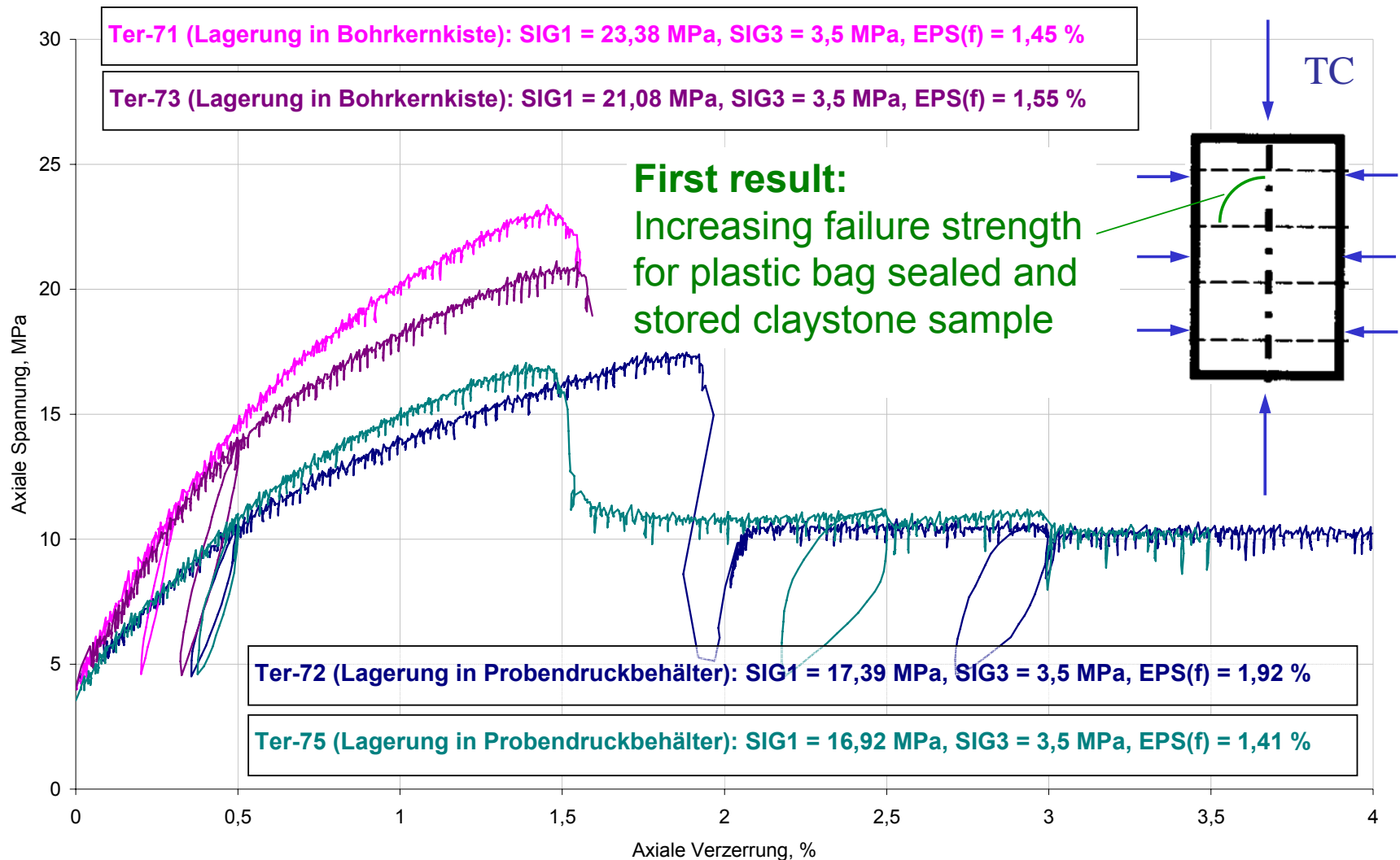
TUC storage container



Impression of the installation sequence

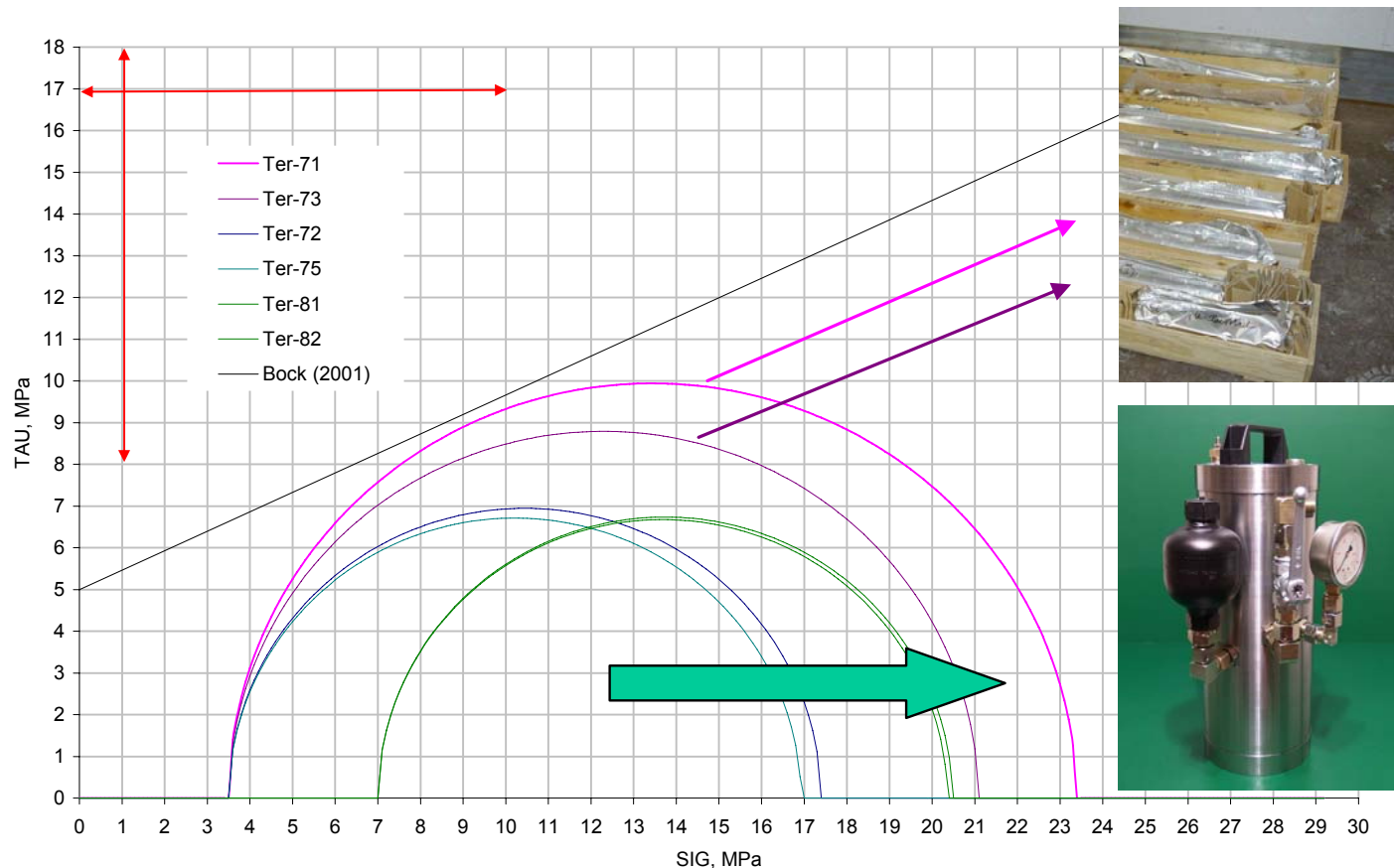


Results of short-term TC tests depending on storage conditions



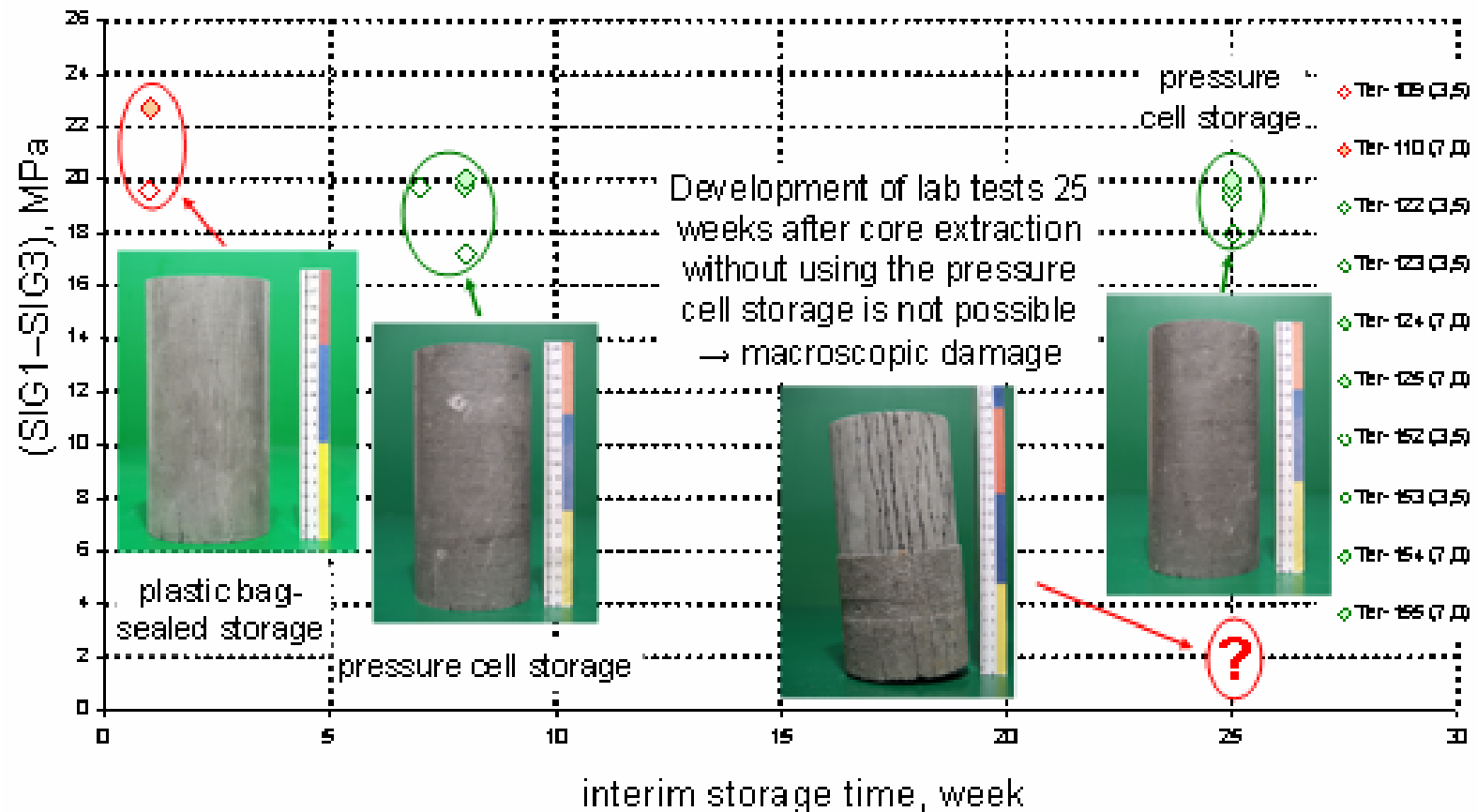
Results of short-term TC tests depending on storage conditions

- A comparison of the results of triaxial compression experiments on claystone from the same extraction location and after the same storage time in dependence on the type of storage



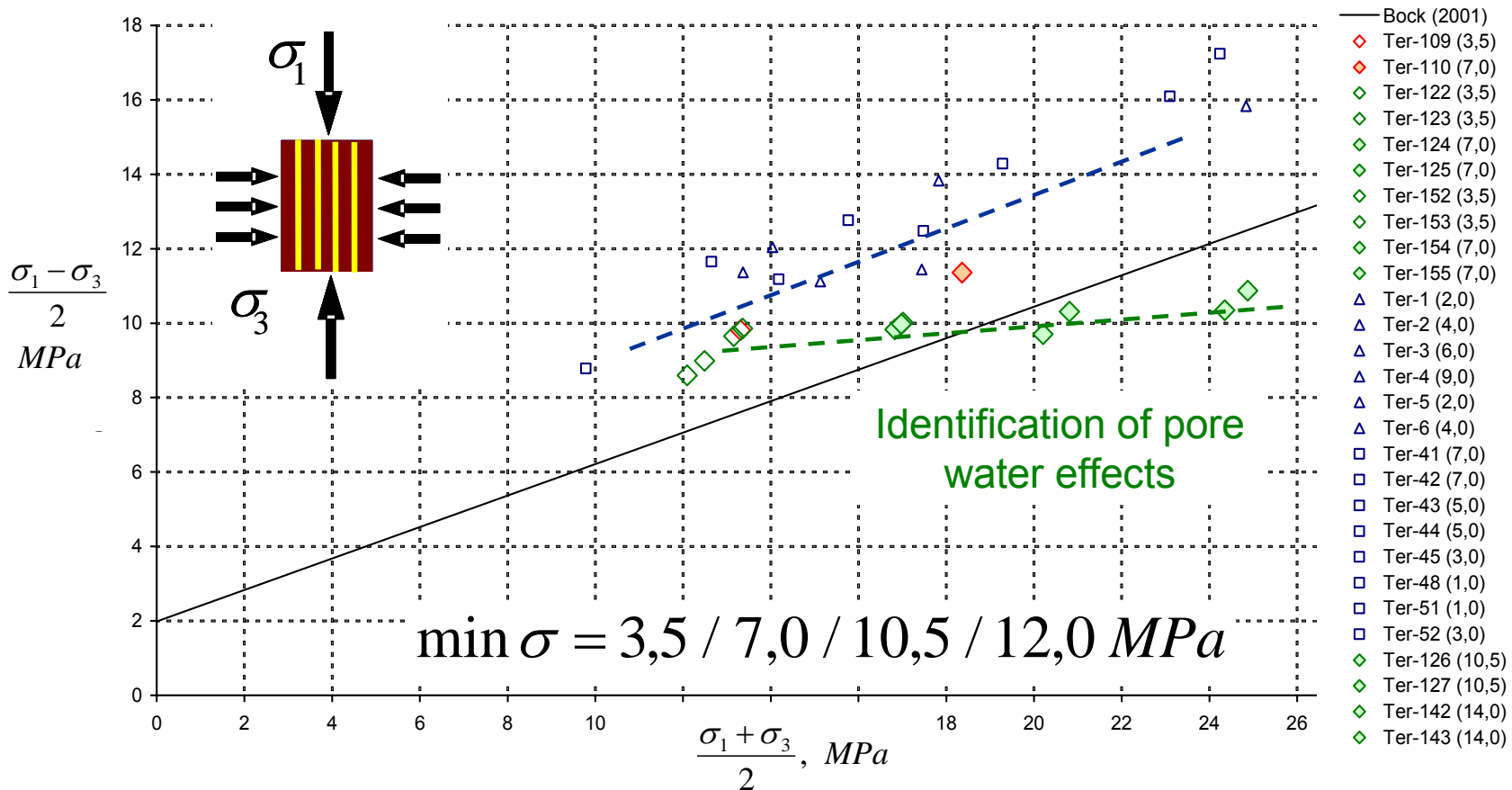
Results of short-term TC tests depending on storage conditions

- Current results of triaxial compression tests P-samples from Mont Terri (same drilling location) in dependence on interim storage time and type of storage (red – plastig bag sealed interim storage / green – interim container storage)



Results of short-term TC tests depending on storage conditions

- Current results of triaxial compression tests P-samples from Mont Terri in dependence on the type of storage (red/blue – plastig bag sealed interim storage / green – interim container storage)

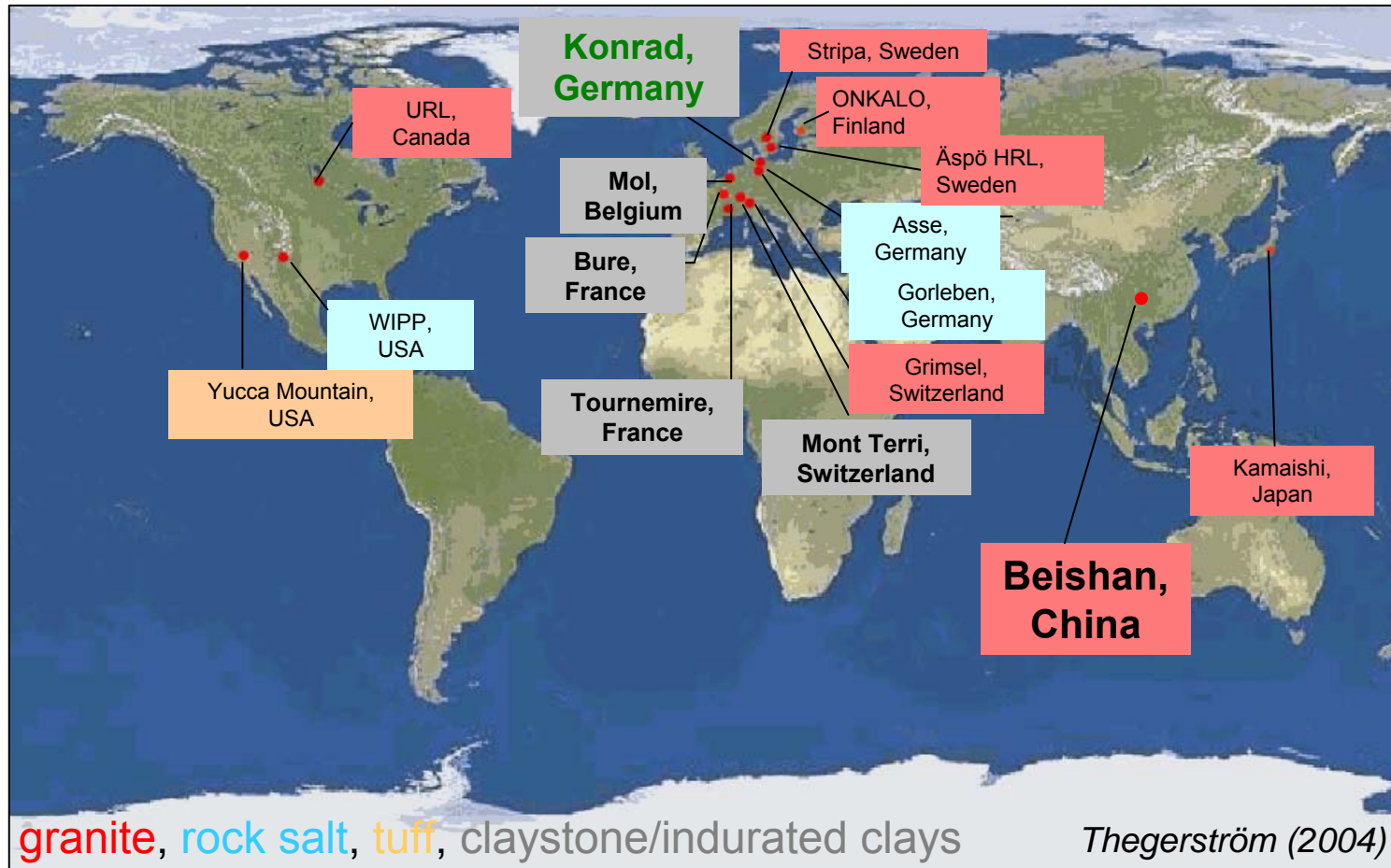


Conclusion *on lab testing results*

- As, in pressure cell storage, **desaturation processes** to the extent of those given in wooden box storage are prevented,
 - lab test **results** are **reproducible**,
 - the **pore water pressure** described in the introduction is assumed to be the **major cause** of storage-dependent effects.
- ⇒ In order to make this thesis more precise, work is in progress to integrate a **pore water pressure measurement** in the experimental set-up for future laboratory experiments.

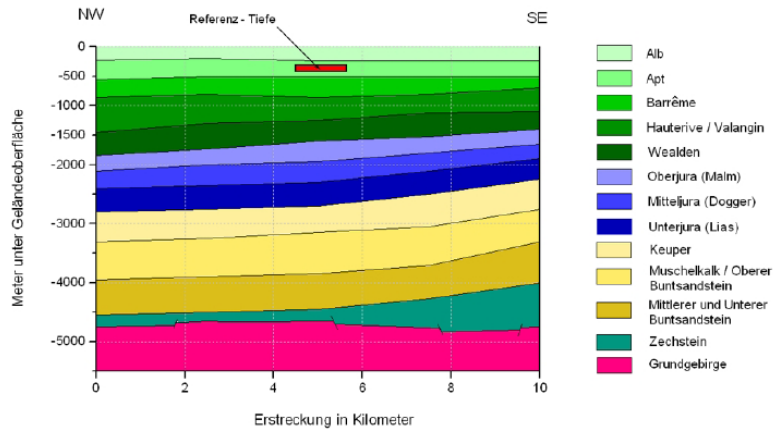


Germany

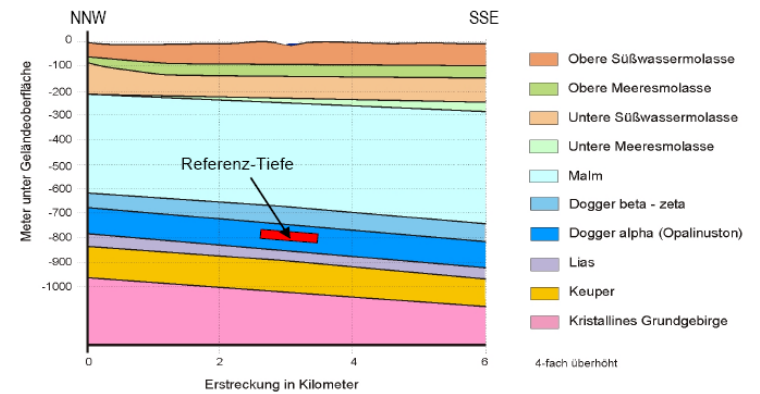


Generic Investigations in Germany

Generisches Modell Niedersächsisches Becken



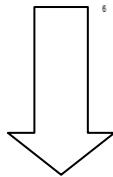
Generisches Modell Süddeutschland



www.dbe-technology.de

TEC-ES – Amelung
Workshop GEIST, Peine, 19. u. 20.01.2005

DBETEC
DBE TECHNOLOGY GmbH

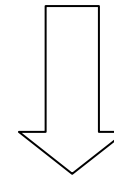


**Indurated Clay –
Marlstone mixture**

www.dbe-technology.de

TEC-ES – Amelung
Workshop GEIST, Peine, 19. u. 20.01.2005

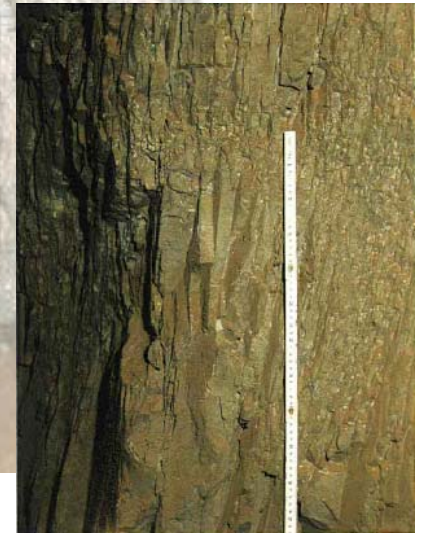
DBETEC
DBE TECHNOLOGY GmbH



**Claystone / Opalinusclay
(similar to Switzerland)**



In situ



Physical Modelling and numerical Simulation (3D)

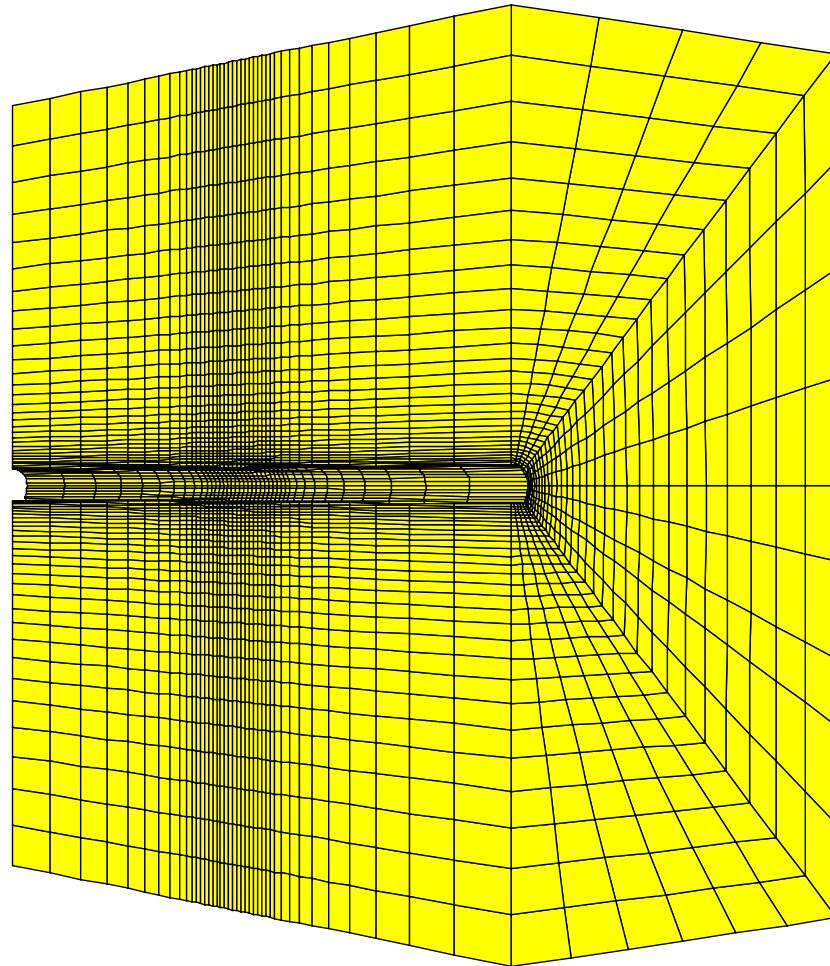
FLAC3D 2.10

Step 50089 Model Perspective
11:07:30 Thu Oct 12 2006

Center:	Rotation:
X: 2.388e+001	X: 0.000
Y: -1.004e+001	Y: 0.000
Z: -2.650e+002	Z: 40.000
Dist: 3.918e+002	Mag.: 1.1
	Ang.: 22.500

Block Group

 Gebirge



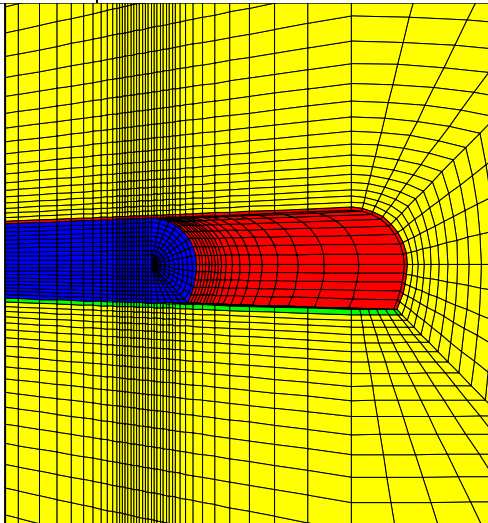
FLAC3D 2.10

Step 50089 Model Perspective
11:11:45 Thu Oct 12 2006

Center:	Rotation:
X: 4.350e+000	X: 0.000
Y: 2.159e+000	Y: 0.000
Z: -2.650e+002	Z: 10.000
Dist: 3.918e+002	Mag.: 5.96
	Ang.: 22.500

Block Group

 Tunnel
 Spritzbeton
 Gebirge
 Fahrbahn

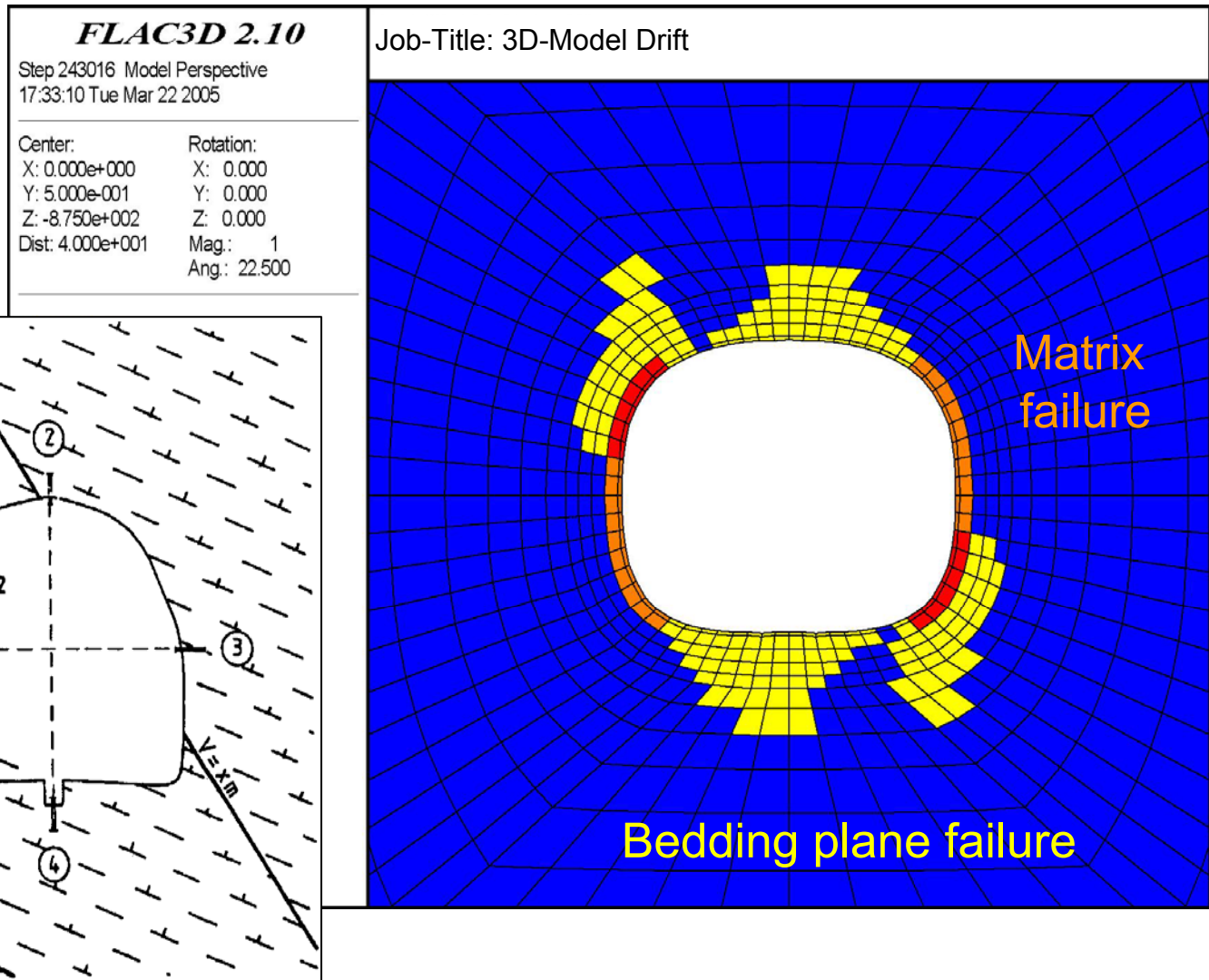


TU-Clausthal
Deponietechnik und Geomechanik

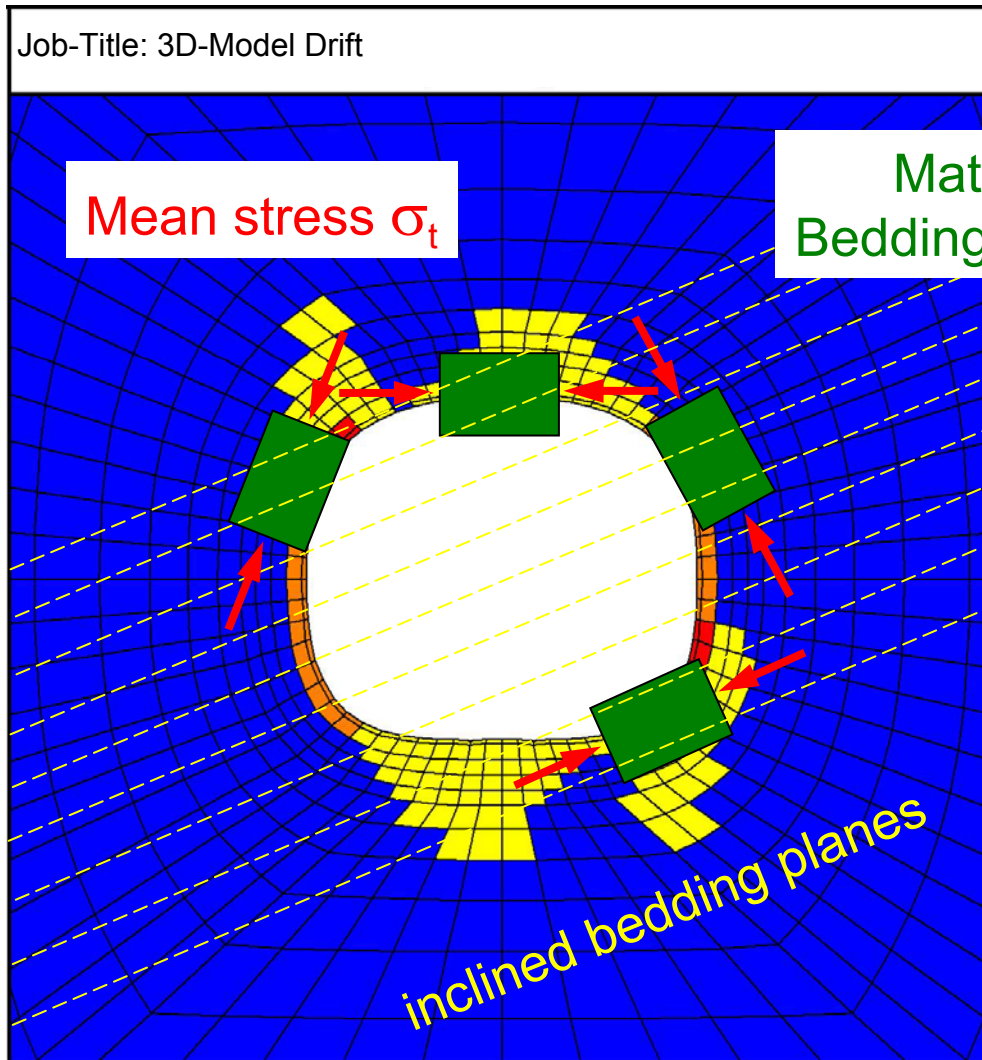
TU-Clausthal
Deponietechnik und Geomechanik



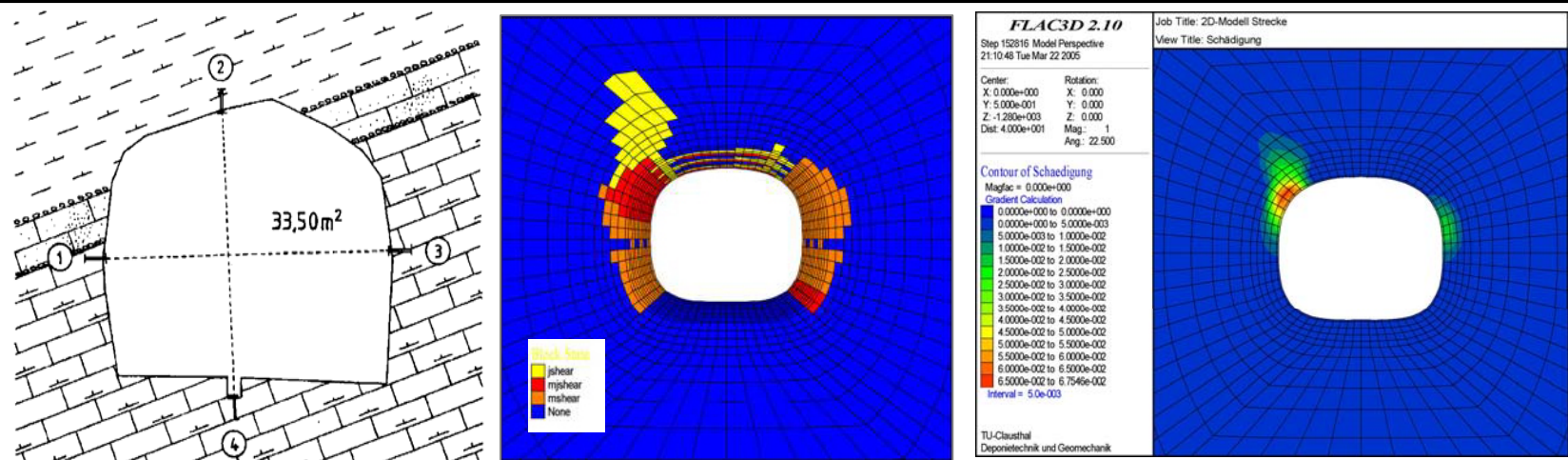
What is possible? – Identification of (potential) failure processes (zones)



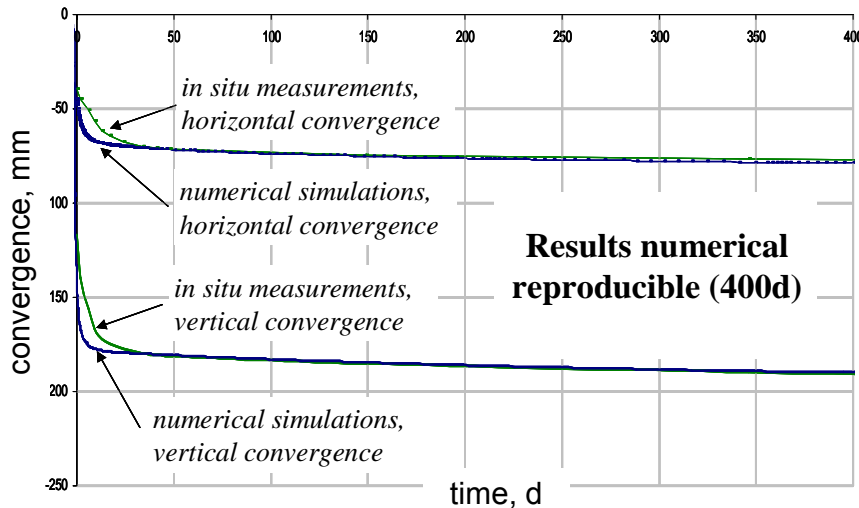
Determination of anisotropic effects on rock mass failure



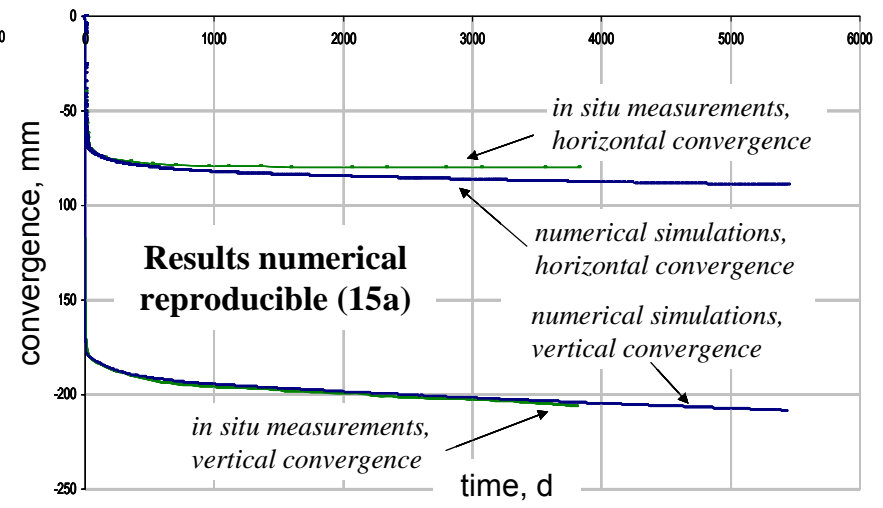
Selected drift in argillaceous rock mass with simulation results



a) drift cross section area , b) damaged zones, c) intensity of damage

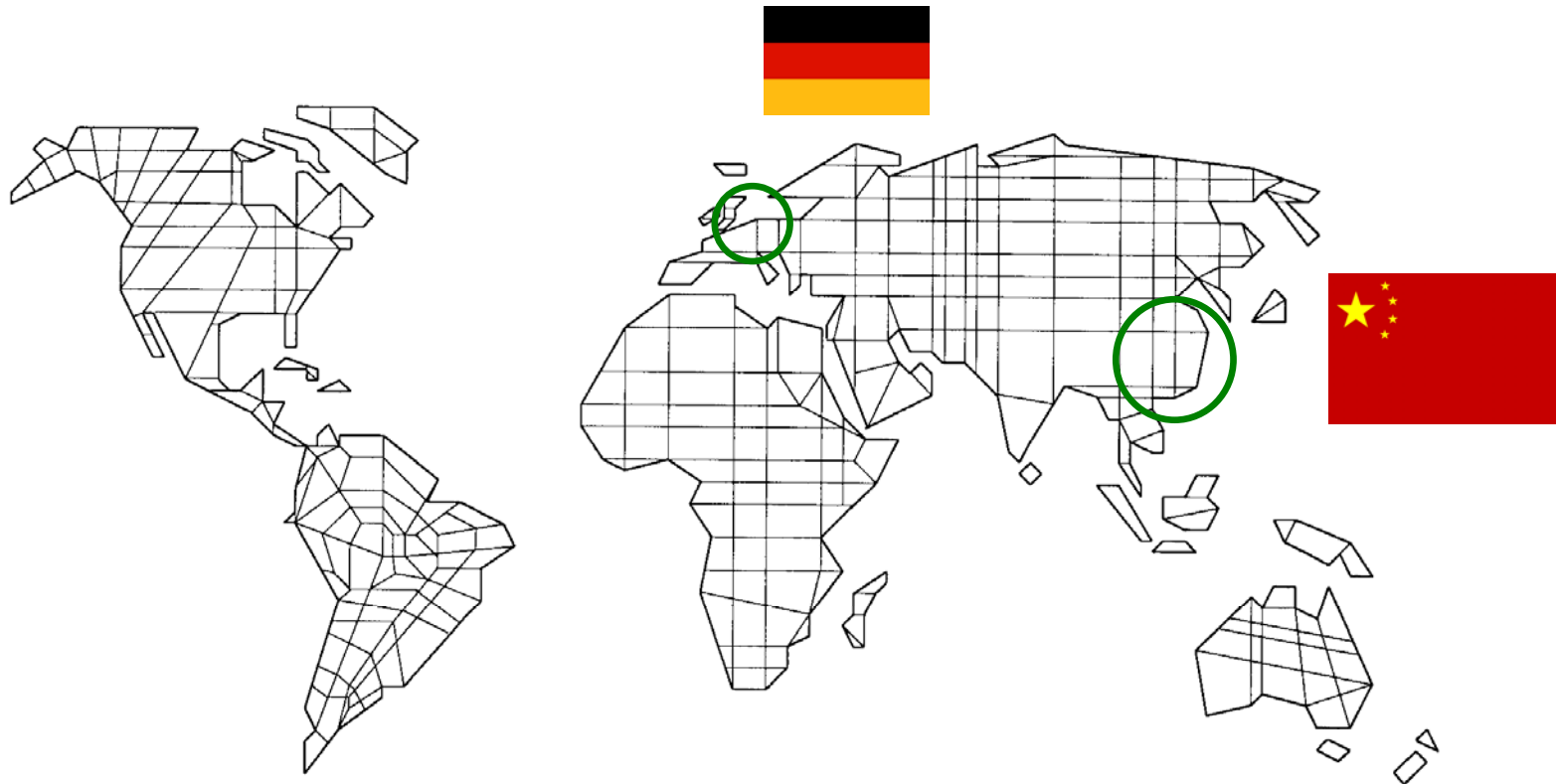


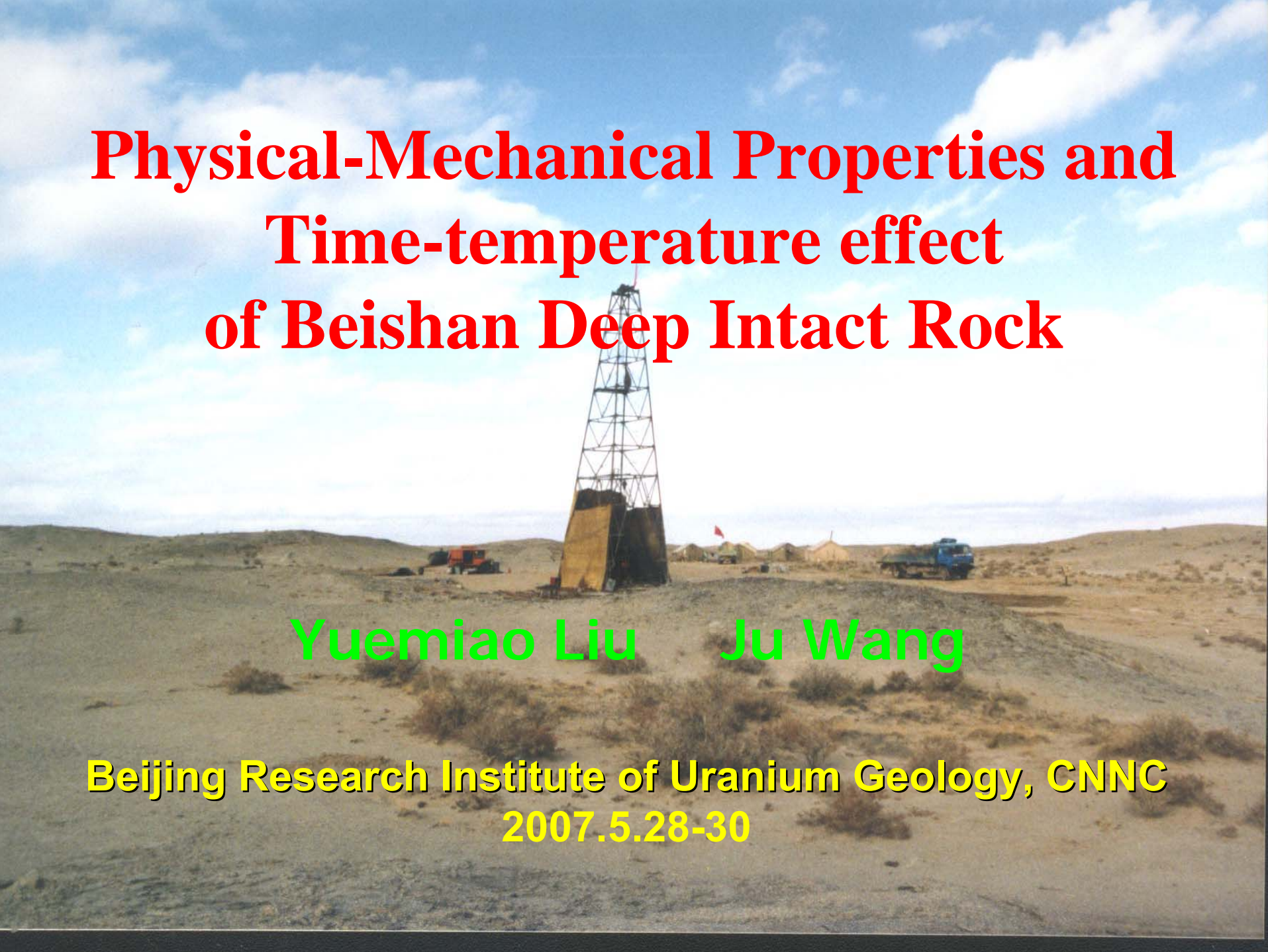
Deformation process during the first year



Observation period of 15 years

Hope for beneficial scientific cooperation!





Physical-Mechanical Properties and Time-temperature effect of Beishan Deep Intact Rock

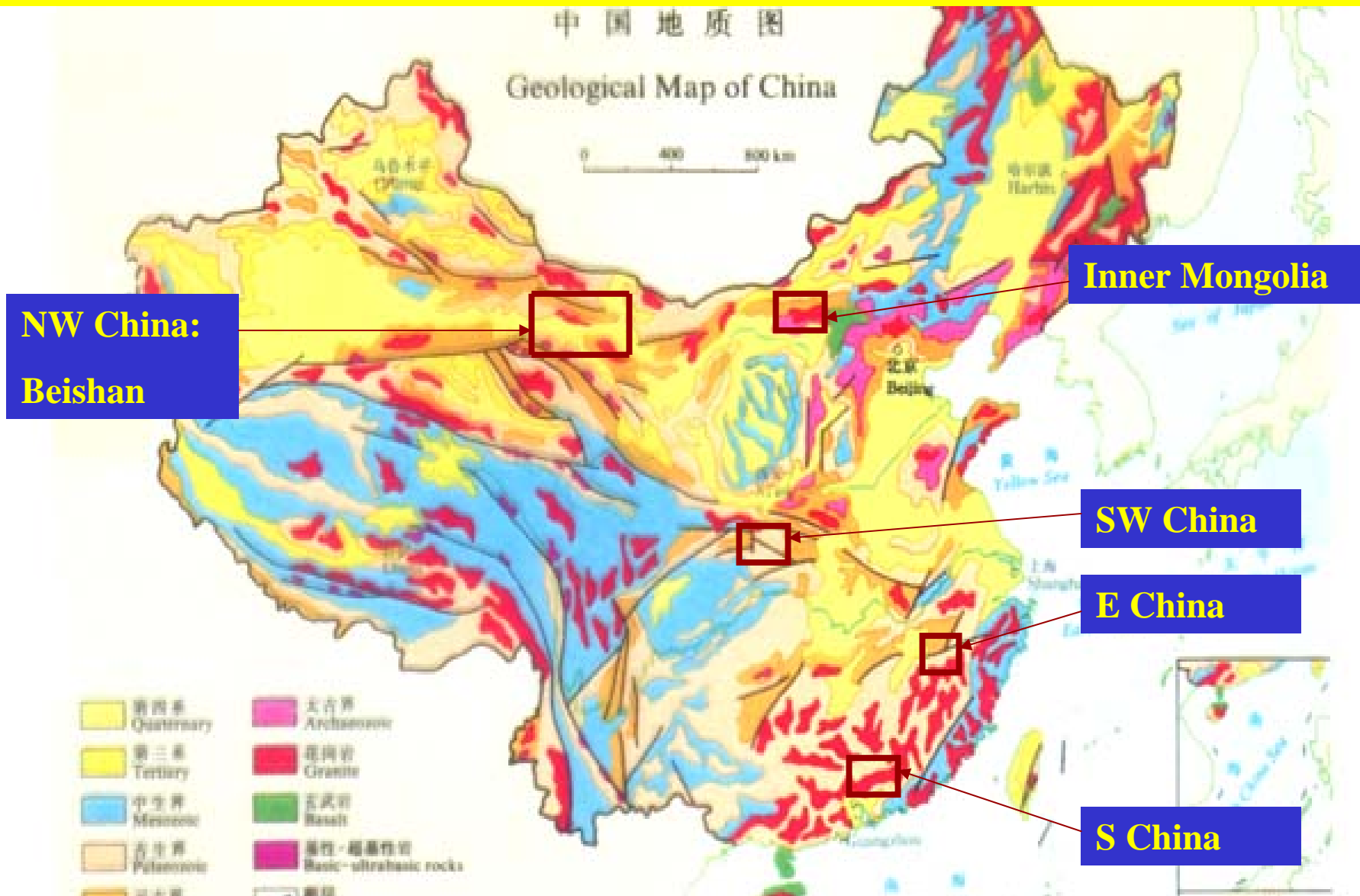
Yuemiao Liu Ju Wang

**Beijing Research Institute of Uranium Geology, CNNC
2007.5.28-30**

Contents

- **Introduction**
- **Physical Property**
- **Mechanical Property**
- **Long-Term Behaviour at High Temperature**
- **Conclusion**

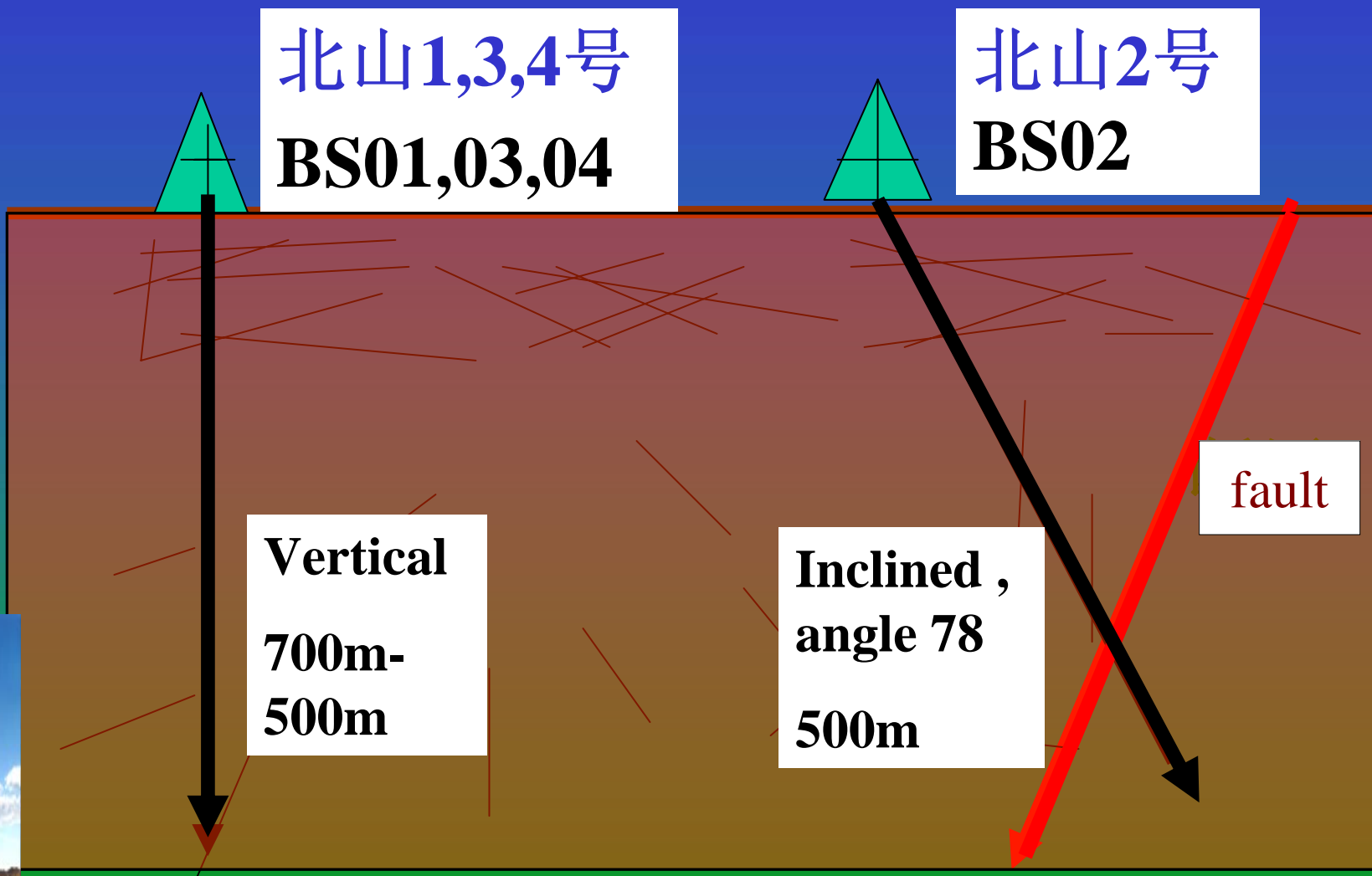
Major Activities: Site selection and site characterization



Preselected regions for HLW repository in China



Bore holes BS01, 02, 03, 04



Main rock



BS01, 271 $\frac{2}{3}$, 404.20 m,

典型岩性: 似斑状花岗岩闪长岩

BS01, 471 $\frac{10}{12}$, 699.46

黑云母英云闪长岩.

porphyritic
monzonitic granite

tonalite



core sample from BS01: the integrity



core sample with fracture



Intact Sample for Rock Mechanics

556 m

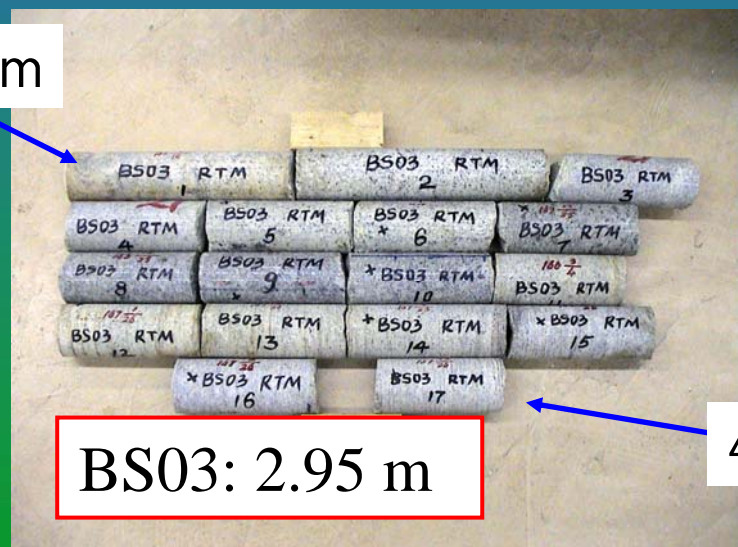


BS01: 19.54 m

676 m



411 m



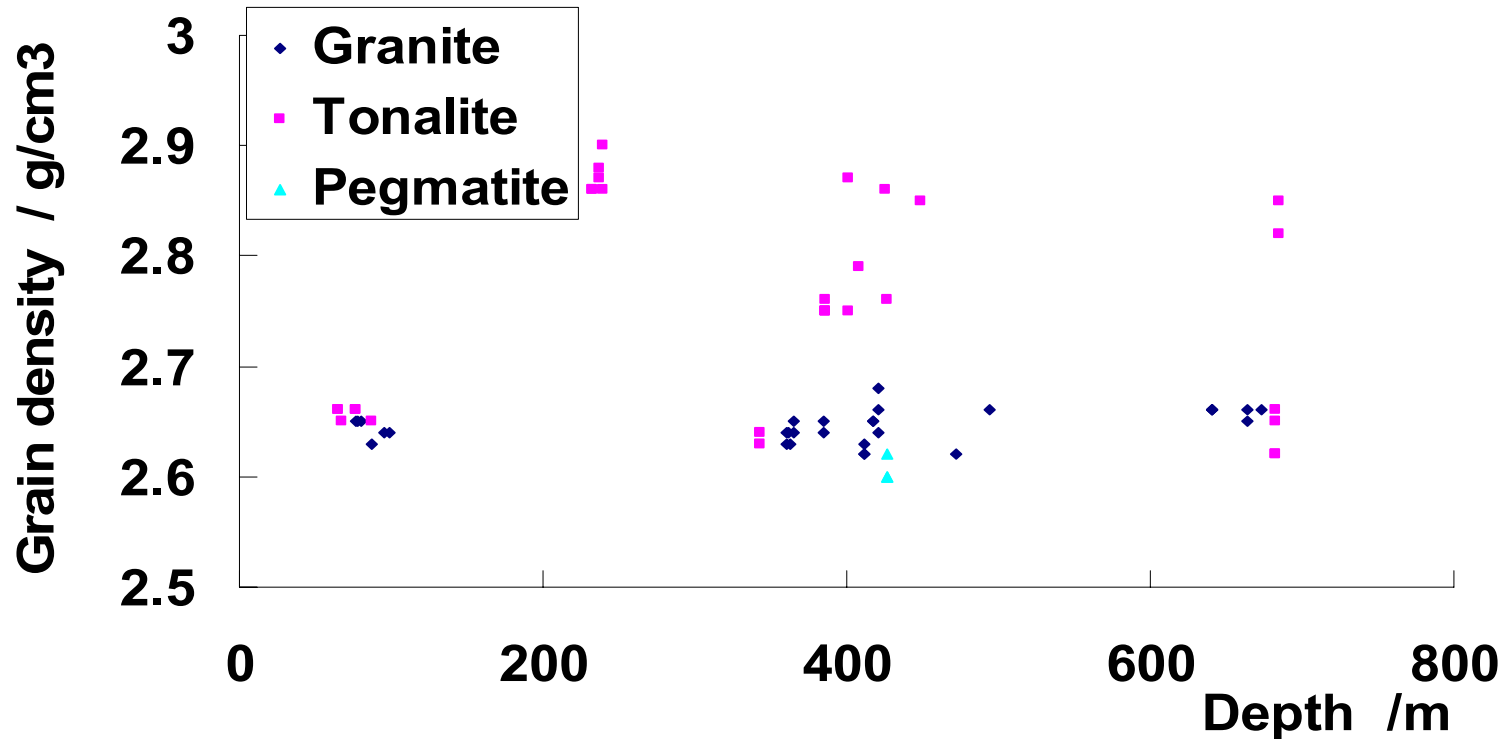
BS03: 2.95 m

420 m

Physical property

- **Density**
- **Water content**
- **Percent sorption**
- **Porosity factor**
- **Sound wave property**

Density

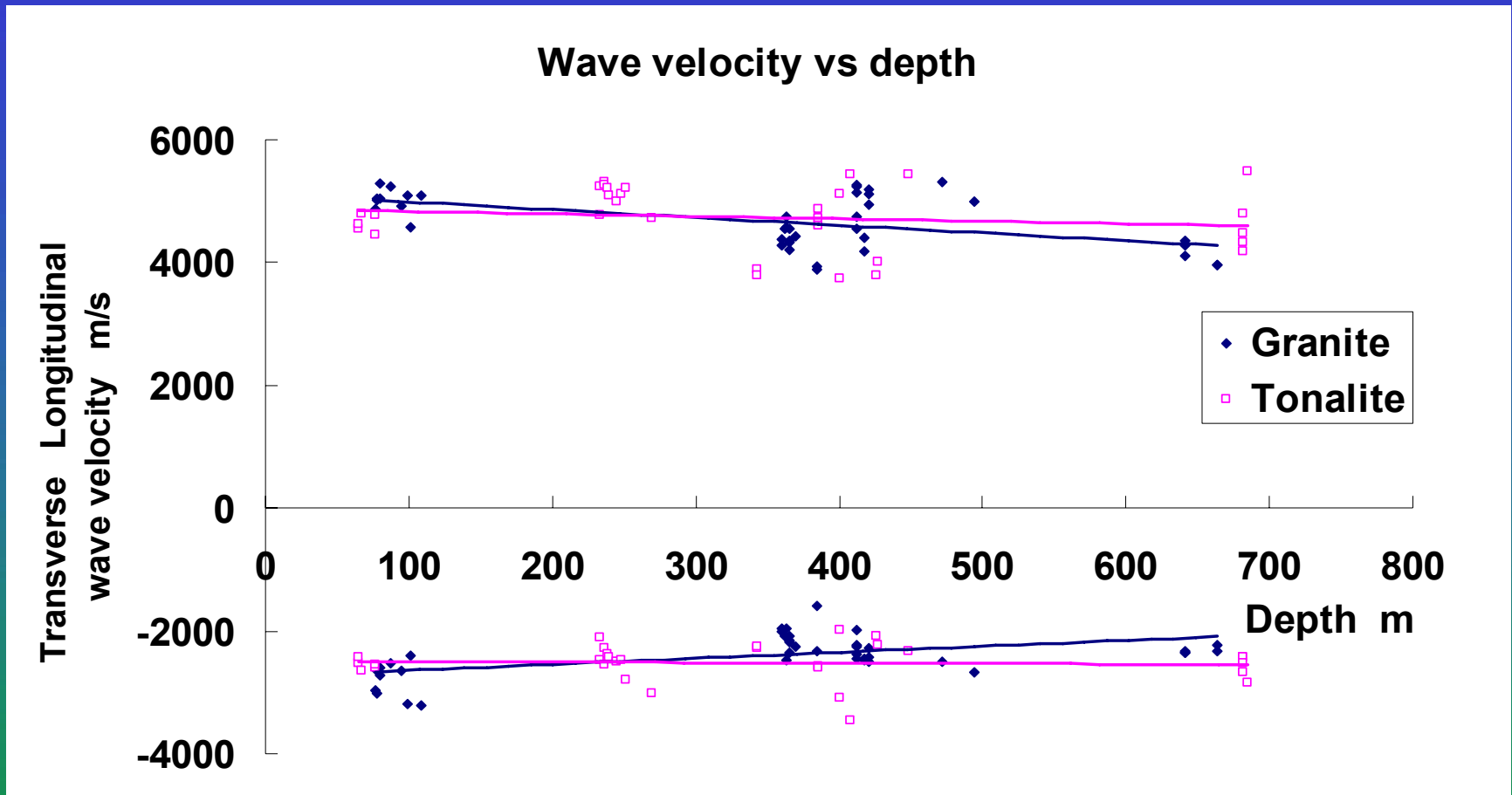


- The density of tonalite is bigger than granite's.
- The density of granite is homogenized.

Percent sorption and porosity factor

- Percent sorption 0.10~0.23%
- Saturation percent sorption 0.15~0.28%
- open porosity factor 0.34~0.65%
- close porosity factor 0.04~0.11%
- total porosity factor 0.44~0.77%

Sound Wave Analyses



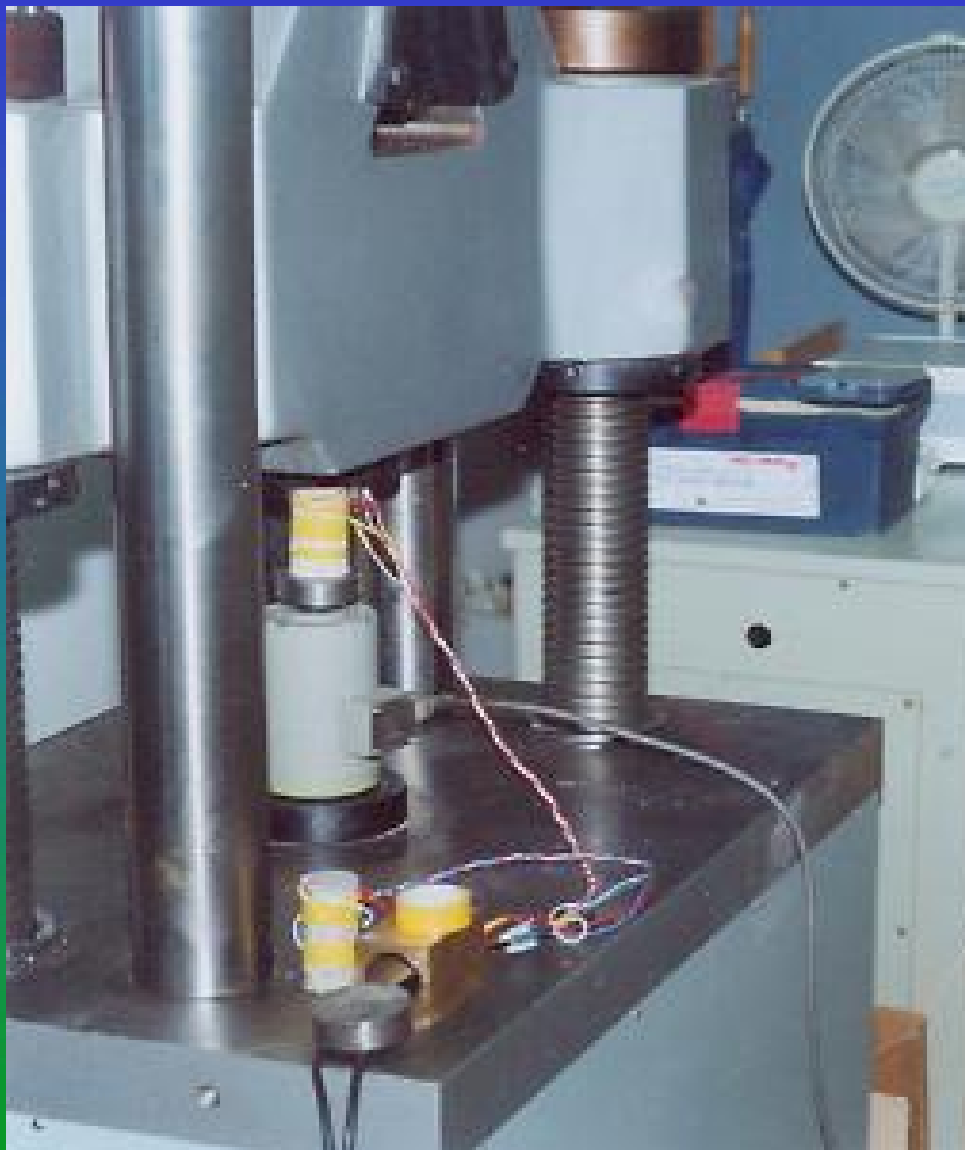
- The wave velocity of granite is less discrete than tonalite.
- Homogenization of granite is higher than tonalite.

- High Density
- High Homogenization
 - porphyritic monzonitic granite
- Low water content
- Low porosity

Mechanical property

- **Uniaxial compressive strength,
Elastic modulus, poisson's ratio**
- **Brazilian tensile strength**
- **Shear strength**
- **Triaxial strength, internal friction angle,
cohesion**

Test of Uniaxial compressive strength

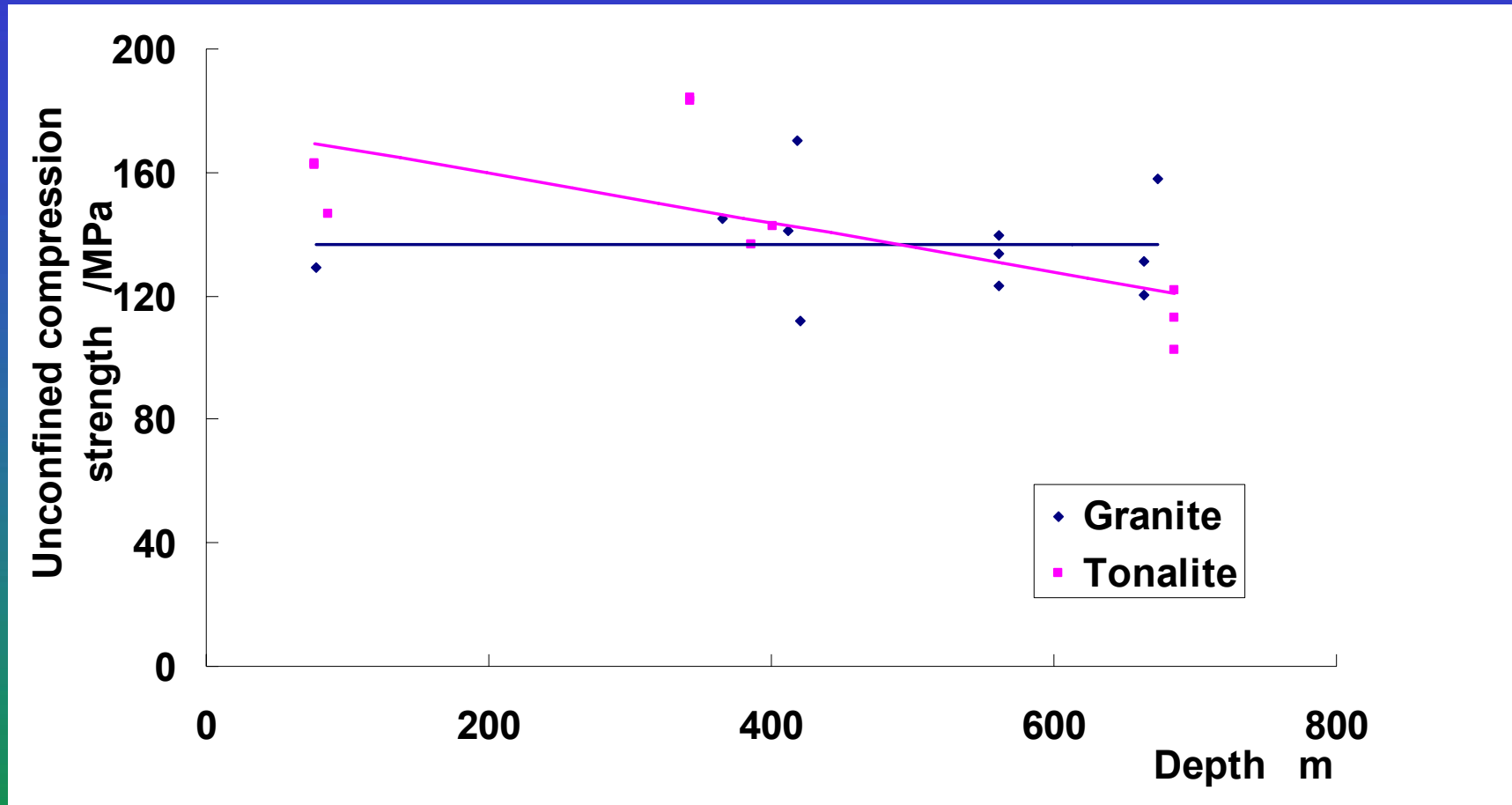


Sample of before compression



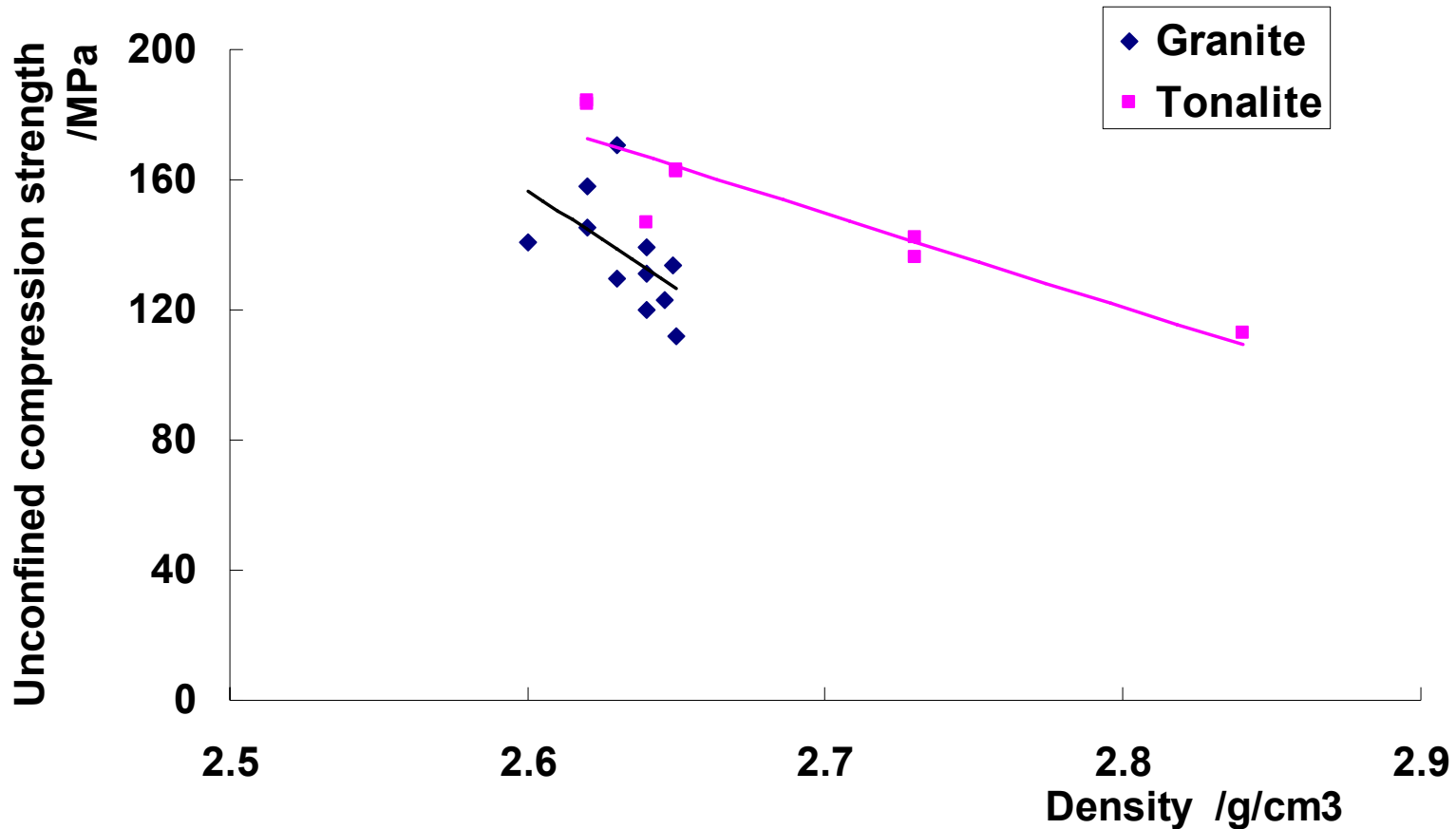
Sample of after compression

Uniaxial compressive strength Analyses



- tonalite 102~184MPa
- porphyritic monzonitic granite 111~171MPa

Uniaxial compressive strength Analyses



The unconfined compression strength of the rock decrease with the density of the rock increase.

Uniaxial compressive strength Analyses

porphyritic monzonitic granite Tonalite

- Uniaxial compressive strength 111~171 102~184Mpa
- Elastic modulus 57~67 41~67Gpa
- Poisson's ratio 0.23~0.31 0.15~0.31

Brazilian Tensile Test

Brazilian Tensile Test

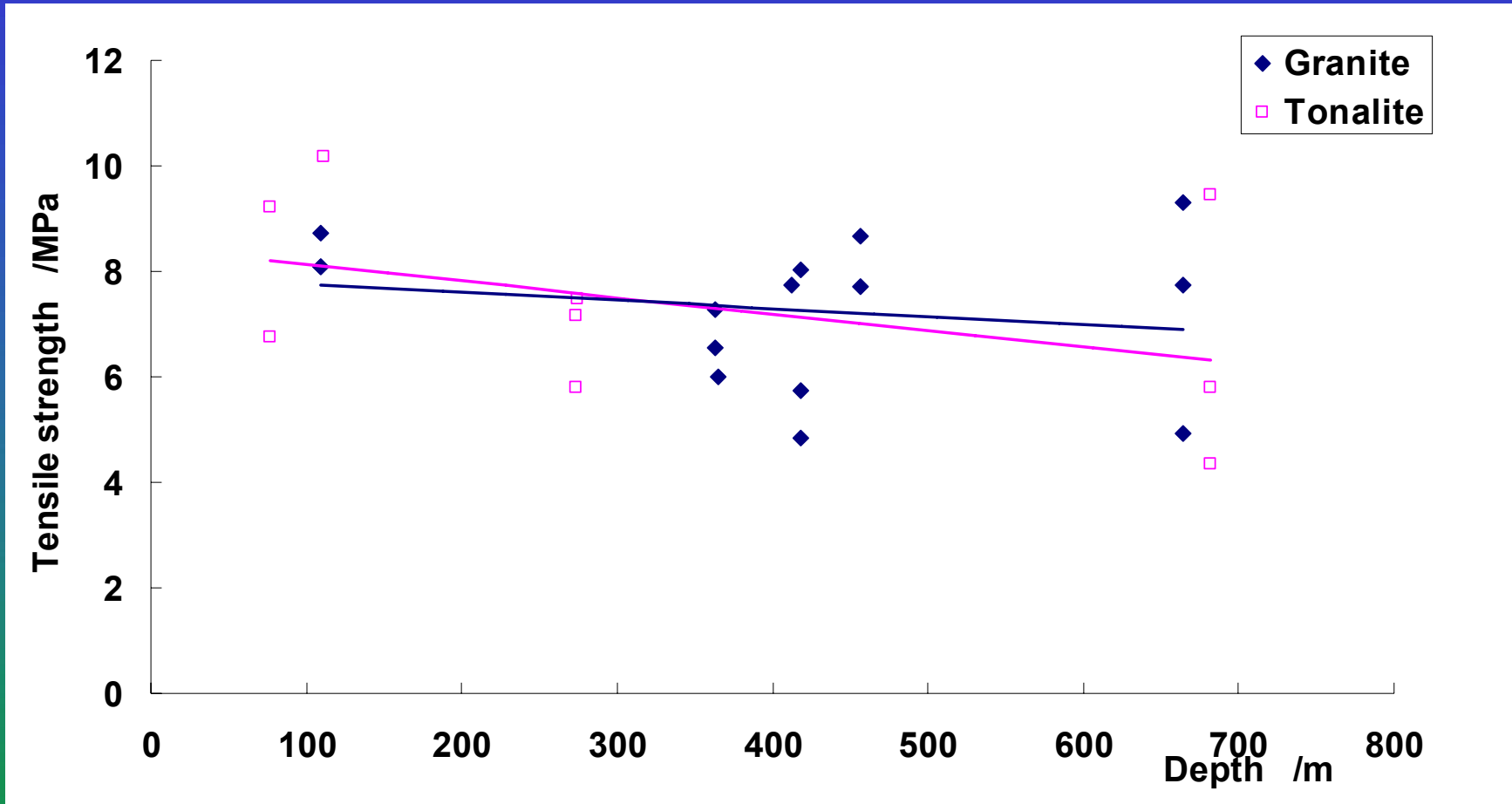


Sample of after tension



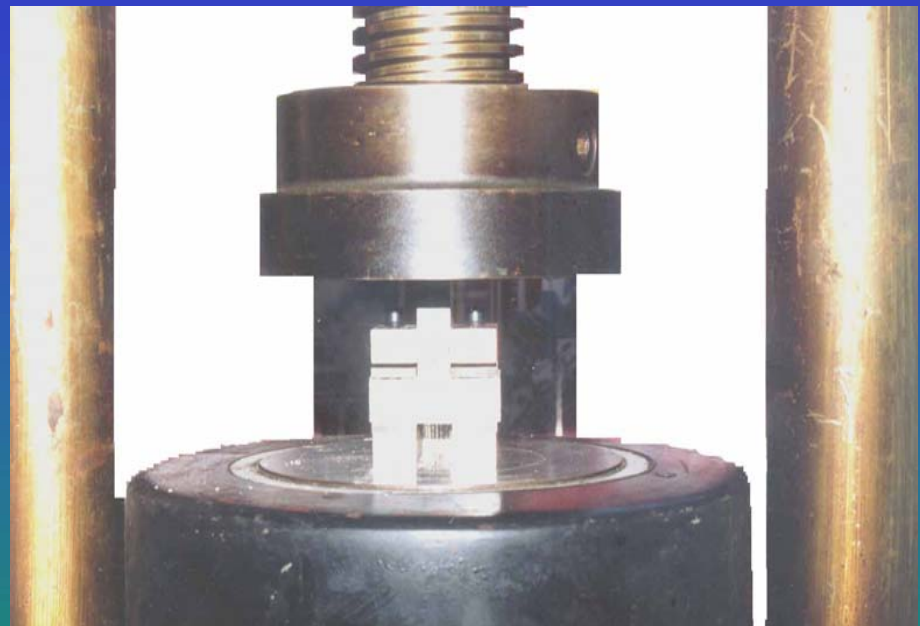
tonalite	Tensile strength 4.36-10.17Mpa
porphyritic monzonitic granite	4.83-9.31Mpa

Brazilian Tensile



Tensile strength decreased appreciably with depth.

Shear Strength Test



Shear Strength Test



Sample of after shear

tonalite

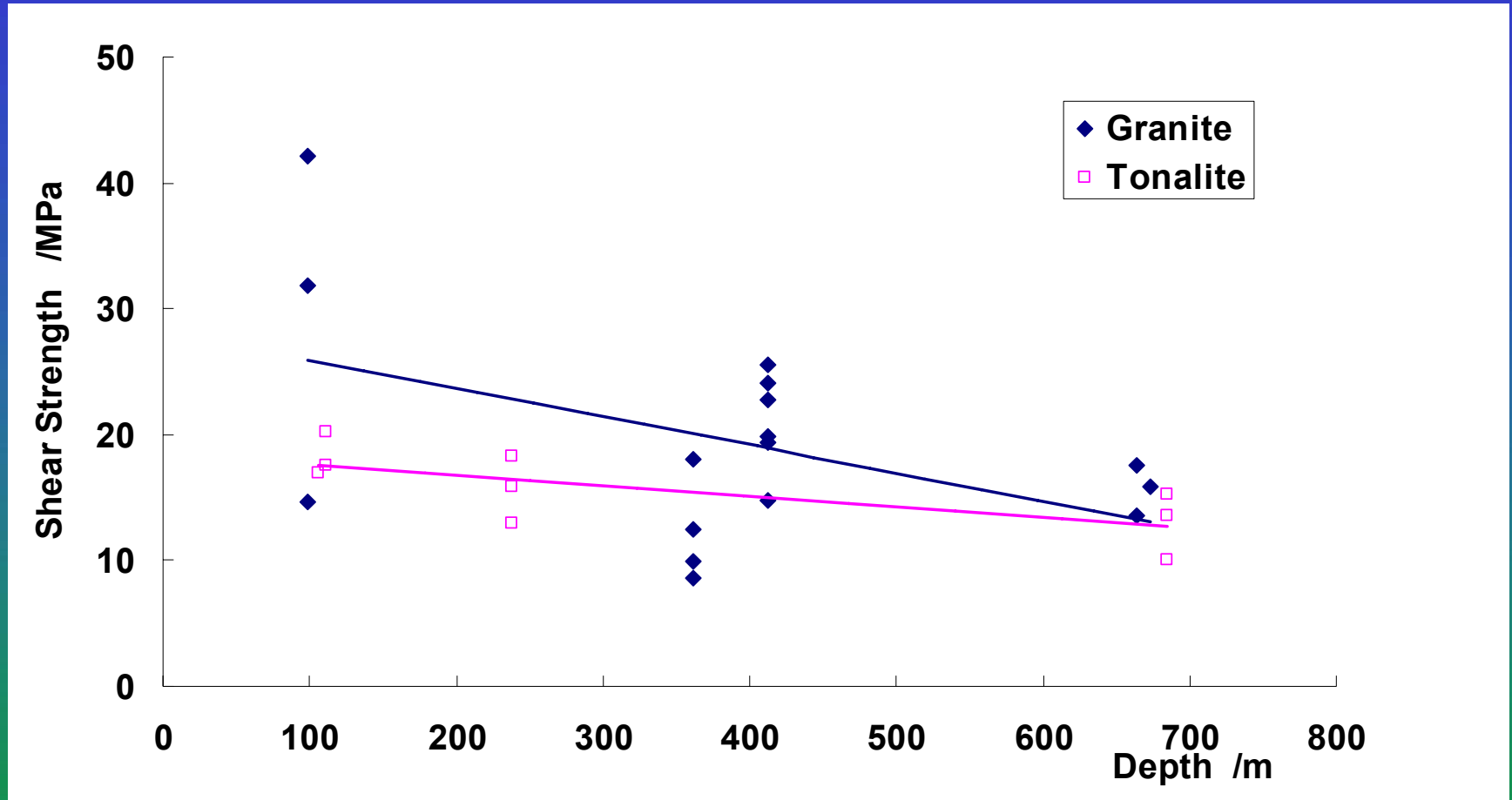
Shear strength

10.1~20.2Mpa

porphyritic monzonitic granite

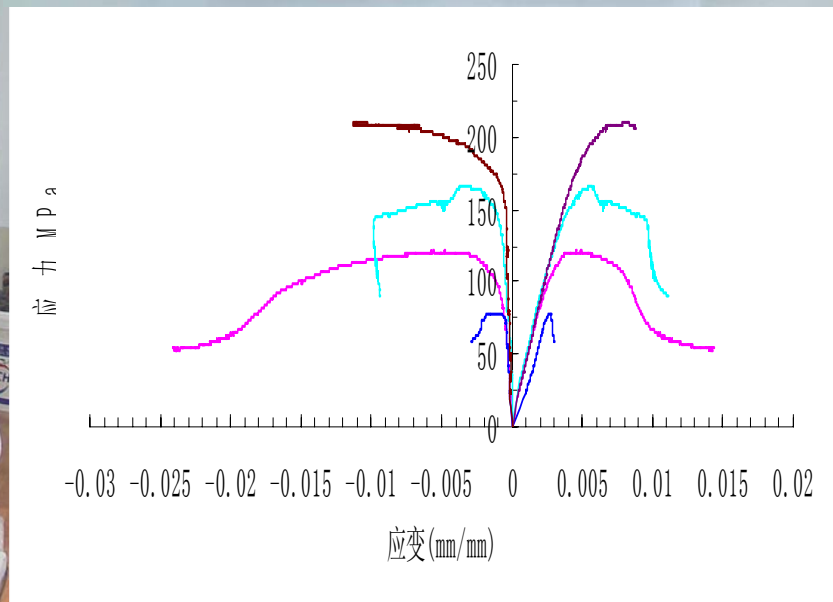
13.6~22.7Mpa

Shear Strength



Shear strength decreased appreciably with depth.

Triaxial strength



Triaxial Compress results analysis

	Internal friction angle	Cohesion
tonalite	45.8~56.2°	29.4~49.9Mpa
porphyritic monzonitic granite	47.7~52.3°	31.1~54.9Mpa

Summary --Mechanical property

- High Uniaxial compressive strength
- High shear strength
- High tensile strength
- Low strain and high brittle

Long-Term Behaviour of Granite under Constant Loading and High Temperature Condition

花岗岩在恒定荷载与高温条件下的长期性状

**Beijing Research Institute of Uranium Geology, CNNC
Department of Civil Engineering, The University of Hong Kong**

Beijing Research Institute of Uranium Geology, CNNC

Test plan

<i>Confining pressure (MPa)</i>	<i>Stress ratio</i>	<i>Temperature (°C)</i>		
		<i>RT(23)</i>	<i>50</i>	<i>90</i>
<i>0</i>	<i>1.10</i>	✓	✓	✓
	<i>1.15</i>	✓	✓	✓
	<i>1.20</i>	✓	✓	✓
	<i>1.25</i>	✓	✓	✓
<i>10</i>	<i>1.20</i>	✓	✓	✓
	<i>1.25</i>	✓	✓	✓
	<i>1.30</i>	✓	✓	✓
	<i>1.35</i>	✓	✓	✓
<i>30</i>	<i>1.25</i>	✓	✓	✓
	<i>1.30</i>	✓	✓	✓
	<i>1.40</i>	✓	✓	✓
	<i>1.55</i>	✓	✓	✓

Test facilities

MTS 815



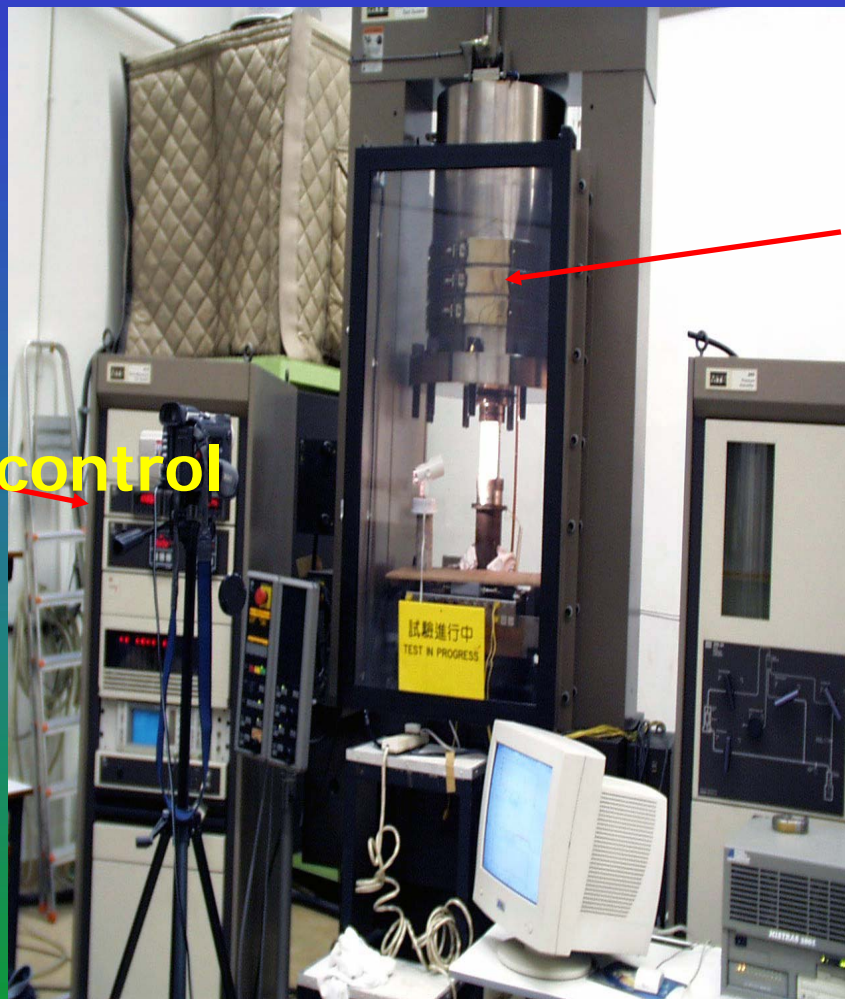
MISTRAS 2001
(Acoustic emission rate)



前置

数据
采集
计算机

High temperature tests



Temperature control

Heat band

Sample



$\Phi 50 \times 125 \text{mm}$ (ASTM D4543)

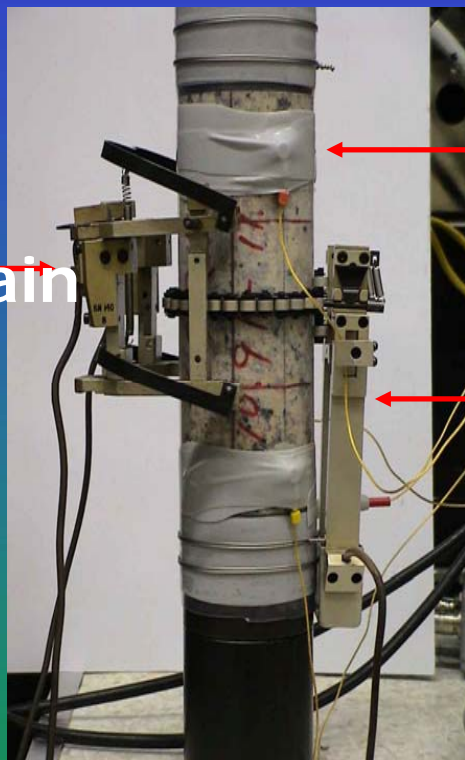
Before test:

Put in water more than 30 days

Measure P wave velocity



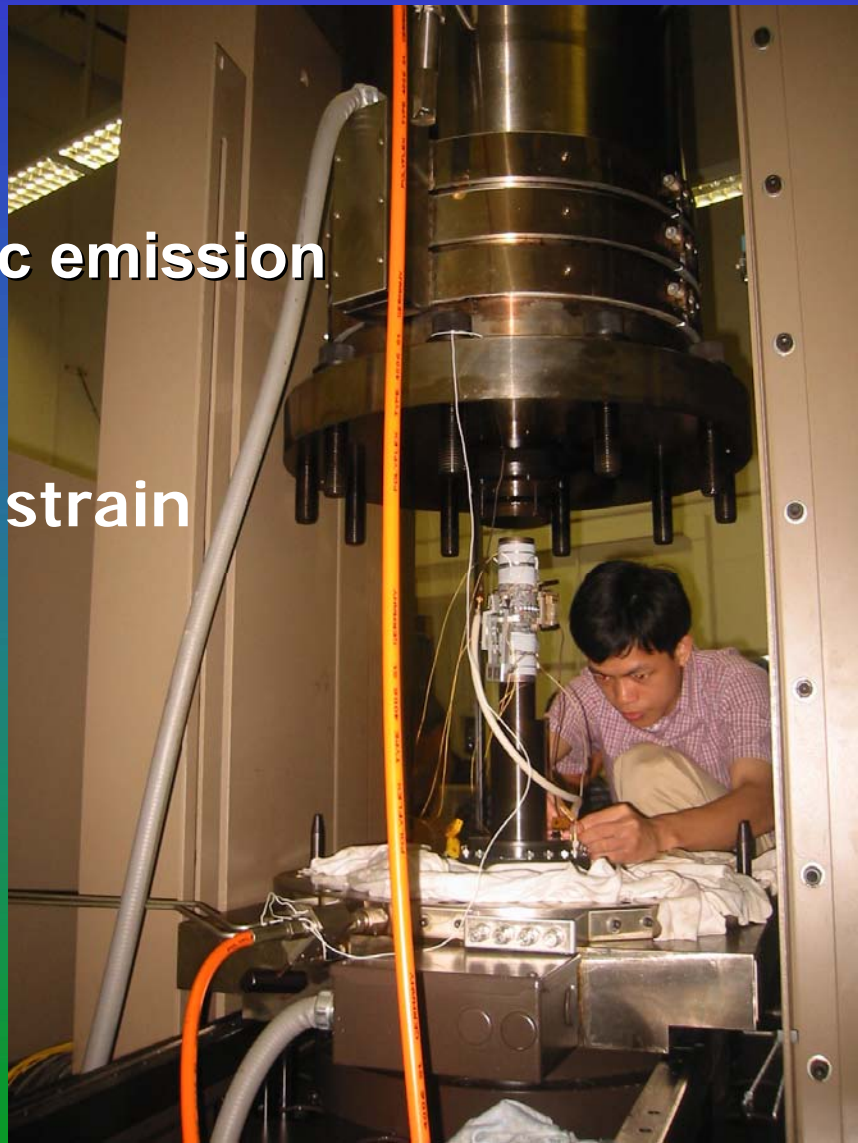
Assemble sample



Acoustic emission

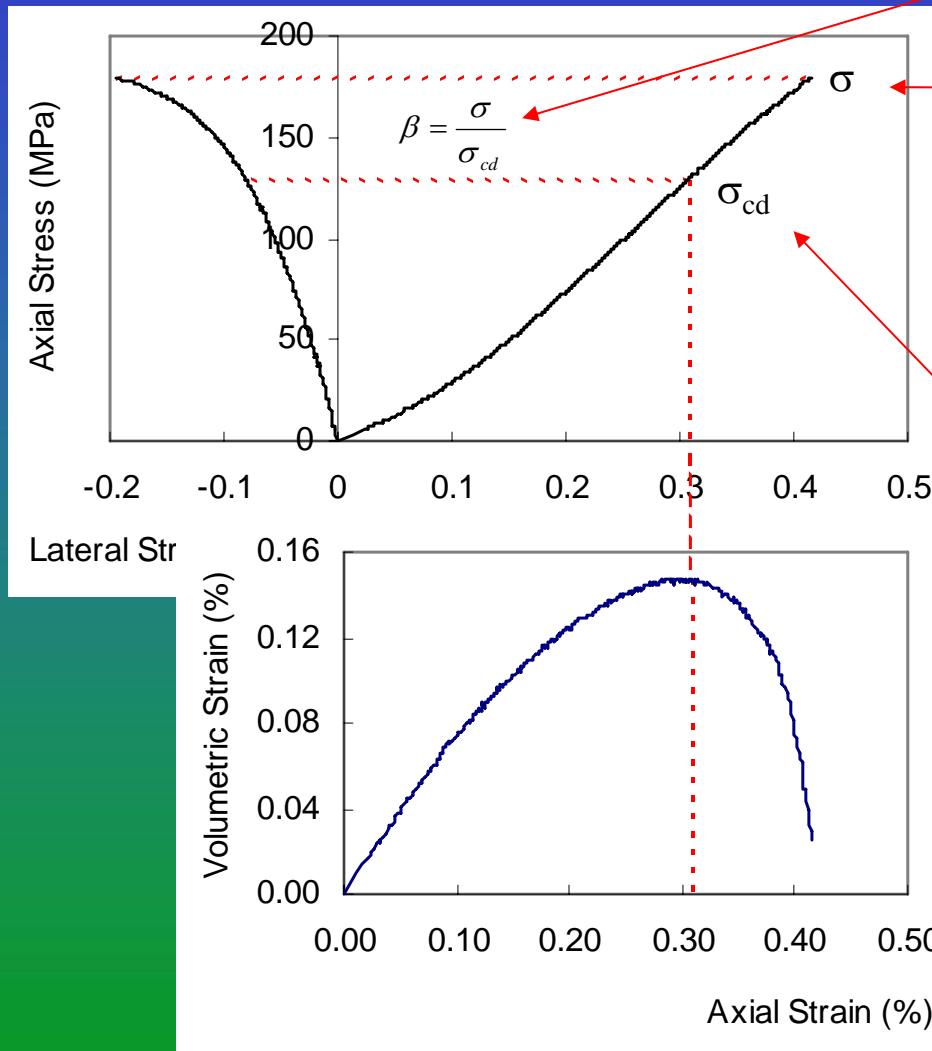
Axial strain

Lateral strain



Test procedure

Stress ratio



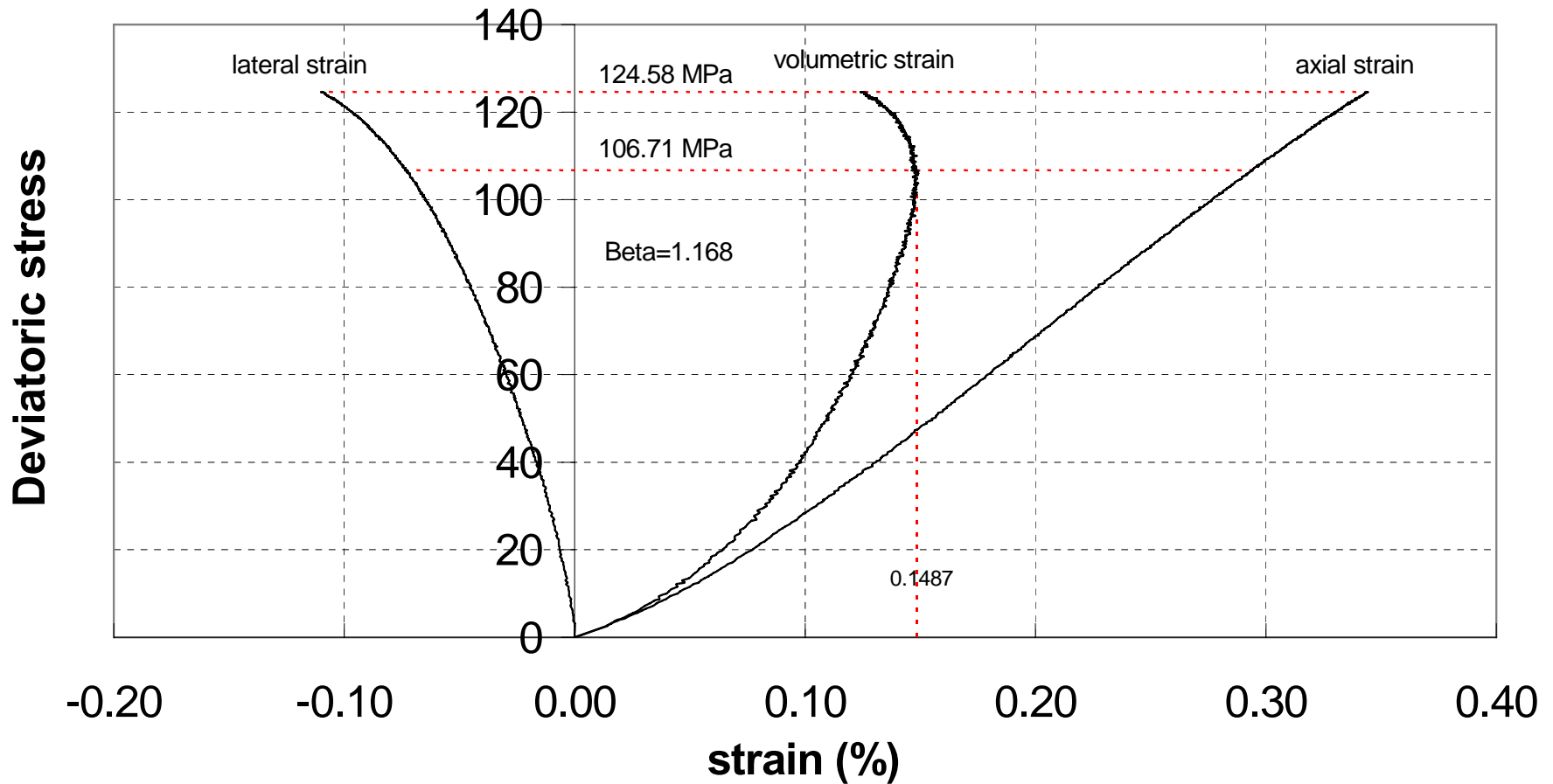
2. Hold constant loading

1. determine σ_{cd}

- Vol. strain reversal
- Unstable crack growth
- Related to long-term strength

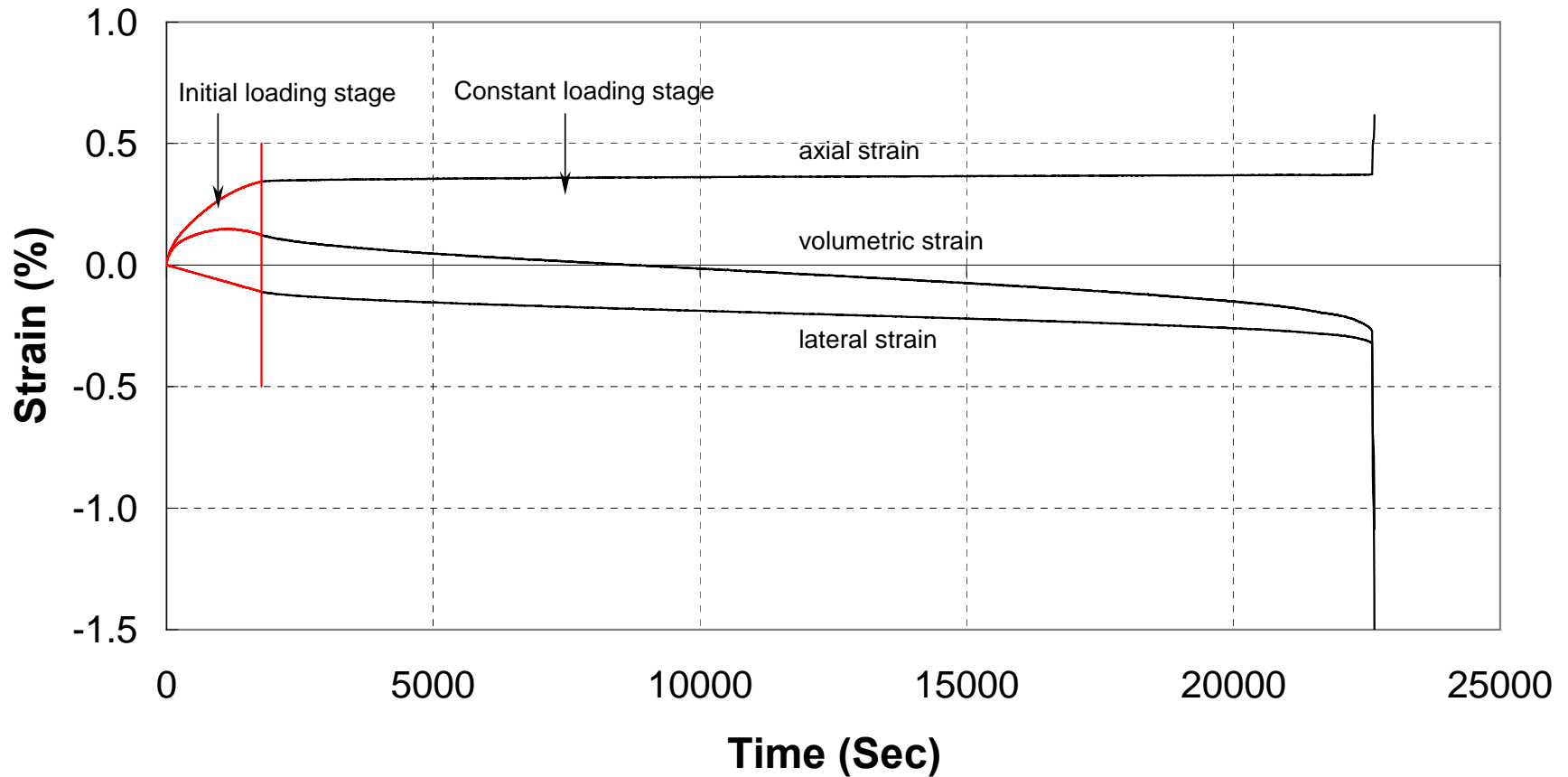
Stress-strain curve

Initial loading stage stress-strain curve (BS01RTN02-2)



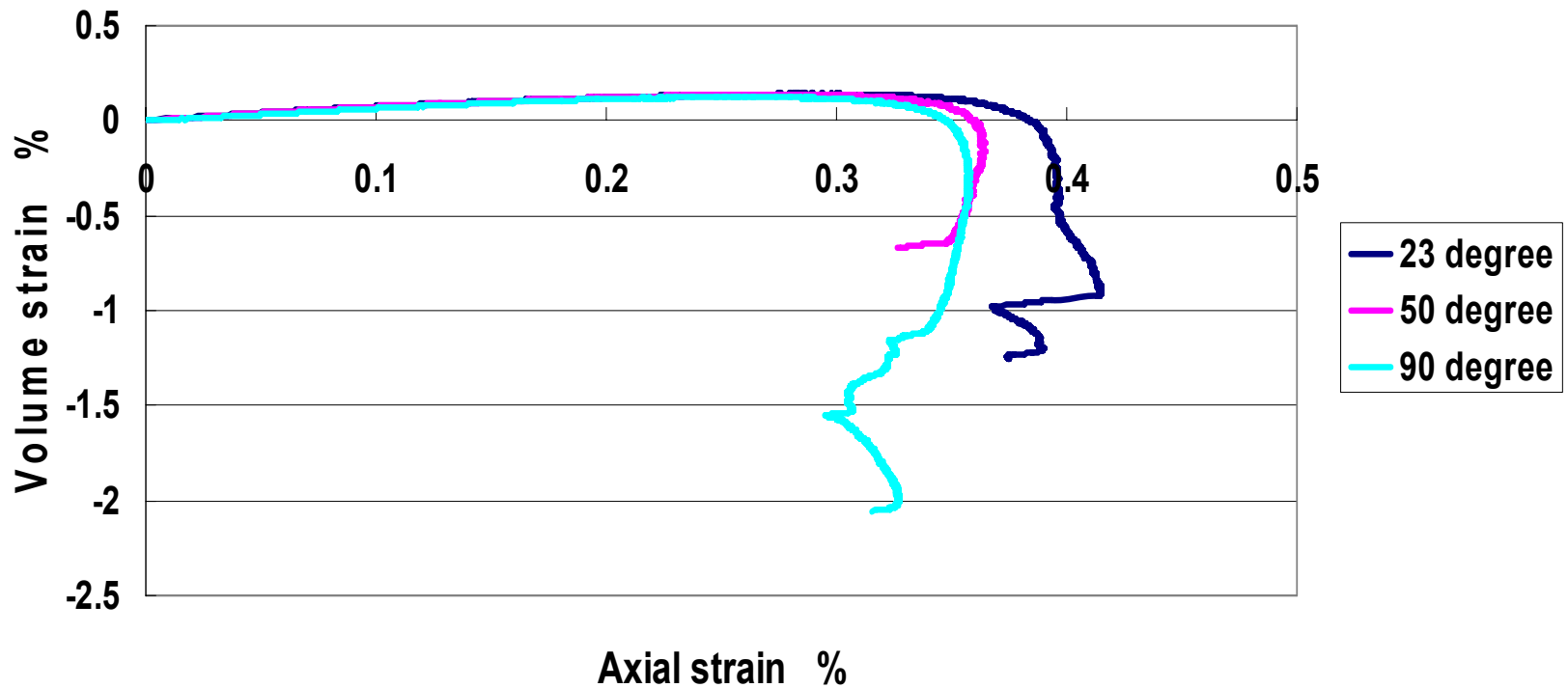
Strain-time curves

Combined strain vs time curve (BS01RTM02-2)



Vol. strain vs Axial strain

Axial strain vs volume strain



Axial strain and volume strain decrease as temperature increase.

Sample failed

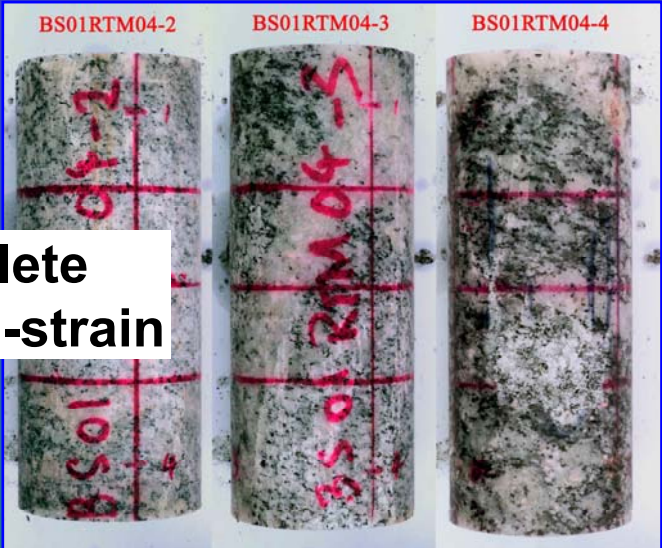


Φ50 X 125 mm, 90℃, 恒载223KN,
破坏时响声很大, 岩样分为两大块

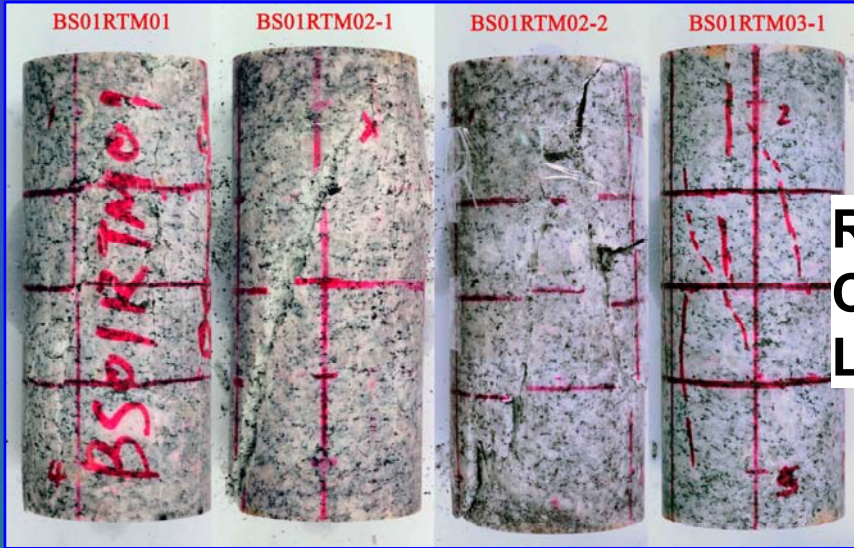
2004. 07. 2—07. 20



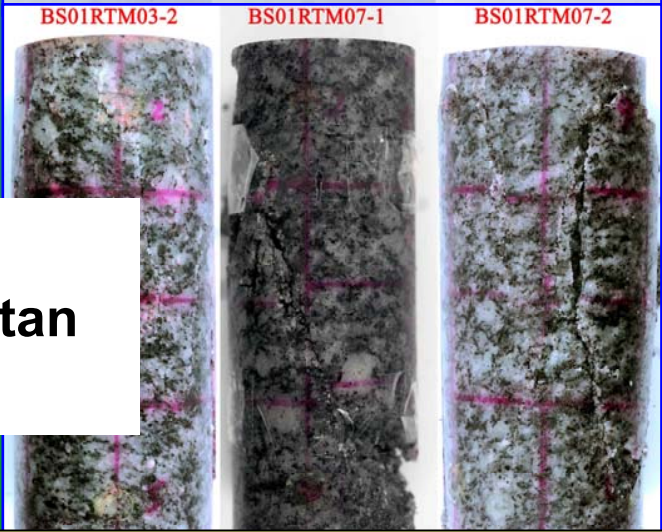
Samples after tests



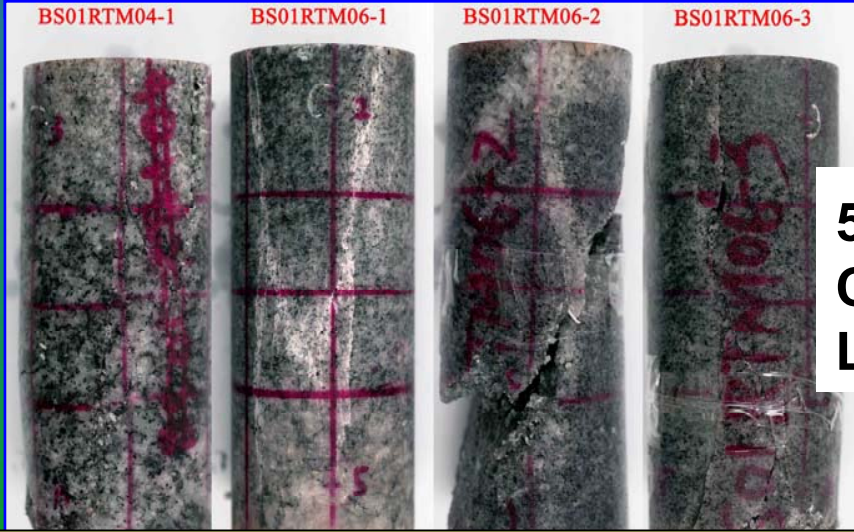
Complete stress-strain



RT Constant Load



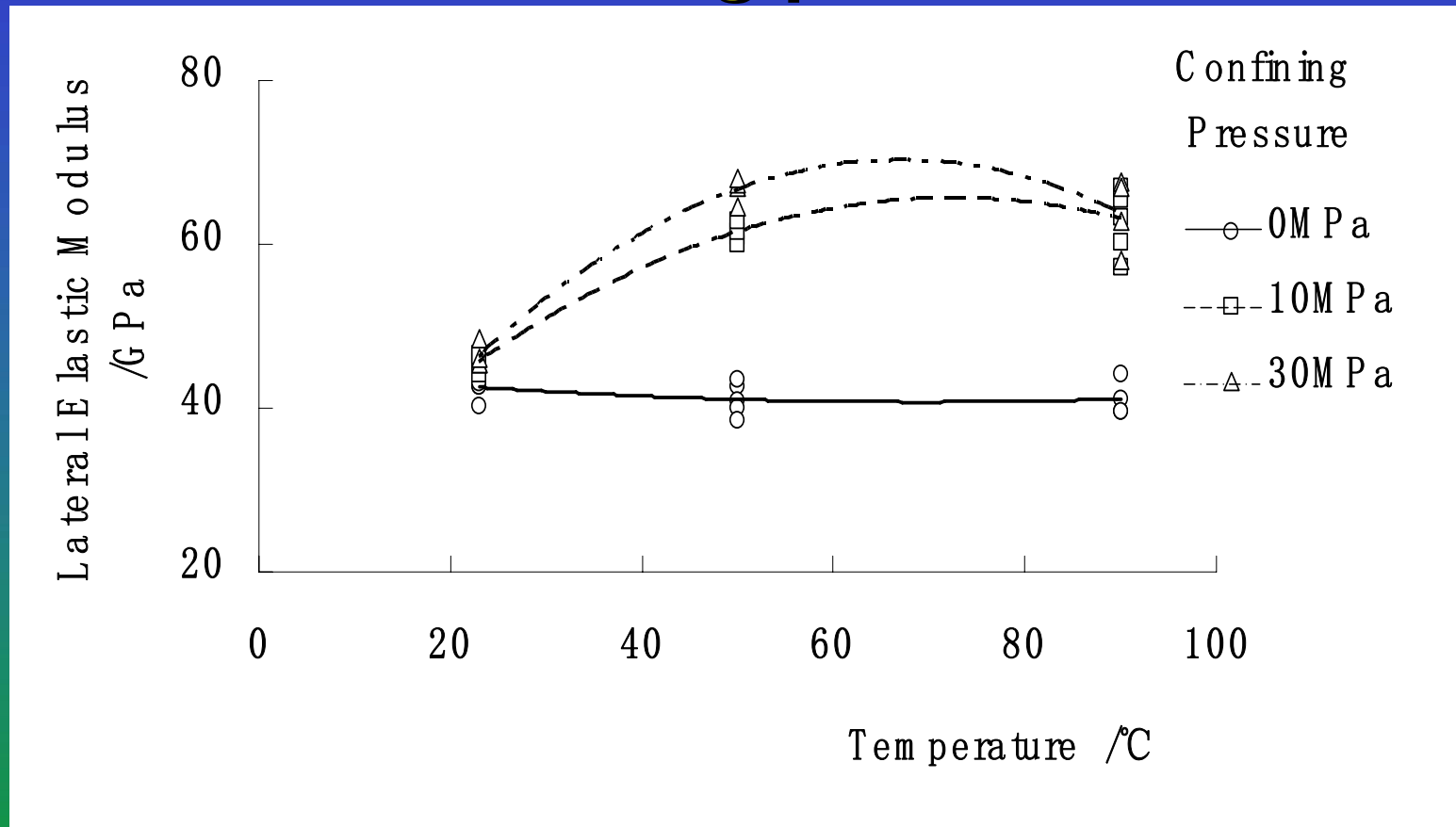
90 °C Constant Load



50 °C Constant Load

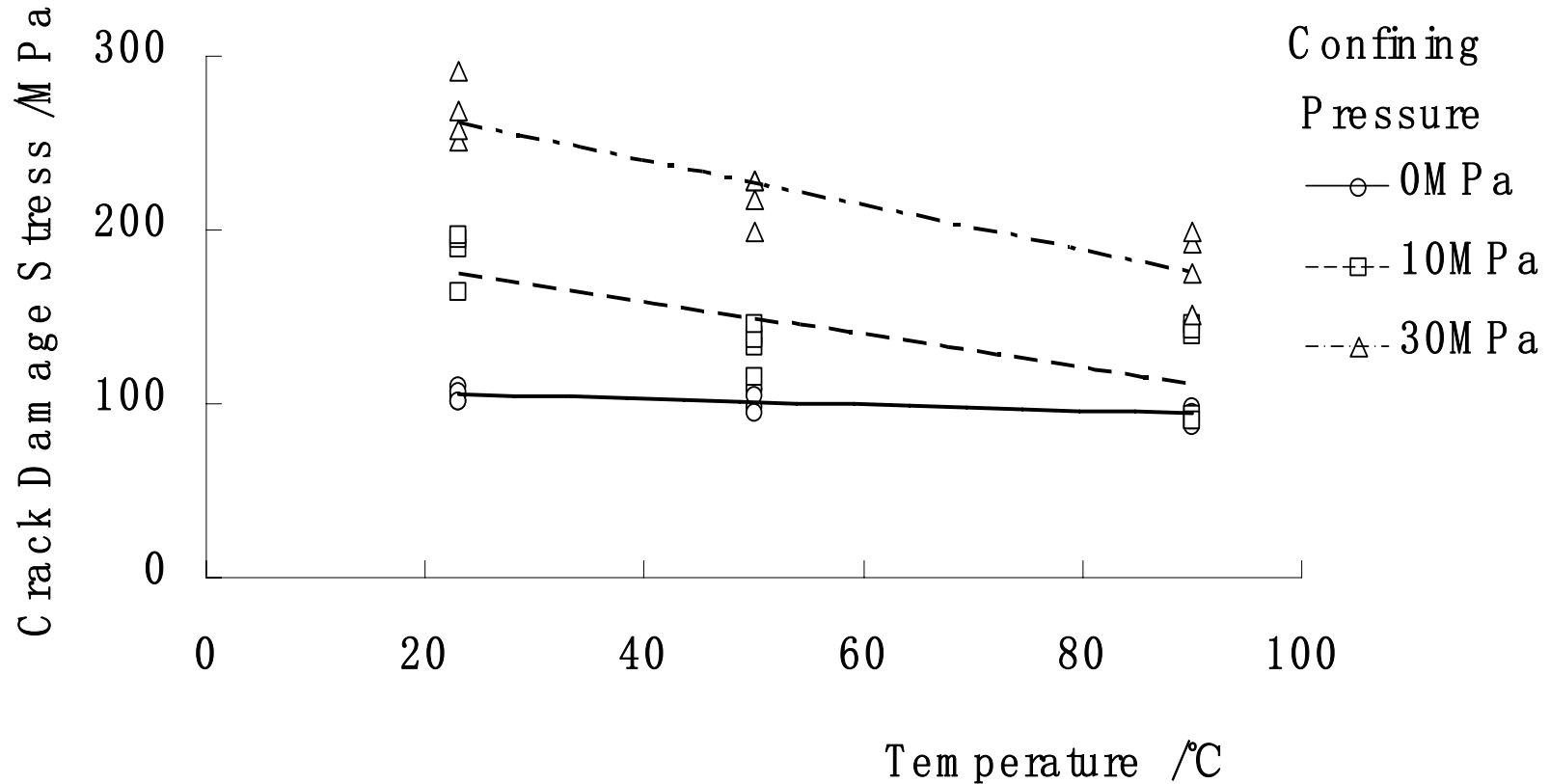
The tests are done under uniaxial and different temperatures.

Elastic modulus with Temperature and Confining pressure



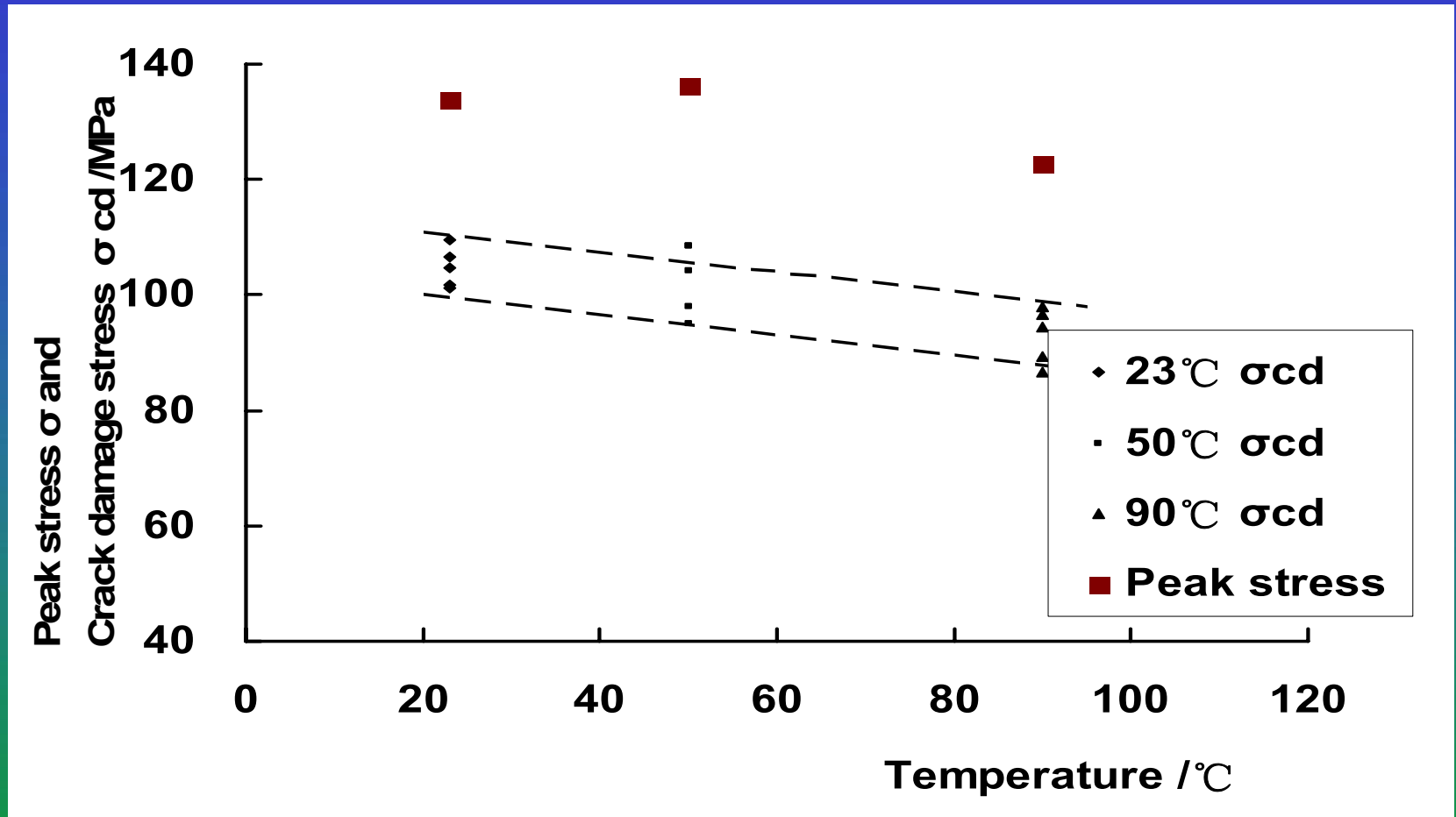
Elastic modulus increase when confining pressure increase, increase then decrease when temperature increase.

Crack damage stress with Temperature and Confining pressure



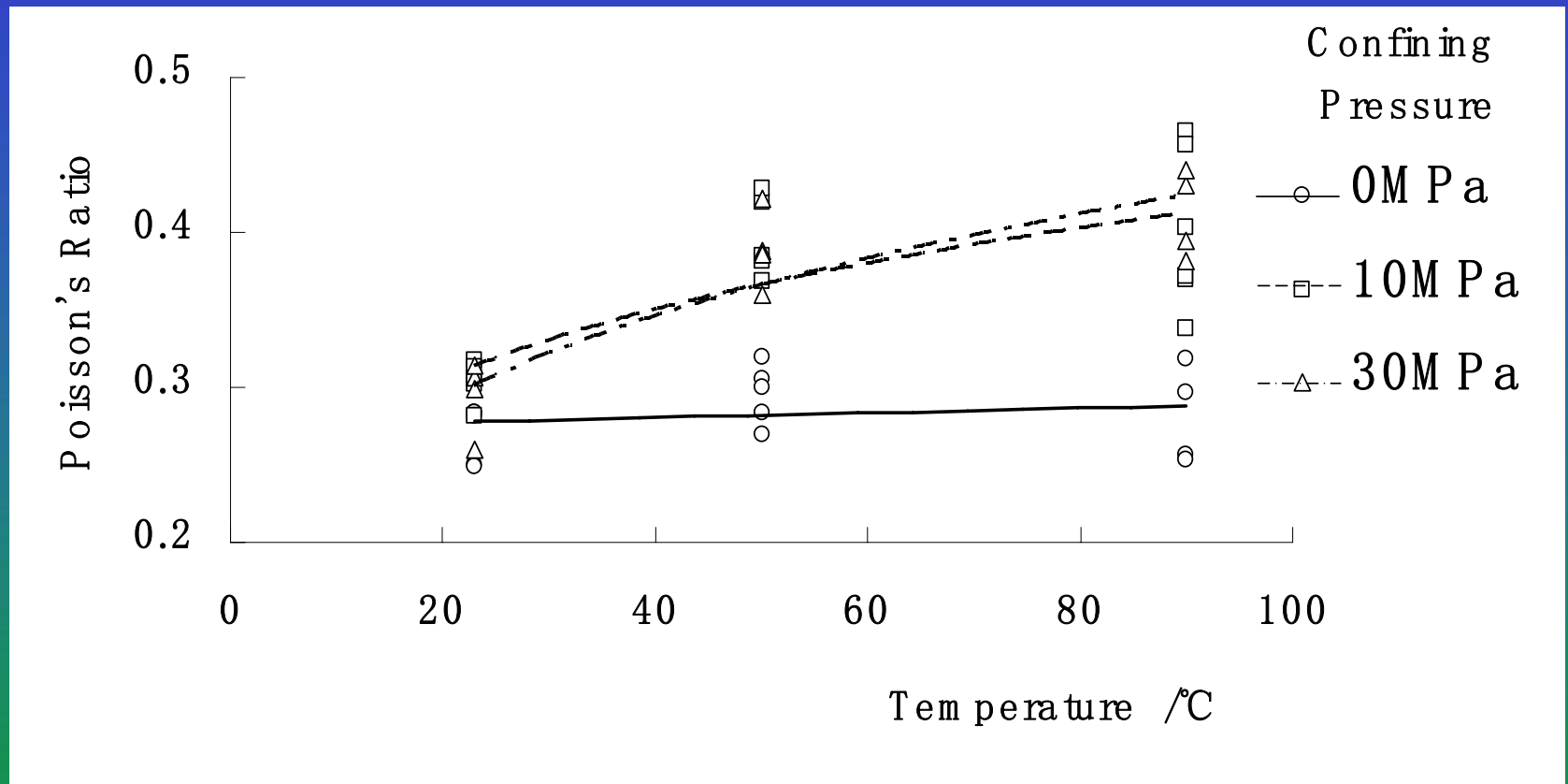
Crack damage stress increase when confining pressure increase and decrease when temperature increase

Peak and Crack damage stress with T



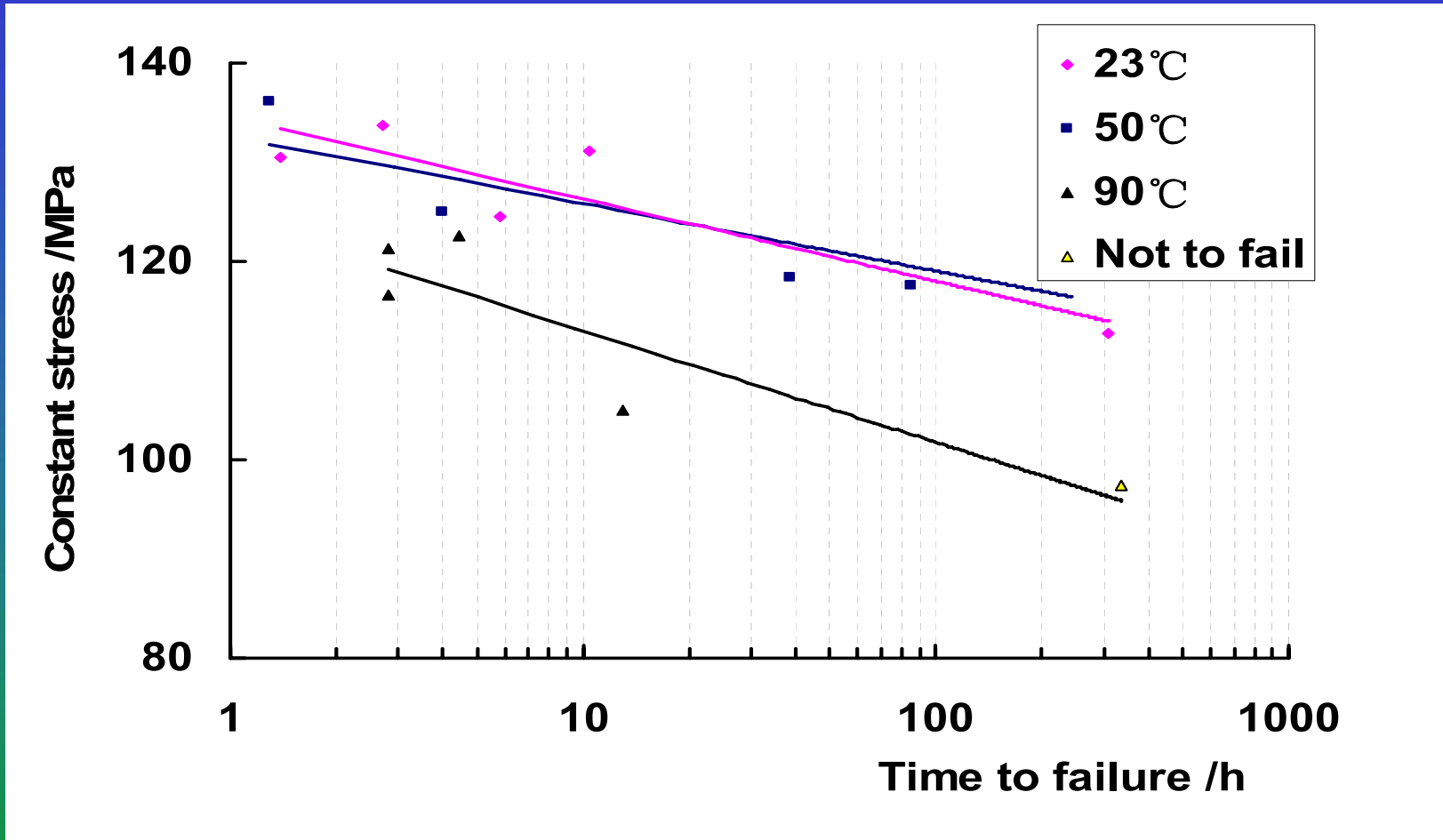
Peak stress and Crack damage stress decrease when temperature increase

Poisson's ratio with Temperature and Confining pressure



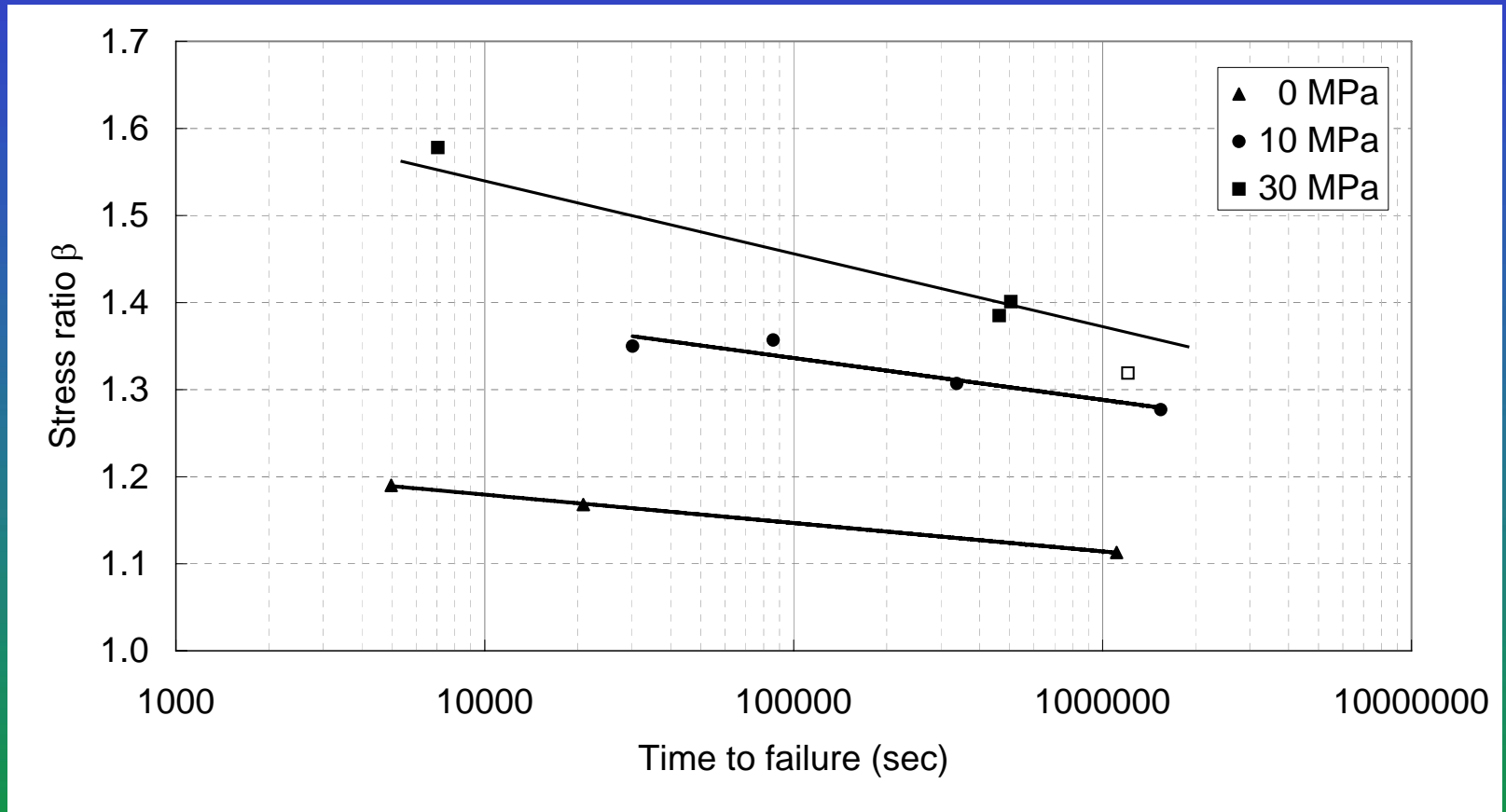
Poisson's ratio increase when confining pressure and temperature increase

Constant stress with time



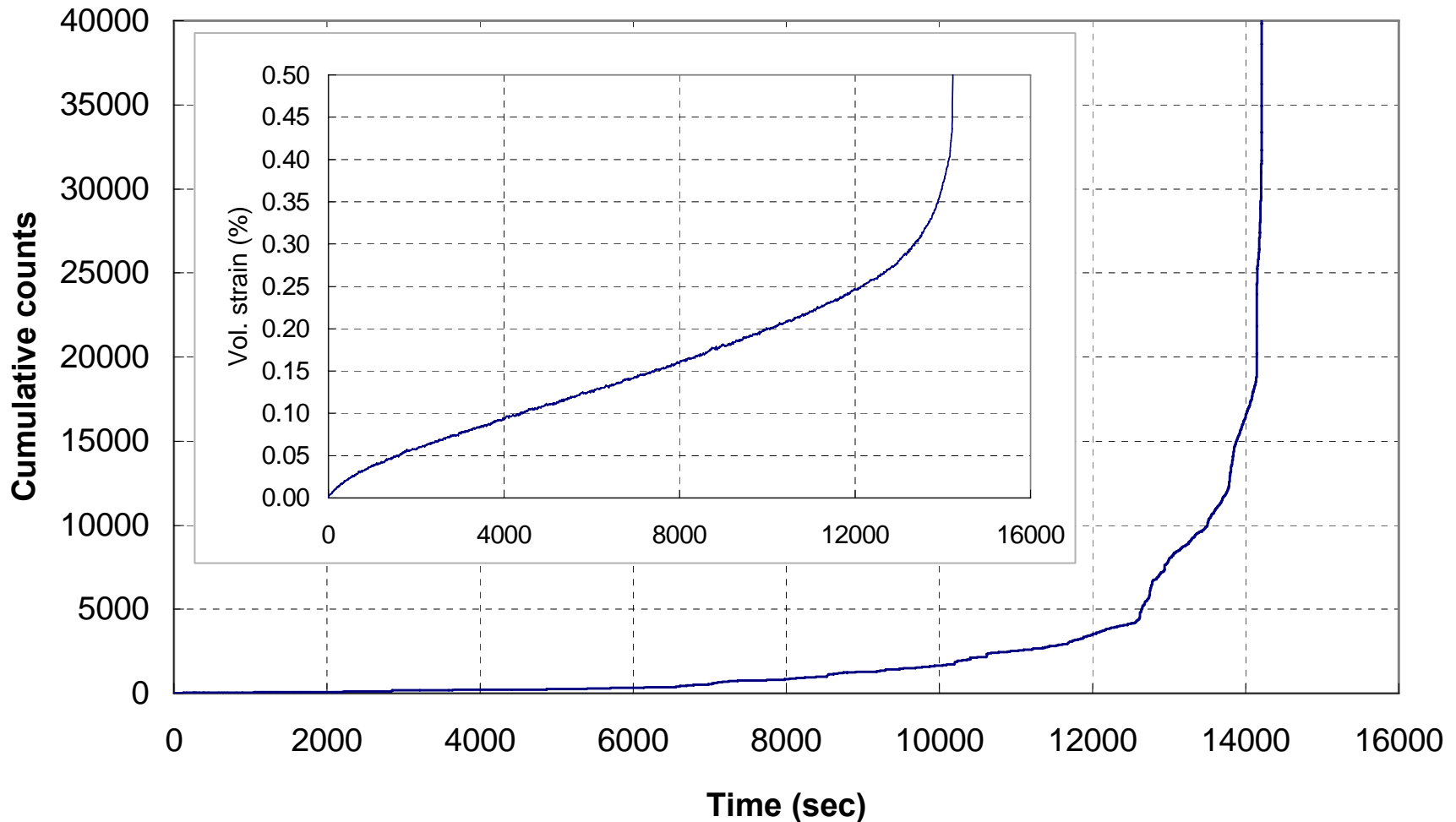
The time to failure increases rapidly when the constant load decreases.
 Time to failure decrease when temperature increase.

Constant stress with confining pressure



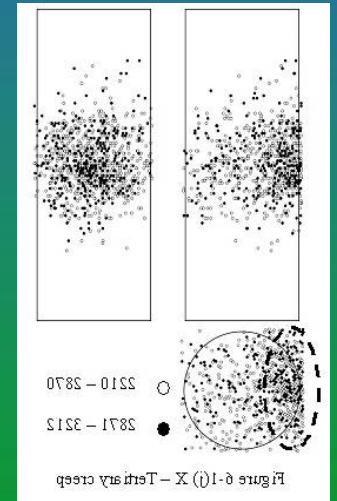
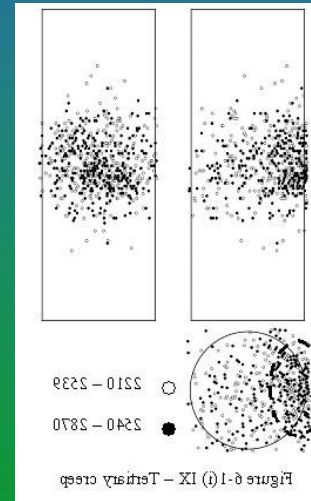
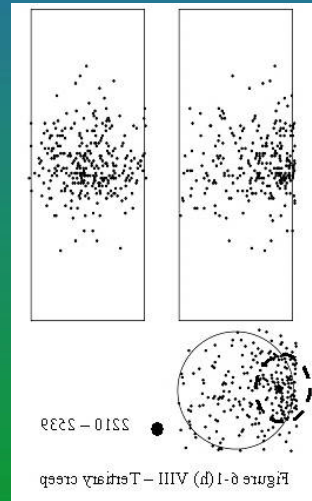
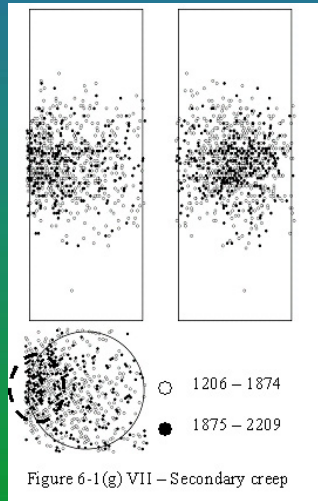
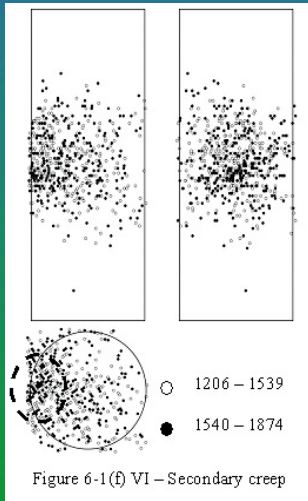
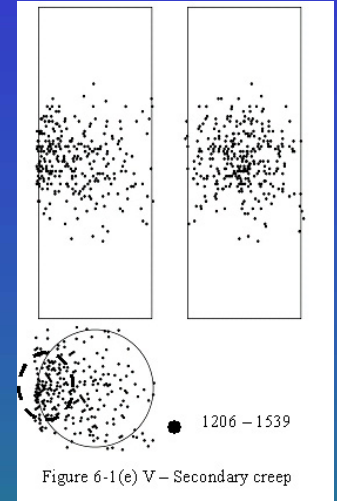
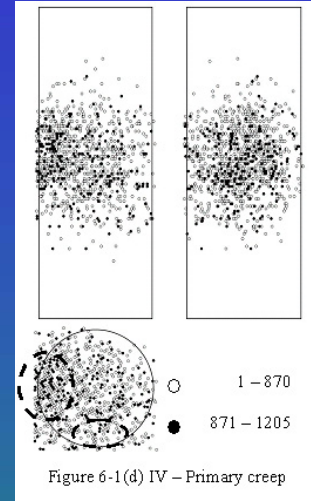
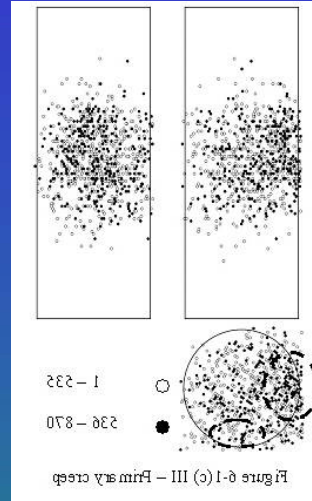
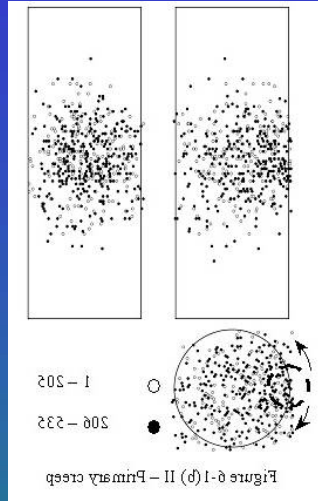
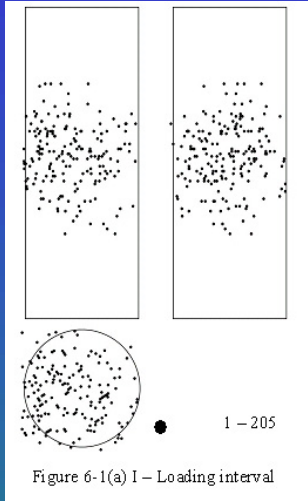
The time to failure increases rapidly when the stress ratio decreases and confining pressure increase

AE rate and Vol. strain vs time



The trend is quite similar, but AE is more sensitive and well represent the start of accelerating creep stage.

Acoustic emissions record



Acoustic emissions record

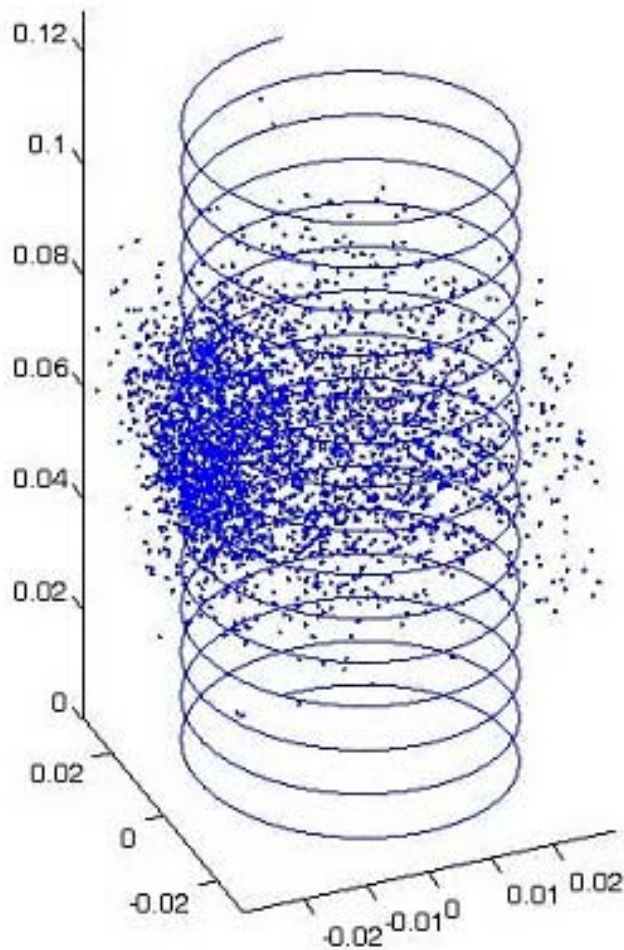


Figure 6-2 Stereoscopic projection of acoustic emission hypocentres

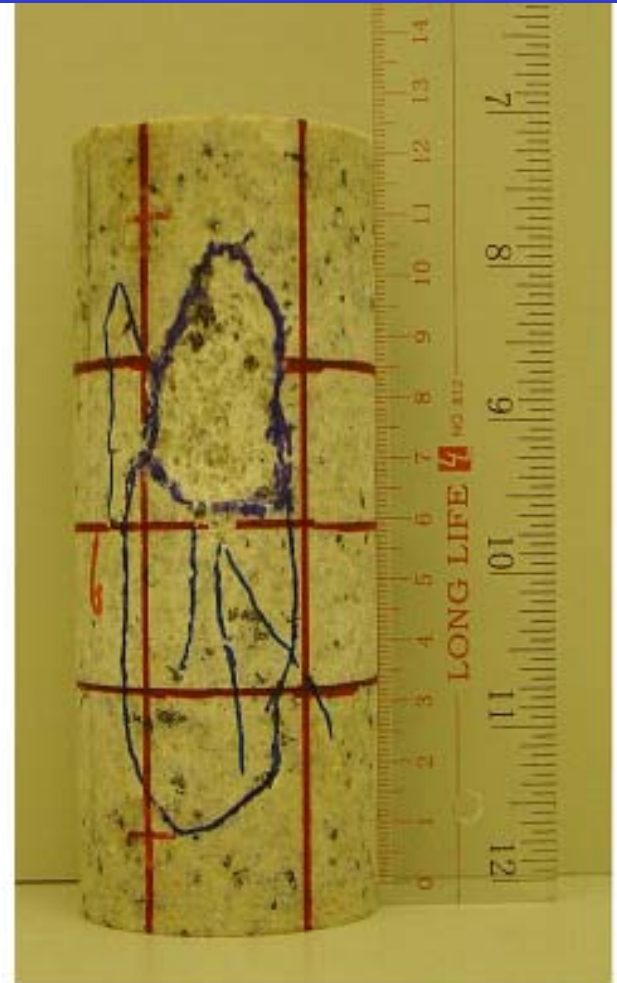


Figure 6-3 Photo of the failed sample showing the actual faulting

Conclusion-1

- **High Density and high homogenization (porphyritic monzonitic granite)**
- **Low porosity, Low water content**
- **High Uniaxial compressive strength, shear strength and tensile strength**
- **Low strain and high brittle**

Conclusion-2

- Temperature has significant influence on the property of granite when confining pressure increase.
- Elastic modulus, Crack damage stress, Poisson's ratio and peak stress increase when confining pressure increase.
- when temperature increase, Elastic modulus increase then decrease, Crack damage stress decrease and Poisson's ratio increase

Conclusion-3

- Time to failure decrease when temperature increase.
- The time to failure increases rapidly when the constant load or the stress ratio decreases and confining pressure increase
- AE is more sensitive and well represent the start of accelerating creep stage.

谢谢!

Thank you!

Handling of Nuclear waste in Germany in the Light of Final Disposal

Dipl.-Ing. Michael Sailer

中德放射性废物处置研讨会
**CHINESE-GERMAN WORKSHOP ON RADIOACTIVE WASTE
DISPOSAL**

May 28 – 31, 2007

Sino-German Science Centre, Beijing, CHINA

Content

- General overview
- Clearance
- Non heat generating waste
- Heat generating waste
- Conclusions

General overview (1)

- Germany is using nuclear materials and nuclear power since more than 50 years
- Nuclear waste mainly stems from
 - Operation of nuclear power plants
 - Research facilities and research reactors
 - Decommissioning of nuclear installations
 - Industrial and medical application

General Overview (2)

- Basic policy is to dispose German radioactive waste in Germany
- Waste from nuclear activities:
 - Heat generating waste, i.e. high active waste
 - Non heat generating waste, i.e. low and medium active waste
 - waste discarded according to clearance procedures

Clearance (1)

- Clearance is based on the 10 μSv concept
- annual collective dose from entire clearance operations in Germany checked against 1 person-Sv criterion
- Clearance levels
 - available for various clearance options
 - derived from radiological analyses taking account of all relevant characteristics of particular clearance option



Clearance (2)

- Clearance is widely used at decommissioning, more than 95% of the masses of nuclear installations can be handled in that way
- Clearance is also used for waste from operation
- After clearance the material do not remain under governance of the atomic act
- Clearance seriously reduces the amount of low active waste

Final Disposal for Non heat generating waste

- No separation of waste with long living and short living isotopes in Germany
- Deep underground disposal is necessary to provide protection of biosphere
- Disposal facility will be Schacht Konrad
- After court decisions in 2006 and 2007 the way is open to start with construction work
- Start of operation is foreseen for the year 2013

Konrad repository

History	Abandoned iron ore mine
Location	Salzgitter, Northern Germany
Host rock	Coral Oolite
Emplacement depth	800 m to 1,300 m
Type of waste	Non heat generating waste
Volume of waste packages	303,000 m³
Total alpha emitter activity	1.5 · 10¹⁷ Bq
Total beta/gamma emitter activity	5.0 · 10¹⁸ Bq



Actual Inventory of Non heat generating waste

Type of waste December, 31 th , 2004	With negligible heat generation [m ³]	Heat-generating (without spent fuel) [m ³]
Untreated waste (raw waste with residues yet to be recycled)	29,773	56
Interim products	7,902 (2001: 4,675)	
Conditioned waste	82,645	1,743
Disposed waste in Morsleben repository and research mine Asse	83,753	

Handling of Non heat generating waste (1)

- Raw waste has to be conditioned according the Schacht Konrad acceptance criteria
- Conditioning methods used:
 - incineration
 - high pressure compactation
 - evaporation (liquids)
 - fixation by concrete

Handling of Non heat generating waste (2)

- Conditioning provided by
 - external facilities
 - on-site with mobile facilities
 - on-site with fixed installations
- Conditioned packages have to be approved by BfS

Handling of Non heat generating waste (3)

- Conditioned waste has to be stored in interim storage facilities
 - on-site facilities (e.g. NPPs, research centers)
 - external facilities (e.g. Mitterteich, Gorleben interim storage facilities)

Handling of Non heat generating waste (4)

- Package forms according Schacht Konrad acceptance criteria
 - Different kinds of specified drums
 - Container with drums inside



Handling of Non heat generating waste (5)

- Special collection system for small producers
 - Each state provides
 - collection system
 - advises regarding conditioning and characterization
 - state operated interim storage facility, so-called “Landessammelstelle”
- Accepted waste is formally owned by state

Special questions regarding Non heat generating waste

- Characterisation of very old waste (partially lack of information about content)
- Waste with high content of alpha emitting isotopes or other special isotopes e.g. C-14 (exceeds acceptance criteria of Schacht Konrad → other solution for disposal is necessary)

Disposal site for Heat generating waste

- Disposal in deep underground in a special facility for heat generating waste
- Decision on site is pending. Moratorium exists since 2000. Two proposals within federal government:
 - To continue with the research in Gorleben salt dome
 - To compare several other possible sites with Gorleben to check whether a remarkable better site than Gorleben exists

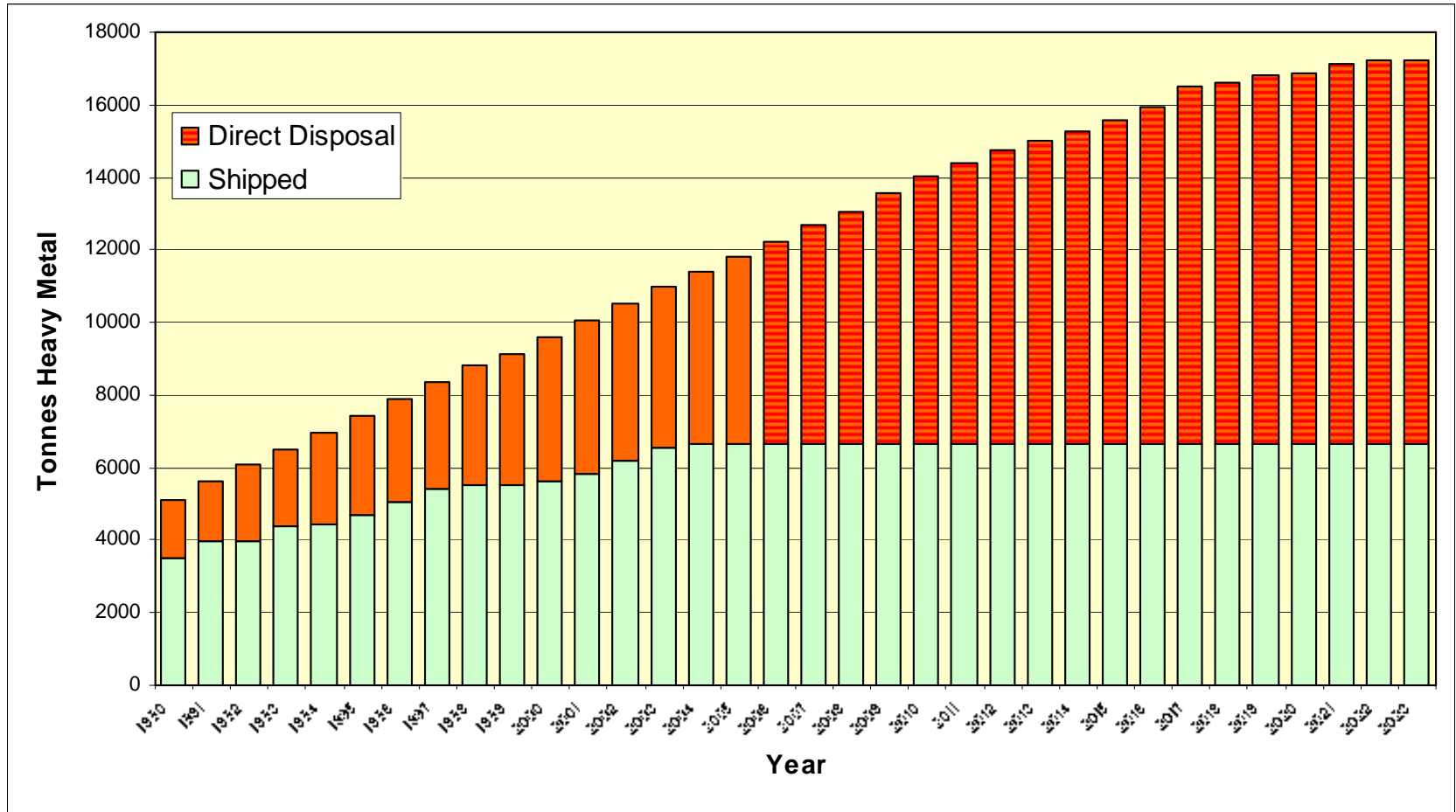
Types of waste for a Repository for Heat generating waste

- From reprocessing
 - Vitrified High level waste (from vitrification plants in La Hague/F, Sellafield/GB, Karlsruhe/D)
 - Compacted fuel structures
- Spent fuel from light water reactors
- Spent fuel from other reactors (high temperature reactors, research reactors)
- core installations with heat generation
- Other waste, which cannot be disposed in Schacht Konrad

Spent fuel from light water reactors

- **Annual unloading per reactor:** 15 to 30 tHM/a
- **Total annual production in Germany:** ~ 400 tHM/a
- **Produced by end 2005:** 11,810 tHM
- **Storage (December 2005):** 5,140 tHM
- **Expected quantity produced by 2025:** ~ 17,200 tHM

- **Decision to stop further reprocessing of German spent fuel**
 - elder spent fuel results in reprocessing products
 - newer spent fuel will be disposed directly



Heat generating waste from reprocessing

- Coquilles with vitrified glass stored in massive casks
- Regular transports to Gorleben interim storage facility



Interim storage of spent fuel

- Storage in massive casks
- Interim storage facility at each NPP site



Packages for Final disposal (1)

- Up to now no formal decision on packages for high level waste
- Possible packages:
 - massive casks especially for final disposal (e.g. Pollux)
 - final disposal coquilles for spent fuel analogue to coquilles of vitrified high level waste
 - Use of the interim storage casks also as final disposal casks

Packages for Final disposal (2)

- The type of package influences
 - the techniques of handling at the final disposal site
 - the details of disposing (galleries or boreholes)
- Special Question to be clarified:
 - Packages for spent fuel other than LWR
 - Packages for waste other than vitrified glasses and spent fuel

Conclusions

- The widespread use of regulated clearance reduces the amount of waste for final disposal seriously
- The way to the disposal of Non heat generating waste is now clear regarding technical questions as also other necessary decisions
- Regarding Heat generating waste: The site decision is pending. Technical decisions have to be made afterwards regarding the type of packages and related issues.

Thank you very much
for your attention

Experiences with Performance of High-Level Radioactive Waste Forms in Various Host Rock Media

Chinese-German Workshop on
„Radioactive Waste Disposal“
May 28-31, 2007, Beijing, China

Bernhard Kienzler
Forschungszentrum Karlsruhe
Institute for Nuclear Waste Disposal (INE)

- Overview on research organizations
KIT, HGF, FZK, INE
- Frame, scenarios and outline of INE's R&D
- Waste Form Investigations
 - HLW glass / Spent LWR Fuel
 - Experiments
 - Modelling
- Conclusions
- Cooperation

The University Karlsruhe (Technical University) and the Forschungszentrum Karlsruhe have founded the „**Karlsruhe Institute of Technology - KIT**”.

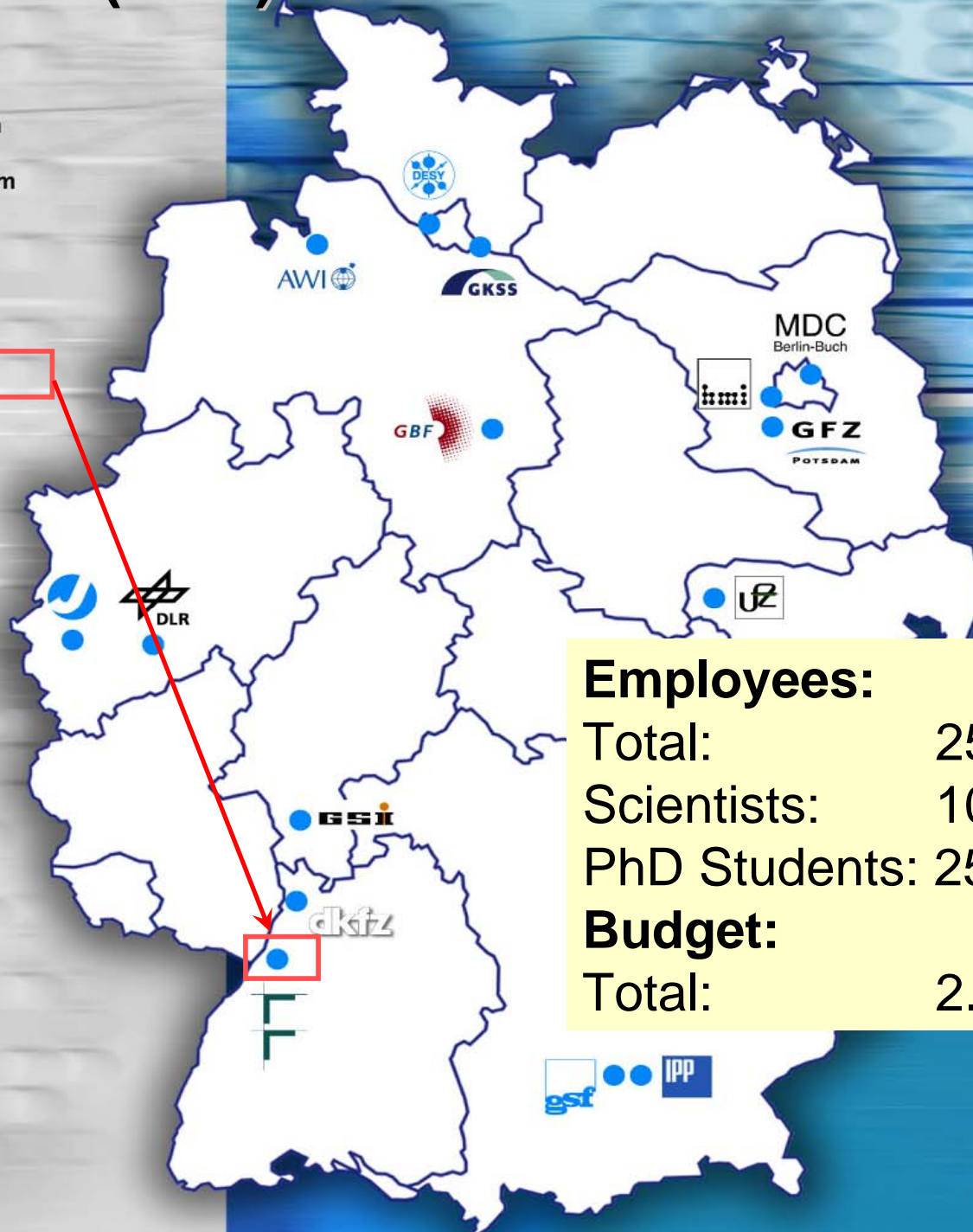
KIT combines the strengths of both partners, in

- micro- and nanotechnologies,
- scientific computing with the focus on grid computing,
- materials research for the energy sector.

KIT is a unique in Germany for the strategic bundling of common issues and resources.

„Helmholtz Association“ (HGF)

- AWI Stiftung Alfred-Wegener-Institut für Polar- und Meeresforschung
- DESY Stiftung Deutsches Elektronen-Synchrotron
- DKFZ Stiftung Deutsches Krebsforschungszentrum
- DLR Deutsches Zentrum für Luft- und Raumfahrt e.V.
- FZJ Forschungszentrum Jülich GmbH
- FZK **Forschungszentrum Karlsruhe GmbH**
- GBF Gesellschaft für Biotechnologische Forschung mbH
- GFZ Stiftung GeoForschungsZentrum Potsdam
- GKSS GKSS-Forschungszentrum Geesthacht GmbH
- GSF GSF-Forschungszentrum für Umwelt und Gesundheit GmbH
- GSI Gesellschaft für Schwerionenforschung mbH
- HMI Hahn-Meitner-Institut Berlin GmbH
- IPP Max-Planck-Institut für Plasmaphysik
- MDC Stiftung Max-Delbrück-Centrum für Molekulare Medizin
- UFZ UFZ-Umweltforschungszentrum Leipzig-Halle GmbH



Employees:

Total: 25,700

Scientists: 10,000

PhD Students: 2500

Budget:

Total: 2.3 billion €/yr.



Research Areas of the „Helmholtz Association“ and FZK

Structure of Matter

Health

Earth and Environment

Energy

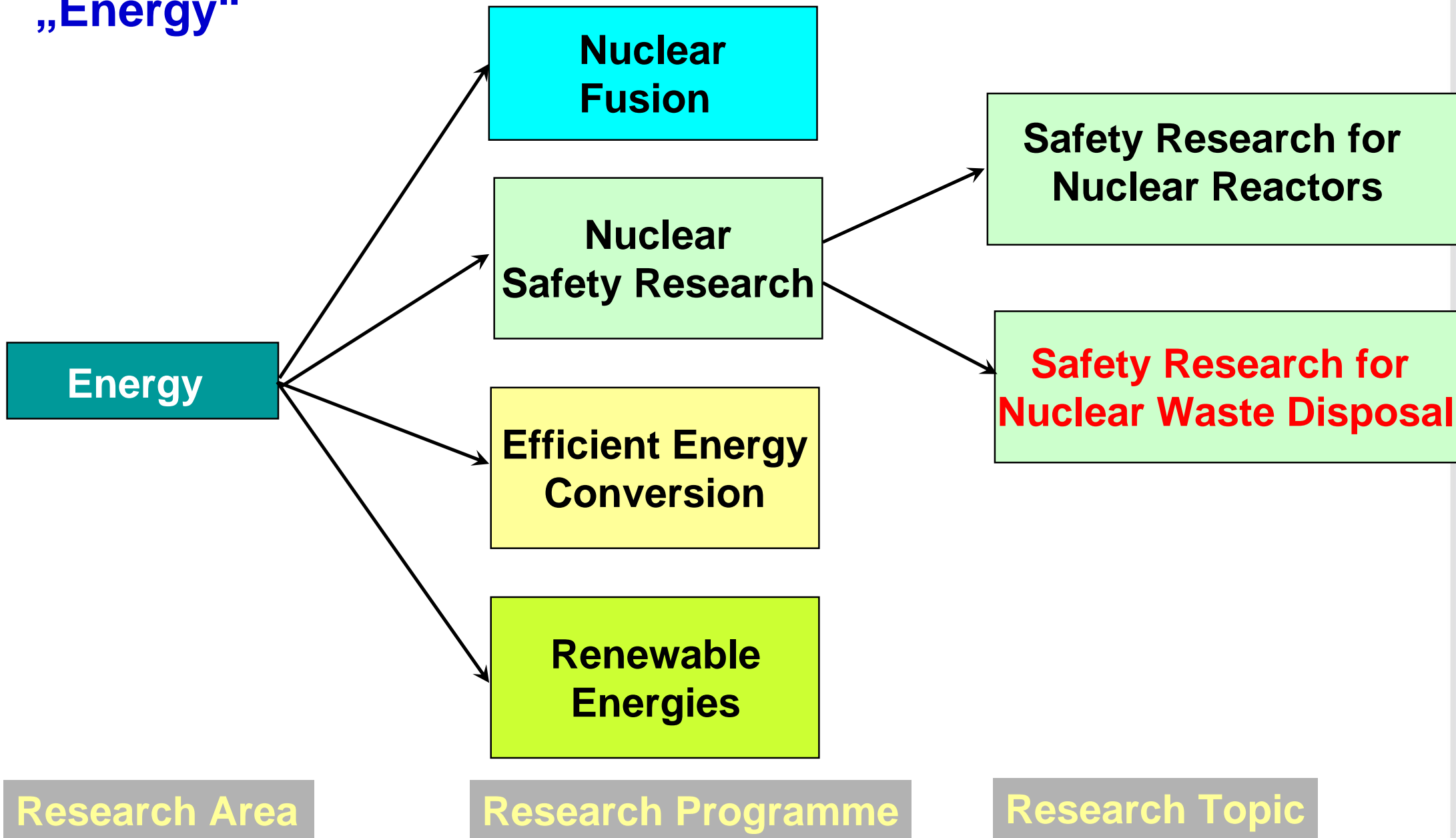
Transport and Space

Key Technologies



FZK contribution

FZK involvement in HGF Research Area „Energy“



Forschungszentrum Karlsruhe

- 2005 -

- 3800 employees (1420 scientists, incl. 190 foreign guests, 185 post docs, 300 trainees)
- Annual Budget:
316 Million € for Research (23 % by contracts)
88 Million € for Decommissioning (25 % by contracts)
- 22 Scientific Institutes
- 11 Programs in 5 Research Areas
- Project Agencies of Federal and State Government
- 2000 publications p.a.
- 1100 cooperative ventures with 250 R&D centers, 140 universities, 150 industrial companies, and 40 authorities, etc. in 47 states

www.fzk.de

Safety Research for Nuclear Waste Disposal

Institut für Nukleare Entsorgung (INE)

Institute for Nuclear Waste Disposal

R+D Topics:

- **Vitrification of High Level Liquid Waste**
- **Reduction of Radiotoxicity (Separation of Actinides)**
- **Long Term Safety of Nuclear Waste Disposal**

Vitrification of High Level Liquid Waste

WAK

- 70 m³ HLLW
- 8.9×10^{17} Bq
- 50 t Glass
- 130 Canisters

INE: Melter and Process Technology

**Active Operation
VEK-Plant (2007-2008)**



Safety Research for Nuclear Waste Disposal

R+D Topics of INE

- **Vitrification of High Level Liquid Waste**
- **Reduction of Radiotoxicity (Separation of Actinides)**
- **Long Term Safety of Nuclear Waste Disposal**

Reduction of Radiotoxicity - MA Partitioning -

Basic studies

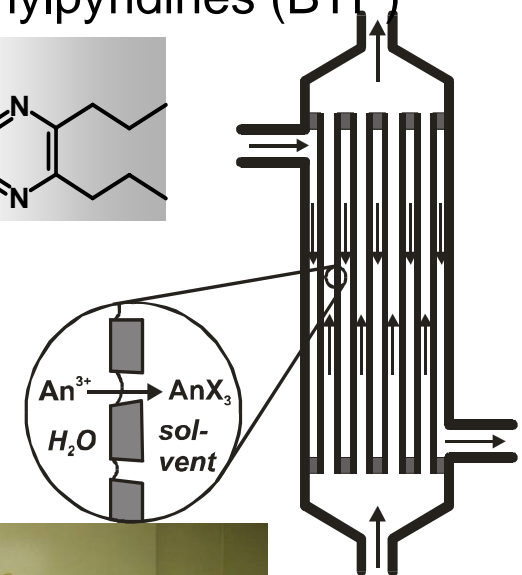
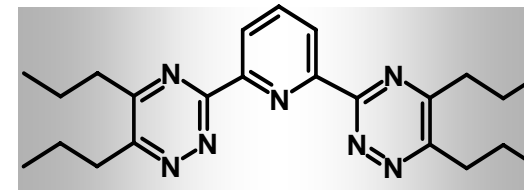
- New stable (hydrolysis, radiolysis) selective extractants (C,H,N,O)
- Study the molecular mechanism (TRLFS, EXAFS, Quantum Chemistry)
- Mass-transfer kinetics (experiments and modelling)

Process design

- Hollow fibres modules as extractors
- Process optimization (Flow Sheet calculations)

(EC FP: 5th PARTNEW, 6th EUROPART)

N-donor extracting agent:
alkylated 2,6-ditriazinylpyridines (BTP)



Safety Research for Nuclear Waste Disposal

R+D Topics of INE

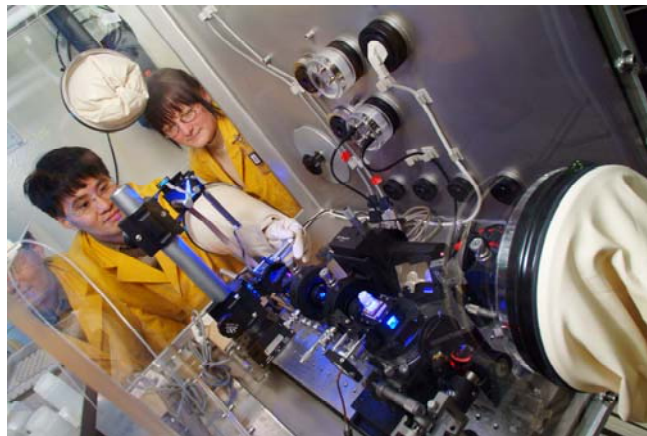
- **Vitrification of High Level Liquid Waste**
- **Reduction of Radiotoxicity (Separation of Actinides)**
- **Long Term Safety of Nuclear Waste Disposal**

R+D-Work on Long-Term Safety

- Geochemically Based Long-Term Safety Assessment -

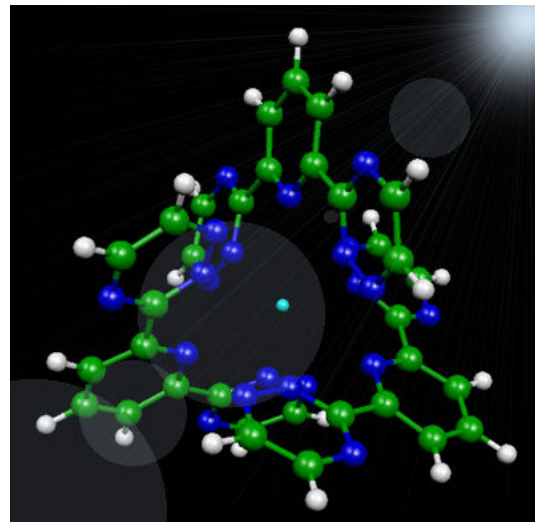
**Basic
Investigations**

**Molecular Process
Understanding**



**Development of
Speciation Methods**

**Molecular Structure
of Trace Actinides**



**Applied
Investigations**

**Radionuclide-Retention
in the Multibarrier System**



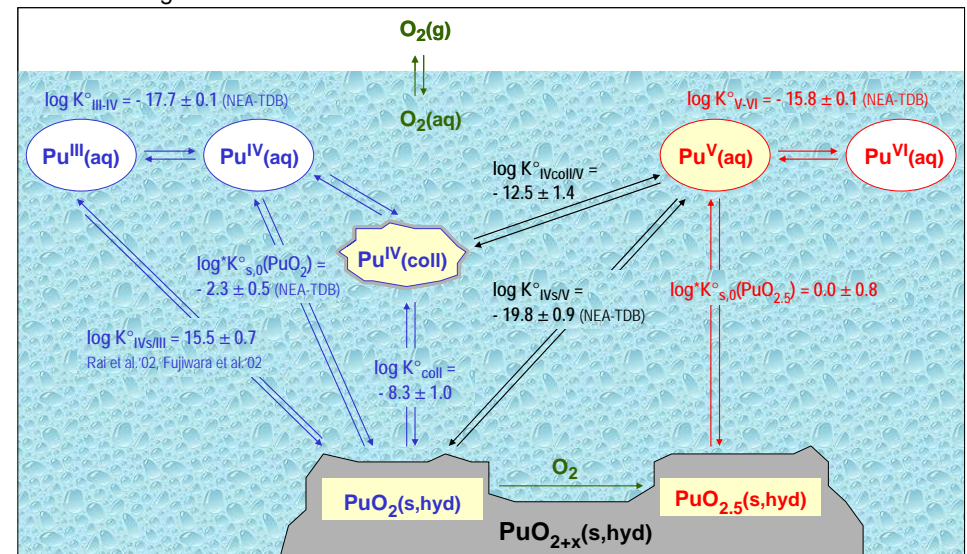
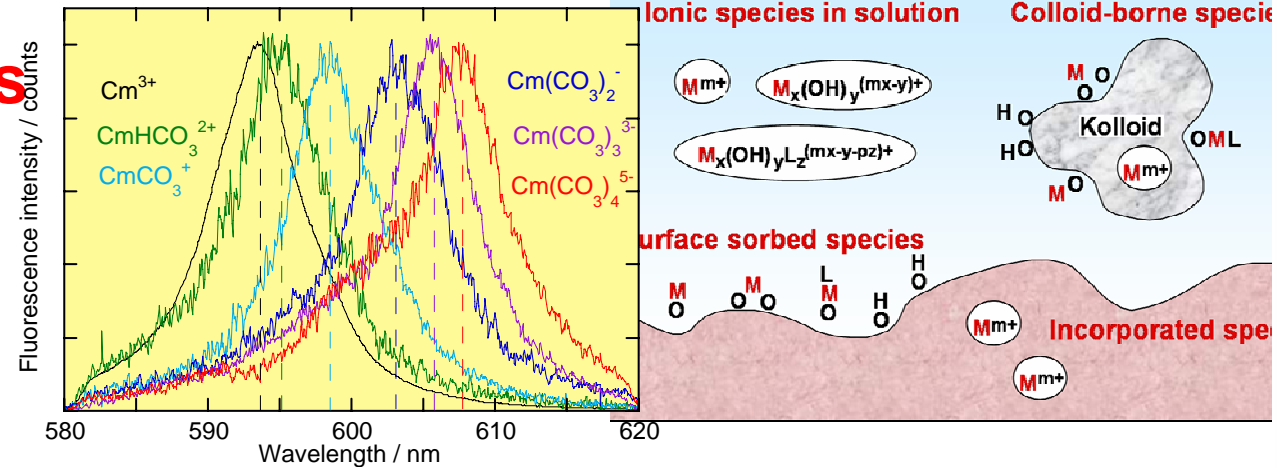
R+D-Work on Long-Term Safety

- Geochemically Based Long-Term Safety Assessment-

Fundamental Investigations

Molecular process understanding

- Aquatic chemistry / thermodynamics of actinides
- Interaction of actinides with mineral surfaces
- Secondary phase formation
- Stability of colloids/ interaction with actinides
- Quantum molecular calculations

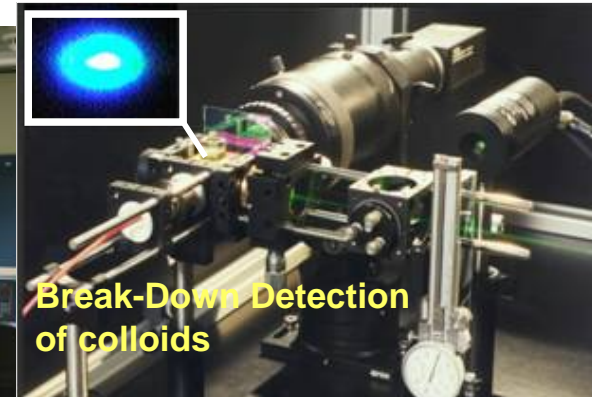


R+D-Work on Long-Term Safety

- Geochemical Based Long-Term Safety Assessment- Development of Speciation Methods

Molecular structure of trace actinides

- Laser spectroscopy
TRLFS, LPAS
- Laser induced break-down detection / spectroscopy
- Sum-frequency-IR-spectroscopy
- X-Ray spectroscopy
(Synchrotron Radiation)
EXAFS, XANES, GIXAFS
 μ -XAFS, μ -XRD



INE-Beamline for actinide speciation at ANKA



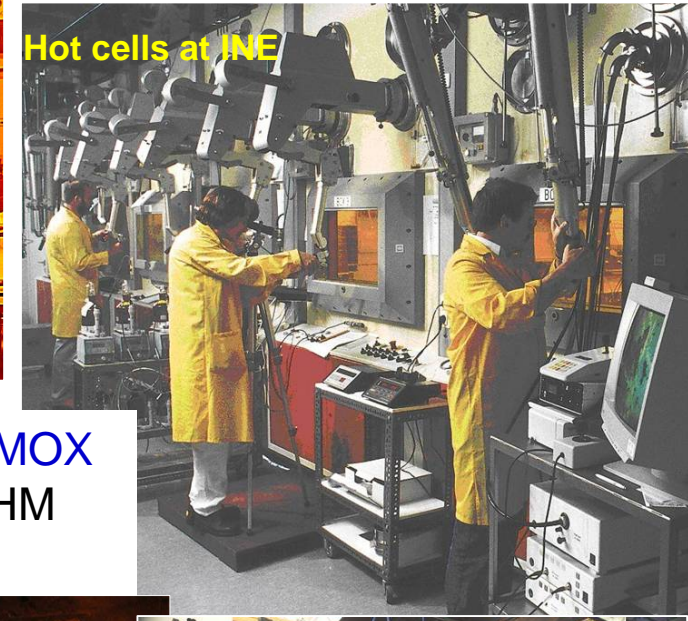
R+D-Work on Long-Term Safety

- Geochemically Based Long-Term Safety Assessment-

Applied Investigations

Radionuclide retention in the multibarrier system

- Waste Forms (spent fuel, HLW glass)
- Radiation chemical effects
- Canister / backfill materials
- Hostrock / far-field
- Large scale experiments (Underground laboratories)
- Reactive transport modelling

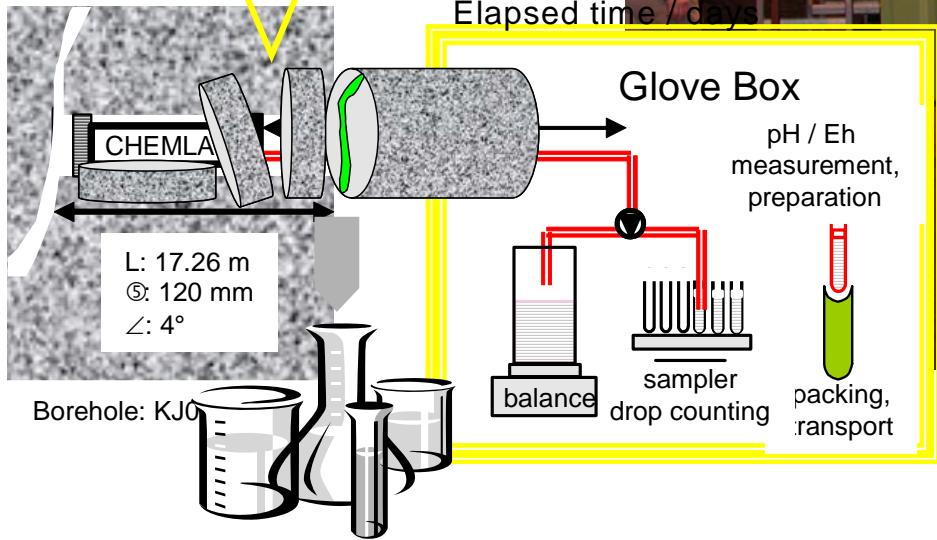
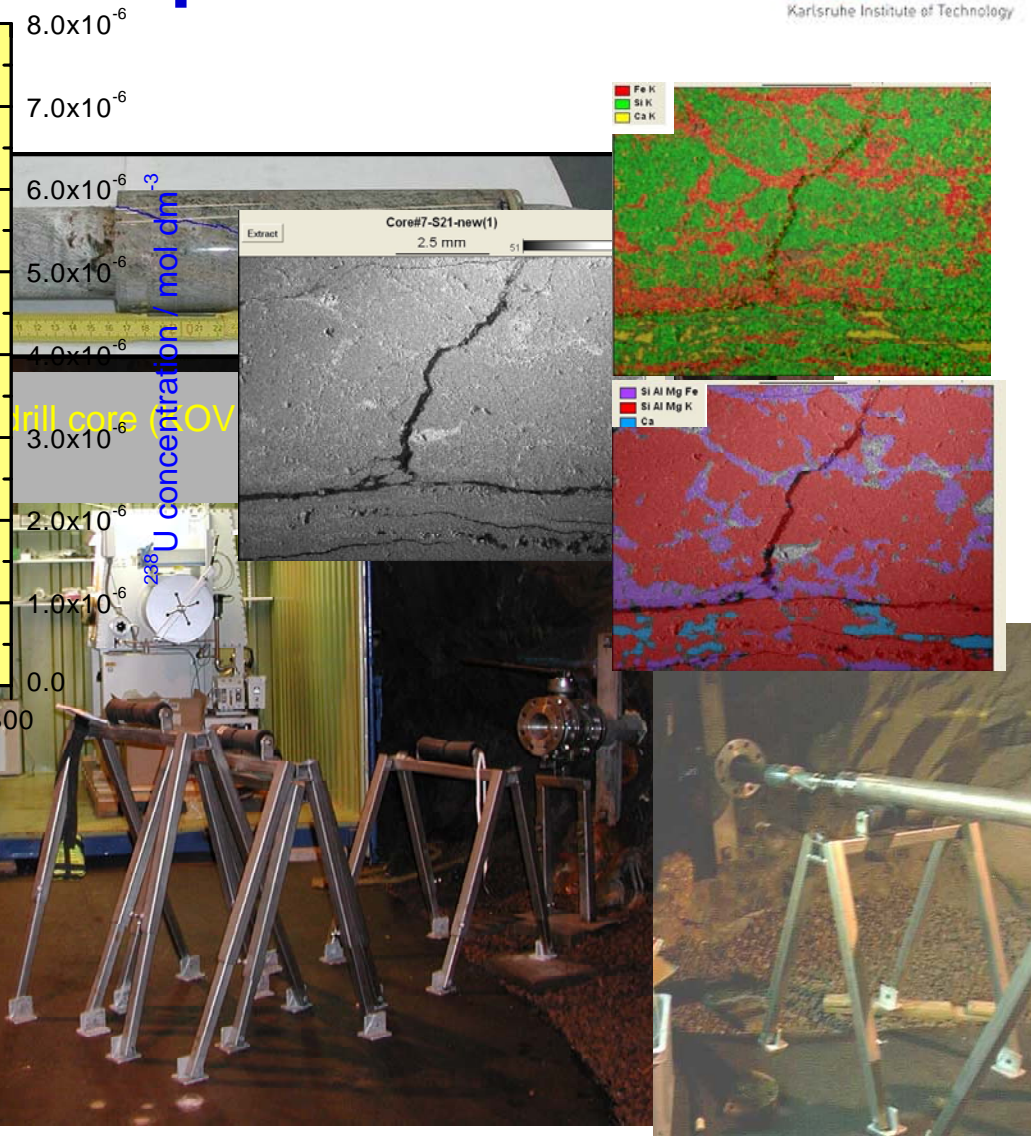
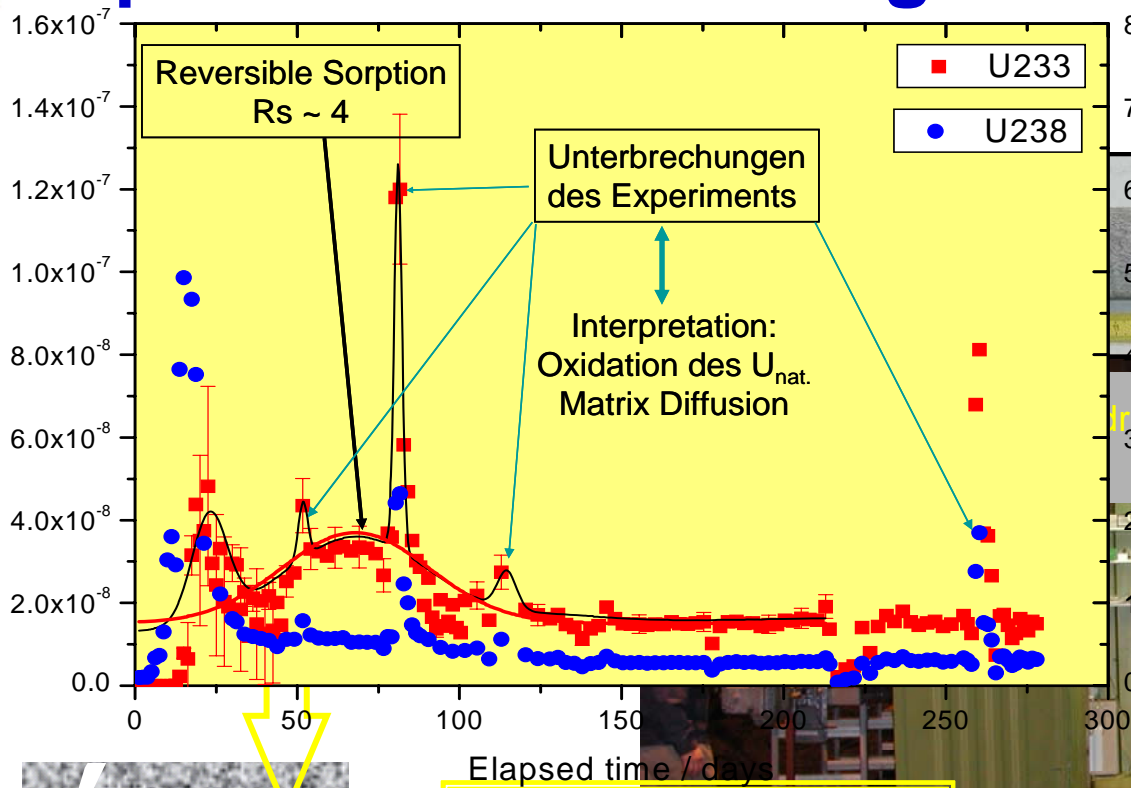


Spent LWR fuel, UOX and MOX
 burn-up: 36 – 52 MWd/kg HM
 activity: $> 10^{10}$ Bq/g

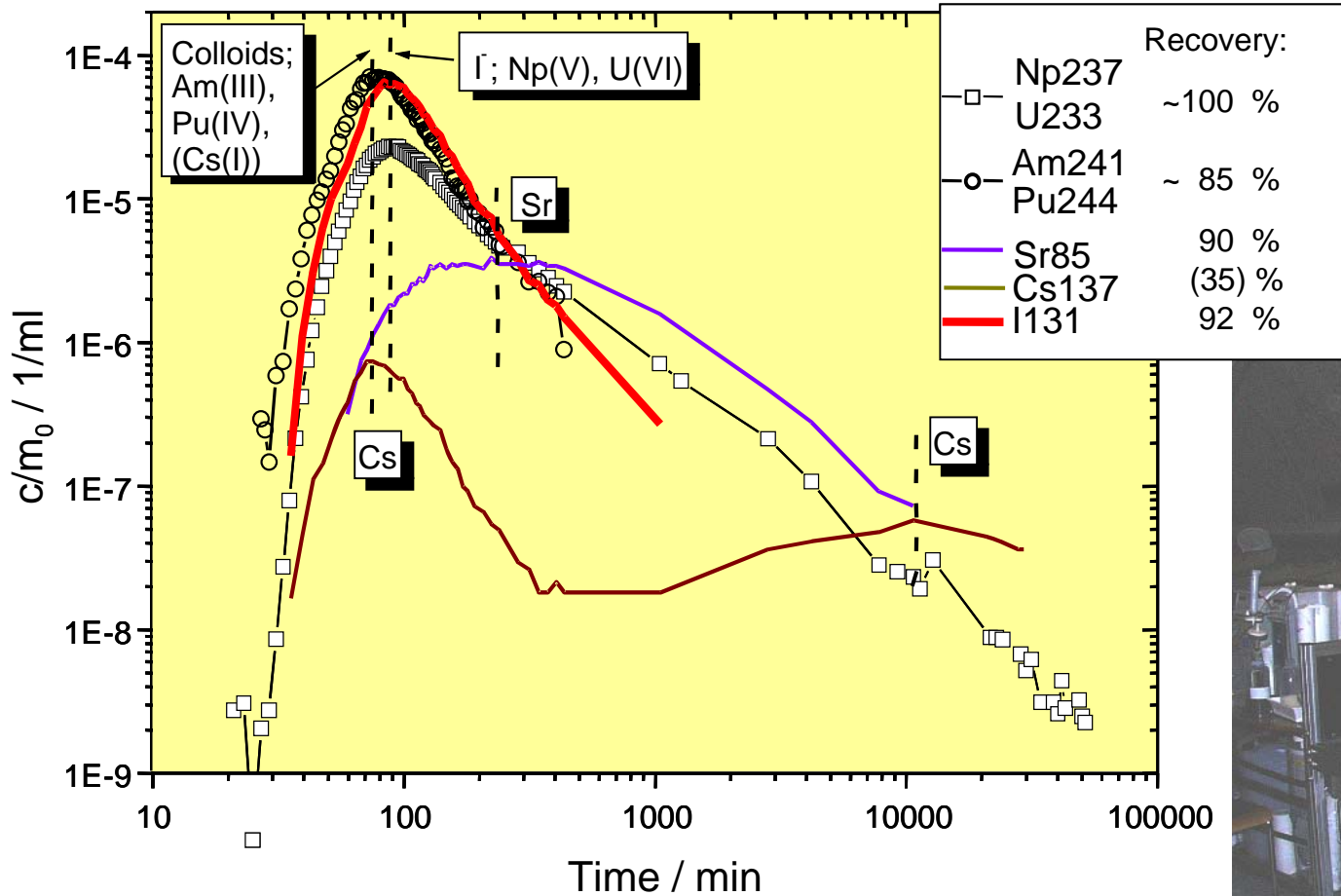


Äspö HRL: Actinide migration experiments

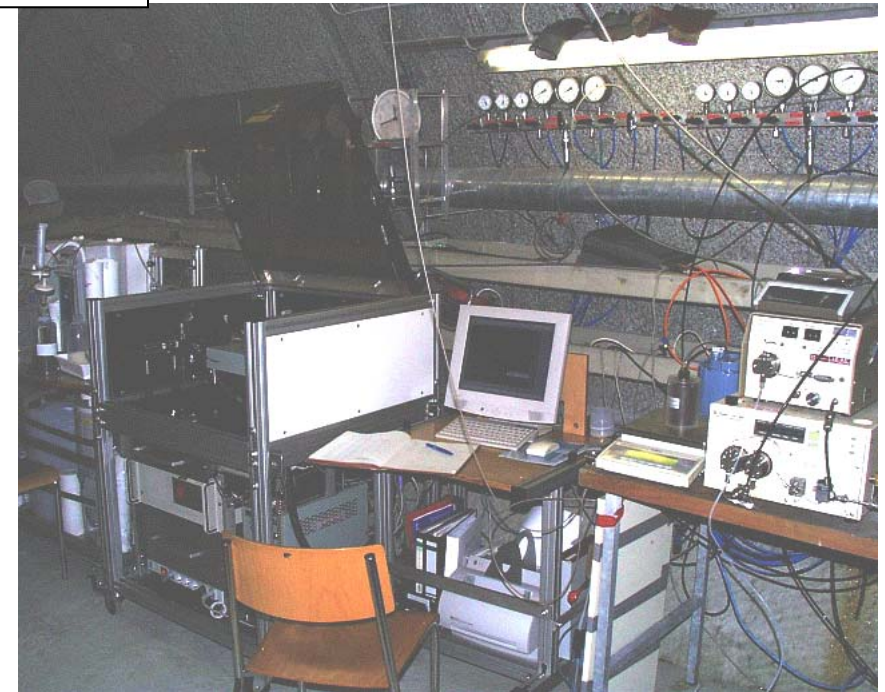
²³³U concentration / mol dm⁻³



Colloid-mediated migration of tri- and tetravalent actinides and a part of Cs

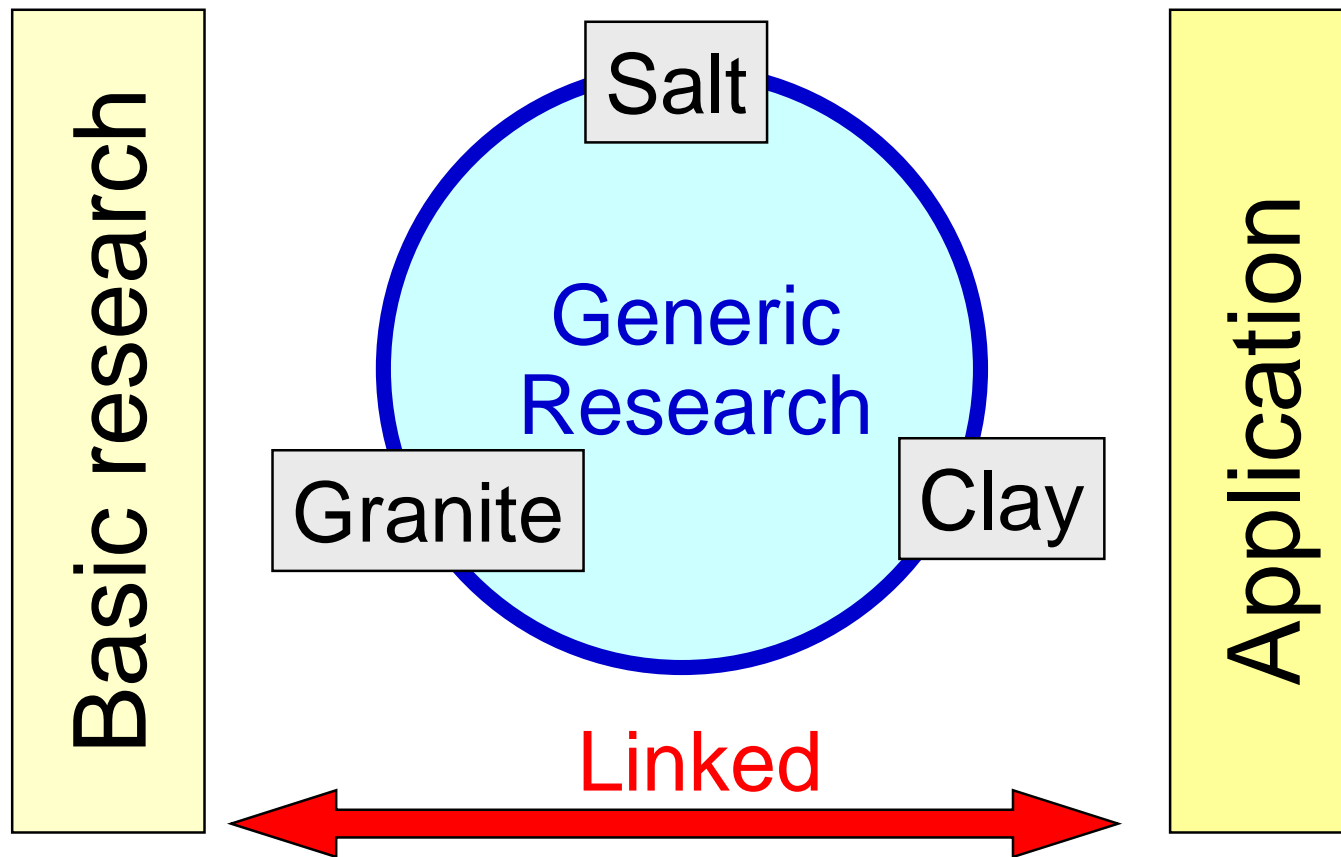


Mobile laser-induced breakdown detection (LIBD) for the in-situ colloid characterisation



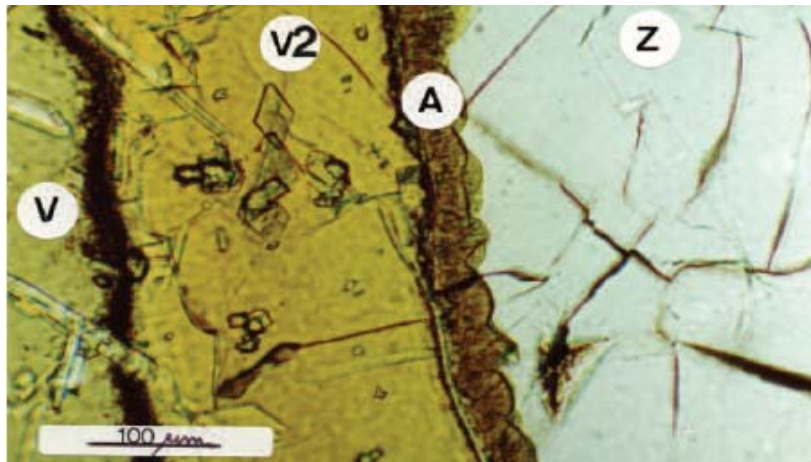
Safety Research for Disposal of Nuclear Wastes

Geochemically based Long-term Safety Assessment

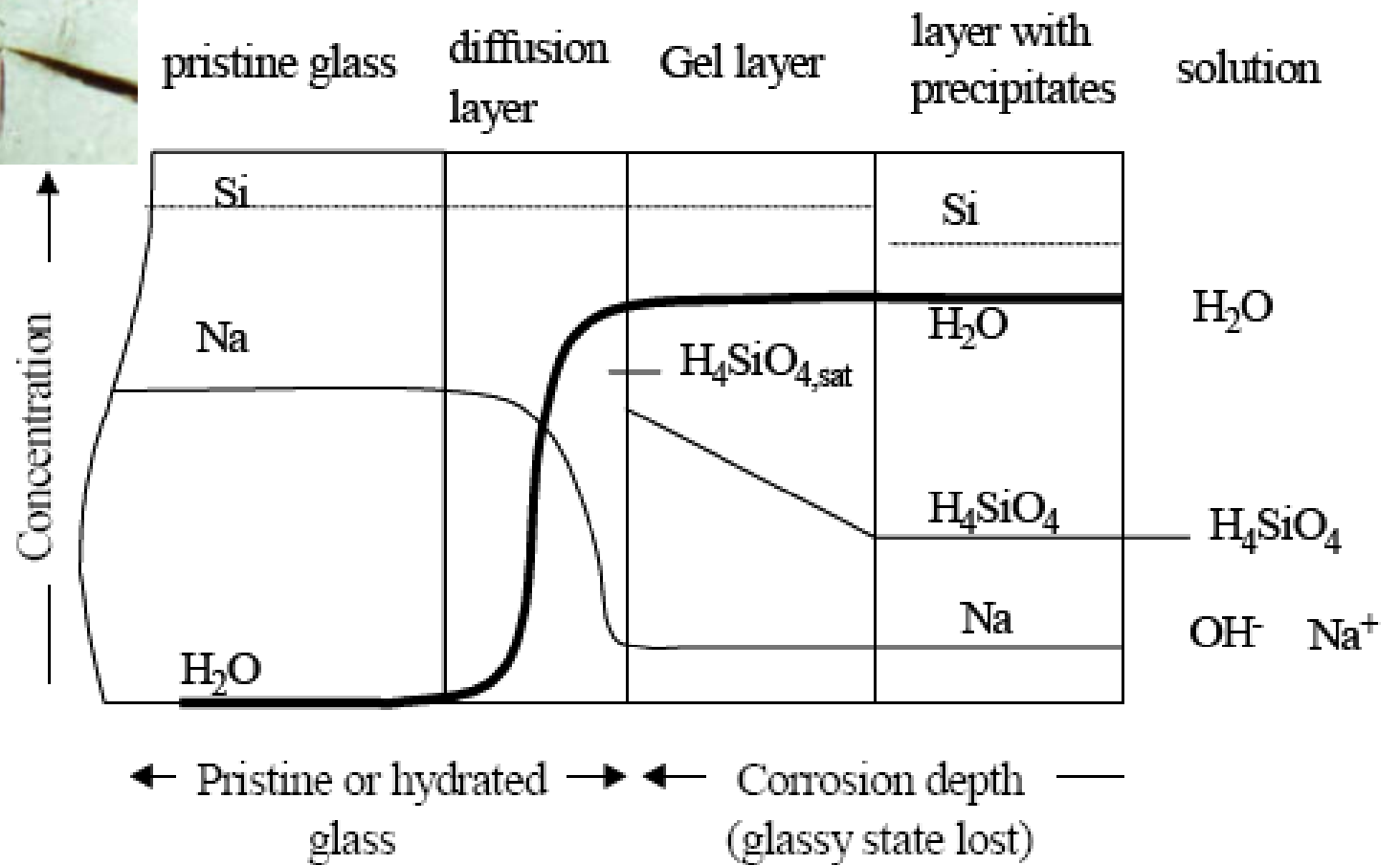


- Boundary Conditions:
 - Rock Salt
 - Clay
 - Granite
- Experimental Set-up
 - Presence of canister / backfill material
 - Specific conditions
- Experimental Results
 - Leachate concentrations
 - Solids
 - Gases
- Modelling

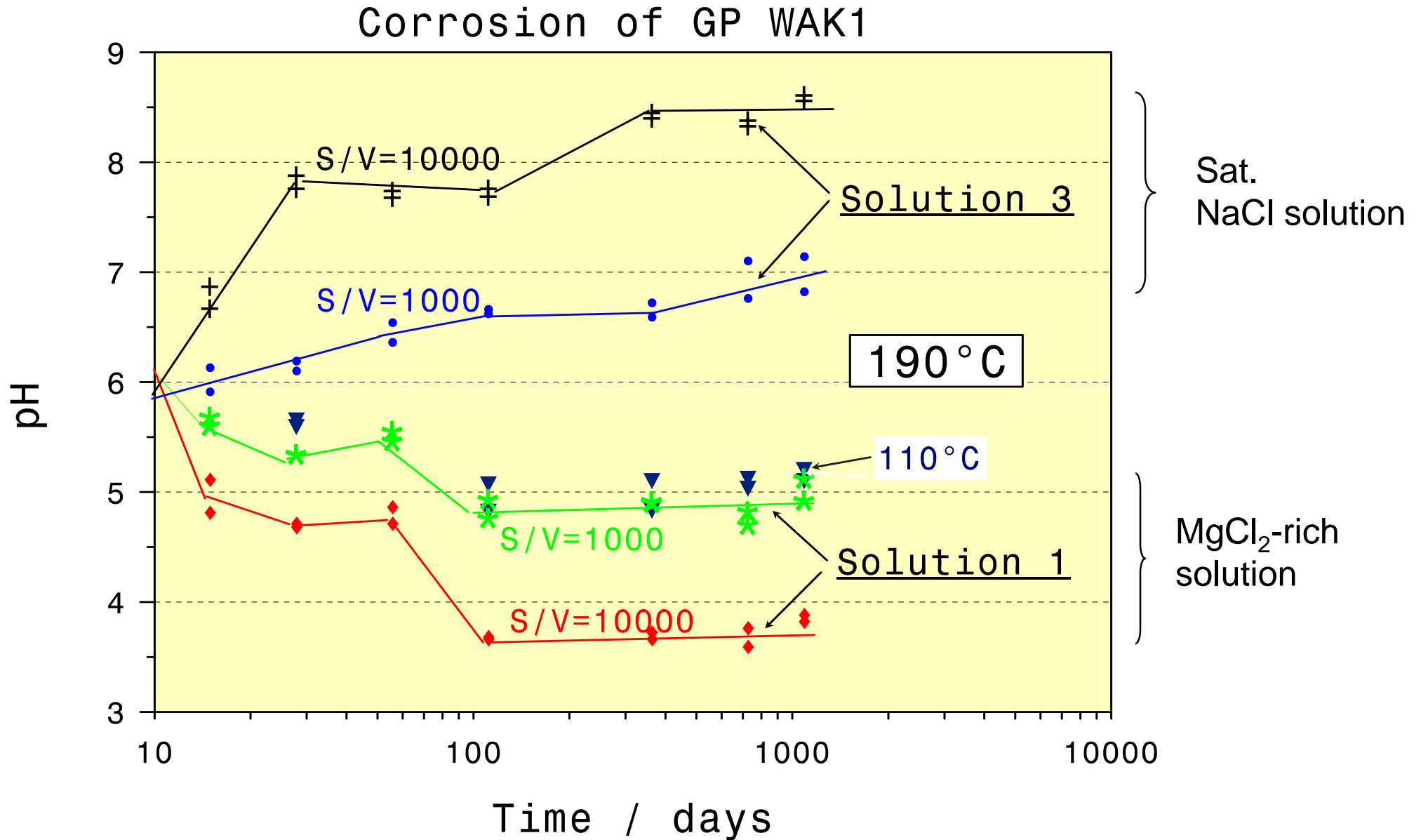
Simplified Scheme of Corroding Glass



V: original glass;
 V2: hydrated glass;
 A: clay;
 Z: zeolite

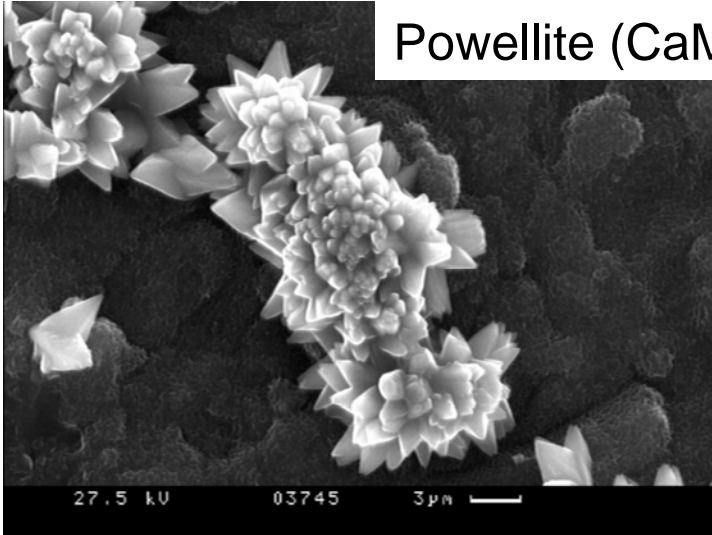


Corrosion of simulated HLW Glass GP WAK1 (pH effect)

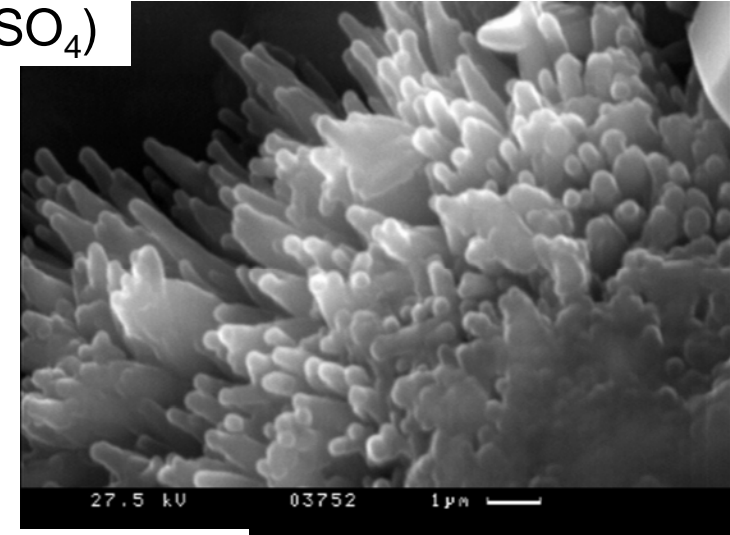


Secondary Phases in Glass Corrosion

Powellite (CaMoO_4)

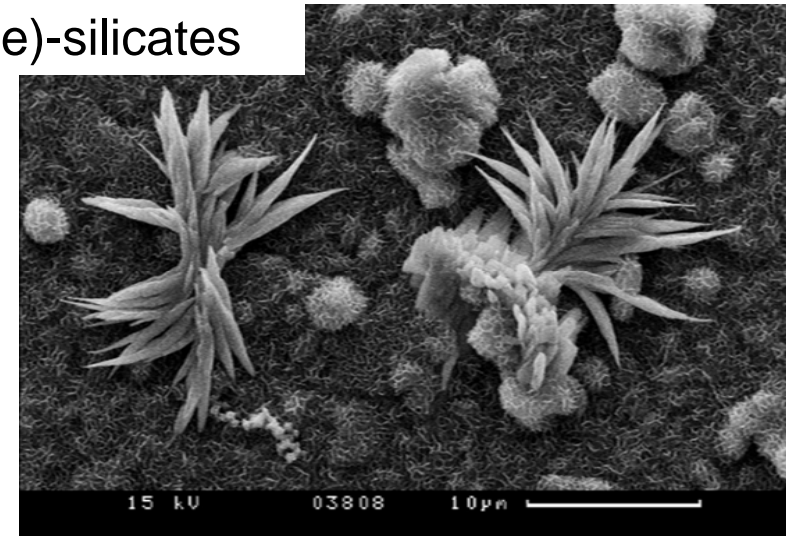
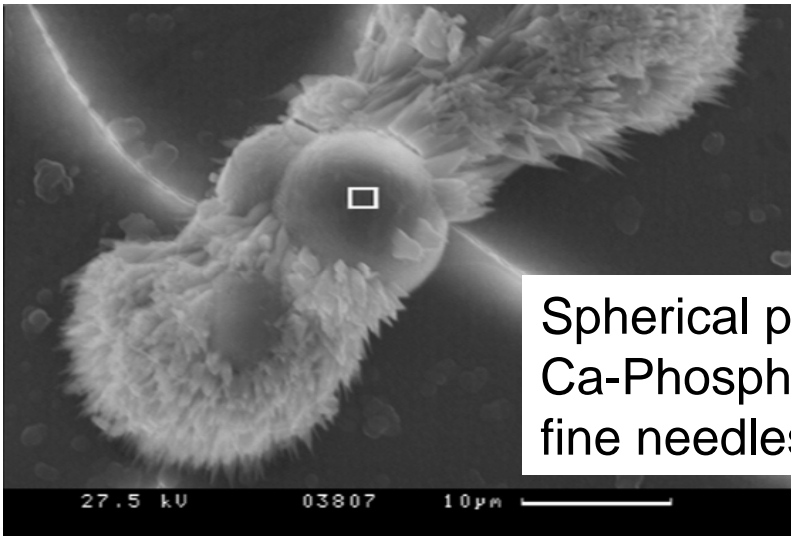


Barite (BaSO_4)

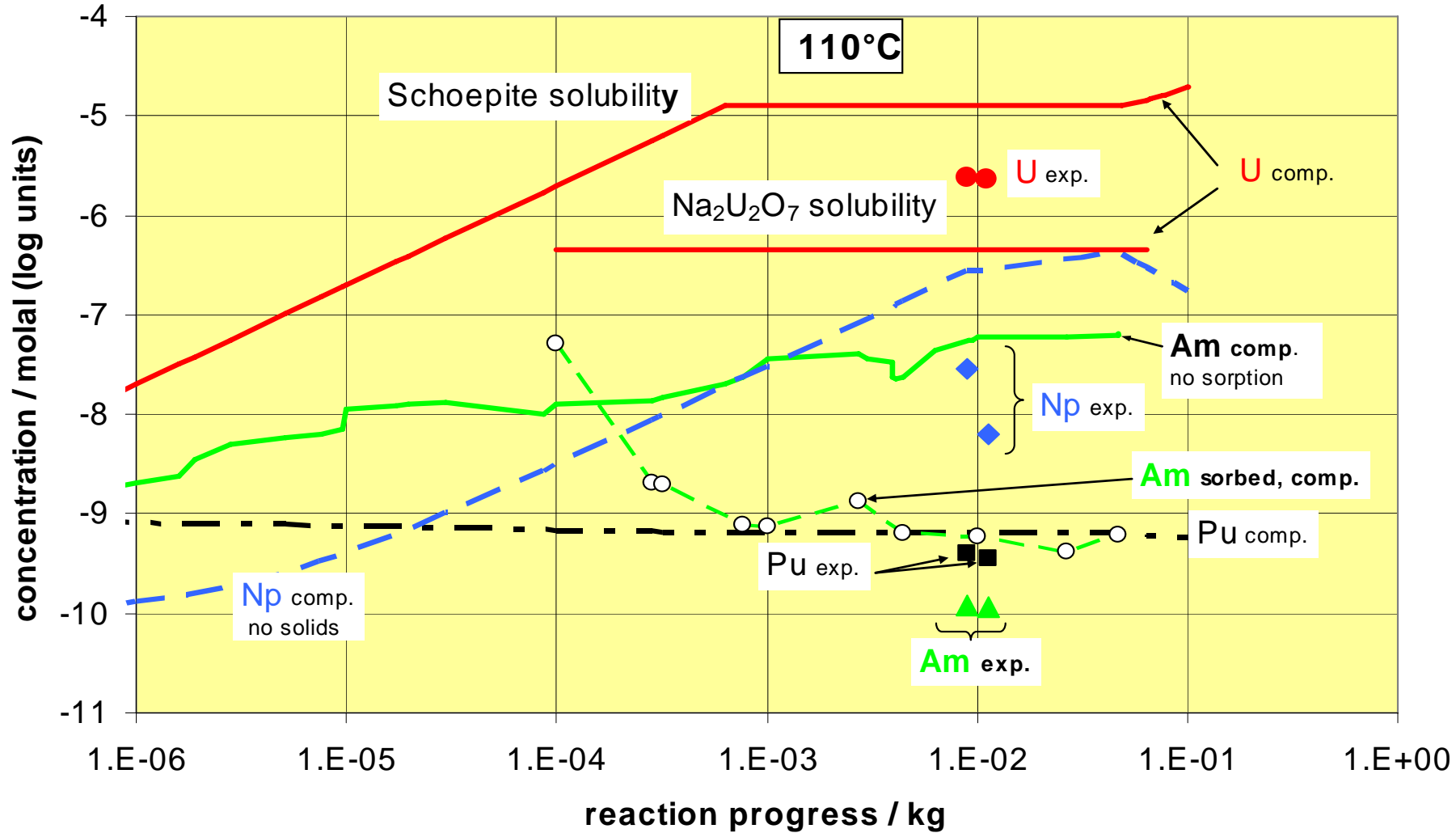


glass surface covered with small clay-like Mg(Ca,Fe)-silicates

Spherical particles: Ca-Phosphate, fine needles: Barite



Concentrations of actinides released from the Glass R7T7 in NaCl brine



„Hot Cells“ at INE



Radiolysis effects,
radiation chemical effects:

Materials: UO_2 , ^{238}Pu -doped UO_2

Solutions: NaCl-brine, Pu doped NaCl sol.

External γ -source

Corrosion Behavior of Spent Fuel

Material: High burnup spent fuel

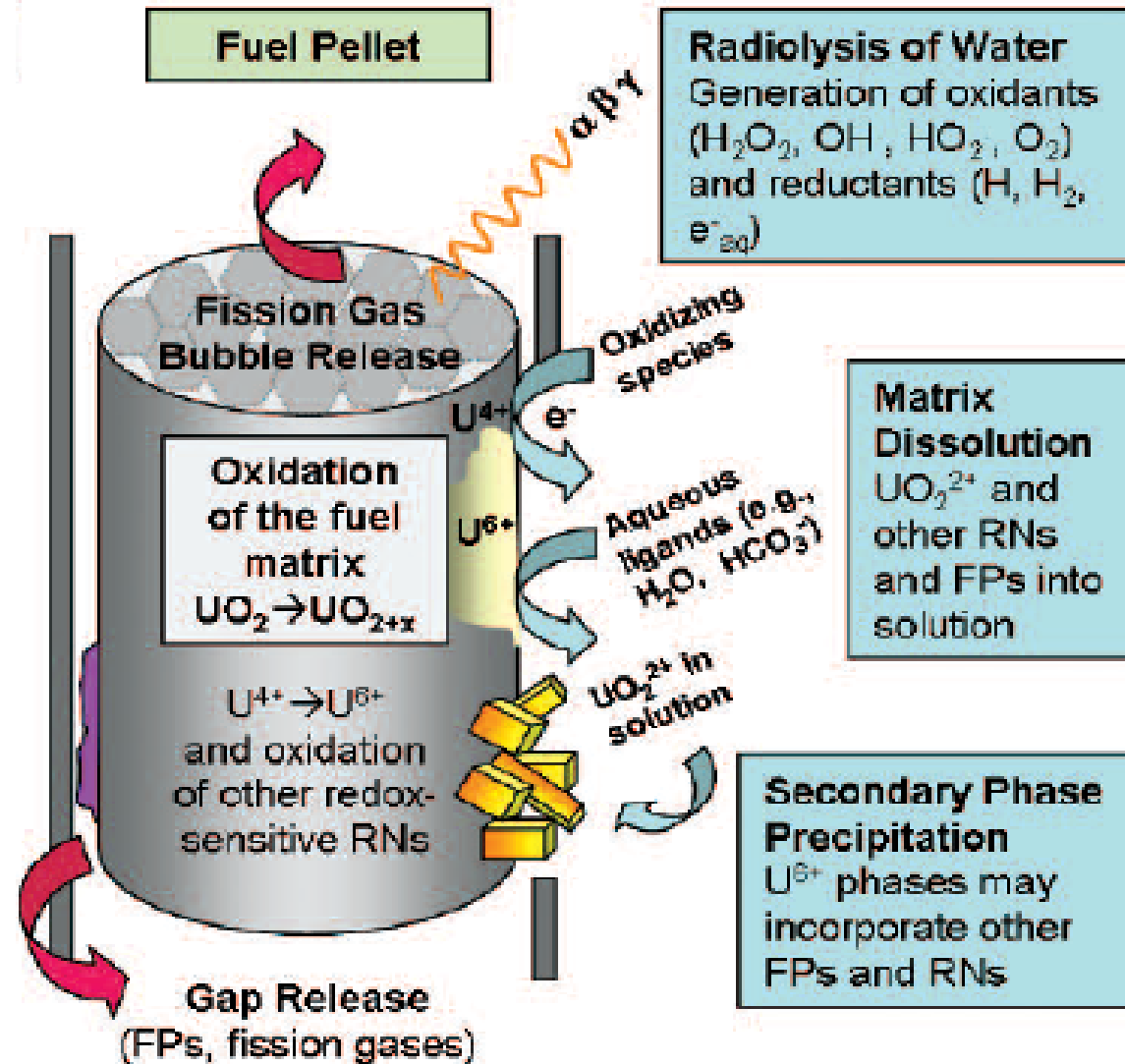
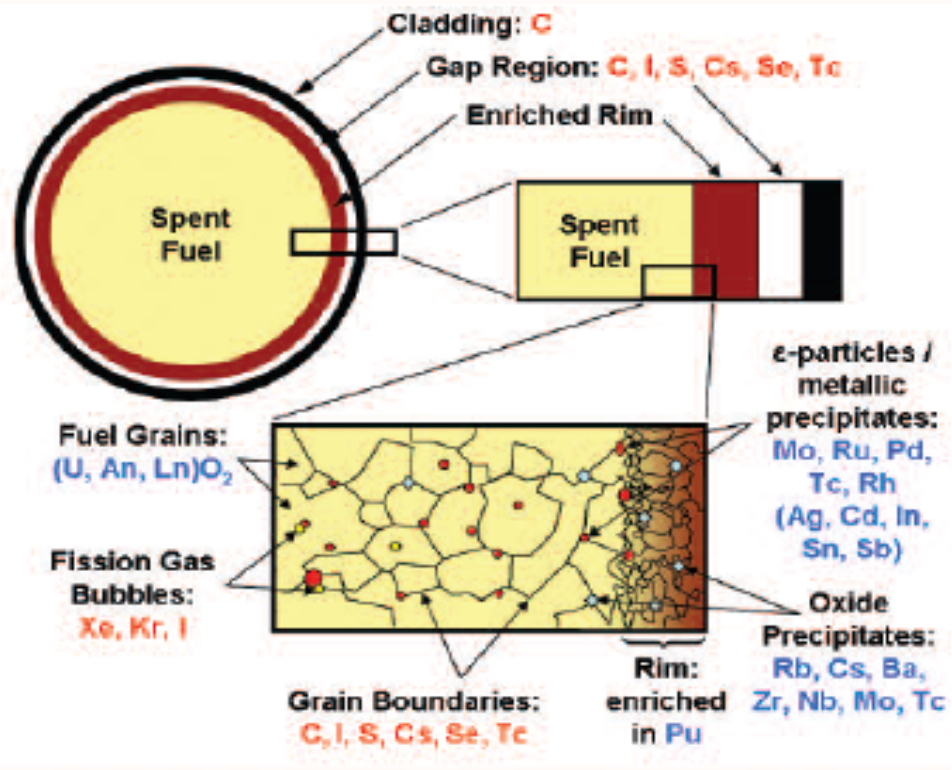
(50.4 MWd/kgU, 30 kW/m, $T > 1700^\circ \text{C}$)

Solutions: NaCl-Solution, Q-brine, DIW,
Granite Waters

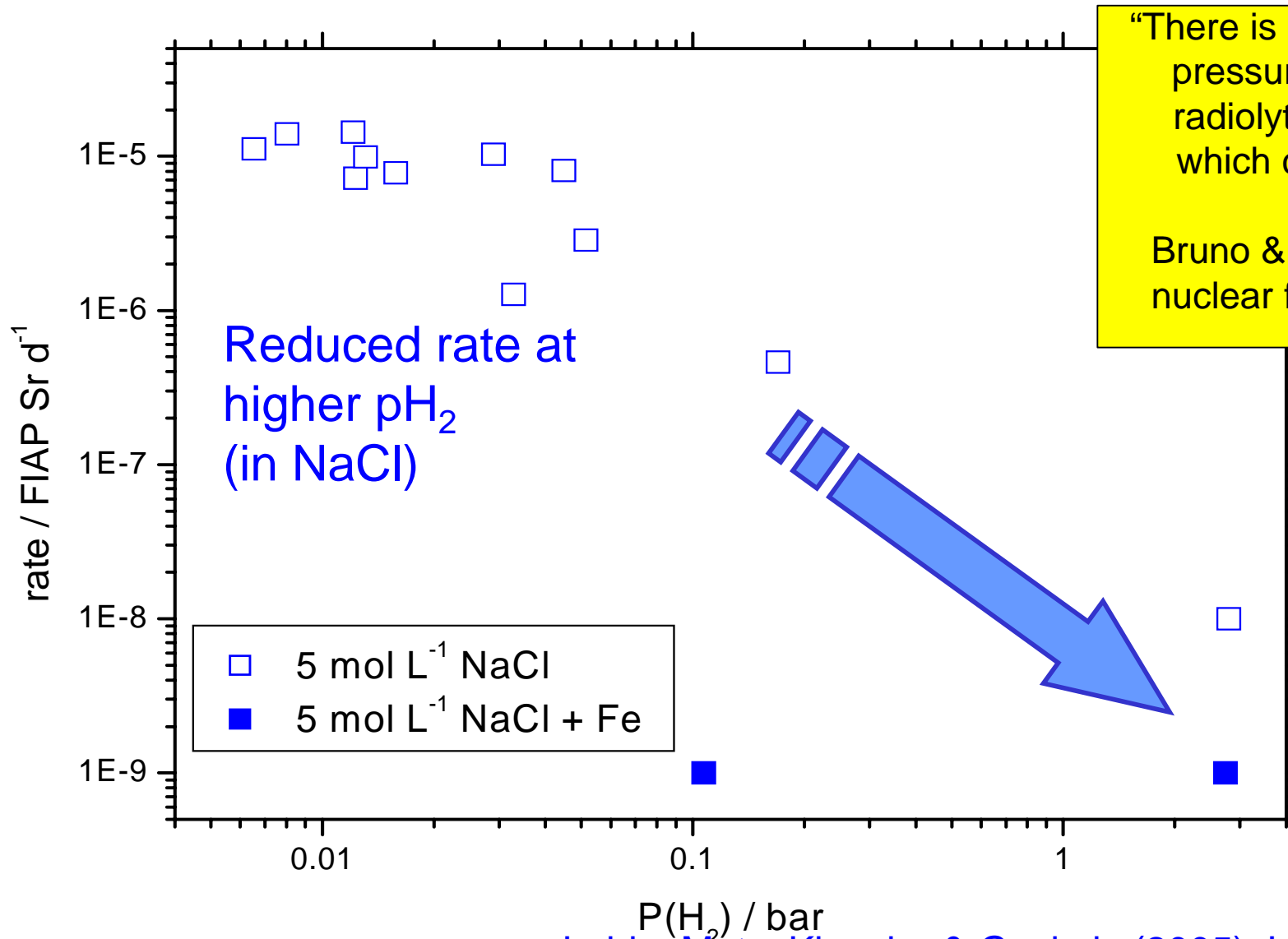
Studies on the effect of

- sample geometry (S/V),
- brine/groundwater composition
- pre-oxidation of the matrix
- container material (Fe powder),
- backfill materials (Magnetite, Apatite)
- impact of hydrogen overpressure
- direct contact between spent fuel and bentonite immersed in granite water

Reactions of spent nuclear fuel



Effect of p_{H_2} on Spent Fuel Leaching: Sr release rate / UO_2 release rate

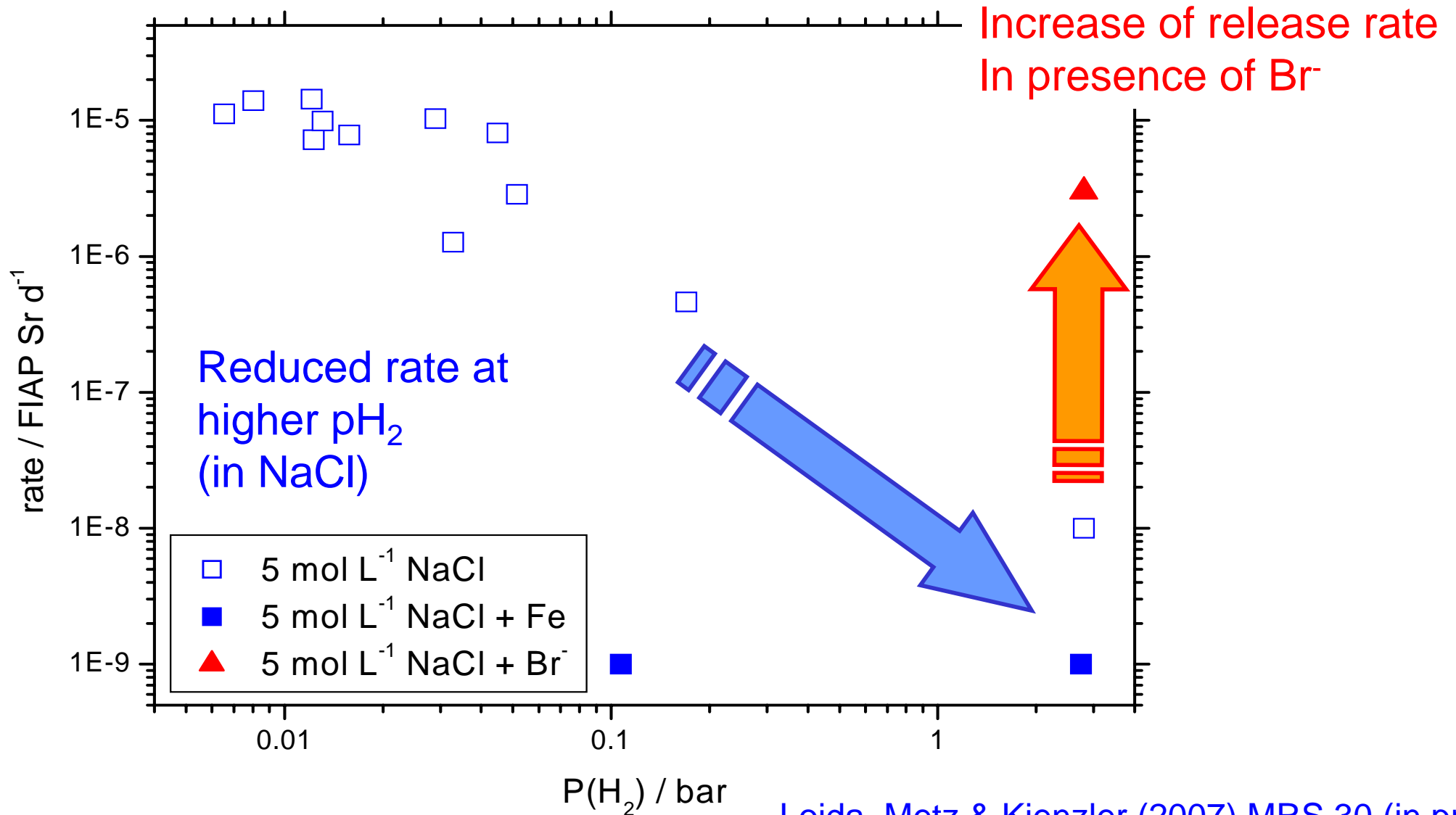


“There is evidence that H₂ overpressures switches off the radiolytic processes (...) in which case no dissolution occurs.”

Bruno & Ewing (2006): Spent nuclear fuel. *Elements* 2, 343

Loida, Metz, Kienzler & Geckeis (2005) J. Nucl. Mat. 346, 24-31

Effect of p_{H_2} on Spent Fuel Leaching: Sr release rate / UO_2 release rate



Loida, Metz & Kienzler (2007) MRS 30 (in press)

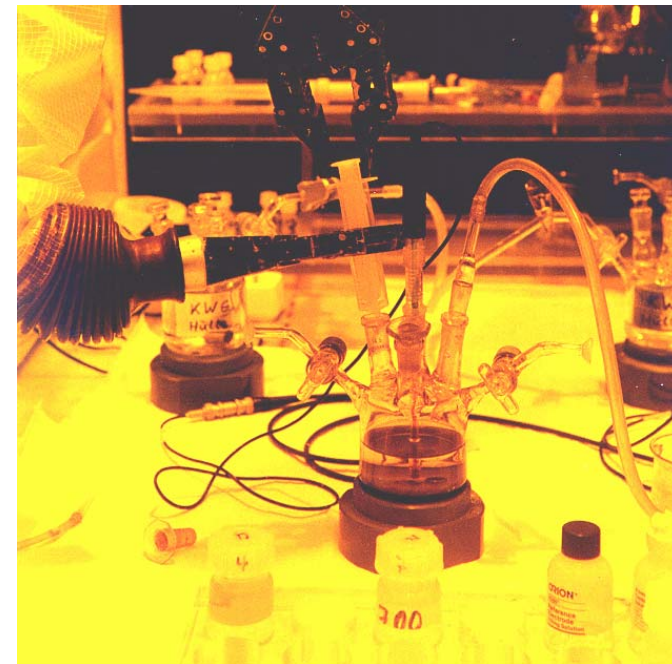
Experimental arrangement

Anoxic conditions (Ar atm), no carbonate,
Spent fuel sample, near field materials, 200 ml NaCl - solution (5m)

Ti/Pd lined autoclave (ca. 500 ml)



Quartz glass vessel (ca. 280 ml)

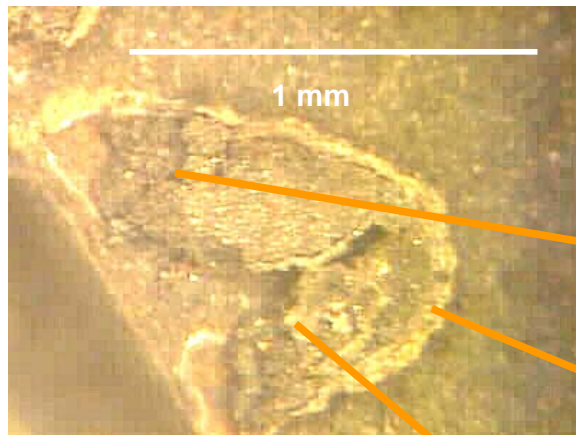


Determination of the reaction progress

- Periodically analyzing of
- solution (0.45 μ m- 1.8 nm filtration)
 - gases (Xe, Kr, H₂, O₂)

End of test:
SEM/XRD-investigation of
all solid phases

Spent fuel corrosion: Solid phases in presence of Fe corrosion products



Fuel,
(non)
oxidized
Fe-
particles



Secondary electron image

3 µm

Backscattered electron image

Fuel-, Fe-powder,
Reaction product
agglomerations

Secondary reaction
products

Mg, Fe, O

(EDX-Analysis)



3 µm



30 µm

Secondary
reaction
products
Fe, Si, O, Cl
(EDS-
Analysis)

- R+D of INE is independent on site selection process and political implications
- R+D covers
 - Basic investigations
 - Speciation methods / development
 - Applied investigations
- R+D oriented towards „geochemically based long-term safety assessment“
- Quasi closed system approach successfully applied to
 - Cemented waste forms (JNST 44(3), 420-456, 2007)
 - HLW glass (Waste Manag. 21(8), 741-752, 2001)
 - Spent Fuel (MRS Conf., EU projects)
- Modeling verified by experiments
- Strong links to INE's „Basic Investigations“ e.g. thermodynamics of actinides and „development of speciation meth.“

- Joint Venture „HLLW Vitrification Project“
 - Germany: Consortium STEAG encotec and EWN (WAK) (Sub-contractor INE)
 - China
 - BINE (Beijing Institute of Nuclear Engineering)
 - CNNC (China National Nuclear Cooperation)
 - CNEIC (China Nuclear Engineering Industry Cooperation)
 - SEPEC (Sichuan Environmental and Protection Engineering Cooperation)
- Research Partnership with CIAE (China Institute of Atomic Energy) in the area of “Safety of Nuclear Waste Disposal)
e.g. laser spectroscopy
- MIGRATION 2011 Conference
Beijing University (Beijing National Laboratory for Molecular Sciences, Department of Applied Chemistry)

Thank you for your attention

Methods available at INE (1)

Chemical and radioactive laboratories

Glove boxes, shielded remote handled boxes

- Radiometrical Methods
- Element and Isotop Analyses
- Solid phase- / surface methods
- Anion / Gas Analysis Methods
- Laser spectroscopy
- Colloid characterization methods:

Methods available at FZK-INE (2)

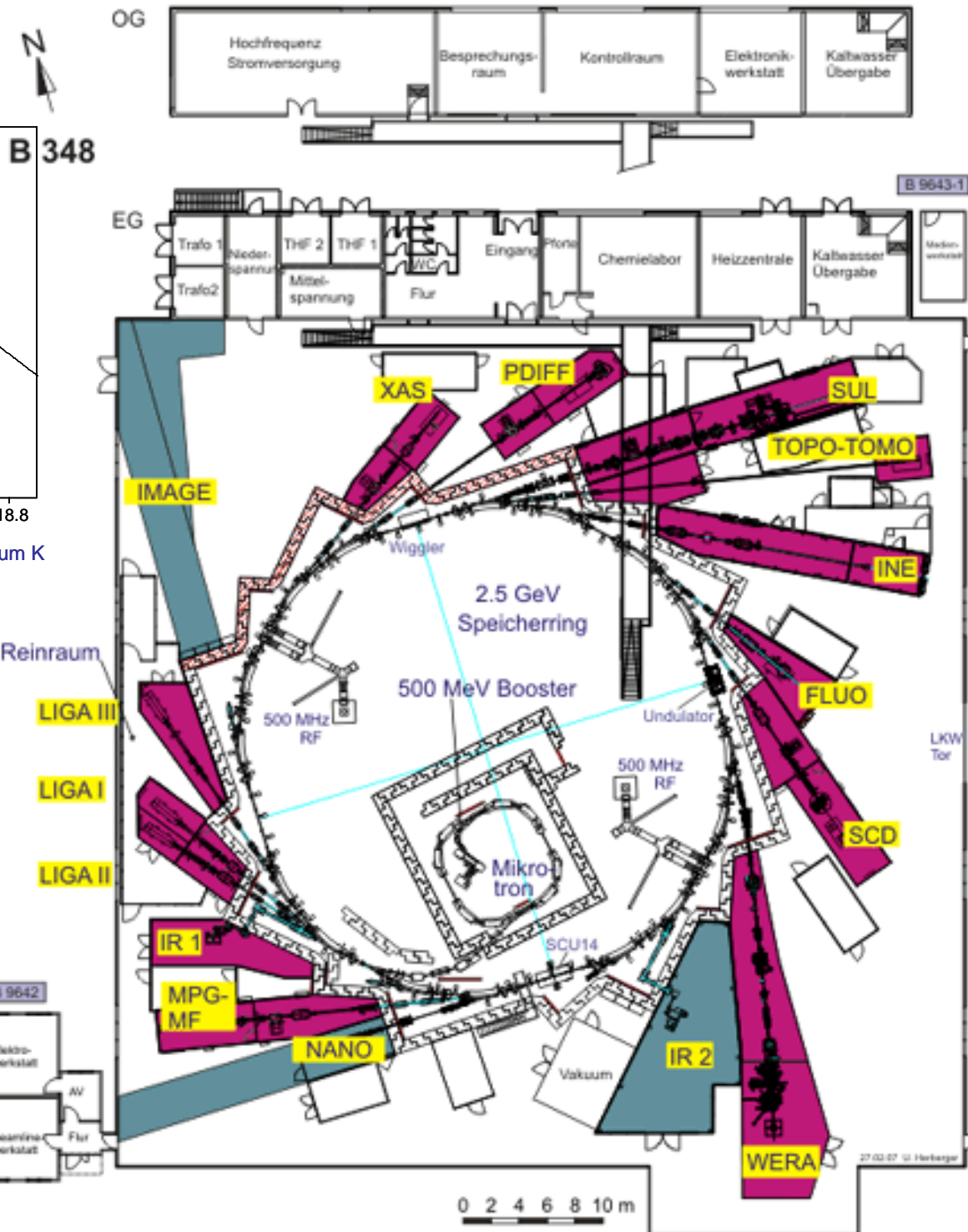
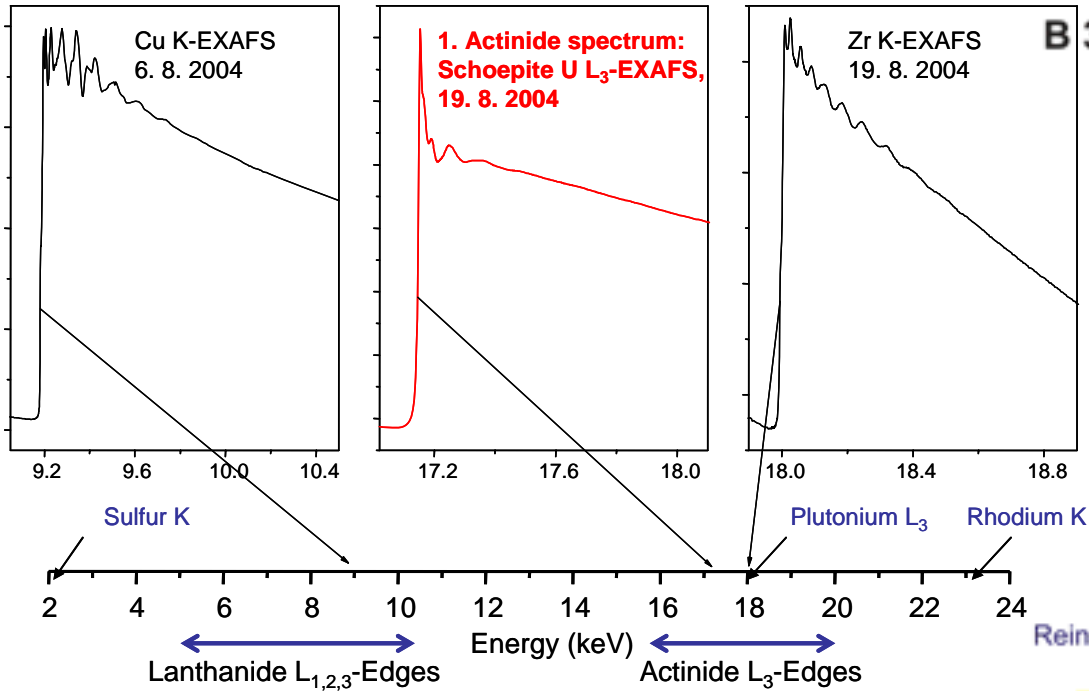
- Chemical and radioactive laboratories
- glove boxes
- shielded remote handled boxes
- Radiometrical Methods:
 - γ -Spectrometry,
 - Low-Level Anti-Compton-Spectrometry
 - HPGe- Detector
 - α -Spectrometry
 - LSC / Low-Level-LSC
- Element and Isotop Analyses:
 - ICP-AES (Glove-Box)
 - ICP-AES Atom Emission Spectrometry
 - FIAS,
 - ICP-MS (glove Box) with FIAS
- Solid phase- / surface methods:
 - XRF
 - X-Ray Diffraction Analysis (XRD)
 - Raman spectroscopy
 - ESCA / Auger Spectroscopy.
 - Electron Microscopy
 - Electron-Probe Microanalysis (SEM-EDX)
 - Laser-Ablation
- Anion / Gas Analysis Methods
 - Ion-Chromatography
 - Gas-Chromatography
 - Carbon Determination
 - Gas- Mass Spectrometry
 - DTA, TG
 - UV-Spectrometry
- Laser spectroscopy:
 - Time Resolved Laser Fluorescence Spectroscopy (TRLFS)
 - LPAS Laser Photo Acoustic Spectroscopy
 - Laser Induced Breakdown Spectroscopy (LIBS)
- Colloid characterization methods:
 - Laser Induced Breakdown Detection (LIBD)
 - Photon Correlation Spectroscopy (dynamic light scattering: PCS)
 - Multi-Angle Laser Light Scattering (MALLS)
 - Flow Field Flow Fractionation (FFFF) coupled with UV-vis, MALLS, ICP-MS, LIBD

INE Beamline for actinide research and for in-situ speciation

- **ANKA facility on site**
- **INE Beamline**
 - ✓ **Research program in synchrotron-based actinide speciation.**
 - ✓ **On-site, *in situ* actinide research backed by know-how and infrastructure.**
 - ✓ **Activities up to 10^6 times the exemption level. Allows studies not possible at other synchrotron laboratories.**
 - ✓ **Multi-purpose beamline → a number of dynamic methods (surface sensitive and spatial resolved techniques)**
 - ✓ **Safe and flexible containment concept**

Fields of possible cooperation with BRIUG

- To be defined during this workshop

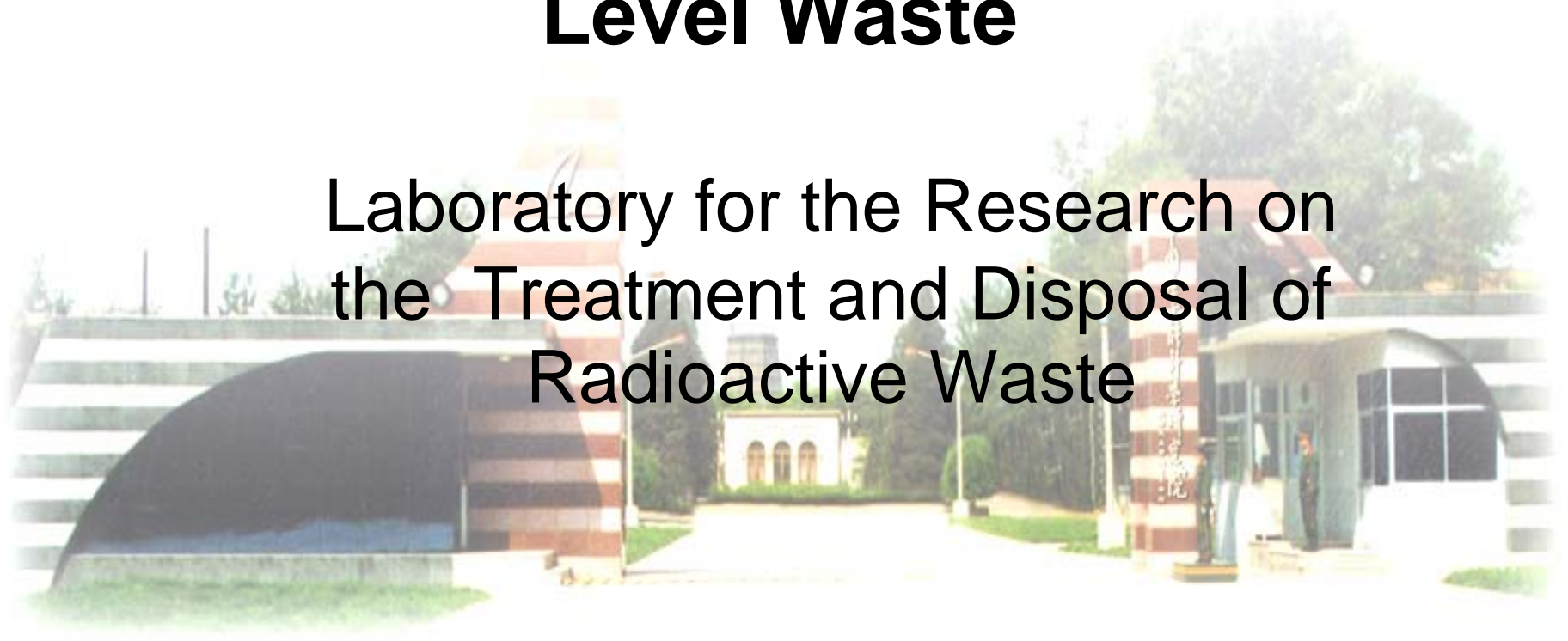


<http://ankaweb.fzk.de/>



Experimental Techniques for the Researches on the Migration of Radionuclides and the Alteration of High Level Waste

Laboratory for the Research on
the Treatment and Disposal of
Radioactive Waste

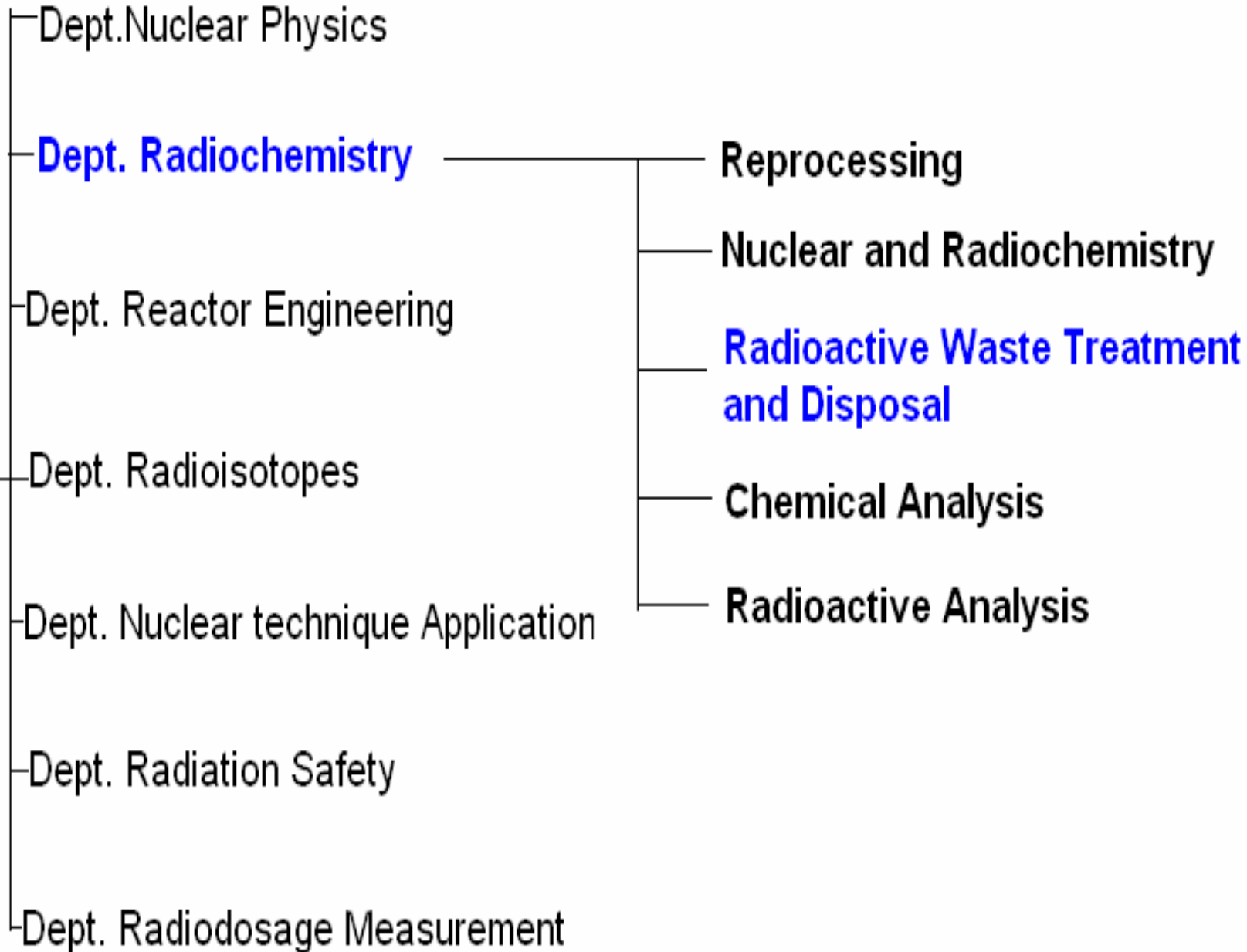




- **1. Introduction of our lab**
- **2. The Disposal of High Level Waste and The Task of Our Lab**
- **3. The Experimental Techniques for the Study of Migration of Radionuclides**
- **4. The Experimental Techniques for the study of the Alteration**
- **5. Summary**



CIAE





- **1. Migration of Radionuclides**
- **2. Vitrification and SYNROC**
- **3. Low and Intermediate Level Waste Treatment**
- **4. Decontamination**



- **1. Migration of Radionuclides**
 - _ **Solubility of Longlived Radionuclides(LLR) in Aqueous Media**
 - _ **Distribution and Diffusion coefficients of LLR in the Backfiling/Engineering Materials**



- **2. Vitrification and SYNROC**
- **-Formulation of HLW Glass**
- **-Immobilization of Minor Actinides by SYNROC**
- **-Glass Ceramique**
- **-Cold Crucible**
- **-Alteration of Waste Matrice in Aqueous Media**



- **3. Low and Intermediate Level Waste Treatment**
 - **-TBP/OK Pyrolysis**
 - **-Cementation**
 - **-Bituminization**
 - **-Polymerization**

- **4. Decontamination**
 - **-Decontamination of Plutonium equipment**
 - **-Decontamination of Big tanks**



2. The Disposal of High Level Waste and The Task of Our Lab

- **The Research Areas on the Disposal of High Level Waste of China:**
 - **_Strategy Study**
 - **_Disposal Engineering Study**
 - **_Disposal Geology Study**
 - **_Disposal Chemistry Study**
 - **_Disposal Assessment Study**



Disposal Chemistry Study

- **-The longterm Stability Study of Glass And the Package**
- **The Alteration of Glass and the Metal Copper**
- **_Aqueous Chemistry of Radionuclides**
- **The Interation of Humic Acids with the Np and Tc**
- **_Migration of Radionuclides in the Near Field of the Repository**
- **The Disposal Behavior of Key Radionuclides**
- **-DataBase and Model of Disposal Chemistry**



- **3. The Experimental Techniques for the Study of Migration of Radionuclides**

- _ **The Characteristics of Minor Actinides**

- _ **The anoxic glove-box**

- _ **low level liquid scintillation spectrometer**

- _ **The Diffusion device**

- _ **Granite Core Diffusion Device**



- **The Characteristics of Actinides**

- _ **Polyvalent**

- _ **Sensitive to Eh-Ph Value**

- _ **Too dilute or even ultra dilute concentration**



The
concentration
of $O_2 < 5\text{ppm}$

_ Solubility of
the Actinides

_ Distribution
and Diffusion
Coefficient



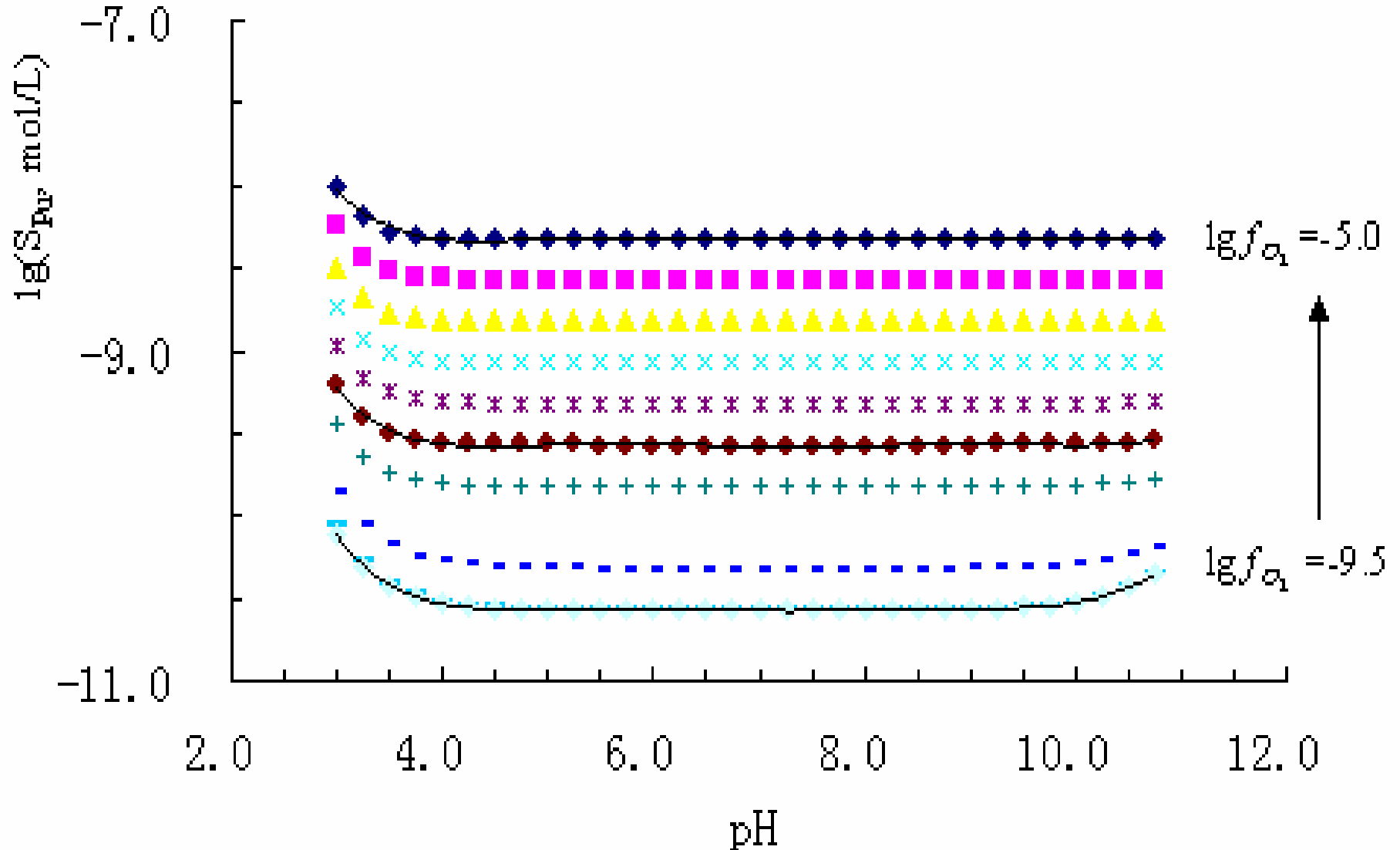
Alpha: 0.22cpm

Beta: 1.55cpm

low level liquid scintillation
spectrometer

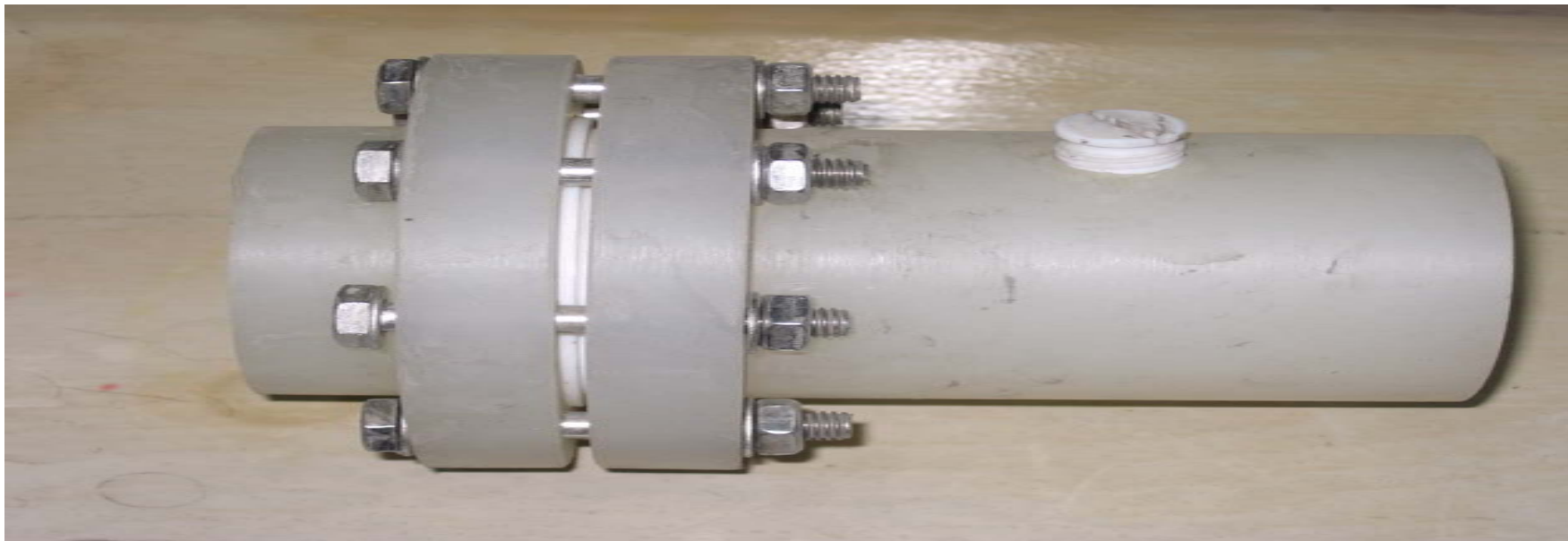
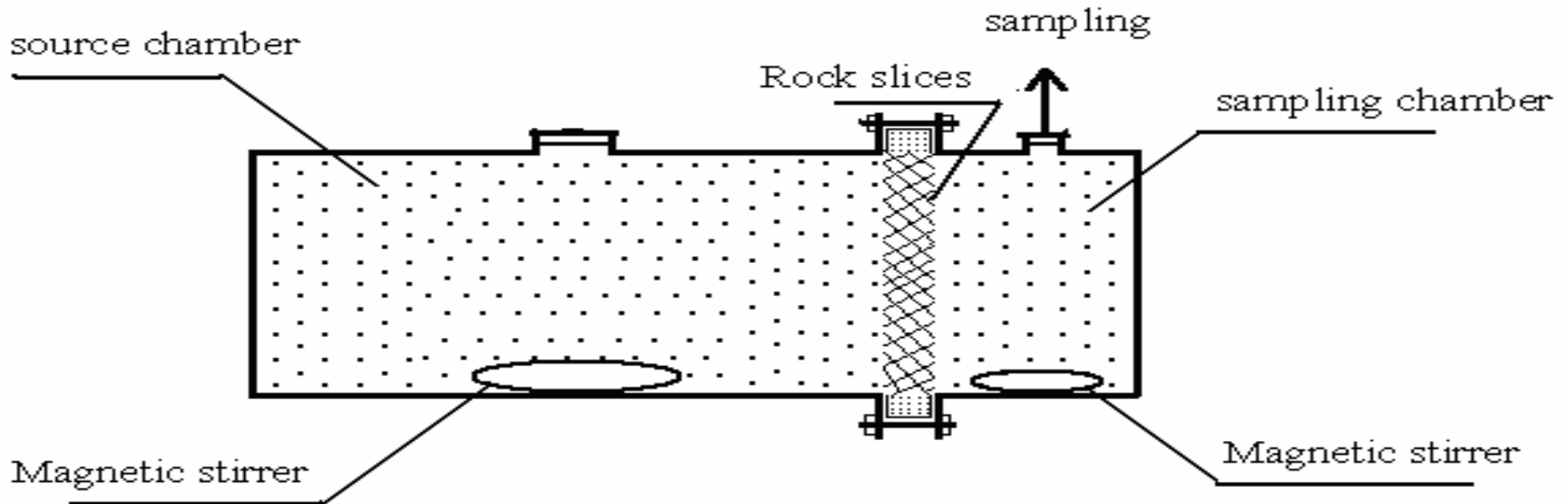


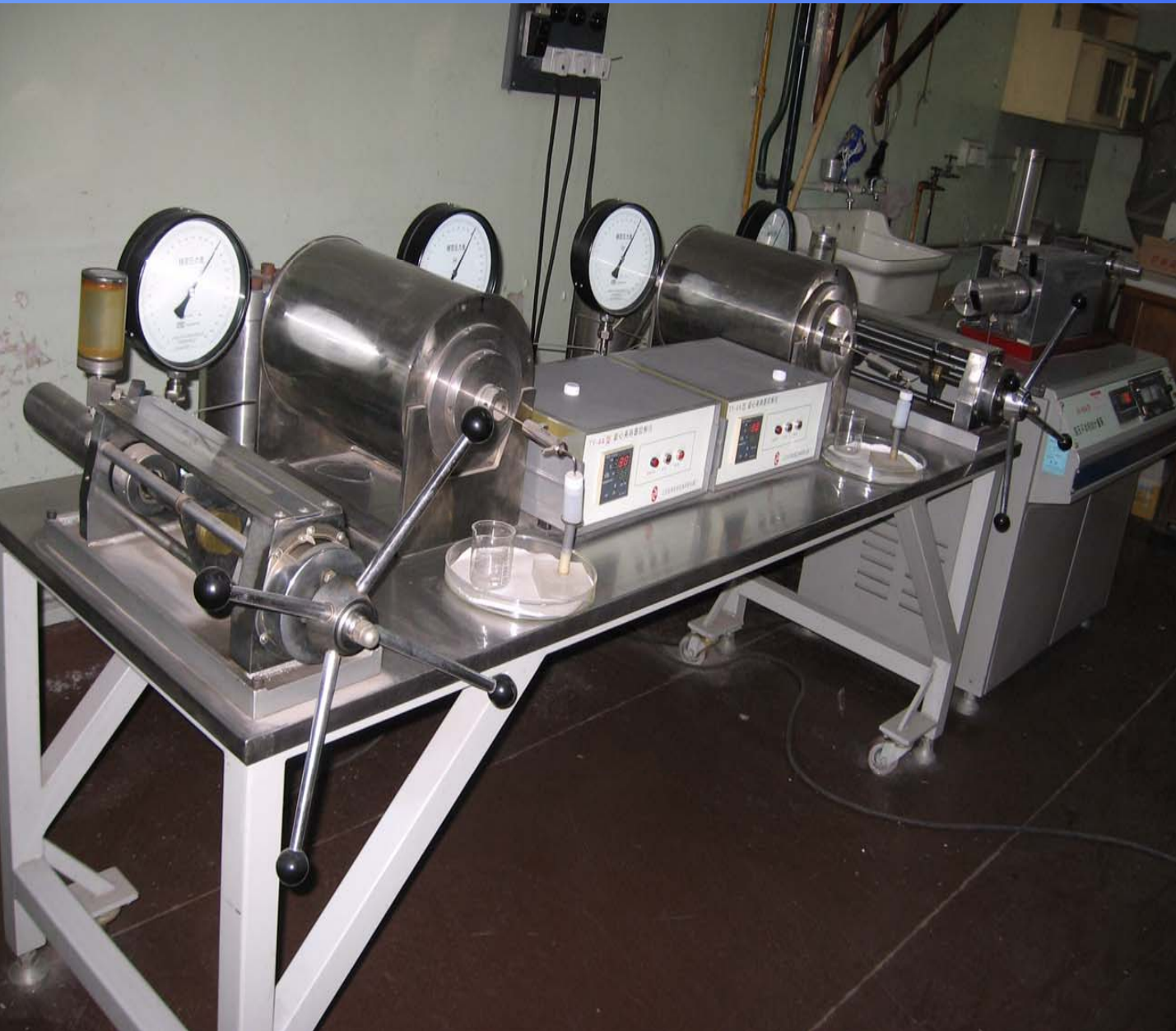
The solubility of Plutonium in Beishan Underground water





The Diffusion device





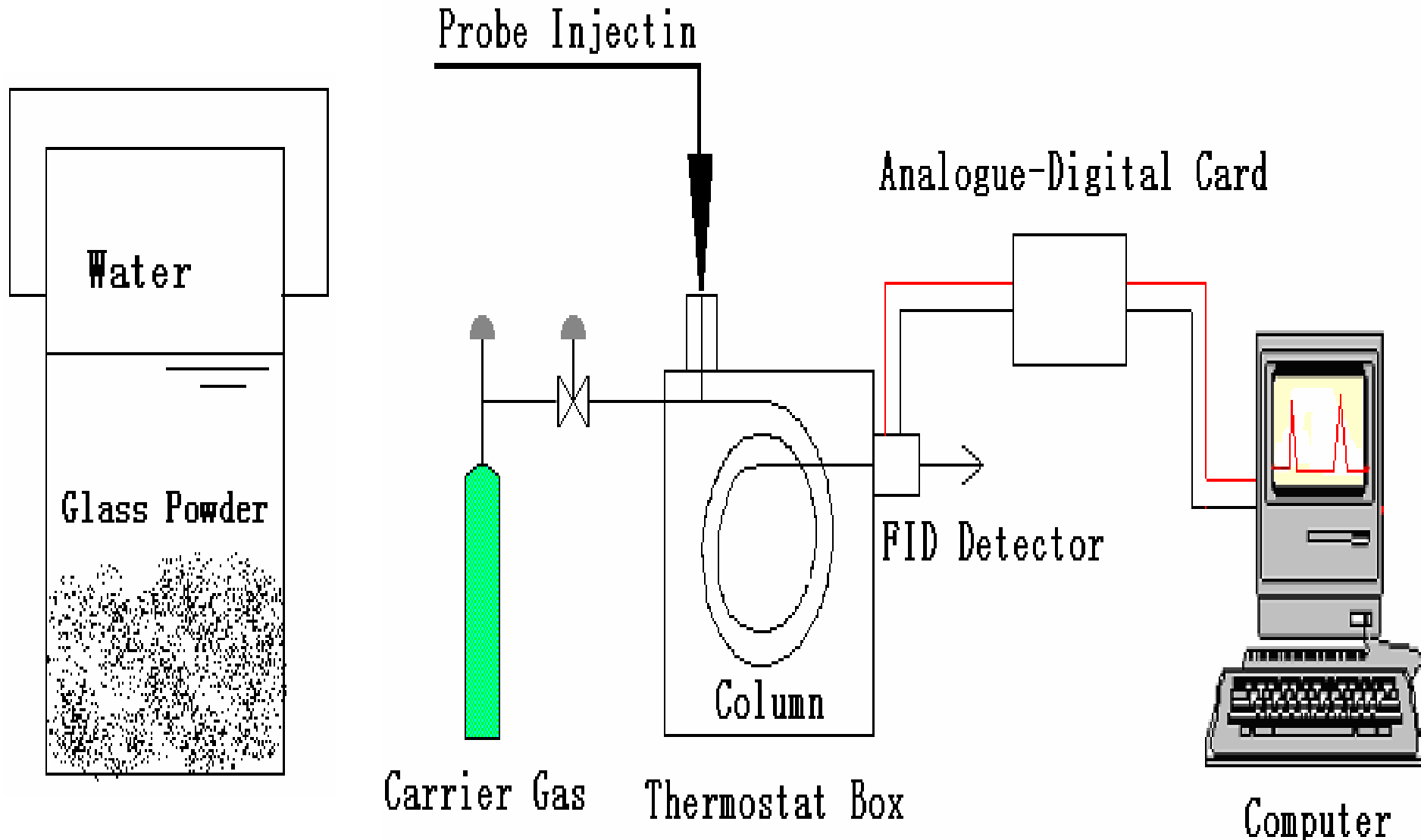
P : 100MPa
T:180 $^{\circ}$ C.



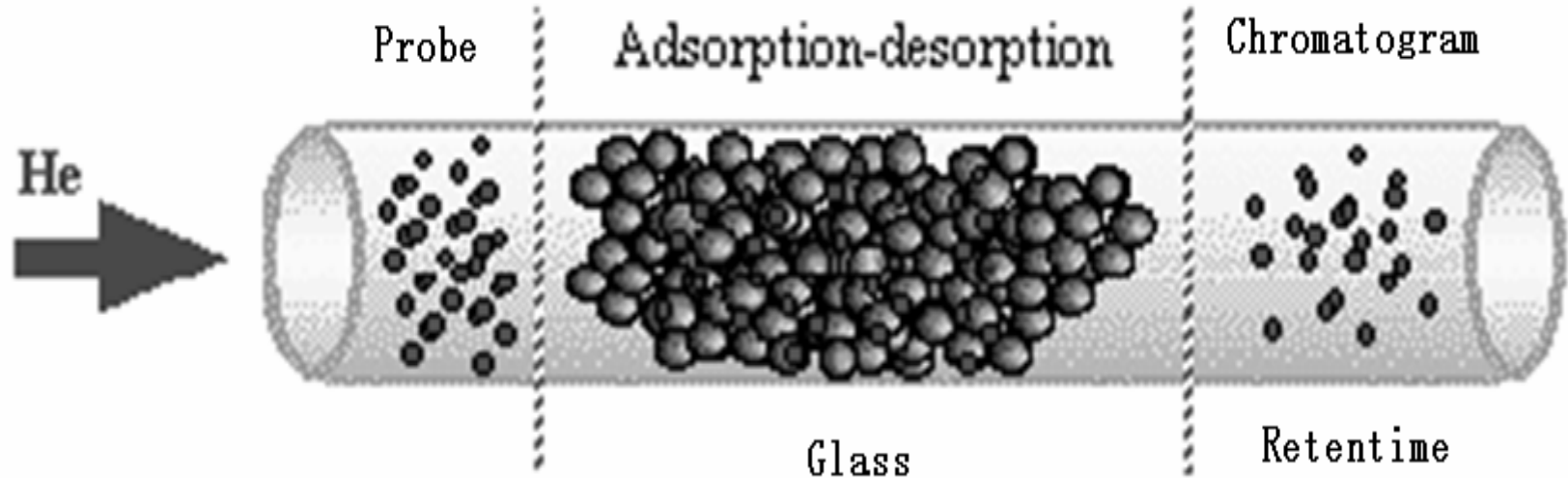
- **4. The Experimental Techniques for the study of the Alteration of HLW Matrix**
- **_The release of radionuclides into the environment is only realized through the alteration of the matrix glass**
- **_The Underground water will contact the waste by seeping into the canister through the corrosion holes.**
- **_The waste block has many fissures and the alteration will start on the fissure surfaces**
- **_We will use the inverse gas chromatography(IGC) to study the evolution of the altered surface**



The Study of Glass Surface Alteration by Inverse Gas Chromatography



The Study of Glass Surface Alteration by Inverse Gas Chromatography

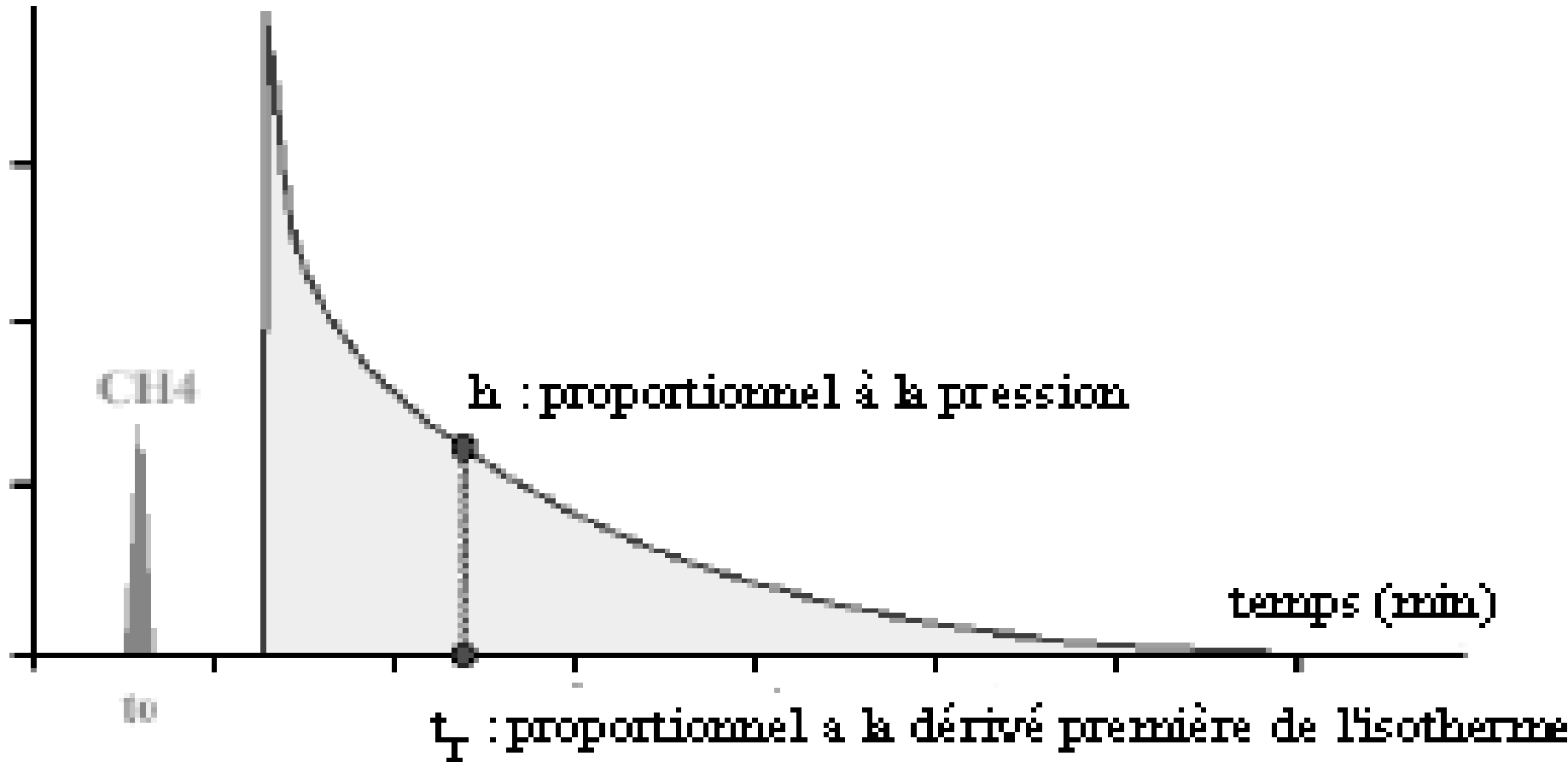


IGC can measure the following surface parameters:

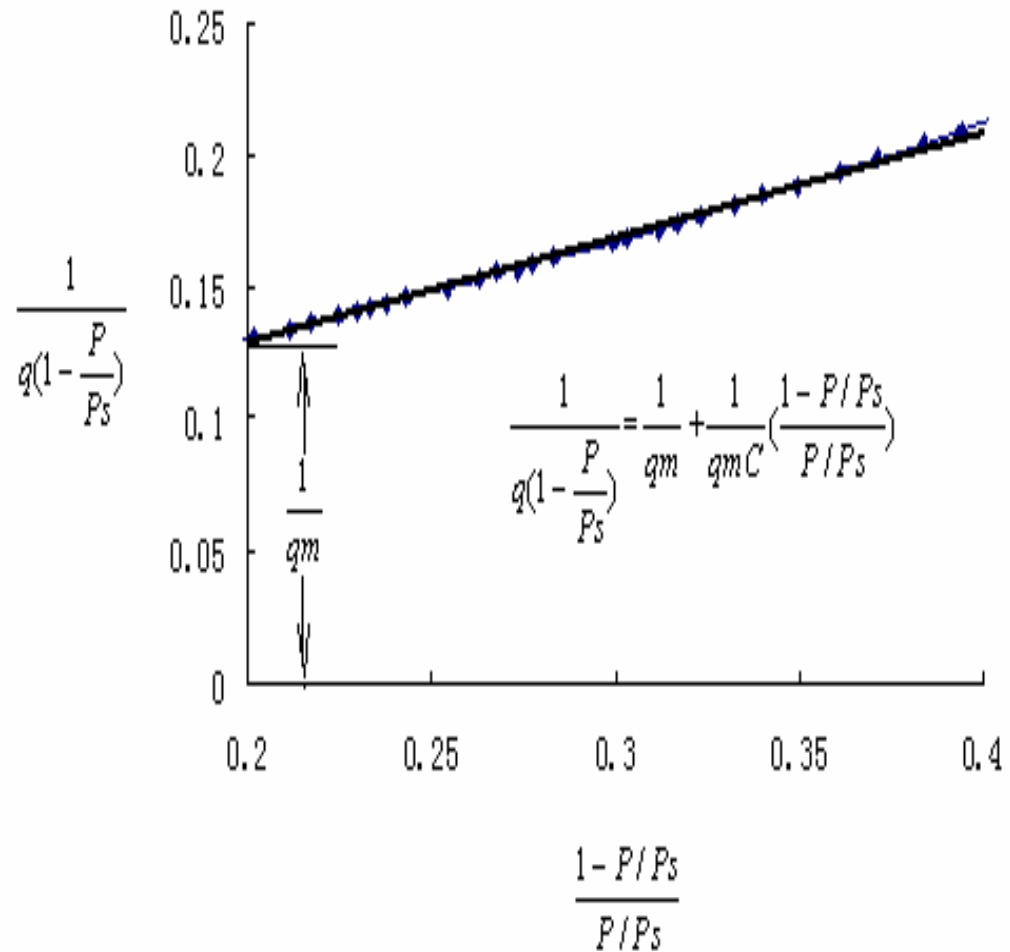
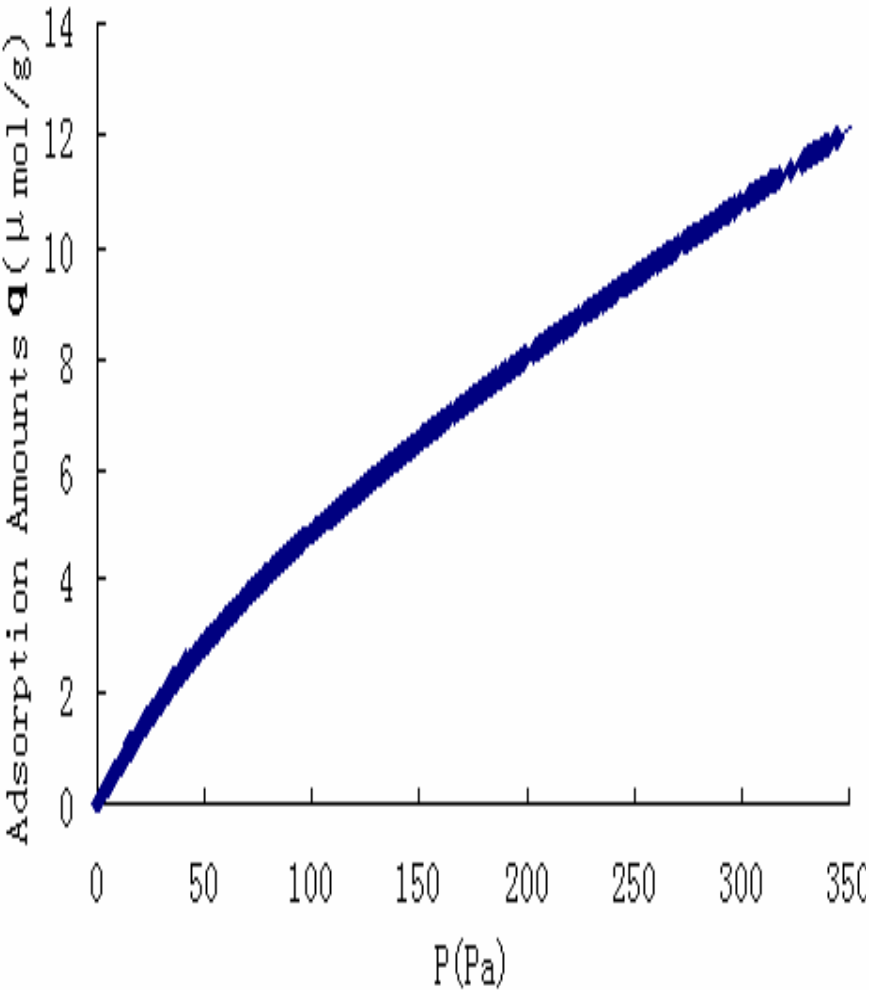
_The Specific Surface Area $S(m^2/g)$

_The Surface Morphology Index IM

From Chromatogram to the Specific Surface Area



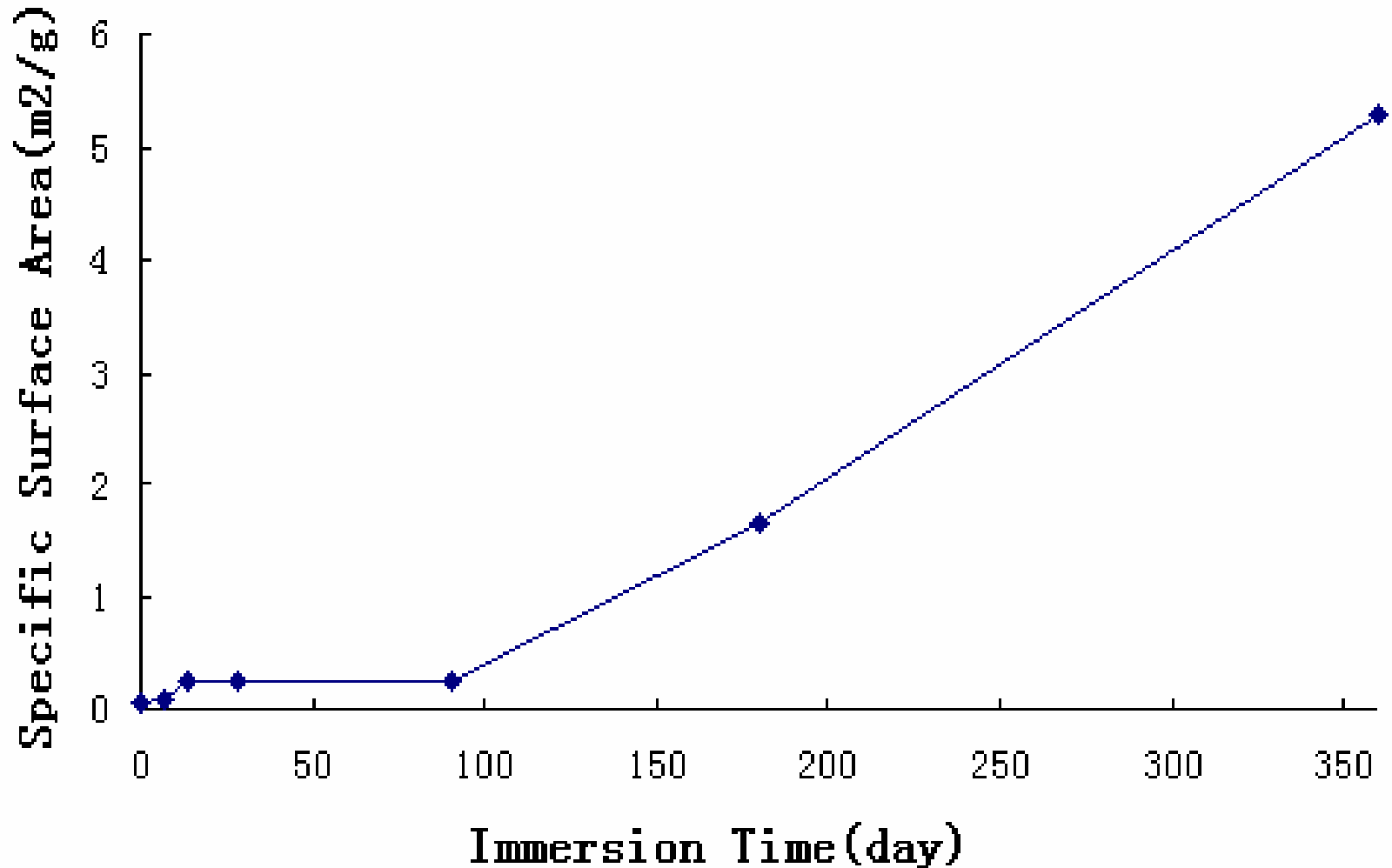
$$\left(\frac{\partial N}{\partial P} \right)_{L, R} = \frac{1}{RT} \frac{D_c}{m} (t_R - t_0)$$

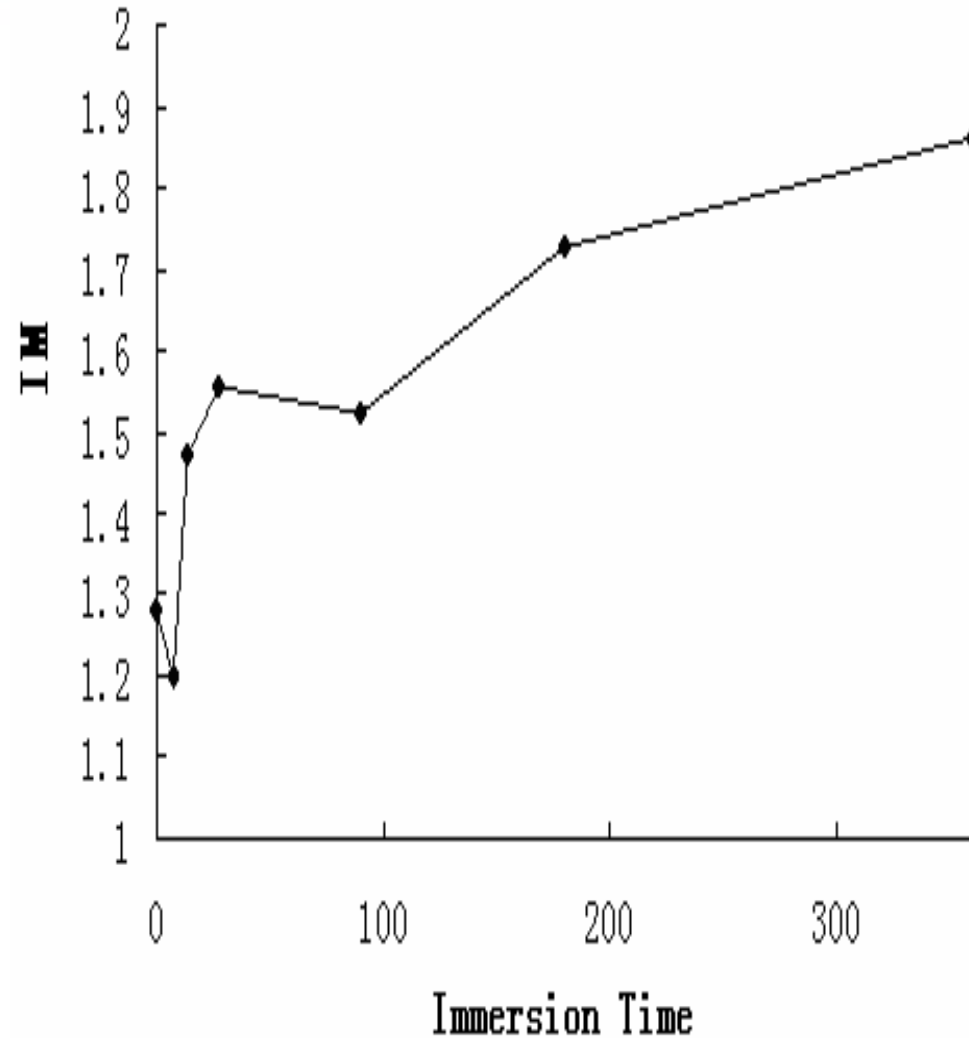
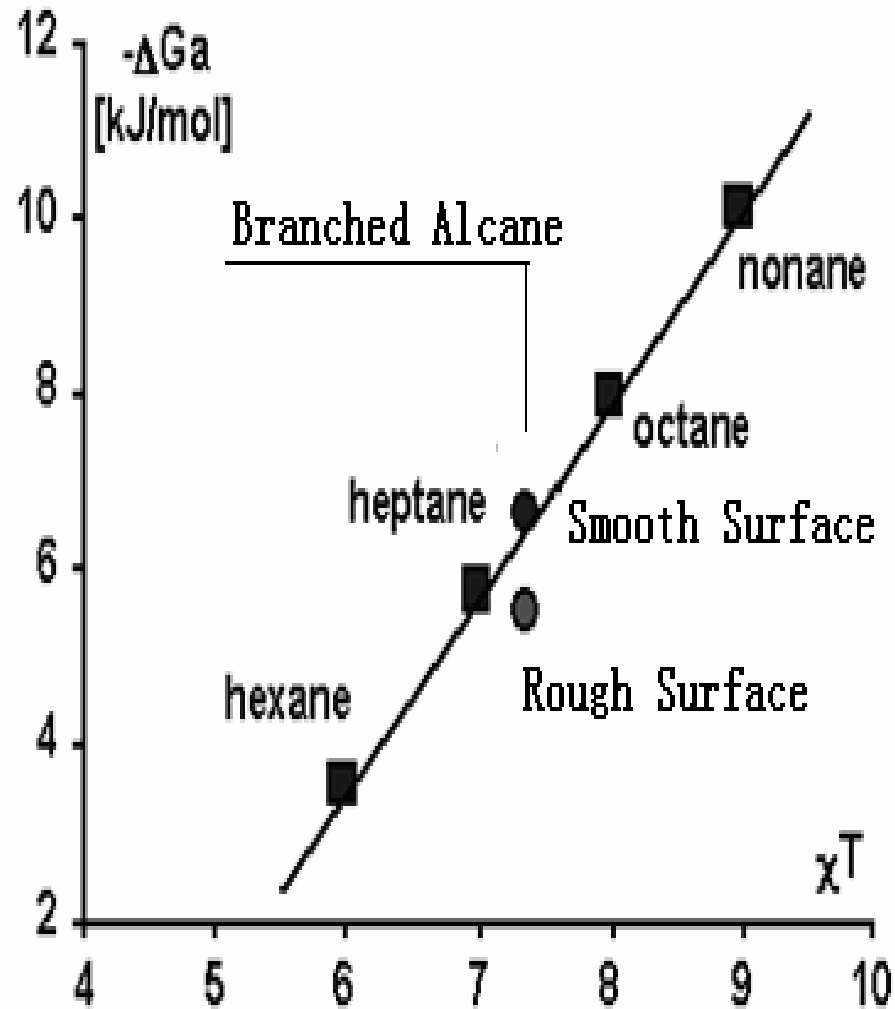


**By linearization of the adsorption isotherm, the monlayer capacity can be calculated ;
Using the monolayer capacity, the specific surface area can be calculated**



Specific Surface Area S vs Immersion Time





$$IM(\text{Branched Alkane}) = \exp[DG_a(M)/DG_a(C)]$$



- **The three-stage** could be explained by the **three-stage model** of glass corrosion
- **The first stage** is dominated by interdiffusion
- **The second stage** is dominated by **matrix dissolution**.
- **The third stage** is due to the formation of surface layers by the **precipitation and adsorption** of the insoluble compounds



- **_We have established some small scale experimental techniques for the Study of Migration and Alteration in the laboratory**
- **_We will develop More large scale techniques to simulate some scenaios.**
- **_We will establish our databases for the Migration and Glass alteration**
- **_We wish to cooperate with German scientists in Waste treatment and Disposal**

Technical Aspects of Direct Disposal of Spent Fuel and HLW

Wilhelm Bollingerfehr
DBE TECHNOLOGY GmbH

Chinese-German Workshop on Radioactive Waste Disposal
May 28 – 31, 2007
Beijing

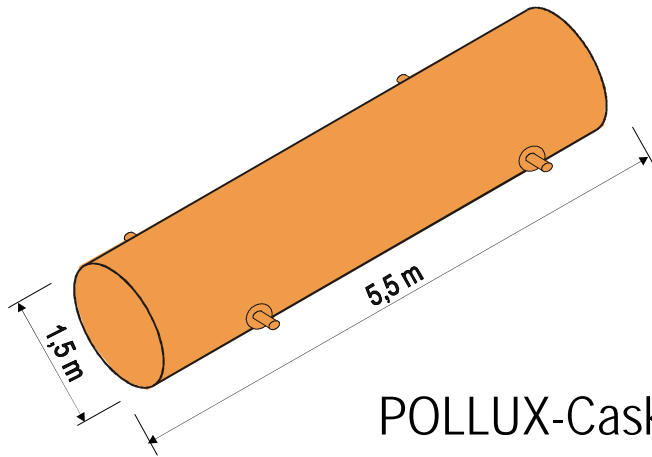
== Outline ==

1. Introductory remarks to spent fuel direct disposal
2. German R & D program on direct disposal
3. Full-scale demonstration program
4. Recent developments
5. Summary and Conclusions

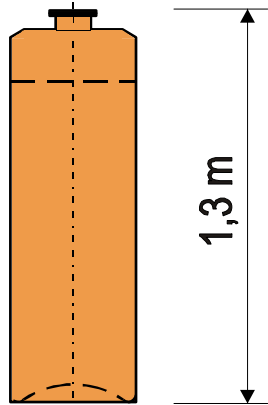
German Waste Accumulation and Forecast

	Until 2000	2001-10	2011-20	2021-30	2031-40	Total	Total [m ³]
• Heat generating waste							24,000.00
HAW-canisters	84.00	4,852.00	112.00	0.00	0.00	4,778.00	908.00
HAW-packages	0.00	840.00	7,576.00	2,400.00	0.00	10,816.00	2,814.00
AVR+THTR SNF elements	908,705.00	0.00	0.00	0.00	0.00	908,705.00	1,890.00
LWR SNF (Mg)	3,142.00	3,962.00	1,819.00	24.00	0.00	8,947.00	18,258.00
Research reactor SNF (Mg)							≈ 130.00
• IL/LLW non-heat generating (m ³)	76,000.00	58,000.00	54,000.00	76,000.00	33,000.00	297,000.00	297,000.00
NNP	23,000.00	23,000.00	46,000.00	73,000.00	22,000.00	195,000.00	
Government facilities	53,000.00	27,000.00	8,000.00	3,000.00	11,000.00	102,000.00	

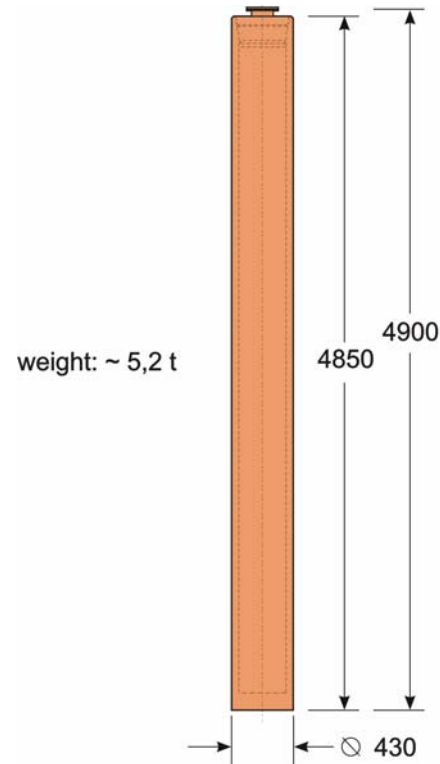
Disposal Canisters



POLLUX-Cask
(spent fuel)
weight: 65 t

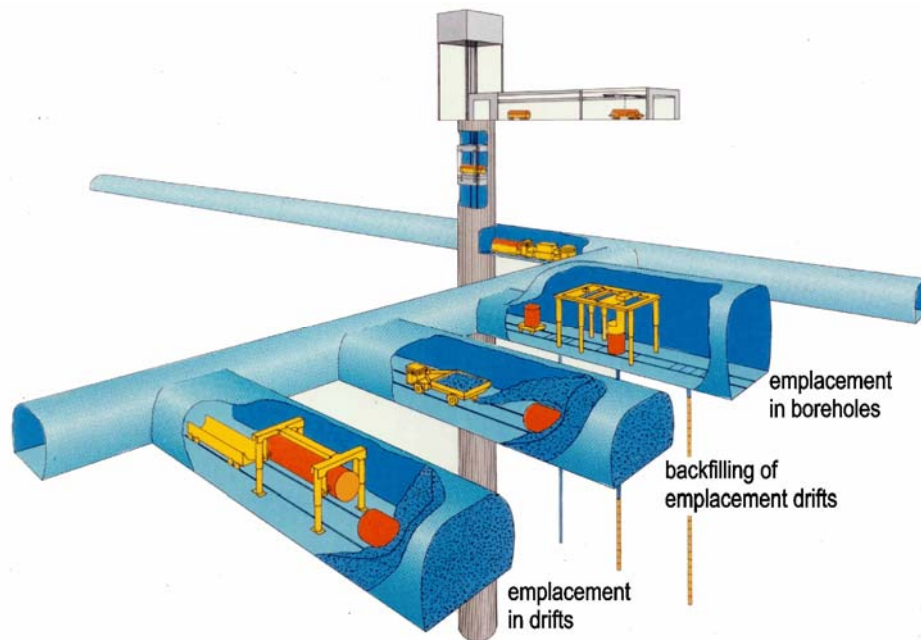


HLW-Canister
(vitrified waste)
weight: ~ 500 kg



BSK 3-Canister
(spent fuel)
weight: ~ 5.2 t

Disposal Concept



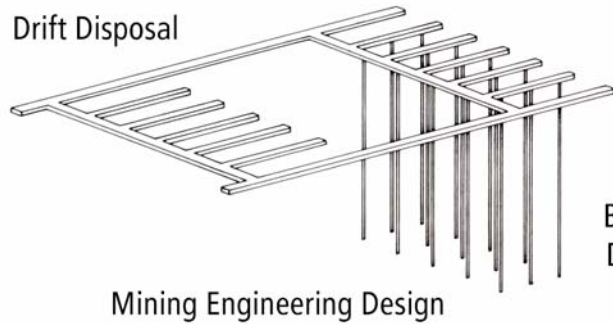
German Reference Concept for HLW and Spent Fuel: Direct Disposal in Rock Salt

- Deep geological disposal (depth: 840 m)
- Emplacement of HLW in boreholes and spent fuel casks in drifts
- Backfill material: crushed salt

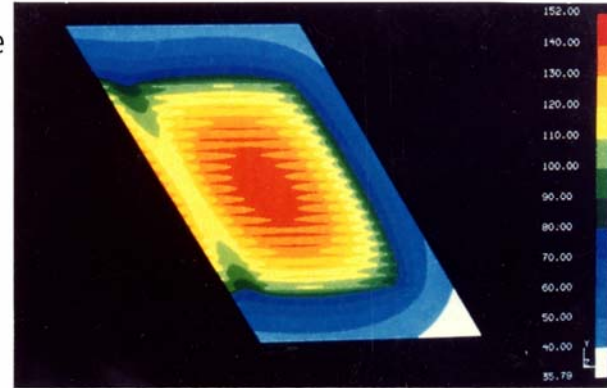
== Objectives of R & D Program ==

- Demonstrate safe and reliable transport of waste canisters
- Demonstrate technical feasibility of safe spent fuel emplacement in rock salt
- Increase the data base on important phenomena and processes in and around a backfilled repository
- Strengthen the scientific basis required for repository design and performance assessment

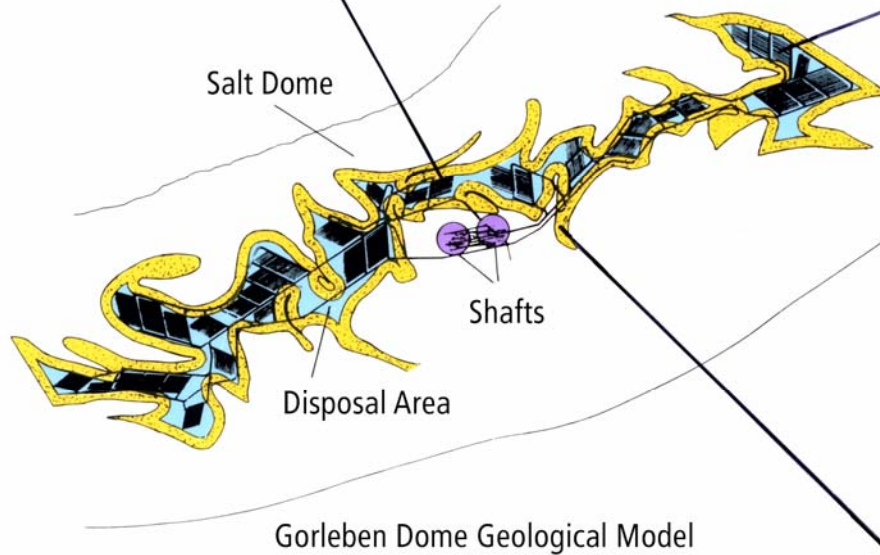
Repository Layout



Temperature Field



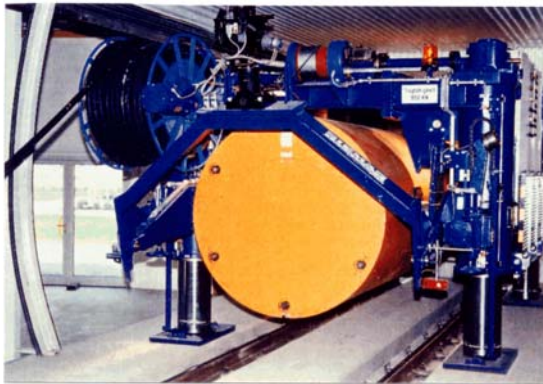
Geomechanical Design



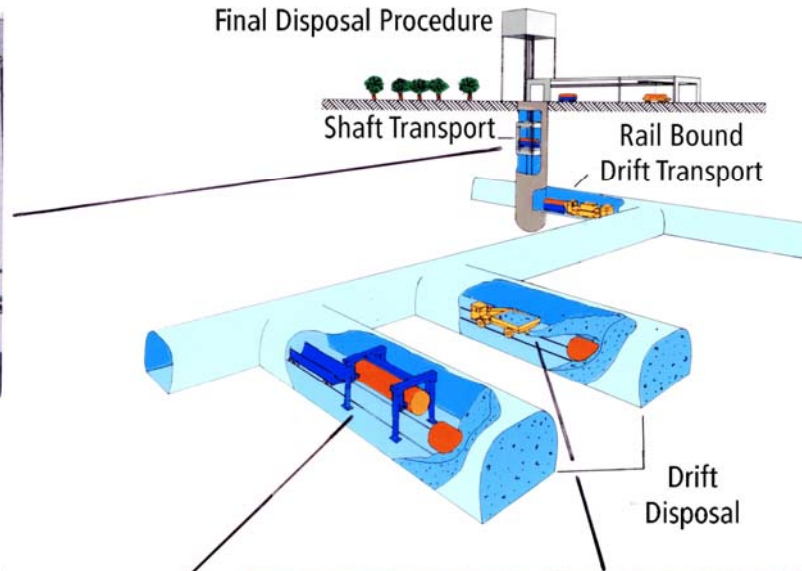
== Scope of Full-Scale Demonstration Program ==



Hoisting Cage for 85t Payload



Waste Emplacement Machine



Backfilling Slinger Truck in a Disposal Drift

Design of a Shaft Hoisting System

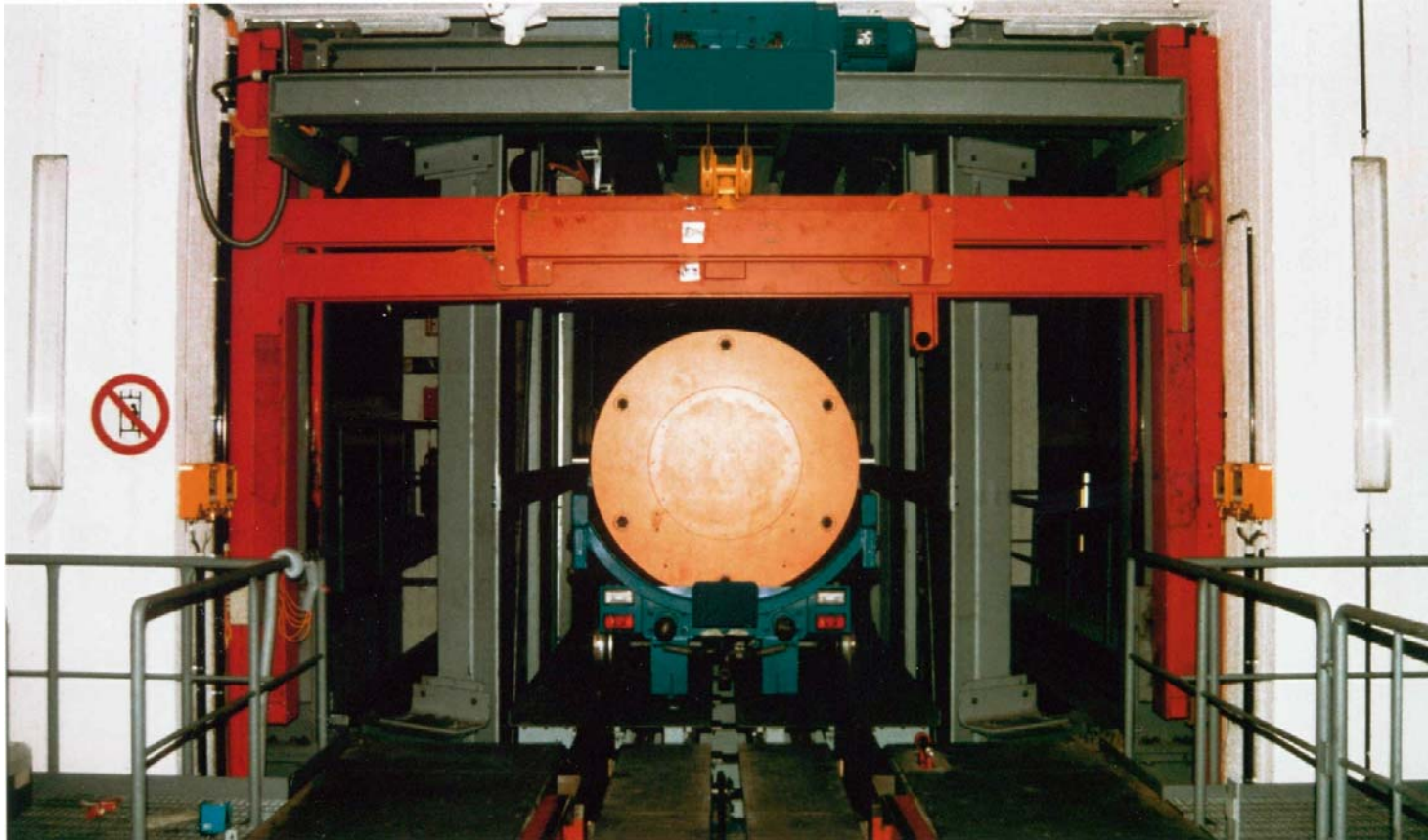


Technical data:

Depth of shaft: 1,000 m
Max. payload: 85 t
Max. speed: 12 m/s at 30 t
 5 m/s at 85 t
Motor power: 2 x 2,800 kW

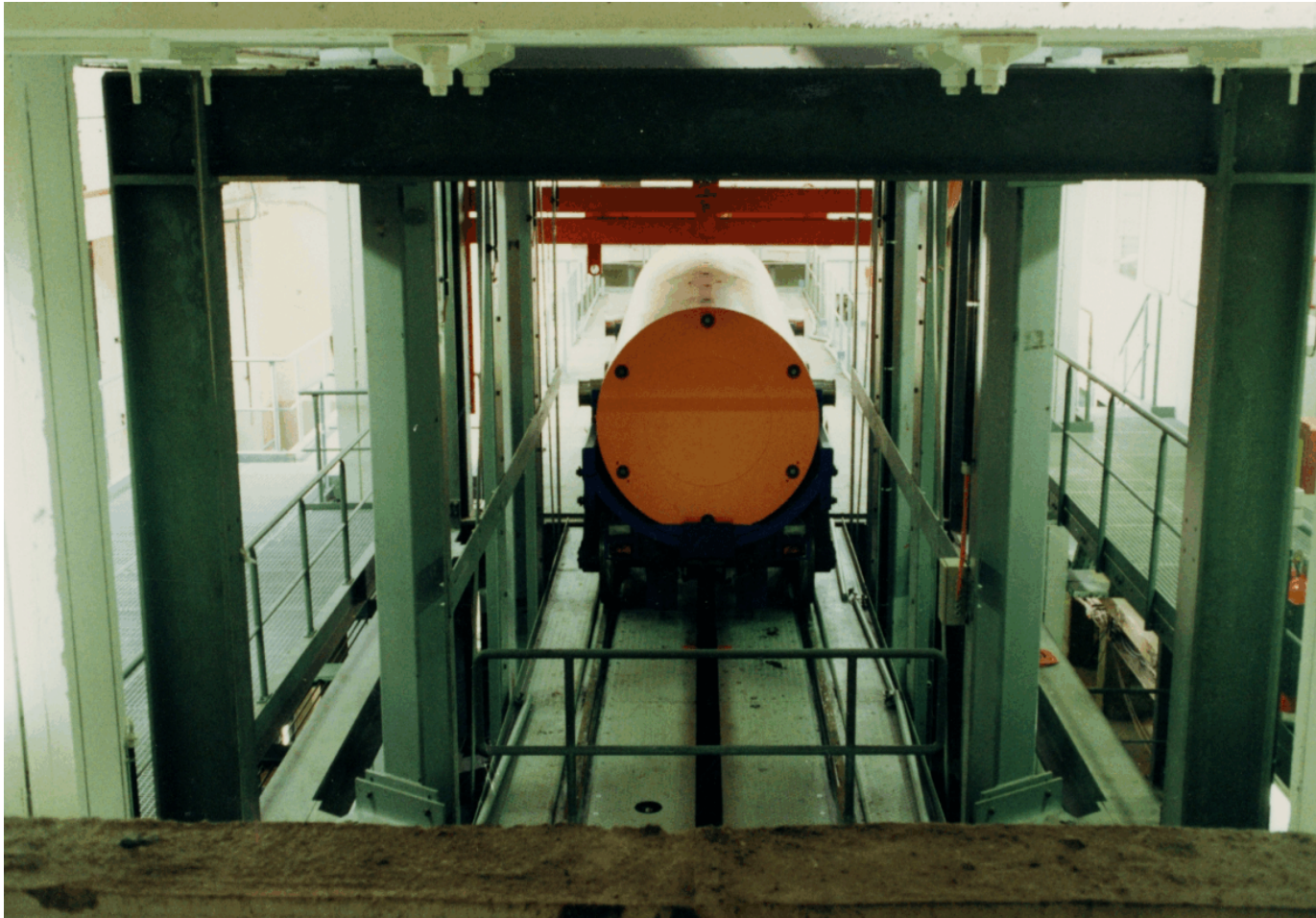
Longitudinal section through the shaft hoisting system

== Shaft Hoisting System ==



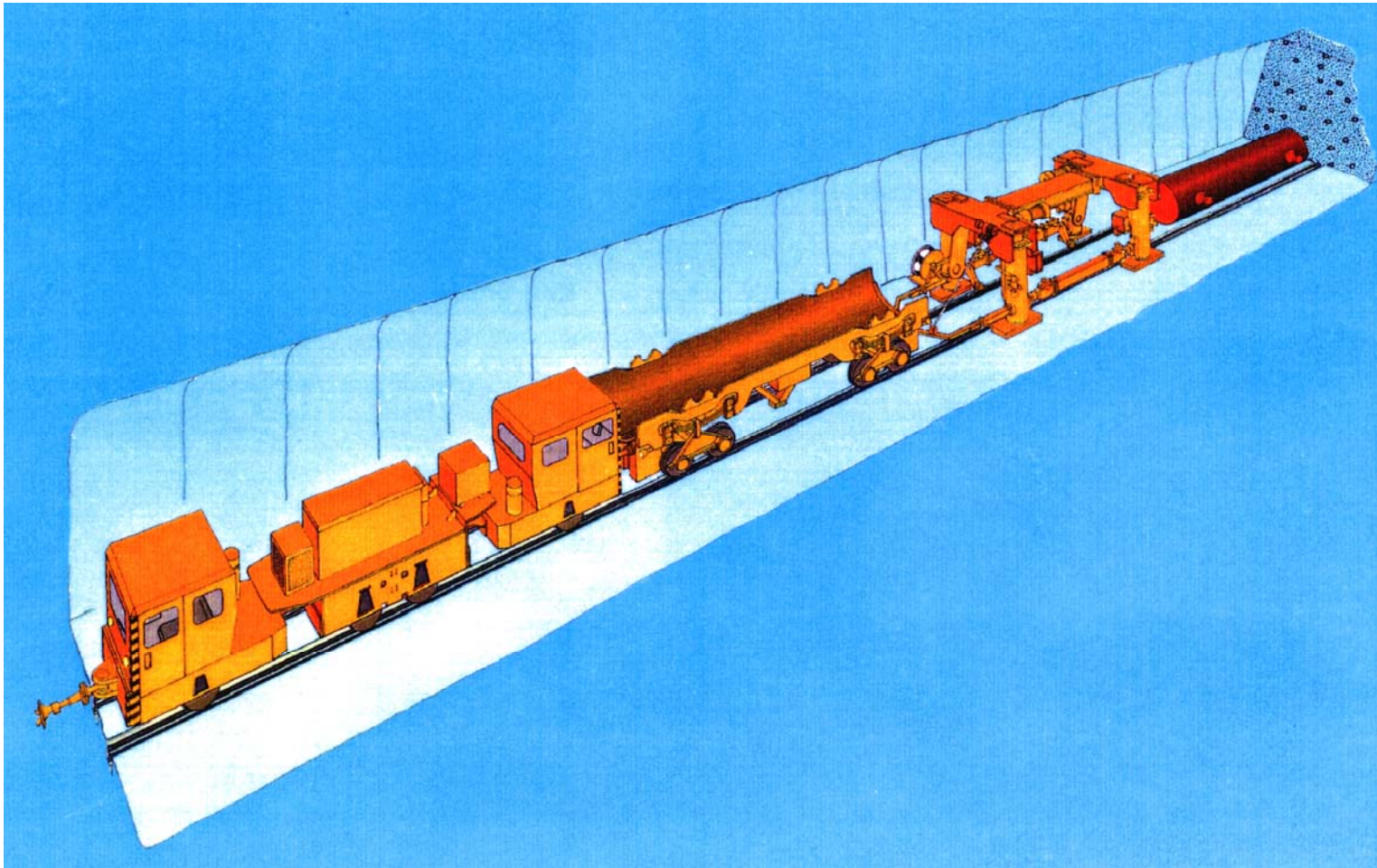
Full-scale demonstration of the shaft hoisting system at the test site

== Shaft Hoisting System ==



Full-scale demonstration of the shaft hoisting system at the test site

Emplacement Technology



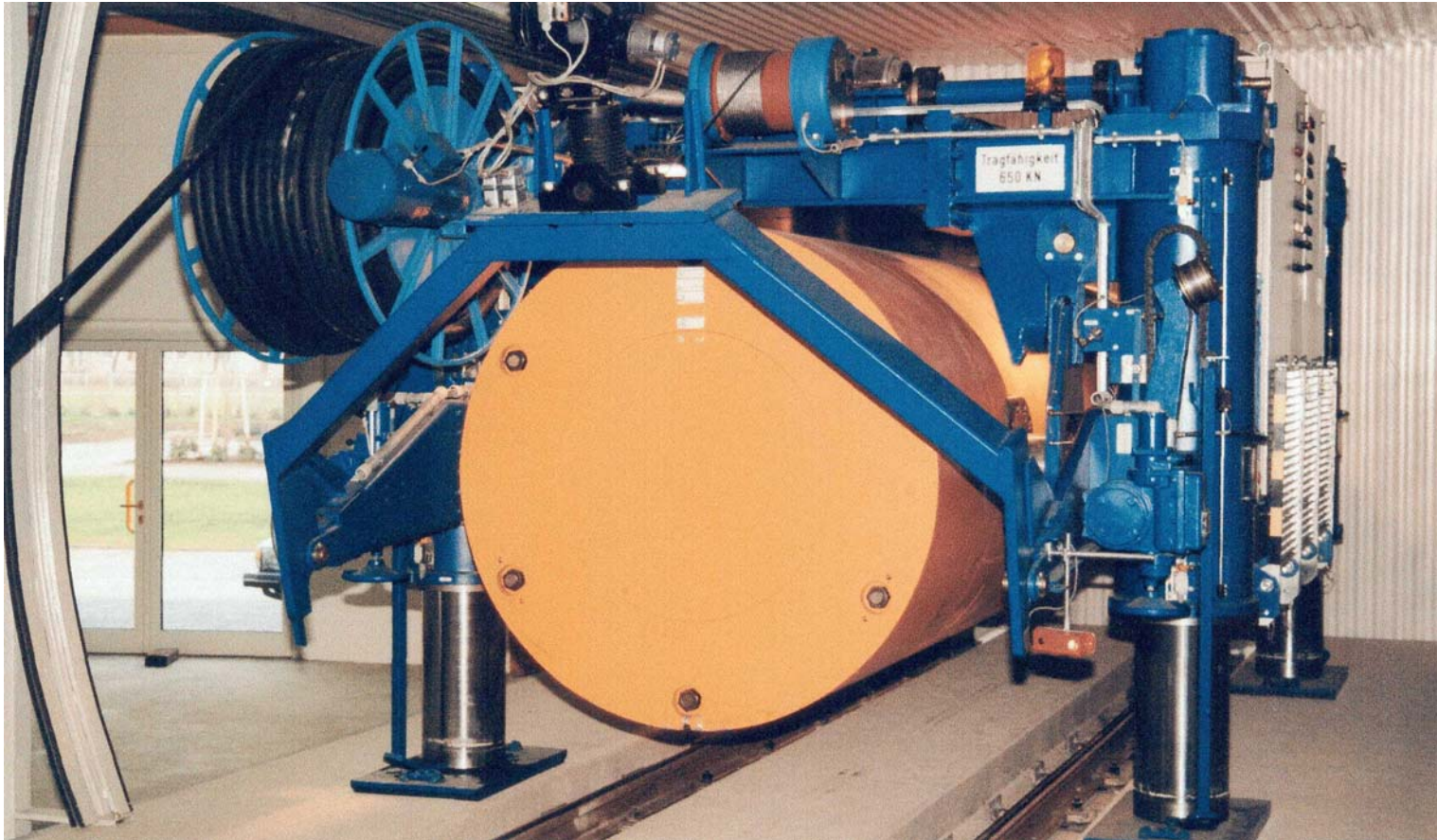
Concept of the emplacement system for POLLUX casks

== Emplacement Technology ==



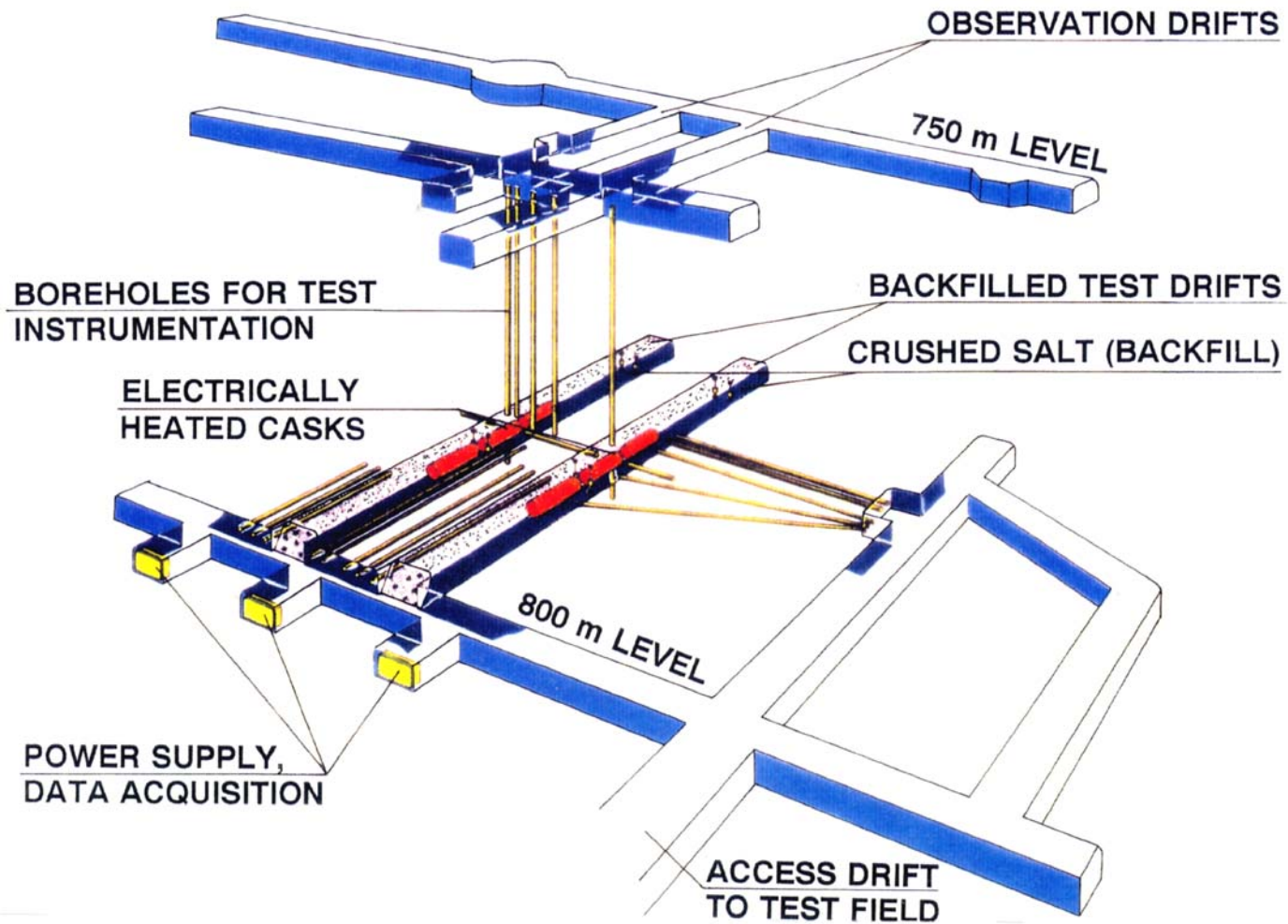
Full-scale demonstration of the POLLUX emplacement system
at the test site in Peine

== Emplacement Technology ==

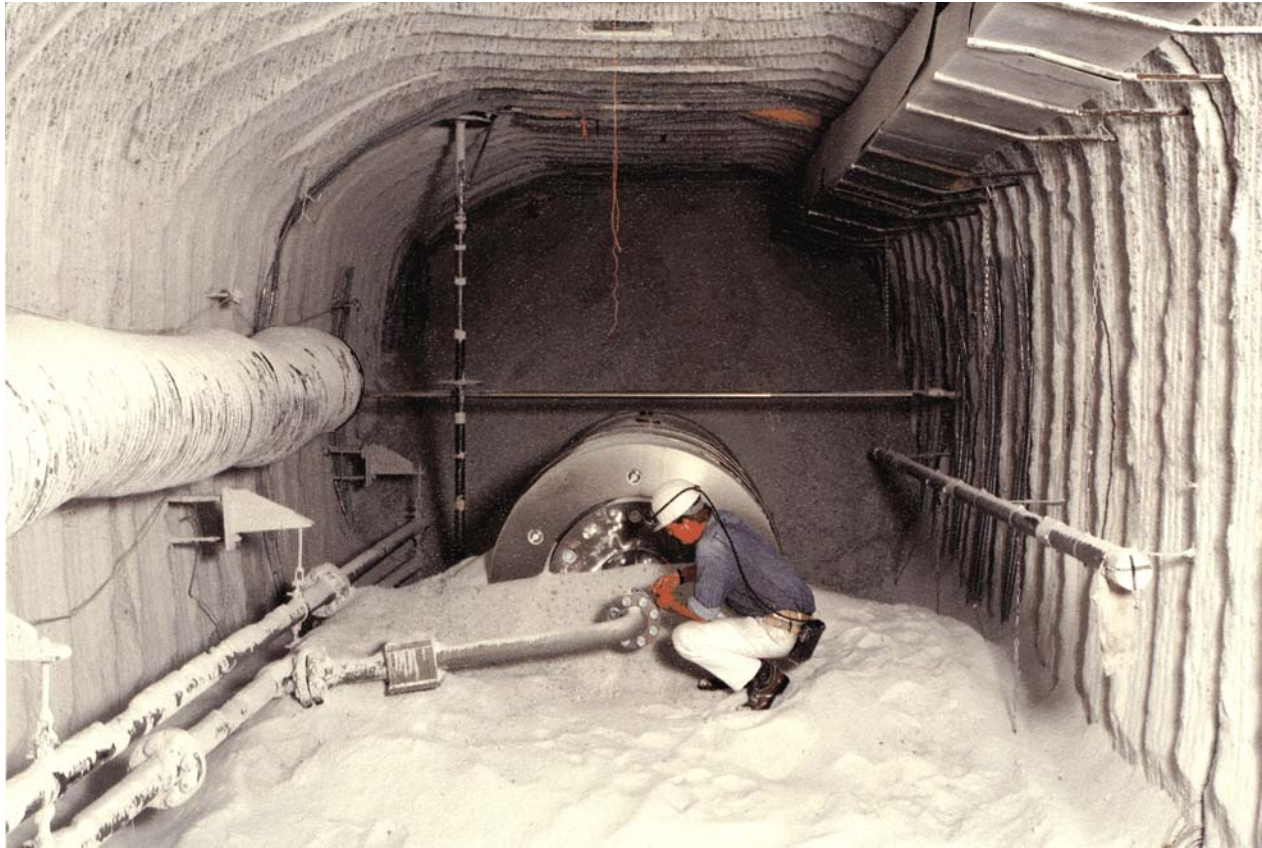


Full-Scale Emplacement machine

In situ-Test in the Asse Mine



— In-situ test in the Asse mine



Full-scale test set up for investigating heat impact on host rock and backfill

== In situ test in the Asse mine

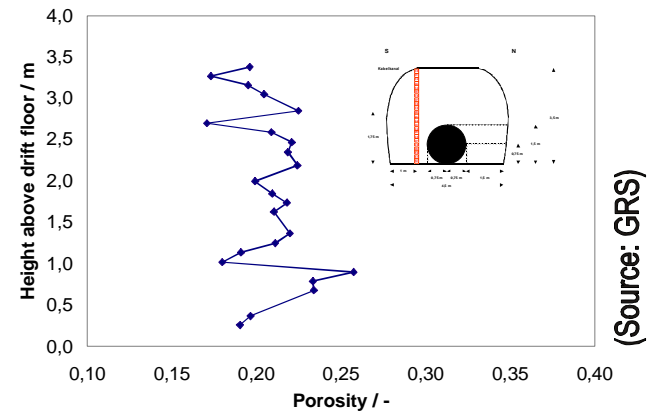


Dismantling of heater casks after approx. 10 years of in-situ operating

Results of Backfill in-situ Tests

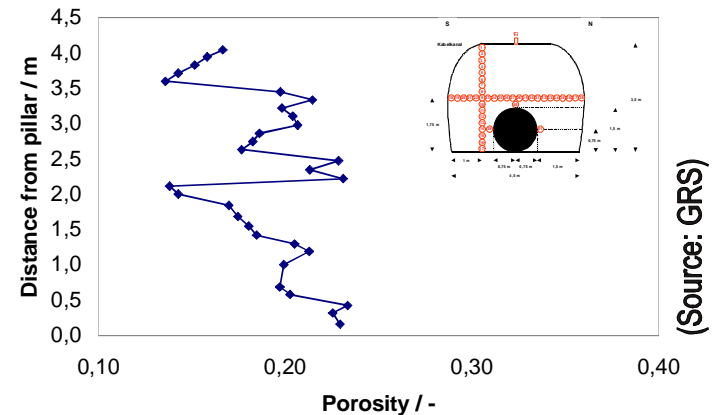


Backfill sampling around the central heater after dismantling



(Source: GRS)

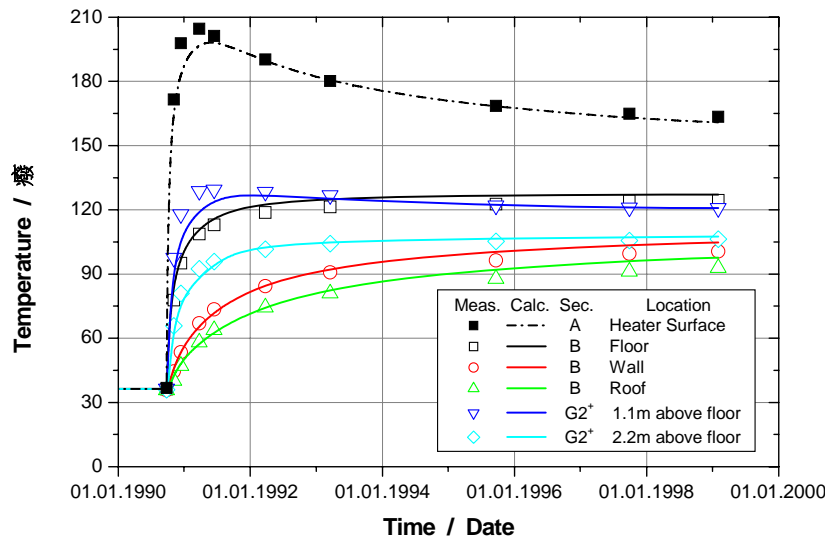
Vertical distribution of backfill porosity at the central heater



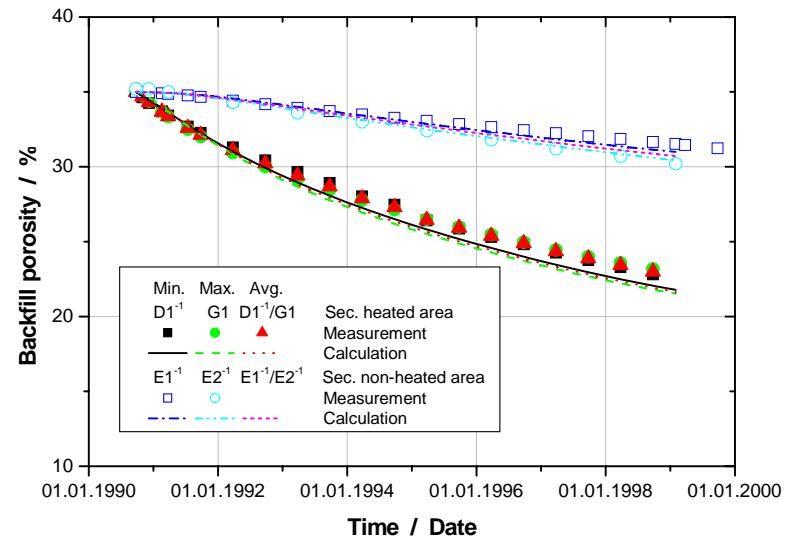
(Source: GRS)

Horizontal distribution of backfill porosity at the central heater

Validation of Predicted Results



Measured and predicted temperature evolution in the TSDE experiment



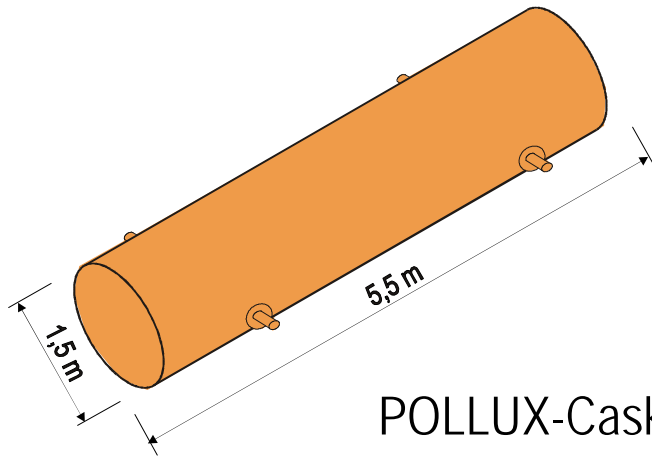
Measured and predicted porosities in the backfill in the TSDE experiment

Recent development

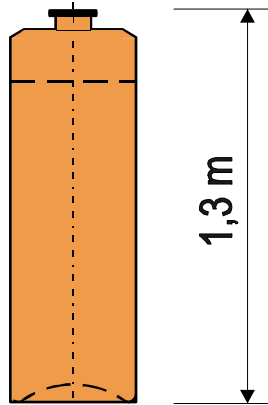
In the context of the 6th framework programme of EC

- Integrated project ESDRED was launched
(Engineering Studies and Demonstration of Repository Designs)
- Objective: Development and demonstration of safe and reliable emplacement technology for deep vertical boreholes
(Mature of nuclear and mining licencing)
- 13 partners from 9 countries cooperating in developing and demonstrating repository relevant transport and emplacement technologies as well as sealings/plugs
- Five years program (from 01/2004 to 01/2009)
- Funded by: EC; PTKA and German Nuclear Industry

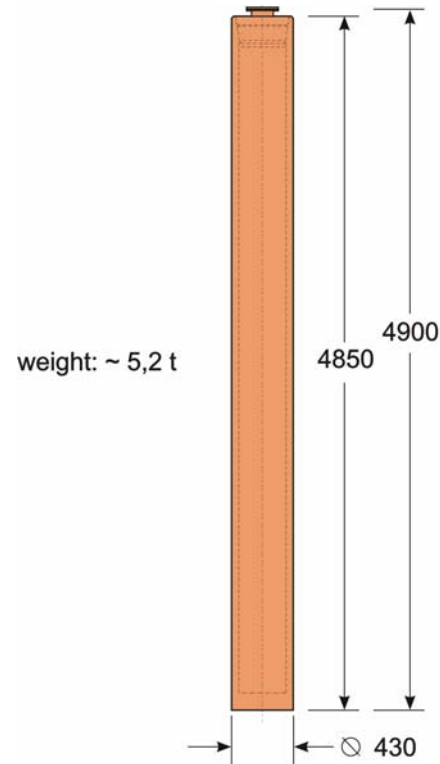
Disposal Canisters



POLLUX-Cask
(spent fuel)
weight: 65 t



HLW-Canister
(vitrified waste)
weight: ~ 500 kg



BSK 3-Canister
(spent fuel)
weight: ~ 5.2 t

Design criteria BSK 3-canister

Design criteria	Explanation	
Inventory of heavy metals	Loading with fuel rods from disassembled fuel assemblies from pressurized and boiling water reactors	Up to 1.63 tHM
Heat	Max. heat output capacity of the canister contents	6 kW
	Max. cladding strain for the storage time by limitation of the cladding temperature	< 1 %
	Max. tangential tension	< 100 MPa
Criticality	Neutron multiplication factor during transport and inspection conditions	$k_{\text{eff}} + 2 \sigma < 0.95$
Tightness	Allowable He-Standard-Leakage rate Sealing of the primary lid	$1 \cdot 10^{-3}$ hPa *l/s
	Allowable He-Standard-Leakage rate after welding of the secondary lid	$\ll 1 \cdot 10^{-7}$ hPa *l/s
Strength	Design for maximum isostatic rock pressure in the repository	30 MPa

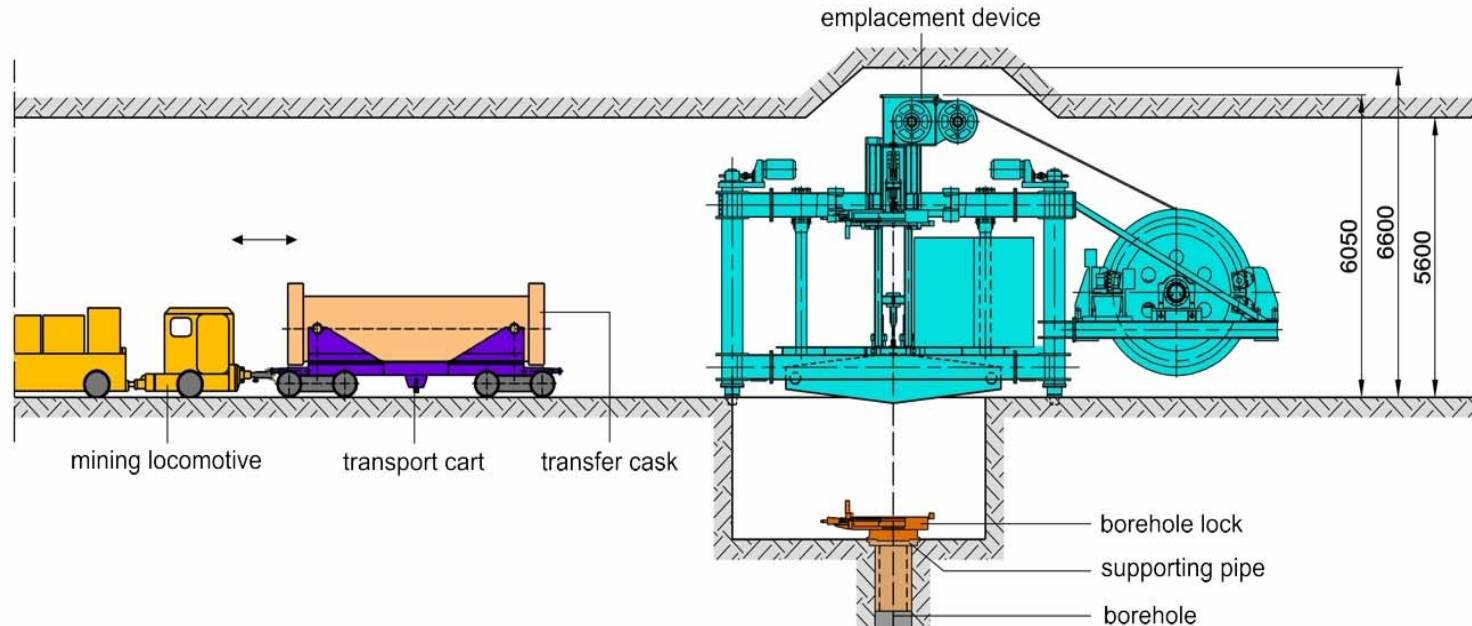
Disposal Canister Characteristics

		HLW Canister	CSD-C Canister	BSK 3 Canister
Number of canisters		4,778	8,764	app. 5,525
Number of boreholes needed		30	55	95
Length	mm	1,338	≤ 1,345	4,980
Diameter	mm	430	≤ 440	≤ 440
Total mass	kg	app. 492	≤ 850	5,226
Mass HM	tHM	-	-	1.6
Heat generation	kW			
• at loading			0.02	21,220
• after 10 years		1.12 ^{*)}		3,030
• after 30 years		0.67 ^{**)}		1,930

***) after 9 years**

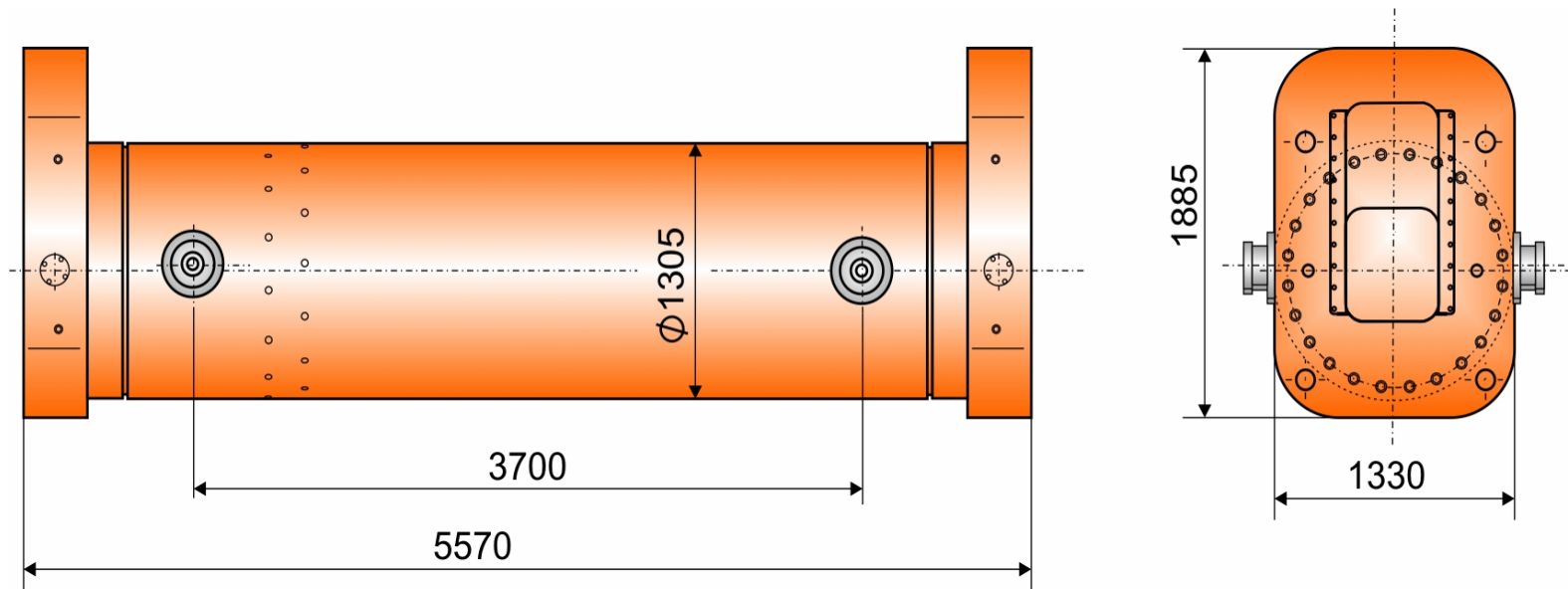
*****) after 29 years**

Another Full-scale demonstration



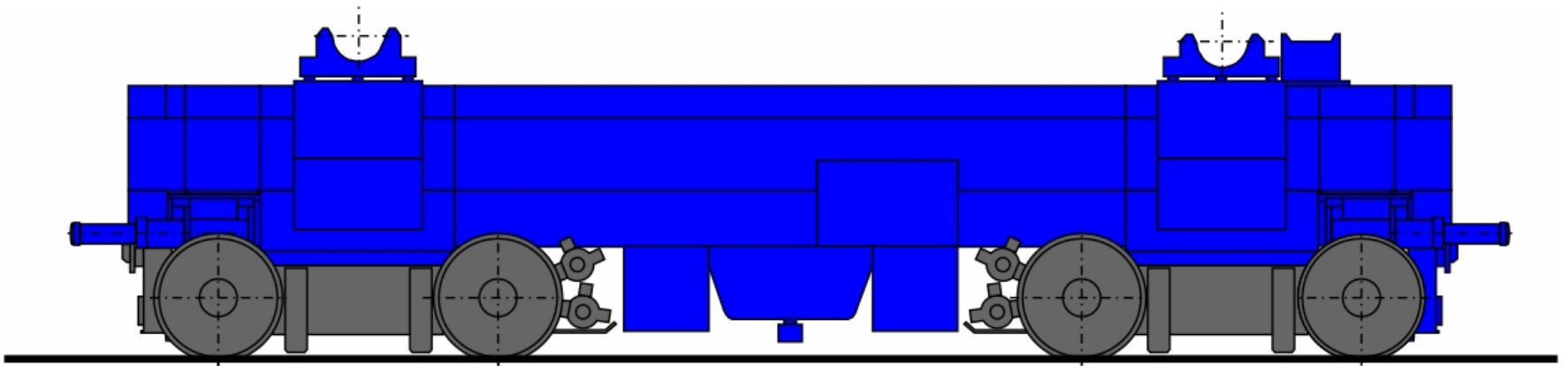
Concept of the emplacement system for BSK 3 canister

Transfer Cask

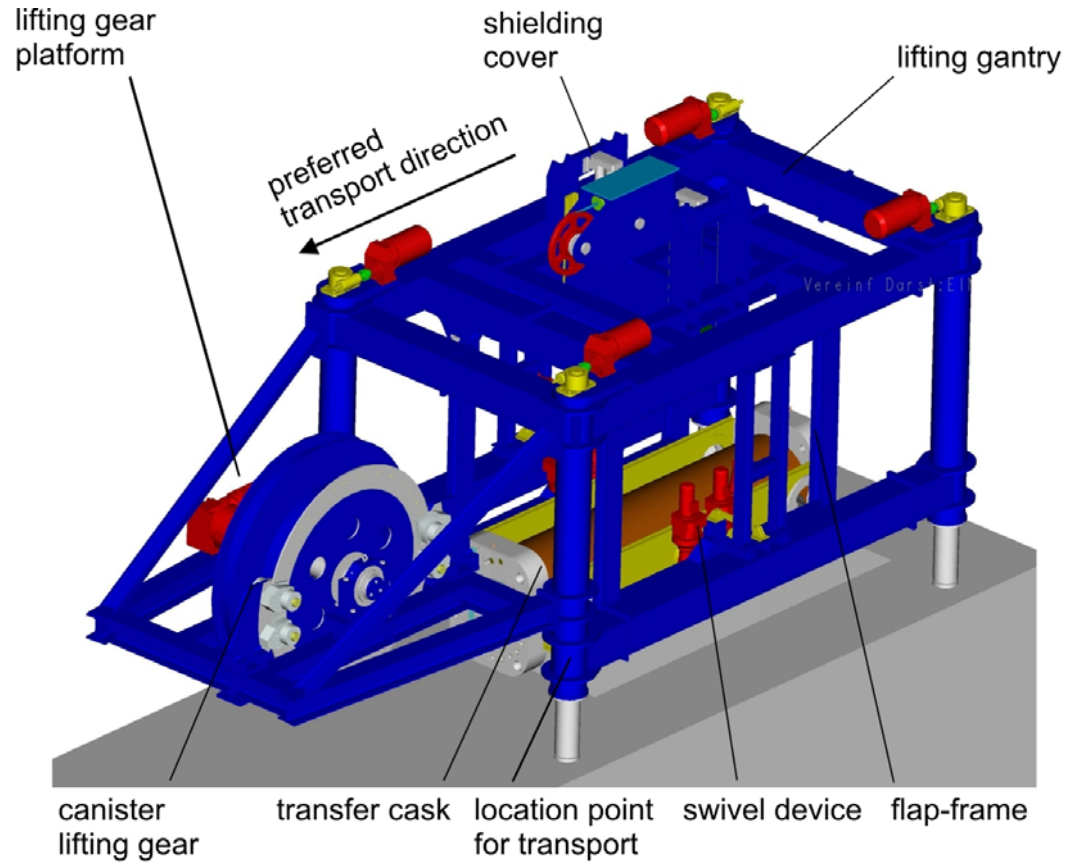


Total weight: 45 t

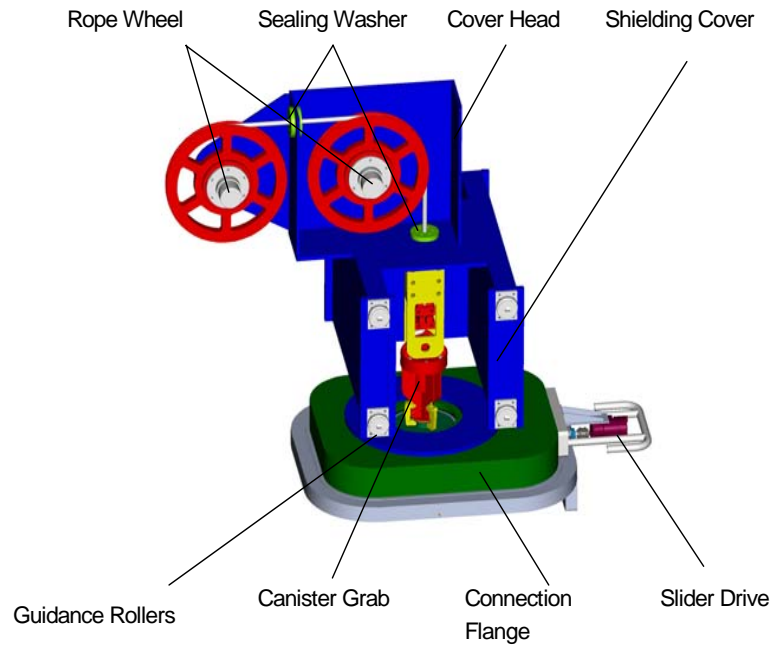
== New Transport Cart ==



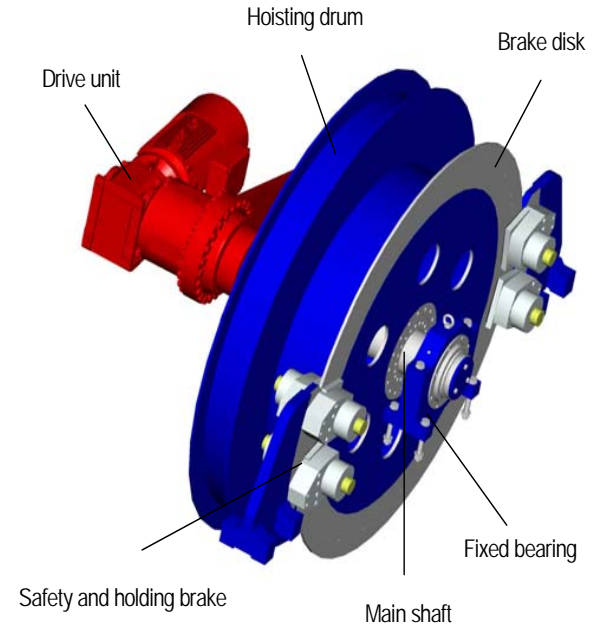
Emplacement Device



Details of Emplacement Device

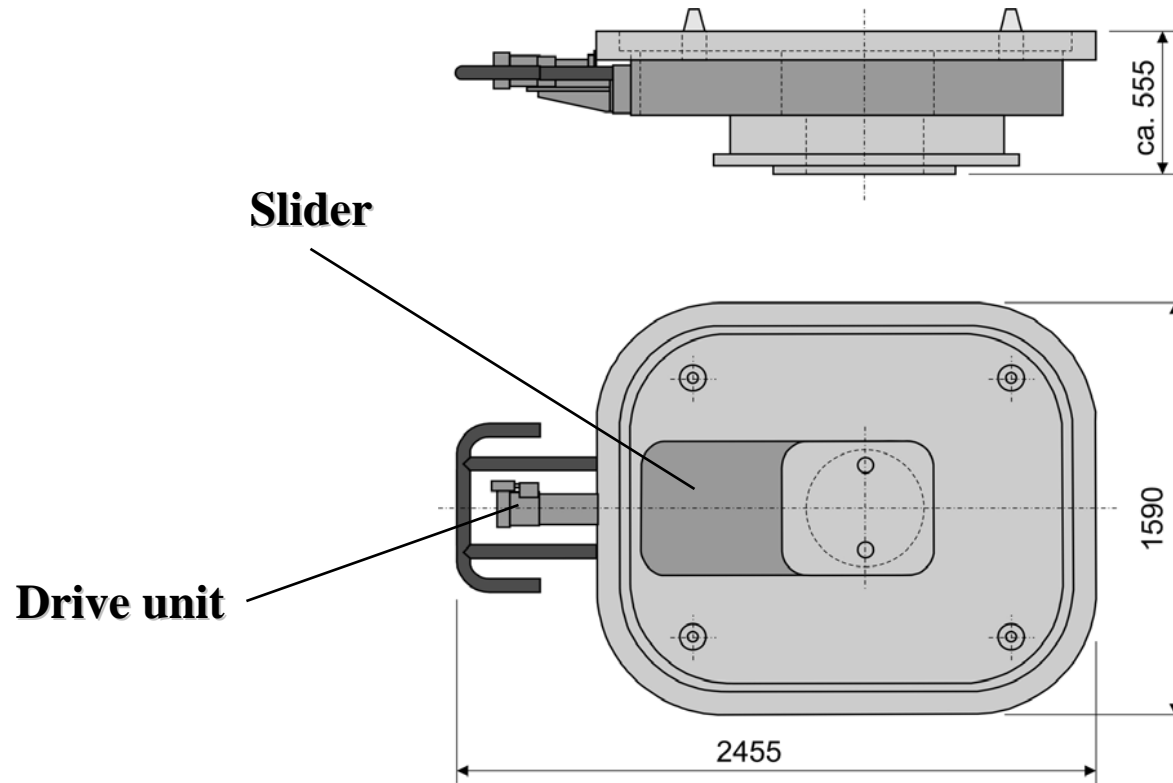


Shielding cover



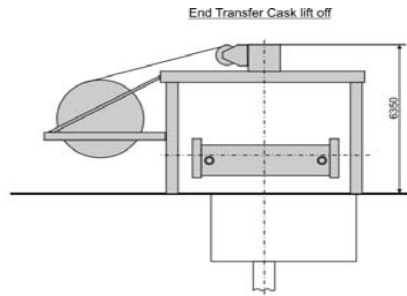
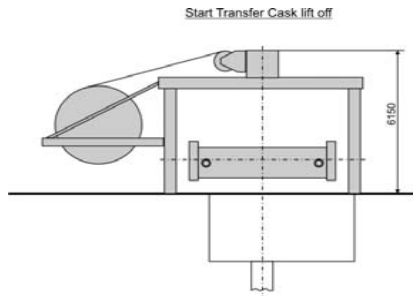
Canister lifting gear

Borehole Lock

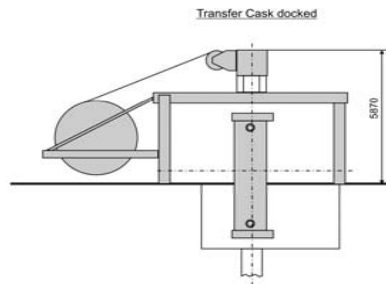
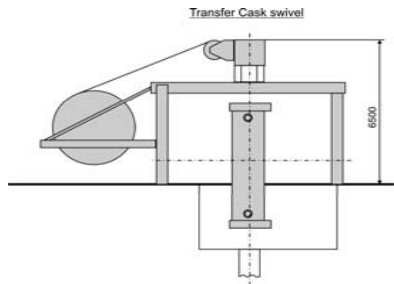


Total weight: 5.2 t

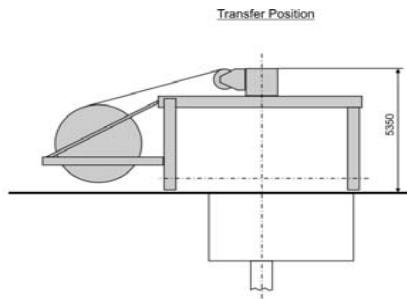
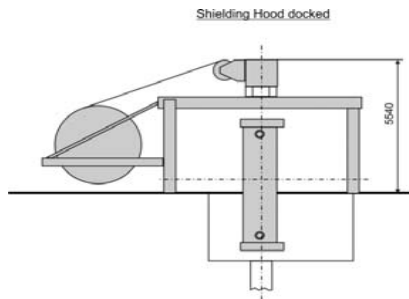
Optimization of Emplacement Drift Height



Emplacement device heights during operation I

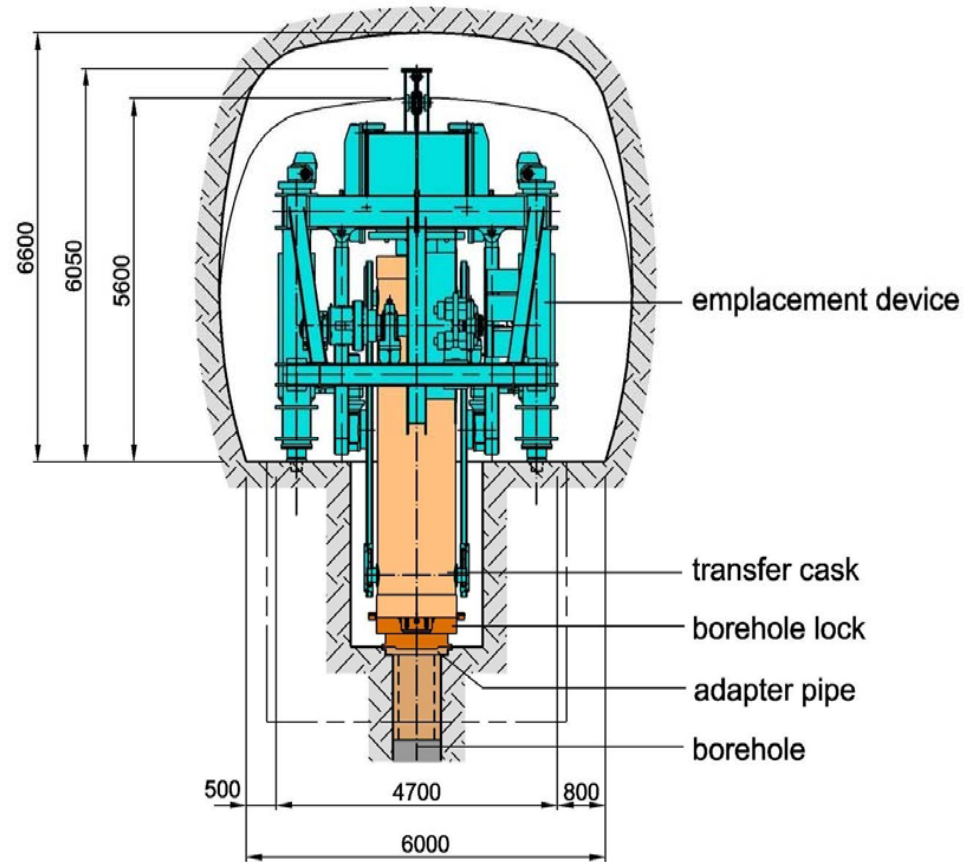


Emplacement device heights during operation II

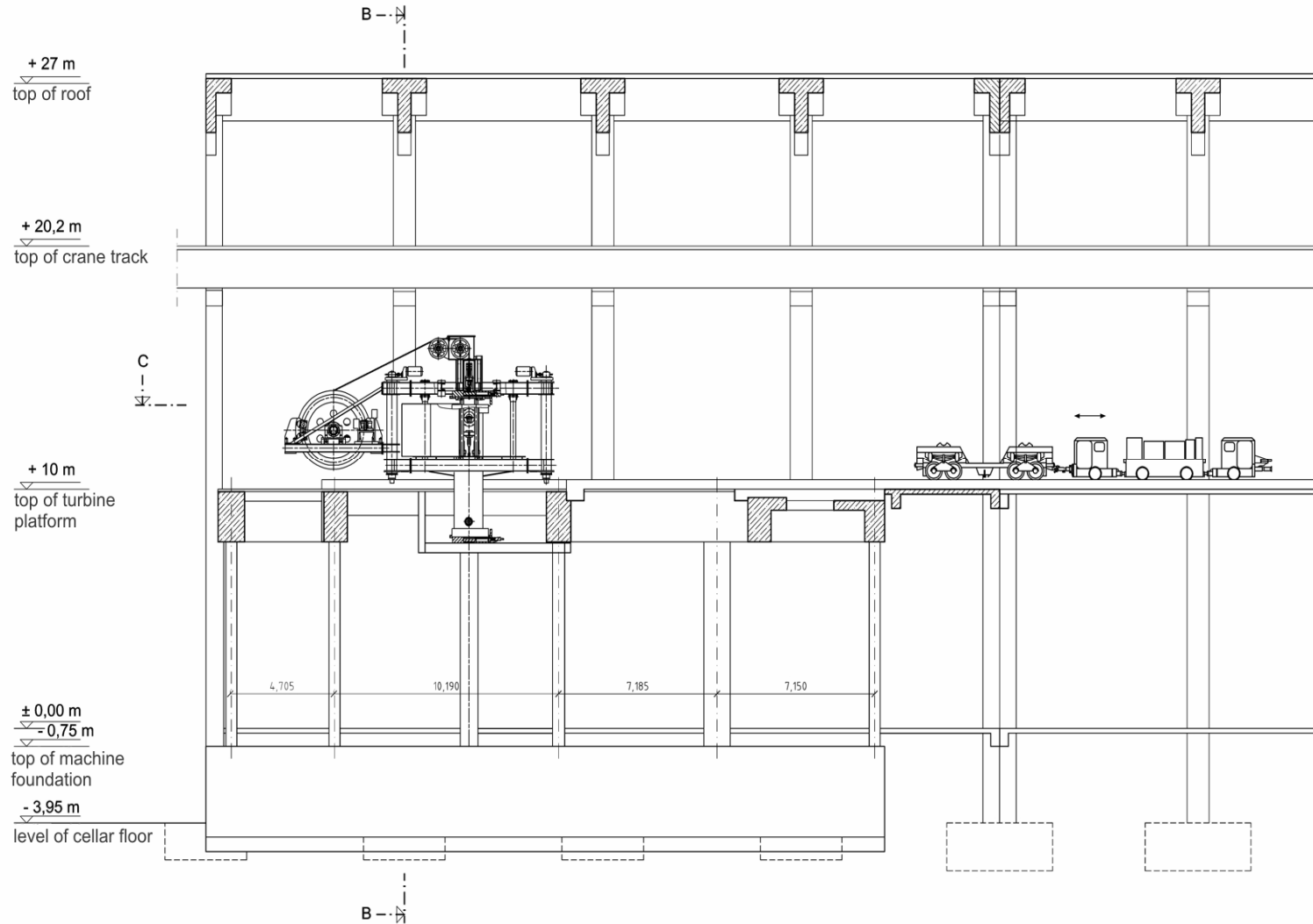


Emplacement device heights during operation III

Emplacement Drift Cross Section



BSK 3 Test Stand in E-ON Power Plant



Next steps

- Manufacturing of components and construction
- Preparation of the test stand (2007)
- Performance of demonstration tests (all 2008):
 - Test site acceptance tests
 - Demonstration of proper emplacement process (reliability and maintenance requirements)
 - Simulation tests (prove design)
 - Tests to solve potential operational malfunctions
- Evaluation of test results and final report (end 2008)

Summary

- Direct disposal of spent fuel elements in horizontal drifts of a repository in salt successfully demonstrated in the 90ies by means of full-scale demonstration tests:
 - Shaft hoisting system
 - Emplacement technology for POLLUX casks
 - Impact of heat on host rock and backfill
- Direct disposal of spent fuel elements in vertical boreholes of a repository in salt is progressing:
 - Emplacement system designed
 - Components to be manufactured 2007
 - Demonstration program in 2008

== Conclusions ==

Benefit of full-scale demonstration:

- Fulfilment of legal requirements (e.g. full-scale testing prior to repository implementation)
- Validation of the functionality and reliability of developed technical repository components (e.g. emplacement machine)
- Validation of predicted thermo mechanical backfill and host rock behaviour by comparison with in-situ measurement results
- Increase public acceptance by means of demonstration of safe and reliable waste transport and emplacement prior to implementation

Thank you for your attention!

Chinese-German Workshop on Radioactive Waste disposal

May 28-31 ,2007, Beijing

Characteristics of GMZ Bentonite as potential buffer/backfill material for China's HLW repository

Zhijian WEN

**Beijing Research Institute of Uranium Geology
China National Nuclear Corporation**



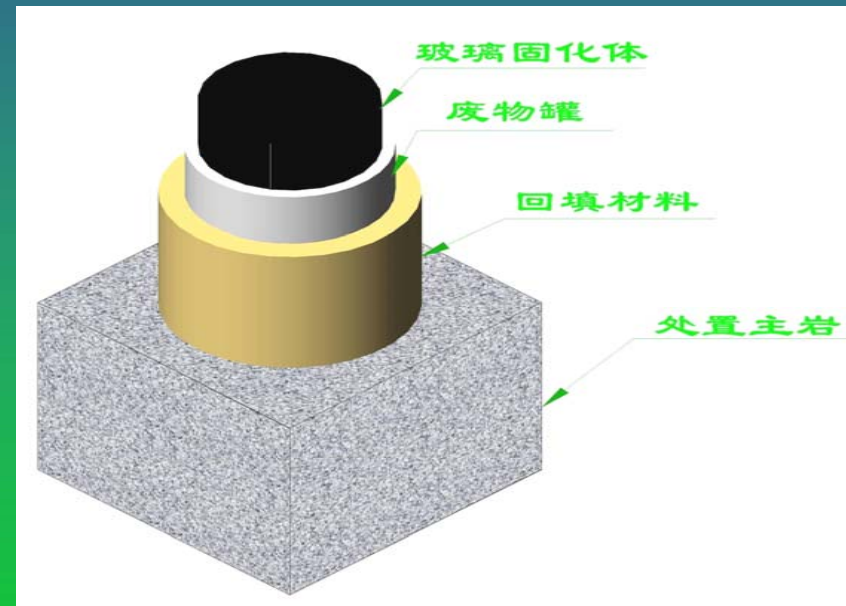
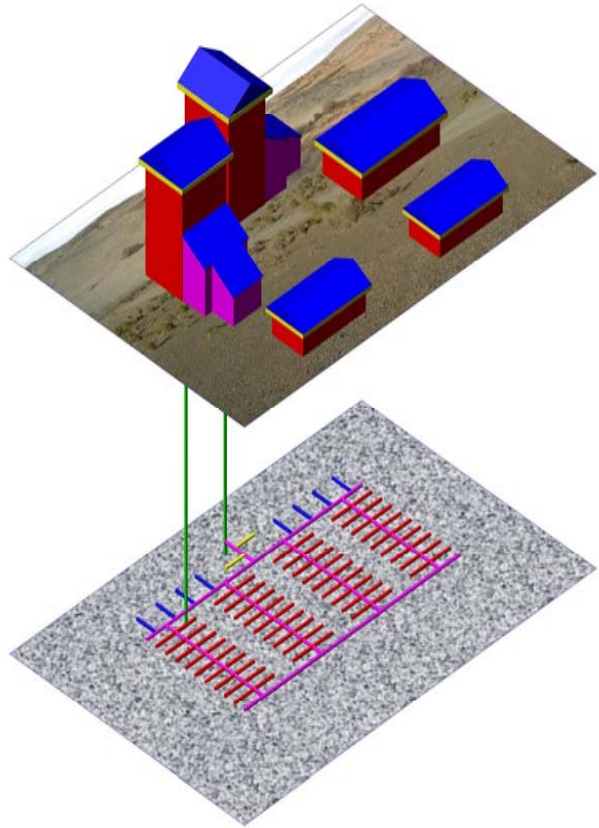
Outline

- 1. Introduction**
- 2. Geological features**
- 3. GMZ Basic property**
- 4. Remarks**

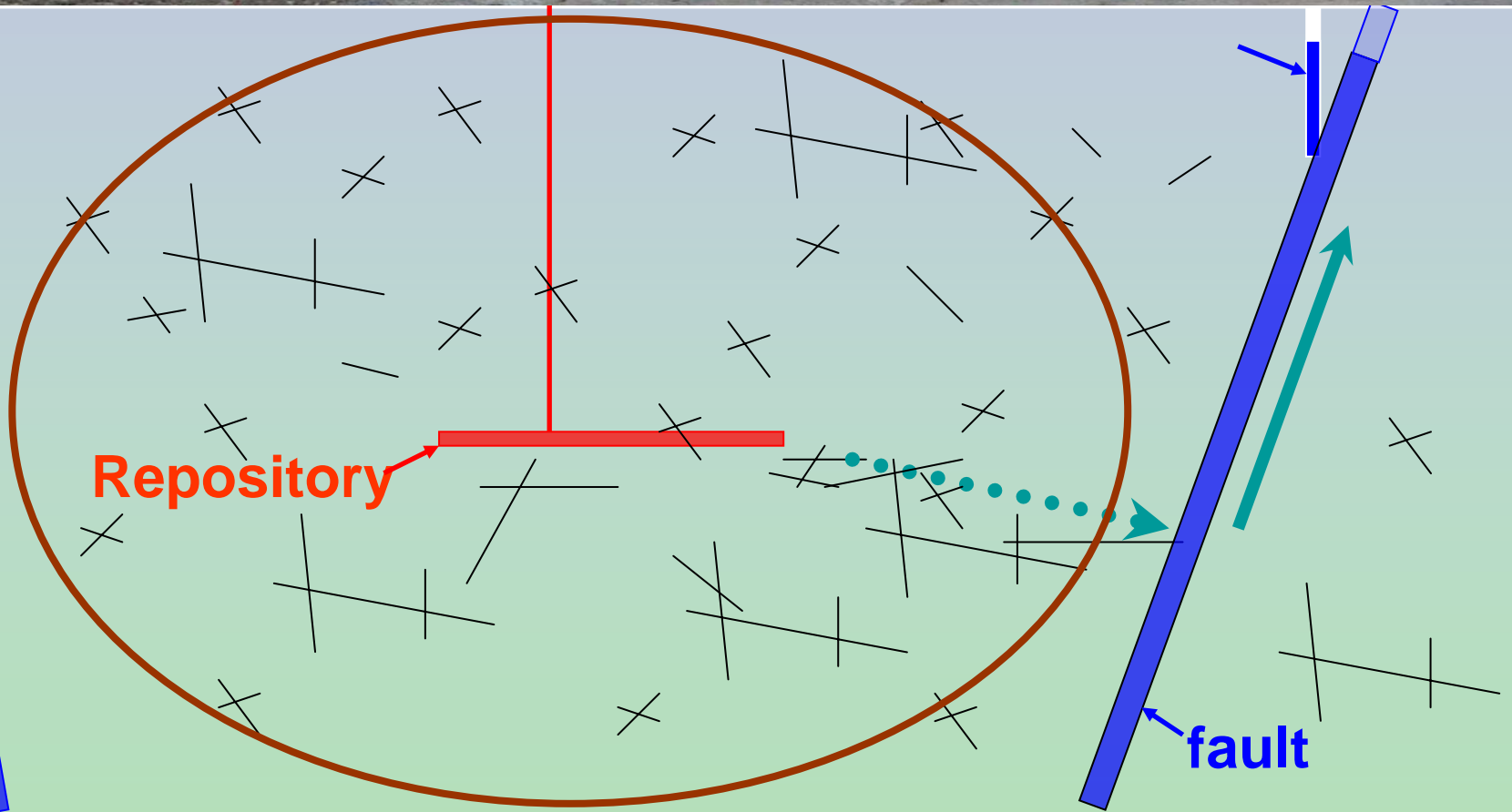
1、 Introduction

- The deep geological disposal is regarded as the most reasonable and effective way to safely dispose high-level radioactive wastes (HLW) in the world.
- The repository is based on a multi-barrier system that combines an isolating geological environment with an engineered barrier system (Inc. vitrified HLW, canister, overpack and buffer/backfill material).

Preliminary Conceptual model



Preliminary Concept model



1、 Introduction

- Due to the very low permeability and excellent retardation of nuclides from migration etc., the bentonite is selected as base material of the buffer/backfill material in HLW repository.
- GMZ deposit is selected as the candidate supplier for buffer material of HLW repository in China.
- Since 2000, systemic study was conducted on GMZ-1 that is Na-bentonite produced from GMZ deposit and selected as reference material for Chinese buffer material study.

History of buffer material study

- 1986-1990 start of R&D program
literature investigation and IAEA CRP “inorganic adsorbent as buffer material for HLW repository”
- 1990-1994 Preliminary study of bentonite
- 1994-1996 bentonite deposit screening in China
GMZ deposit as candidate supplier
- 1996-2000 Study on GMZ Ca-bentonite
Basic property, hydraulic, swelling, mechanical, chemical, compaction, nuclide
- 2001- Systemic study on GMZ Na-bentonite

Bentonite deposits in China

86 bentonite deposits (L12/M31/S43) 60%

- large-scale (proved reserves > 50 million tons)
- middle-scale (5 million tons ~ 50 million tons)
- small scale deposits (proved reserves < 5 million tons)

Main bentonite deposits in China (Xu et al, 1996)



Deposit screening

➤ **Scale**

➤ **Quality**

➤ **Economic limitation**

➤ **Location**

The candidate bentonite deposit should be large-scale deposit in order to meet the demand for the installation of HLW repository 30 or 40 years later.

2、 Geological features



The GMZ deposit is located in the northern Chinese Inner Mongolia autonomous region, 300 km northwest of Beijing .

The GMZ bentonite deposit is a large-scale deposit. In China, the proved reserves of GMZ deposit ranks the third of its kind and the reserves of sodium bentonite ranks the second.

GMZ deposit

The reserves in GMZ is about 160 million tons with 120 million tons Na-bentonite reserves.



Outcrop of GMZ bentonite

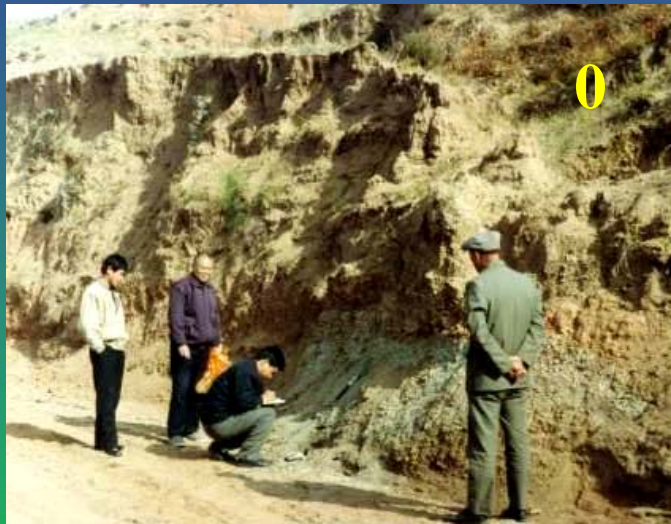


Generic characteristics

The GMZ bentonite deposit is formed in upper Jurassic period. Bentonite is bedded, with a soapy texture and waxy appearance. It ranges in colour from white to yellow to olive green to brown to pink. The mineralization is a process of firstly continental volcanic sediment and then suffering from interaction with ground water and weathering.

Ore bodies

The deposit is composed of 5 ore bed, numbered by 0, I, II, III, IV.. The third ore bed is the most important part that is the main industrial ore bed. All the ores are occurred bedded appearance. The third ore bed extends about 8,150m with thickness from 8.78m~20.47m.





Borehole drilling

Minerals

➤ Ore mineralogy:

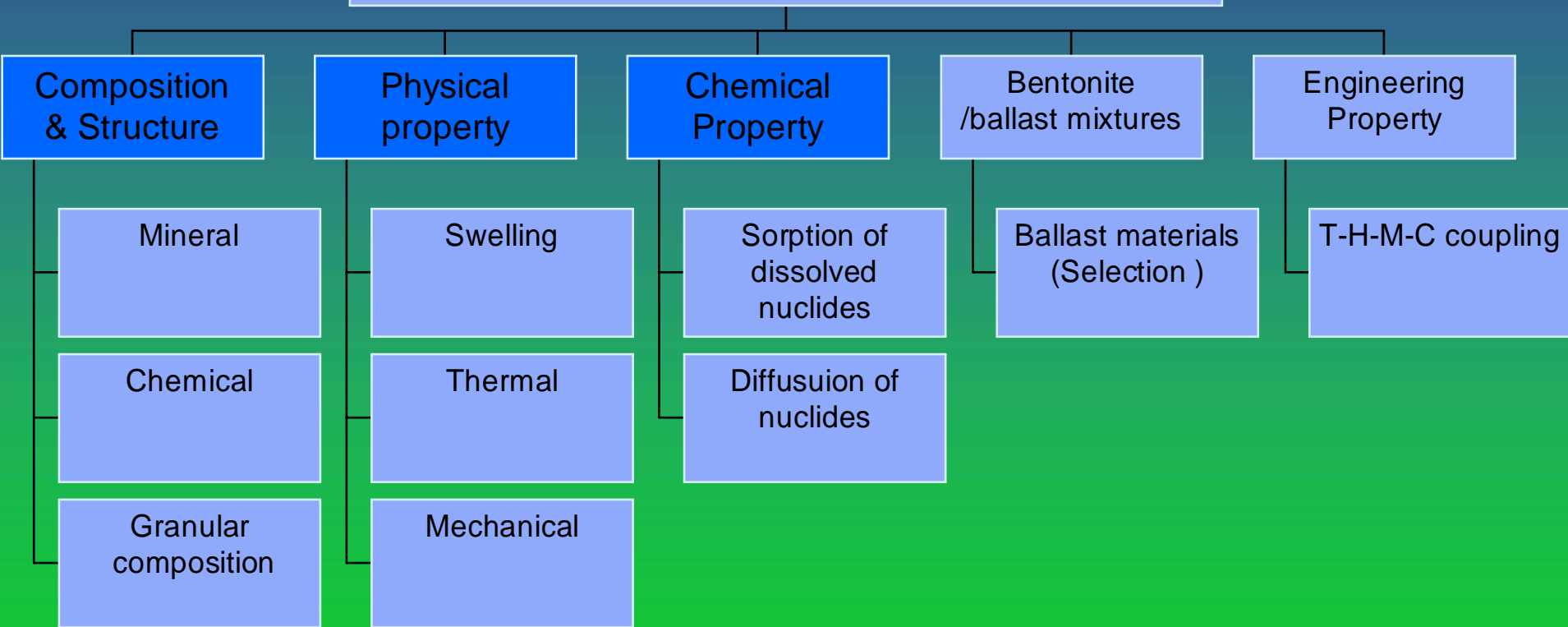
Montmorillonite, sometimes coexist with illite.

➤ Gangue mineralogy:

feldspar, quartz, calcite, zeolites, cristobalite,
unaltered volcanic glass.

At present, the bentonite is mined on a small scale only. Mining is done on a seasonal basis and by primitive manual methods. .

Chinese Buffer study



3 Basic property

- Mineral composition
- Physical property
- Chemical property

Research work completed on GMZ Ca-bentonite

- Composition, Chemical component
- Physical property (swelling, hydraulic, mechanic & thermal property)
- Additive selection
- Nuclides migration

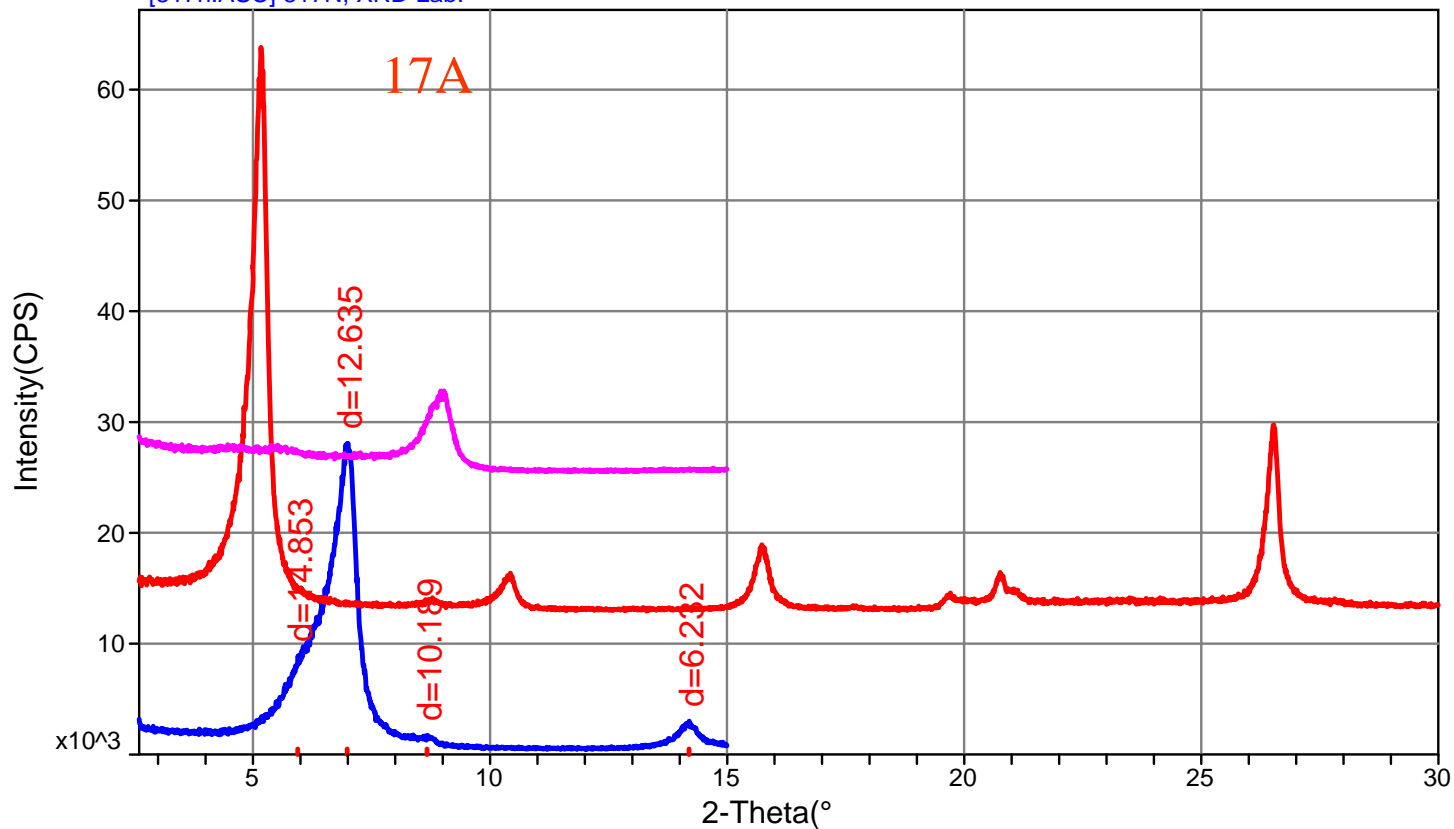
Na-bentonite

X-ray Diffraction pattern

[817t.ASC] 817T, XRD Lab.

[817e.ASC] 817E, XRD Lab.

[817n.ASC] 817N, XRD Lab.

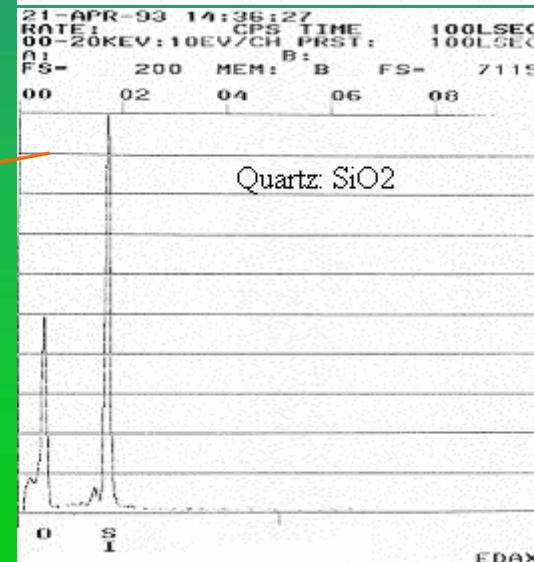
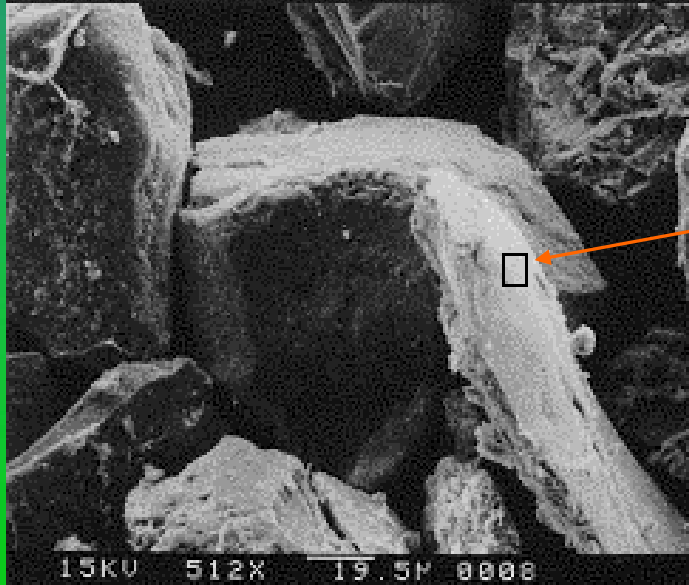
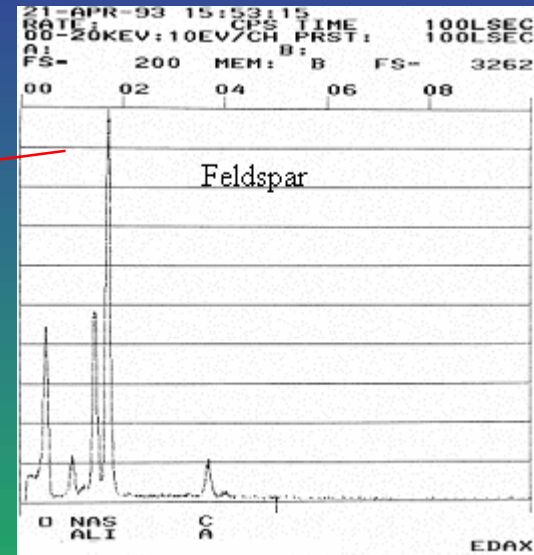
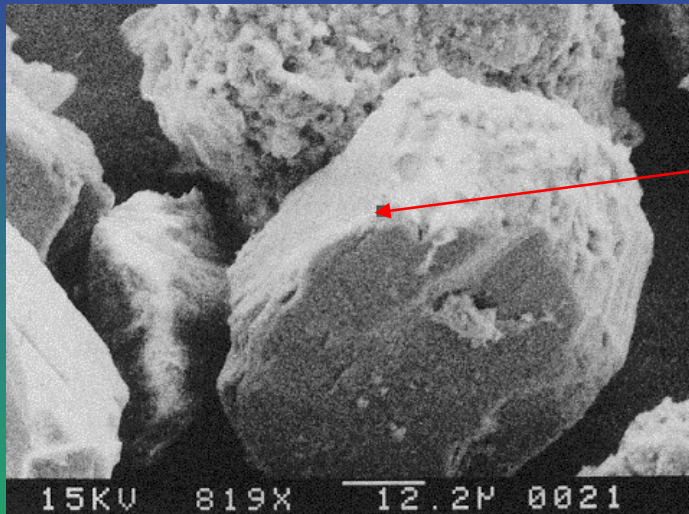


3.1 Mineral composition

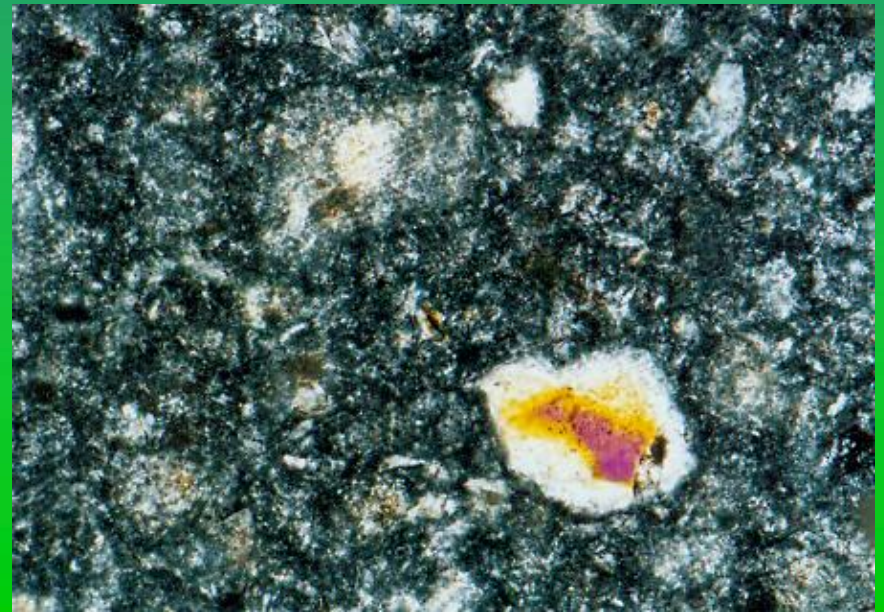
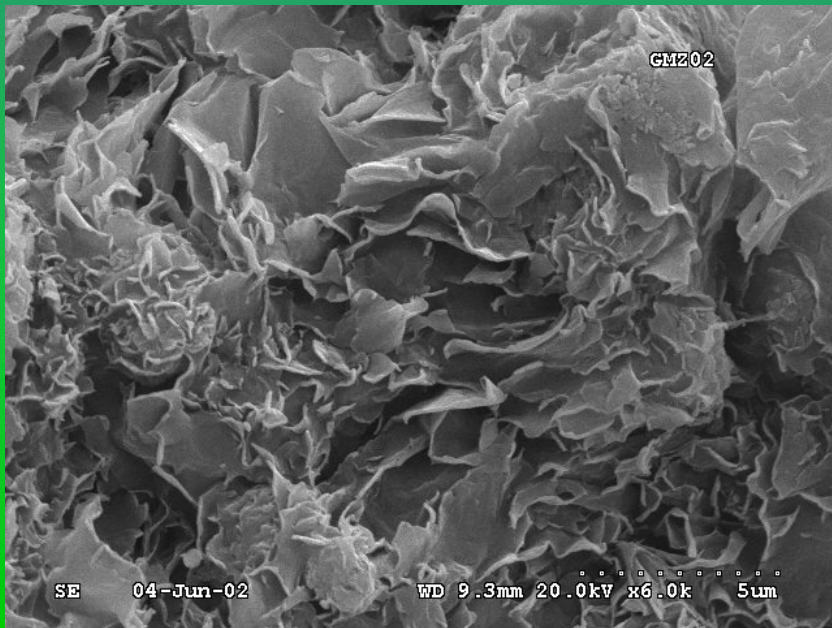
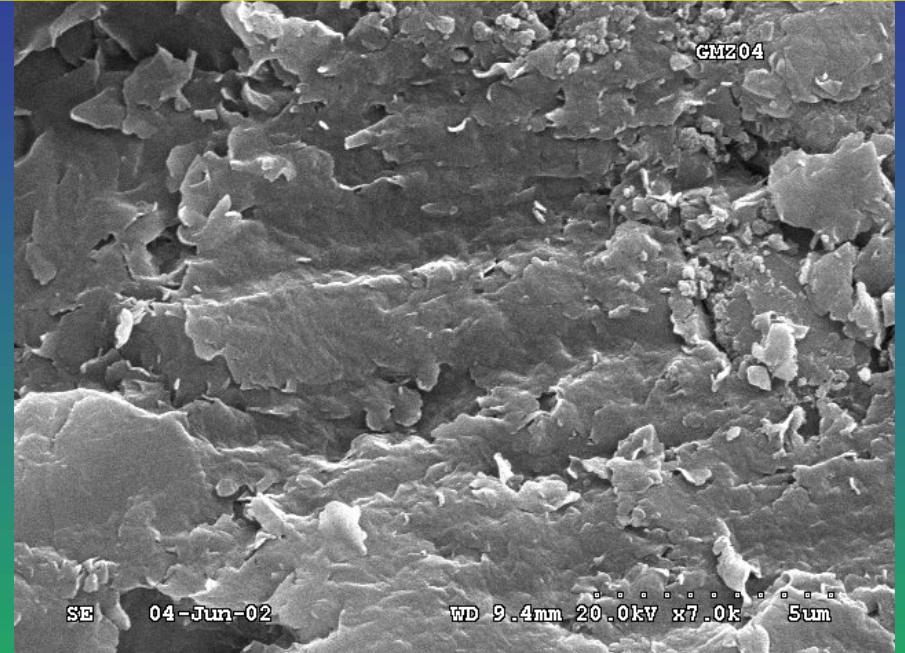
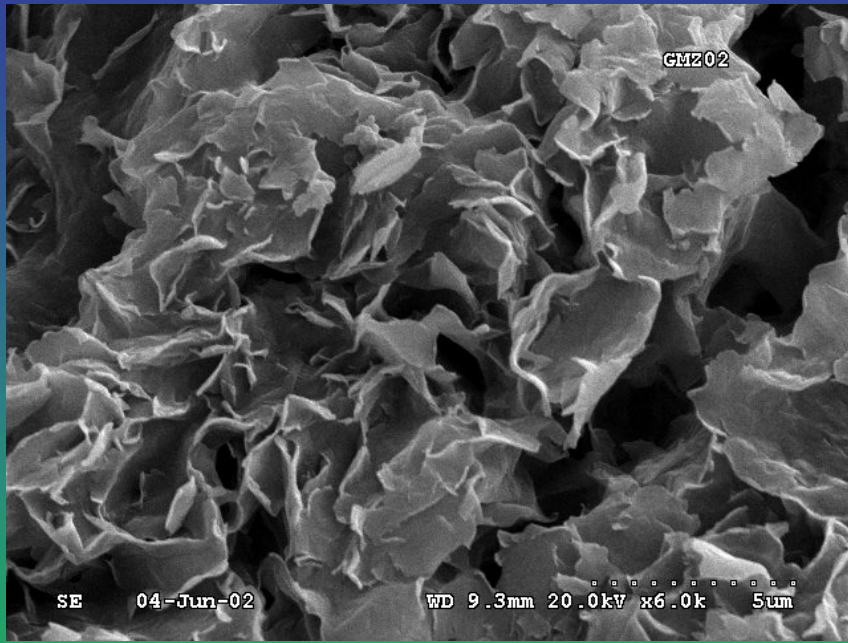
Quartz	Feldspar	Cristobalite	Montmorillonite	Illite	Kaolinite	Carbonate
11.7	4.3	7.3	75.4	/	0.8	0.5 (Calcite)

Content of (%) [*]	Methylene Blue exchange Capacity (MBC)	Cation Exchange Capacity CEC	Real density	Alkali Index
75.4	102 mmol/100g	77.06 mmol/100g	2.66g/cm ³	1.14
Type	Exchangeable cation (mmol/100g)			
Sodium bentonite				
pH	E(k ⁺)	E(Na ⁺)	E(1/2Ca ²⁺)	E (1/2Mg ²⁺)
8.68-9.86	0.55	37.52	23.18	10.17

SEM-XPS measurement



SEM Image



3.2 Physical property

- **Thermal $\phi 50\text{mm} \times h 10\text{mm}$**

Thermal conductivity as function of dry density (1.4, 1.6, 1.8Mg/m³) and water content (9%, 14%, 18%, 24%, 36%) was measured

- **Hydraulic $\phi 50\text{mm} \times h 10\text{mm}$**

Density (1.4, 1.6, 1.8kg/m³)

temperature: 25° C → 60° C → 90° C

Compressed air of 0.3 MPa(1.4kg/m³) /0.6MPa(1.6, 1.8kg/m³)

- **Mechanical $\phi 30\text{mm} \times h 60\text{mm}$**

Mechanical conductivity as function of dry density (1.4, 1.6, 1.8kg/m³) and water content (9%, 14%, 18%, 24%) was measured

- **Swelling $\phi 20\text{mm} \times h 20\text{mm}$**

Swelling stress as function of dry density (1.2, 1.4, 1.6, 1.8kg/m³)

Swelling amount

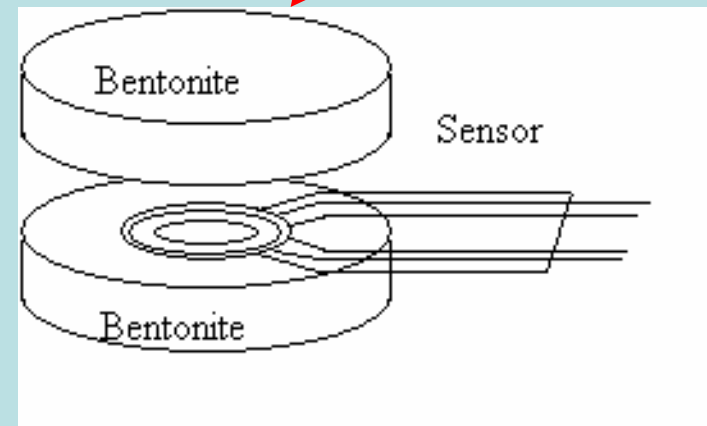
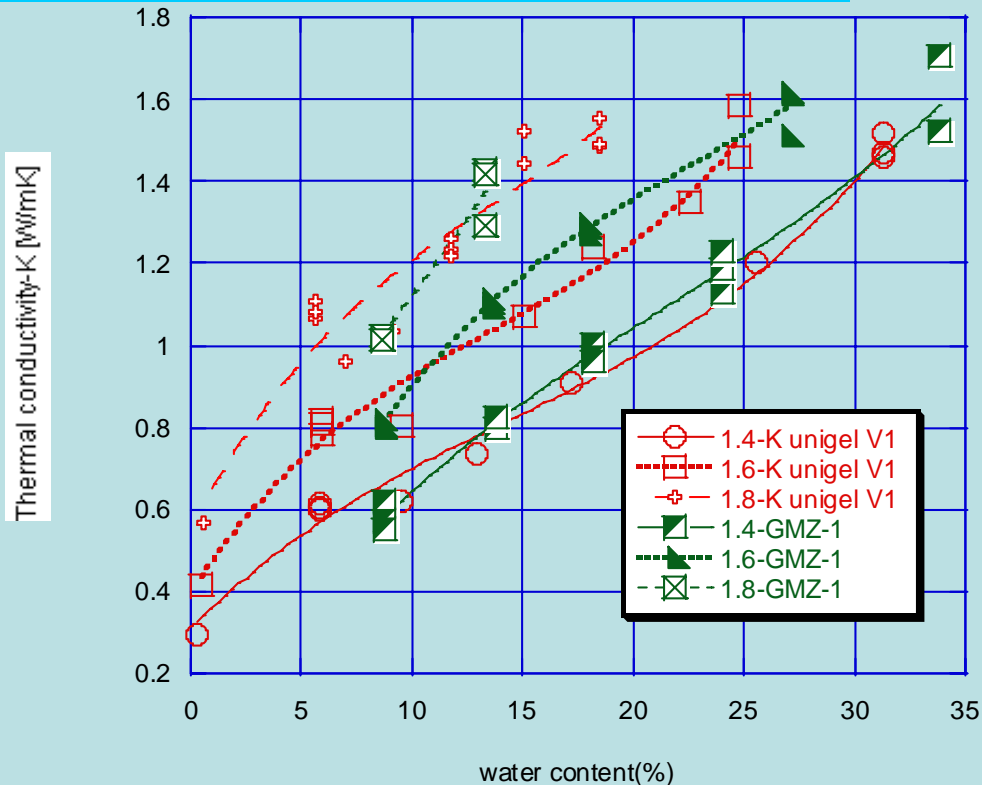
Thermal property

Instrument: Thermophysical Properties Analyzer (TPA 501): surface heat source method

Size: $\phi 50\text{mm} \times h 10\text{mm}$

Dry density : 1.4, 1.6, 1.8 Mg/m^3

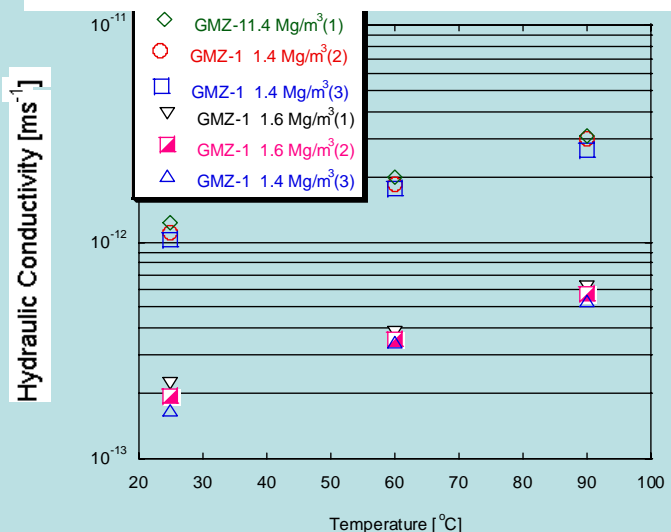
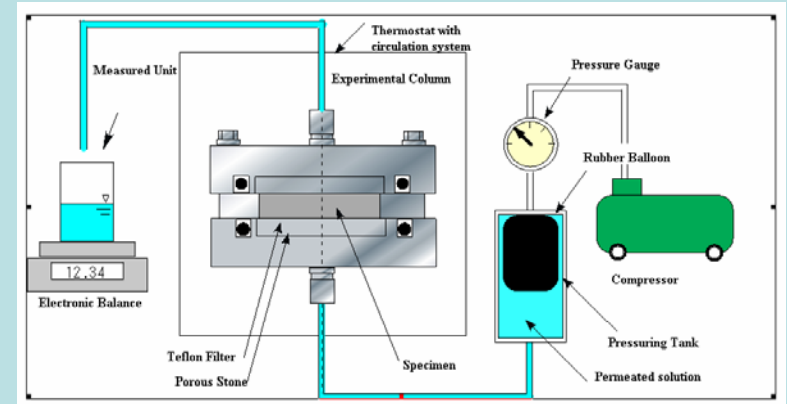
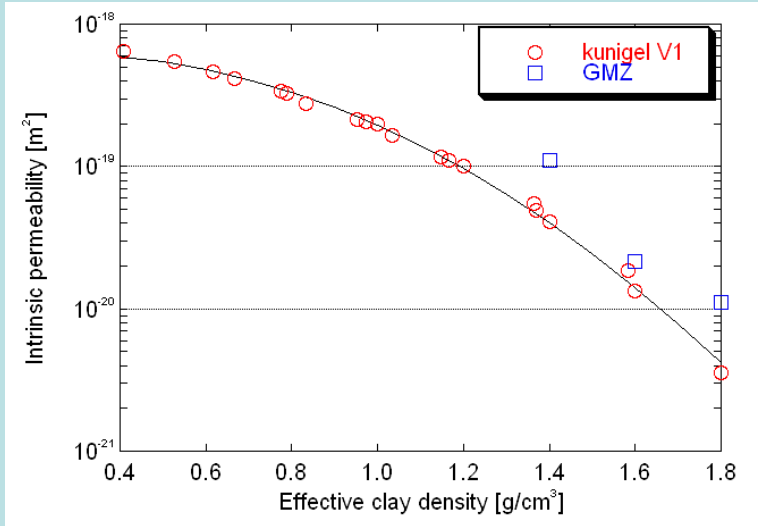
water content : 9%, 14%, 18%, 24%, 36%



Thermal conductivity: increases with water content & dry density

Hydraulic property

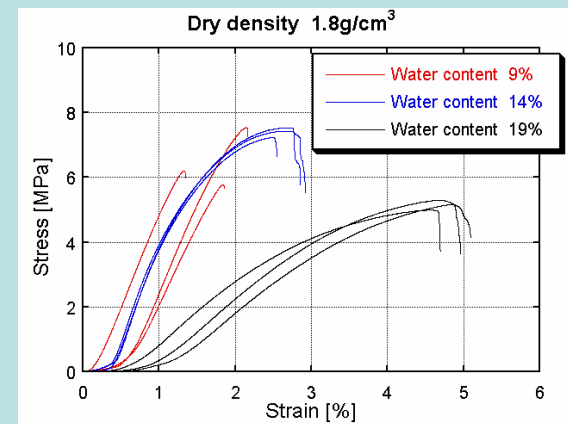
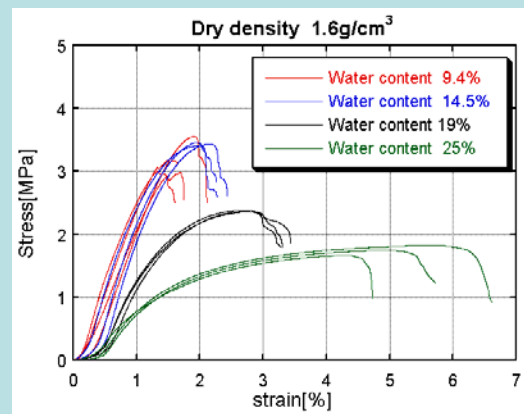
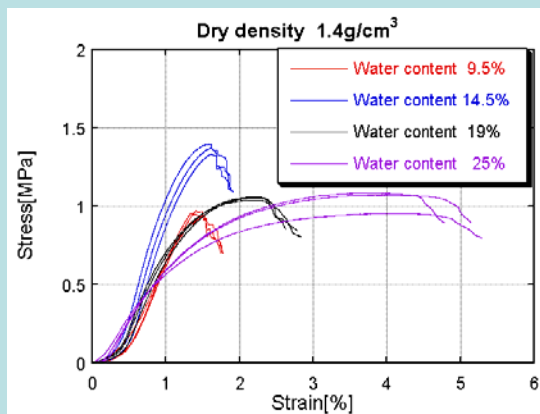
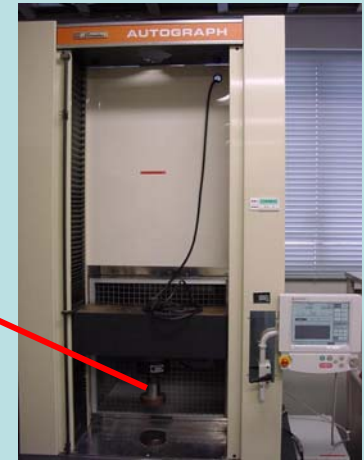
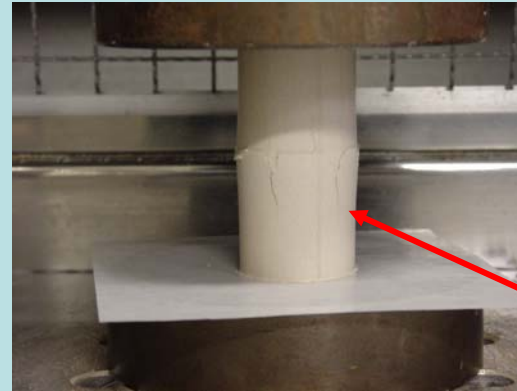
$\phi 50\text{mm} \times h 10\text{mm}$ 1.4, 1.6, 1.8 Mg/m^3 25° C \rightarrow 60° C \rightarrow 90° C
 Compressed air: 0.3 MPa(1.4 Mg/m^3) / 0.6 MPa(1.6, 1.8 Mg/m^3)



Saturated hydraulic conductivity increases as temperature increases and decrease as the effective density increases

Mechanical characteristics

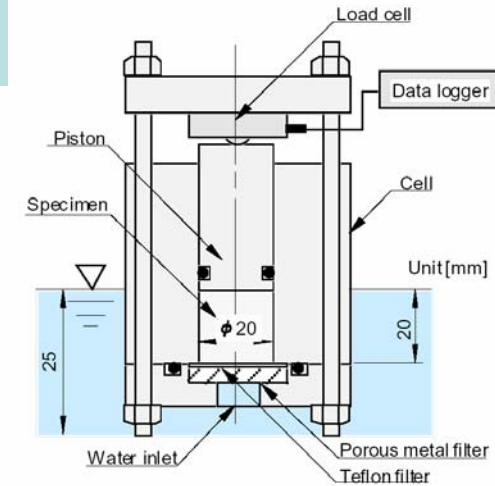
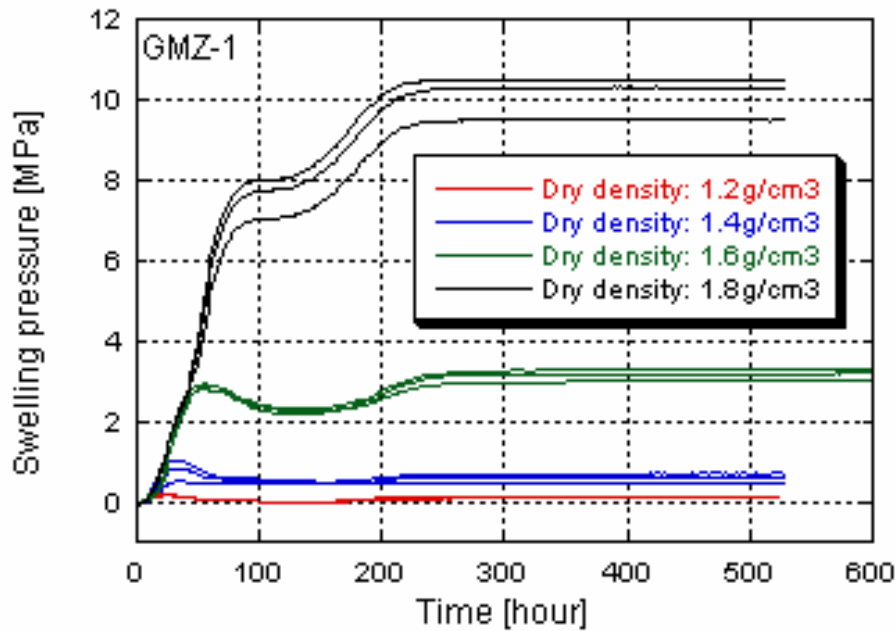
$\phi 30\text{mm} \times h 60\text{mm}$
1.4, 1.6, 1.8 Mg/m^3
9%, 14%, 18%, 24%
Strain rate: $1\% \text{ min}^{-1}$
JGS T511



In general, with the same water content, a larger initial dry density leads to a larger unconfined compressive strength, and with the same dry density, a larger water content leads to a less unconfined compressive strength.

Swelling property

$\phi 20\text{mm} \times h 20\text{mm}$
1.2, 1.4, 1.6, 1.8 Mg/m^3



A key property of the buffer material is its ability to swell by water uptake, thereby filling voids in the engineered barriers and fractures in the surrounding host rock.

Swelling stress increases as dry density increases.

Bentonite (powder) swelling amount



Sample	Kunipia F	GMZ-1	Kunigel V1
Time [hr]	24		
Water	Distilled water		
Swelling amount	68.0	18.0	18.0

3.3 Chemical property

- Batch test

Sample: 100% Chinese GMZ-1

S/L: 10, 100, 200[g/L] Atmosphere

room temperature

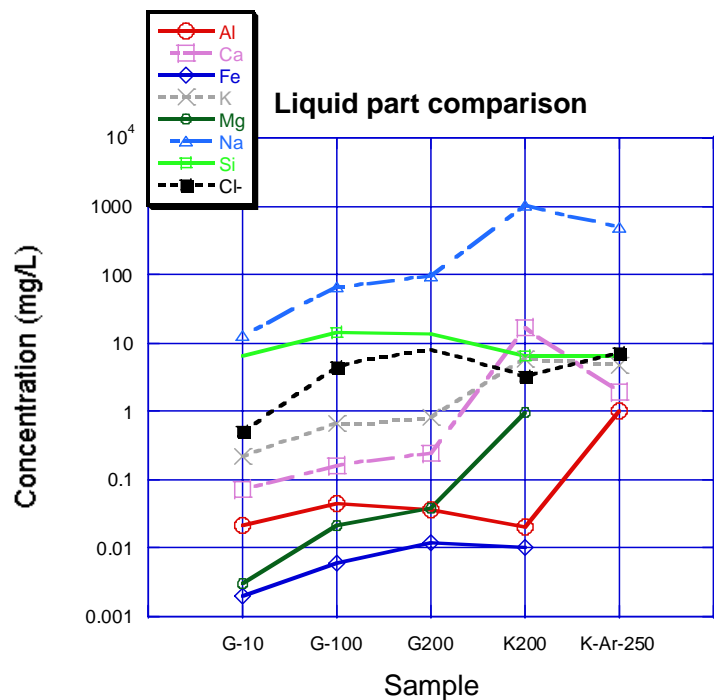
Solution: Distilled water

Time: 14 days

Parallel experiment: 3

- Modeling of bentonite-water interaction

Chemical property



4. Remarks

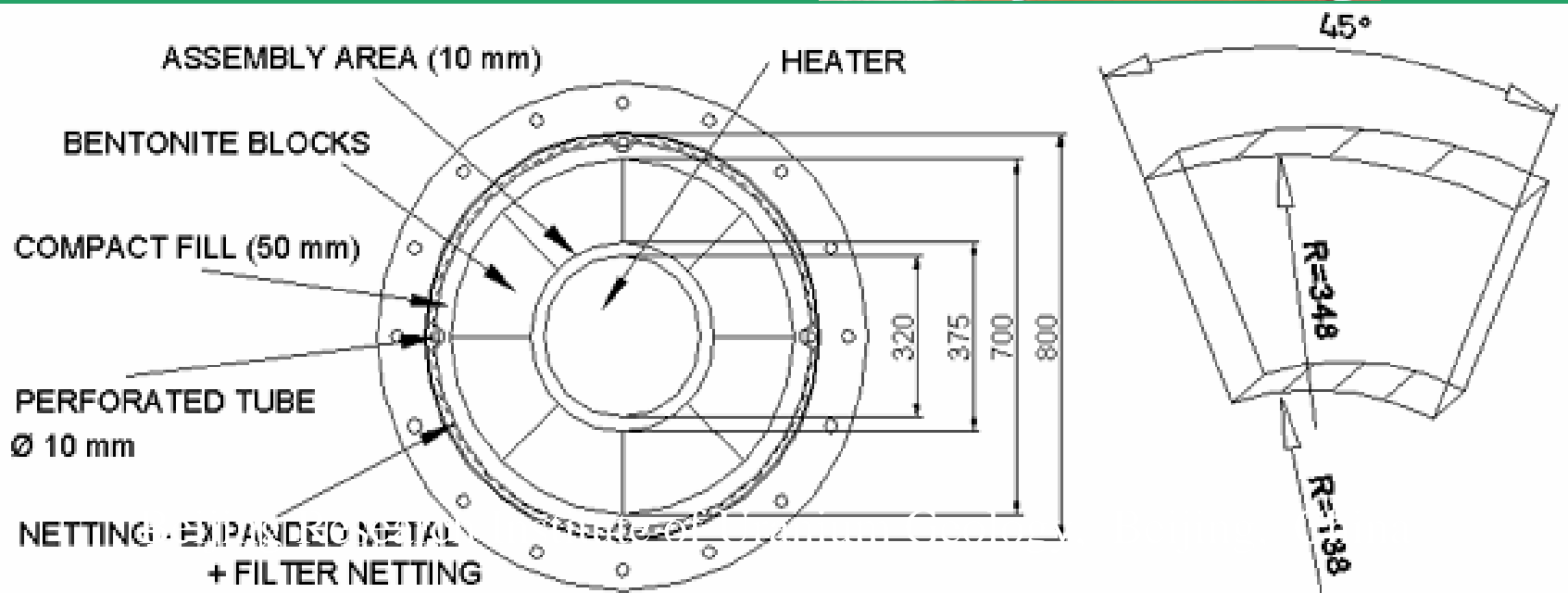
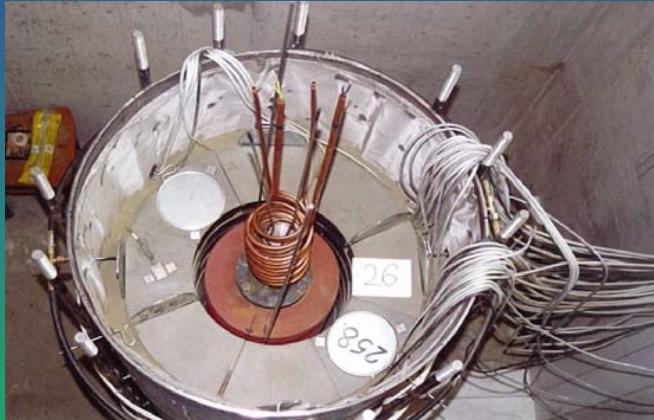
GMZ-1 bentonite is characterized by high content of montmorillonite (about 75%) and less impurities. GMZ-1 is a pure natural material, it comes to be one of the best buffer material with high quality in the world.

Component	MX80 瑞典	S-2 西班牙	Montigel 瑞士	Avonseal 加拿大	Kunigel V1 日本	GMZ 中国
Montmorillonite	75%	84	66	79	46-55	72.5
quartz	15.2	3.6	8.3	5	29-38	19.0
feldspar	5-8	6.1	2-4	3	2.7-5.5	4.3
remark	Na-	Ca-	Ca-	Na-	Na-	Na-

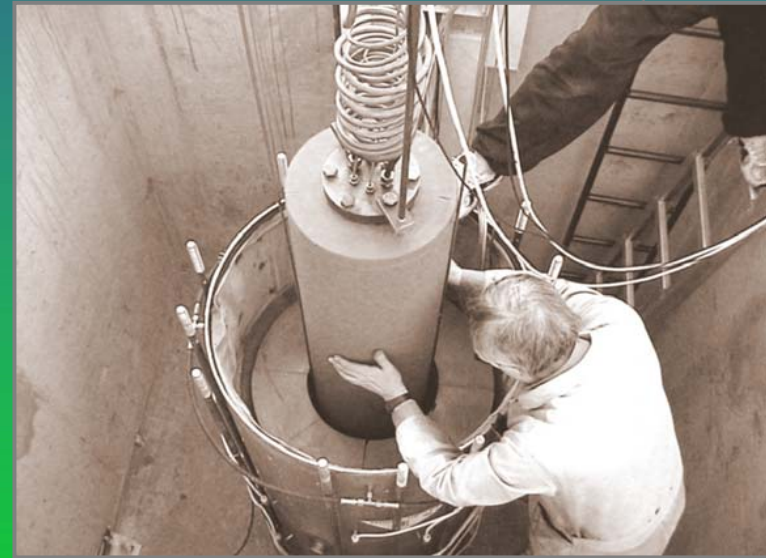
The key point for the further study

- Mock-up
- Porewater Chemistry
- Instrumentation
- T-H-M coupling study
- **Open for international cooperation**

Mock-Up



T-H-M-C coupling study



Beijing Research Institute of Uranium Geology, Beijing, China

THANKS!

Some Basic Properties of Densely Compacted GMZ Bentonite

Prof W. M. YE



百年同濟

TONGJI UNIVERSITY

TONGJI UNIVERSITY



Grand Ceremony of the Centennial Ceremony



百年同濟

TONGJI UNIVERSITY



百年同濟
TONGJI UNIVERSITY

热烈欢迎德国联邦总统霍斯特·克勒访问同济大学

**Wir heißen Bundespräsident Horst Köhler
zum hundertjährigen Jubiläum der Tongji-Universität herzlich willkommen.**



时代的城市发展 TATION AND URBAN DEVELOPMENT



Contents



1 Introduction

2 Basic features of GMZ bentonite

3 Soil Water Characteristics

4 Microstructure investigation

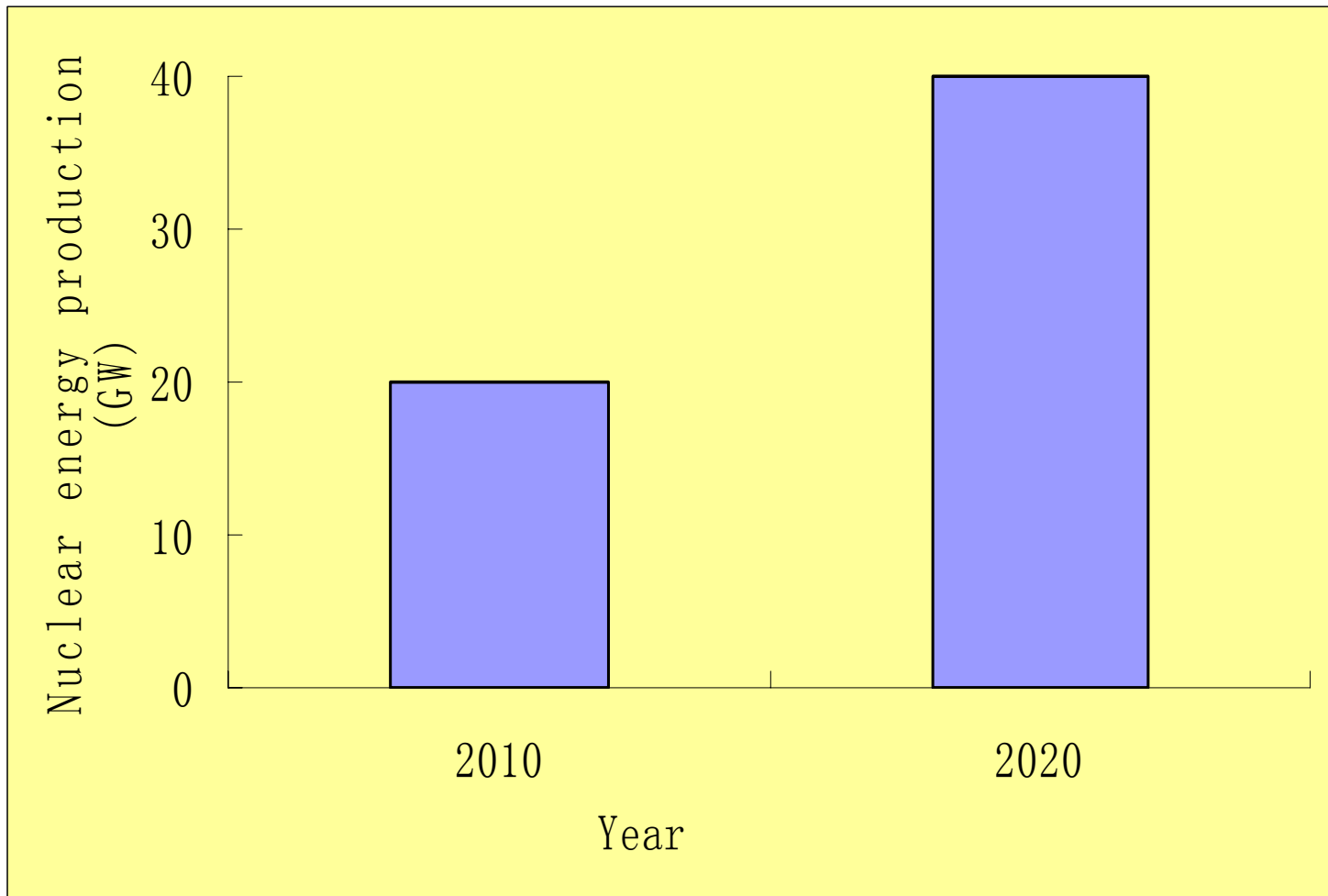
5 Swelling pressure

6 Conclusions

1 Introduction



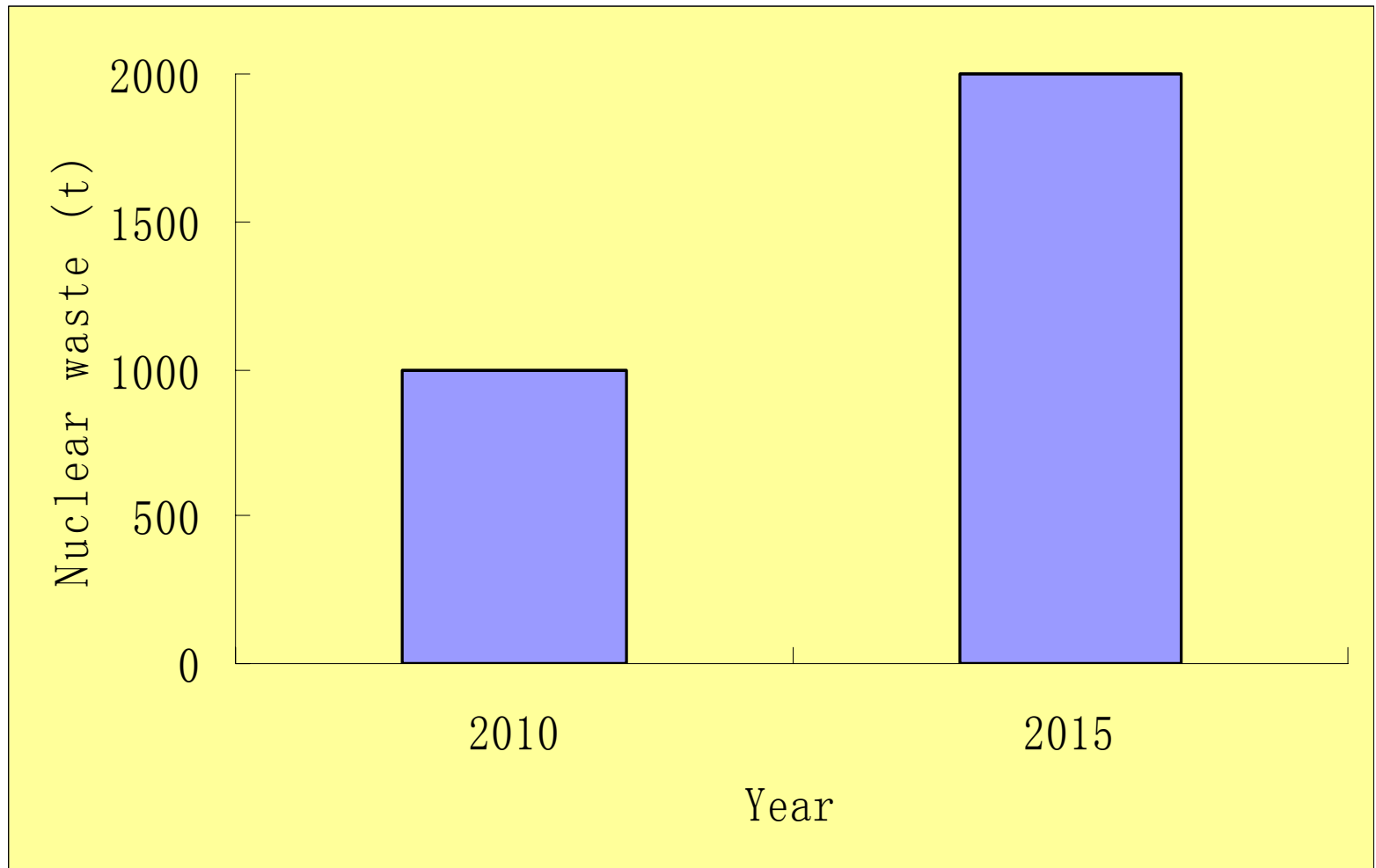
Nuclear energy production in China



1 Introduction



Nuclear waste in China



2 Basic features of GMZ

**GMZ bentonite locates in
Xinghe county, the Inner
Mongolia Autonomous
Region.**

2 Basic features of GMZ

Mineralogical composition of GMZ

Mineral	Content(%)
Quartz	11.7
Cristobalite	7.3
Feldspar	4.3
Calcite	0.5
Kaolinite	0.8
Montmorillonite	75.4

2 Basic features of GMZ

CEC and exchangeable cation of GMZ

Sample	CEC (mmol/100g)	Exchangeable cation (mmol/100g)				Alkali Index
		E(k ⁺)	E(Na ⁺)	E(Ca ²⁺)	E(Mg ²⁺)	
GMZ01	77.06	0.55	37.52	23.18	10.17	1.14

Sample	G_s	w_L (%)	w_P (%)	I_p	S (m ² /g)
GMZ01	2.71	276	37	237	570

3 Soil Water Characteristics



Preparation of specimen

Here, GMZ01 bentonite is compacted to **a cylinder**, height 6mm, diameter 20mm, and the dry density is 1.7g/cm^3 , the initial water content is 12.13%.

3 Soil Water Characteristics



A special metal mold for the test under confined conditions

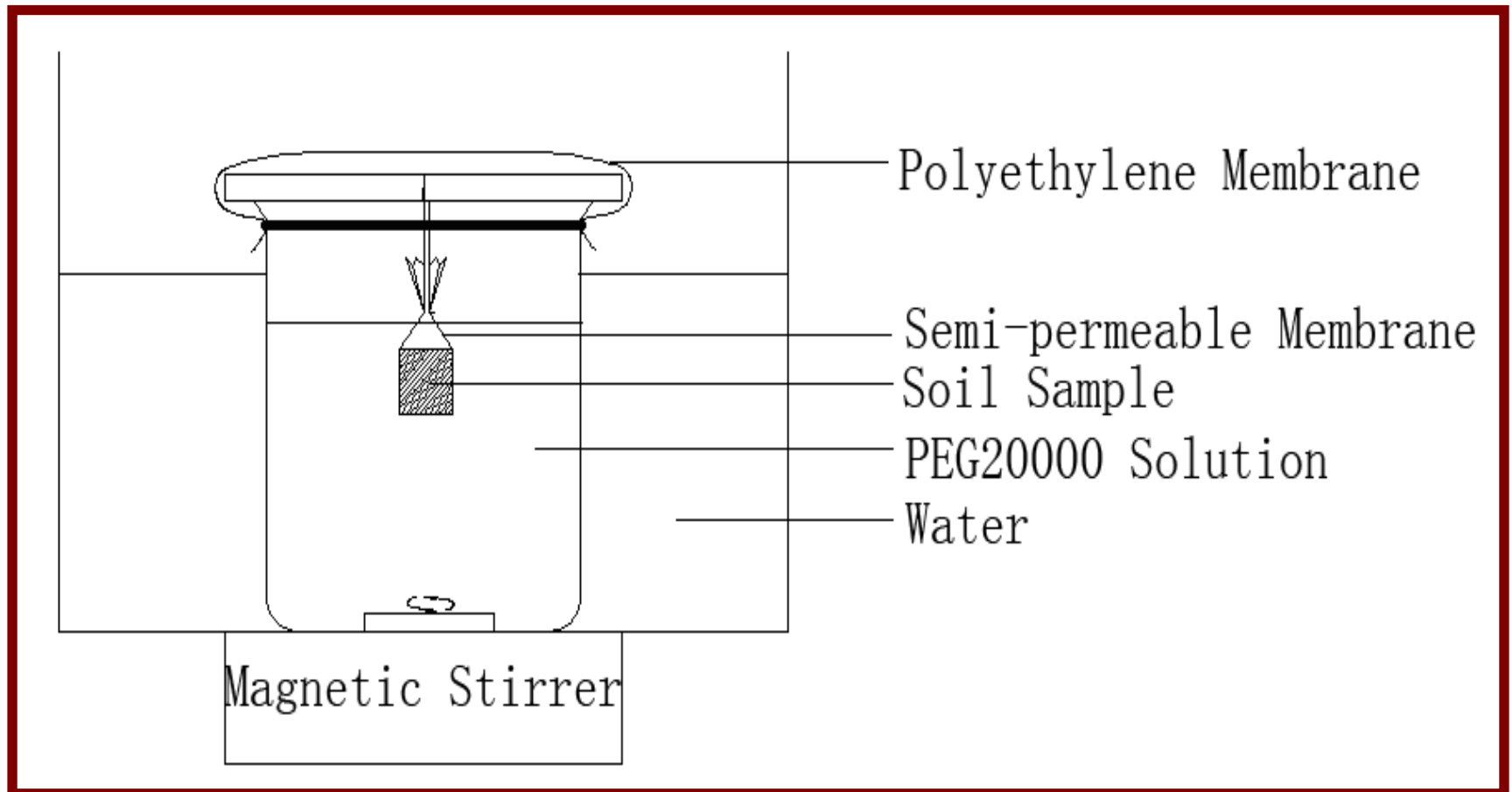
3 Soil Water Characteristics



The osmotic technique and vapour phase technique are employed for controlling suction.

3 Soil Water Characteristics

Osmotic Technique



Osmotic Technique



During the test, the soil specimen is placed in a cellulosic, semi-permeable **membrane**, which is permeable to water, and a solution of polyethylene glycol **(PEG)** is circulated outside the membrane. The large sized PEG molecules cannot penetrate the membrane.

Osmotic Technique



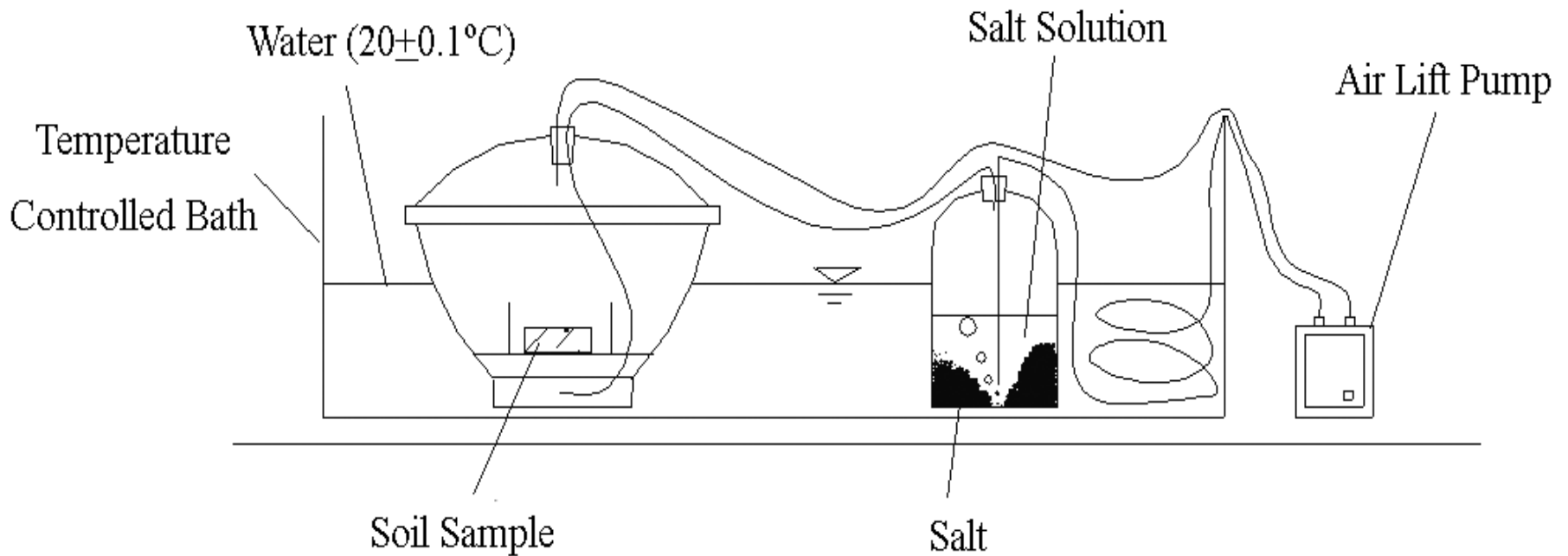
Drainage of the specimen is caused by the process of osmosis.

An osmotic suction applied to the specimen through the membrane.

The suction value depends on the concentration of the solution; the higher the concentration, the higher the suction.

3 Soil Water Characteristics

Vapor Phase Technique



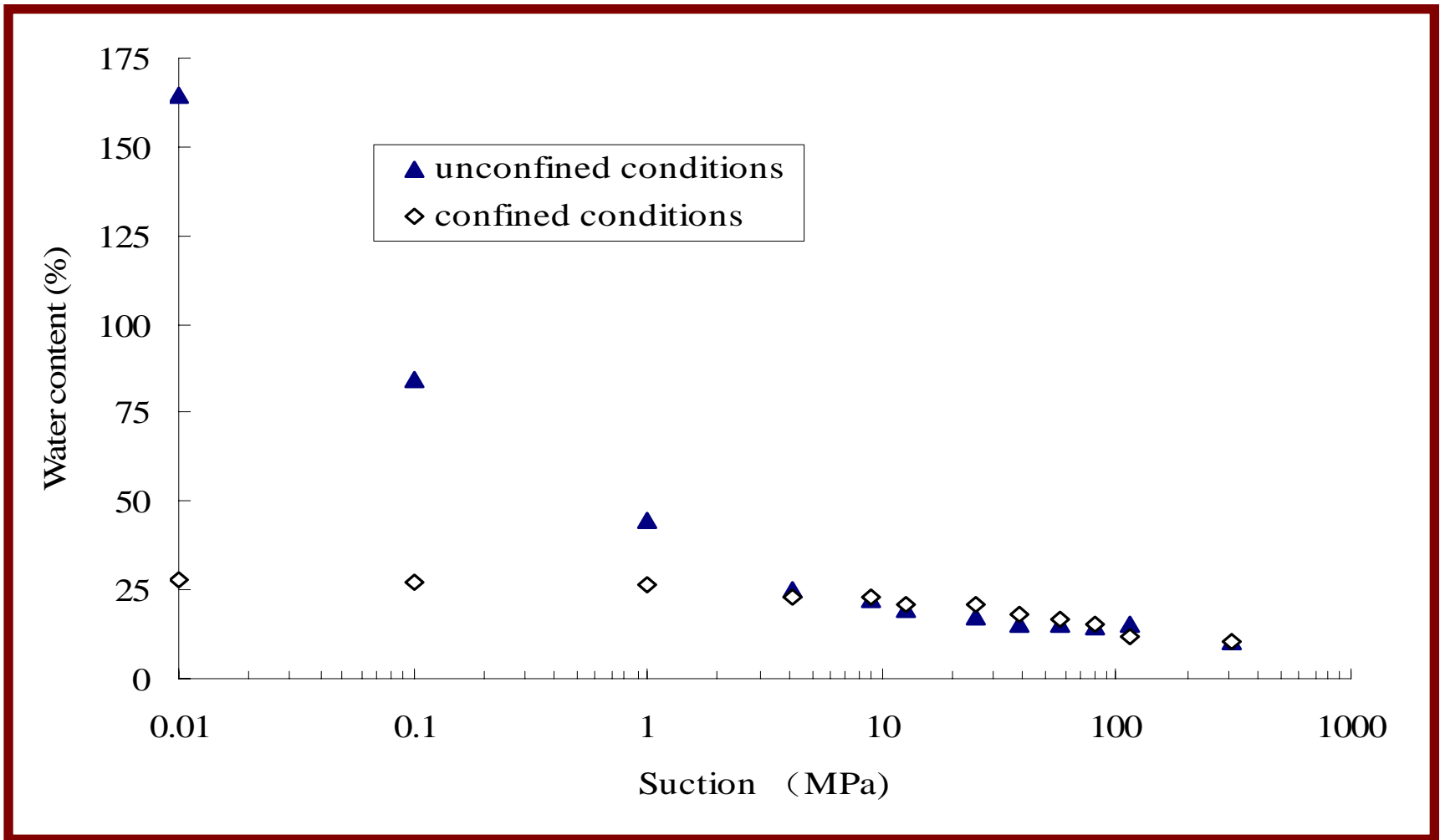
3 Soil Water Characteristics

Salts used and corresponding suctions

Salt	K_2SO_4	KNO_3	$ZnSO_4$	$(NH_4)_2SO_4$
Suction (MPa)	4.2	9	12.6	24.9
Salt	$NaCl$	$NaNO_2$	$MgNO_3$	K_2CO_3
Suction (MPa)	38	57	82	113

3 Soil Water Characteristics

Water Retention Curves

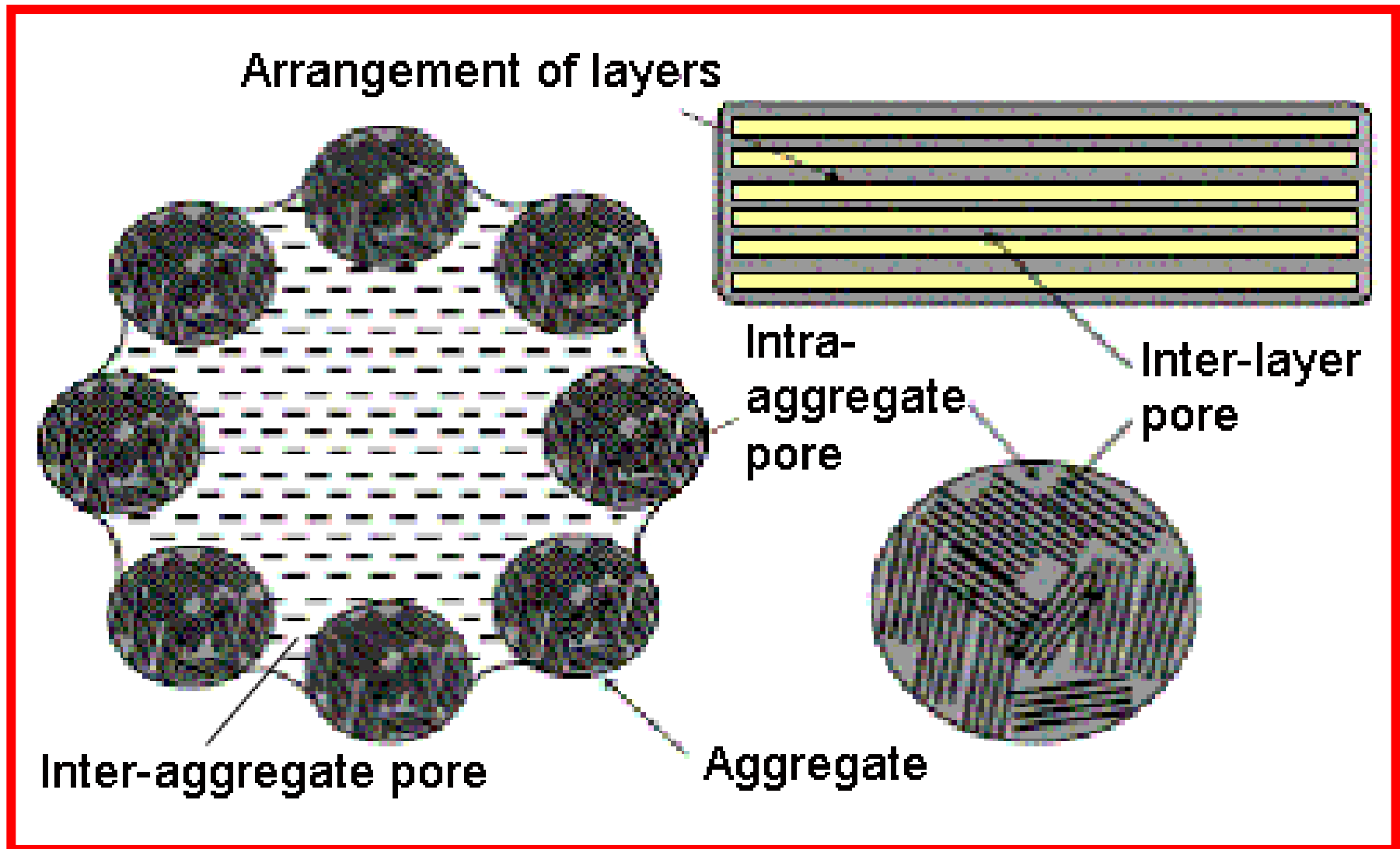


3 Soil Water Characteristics



The fig shows that, starting from the initial suction of 4.2 MPa, the difference between different confining conditions becomes less significant as the suction increases.

4 Microstructure Investigation



4 Microstructure Investigation



Techniques:

**Mercury Intrusion Porosimetry
(MIP)**

**Environmental Scanning Electron
Microscopy (ESEM)**

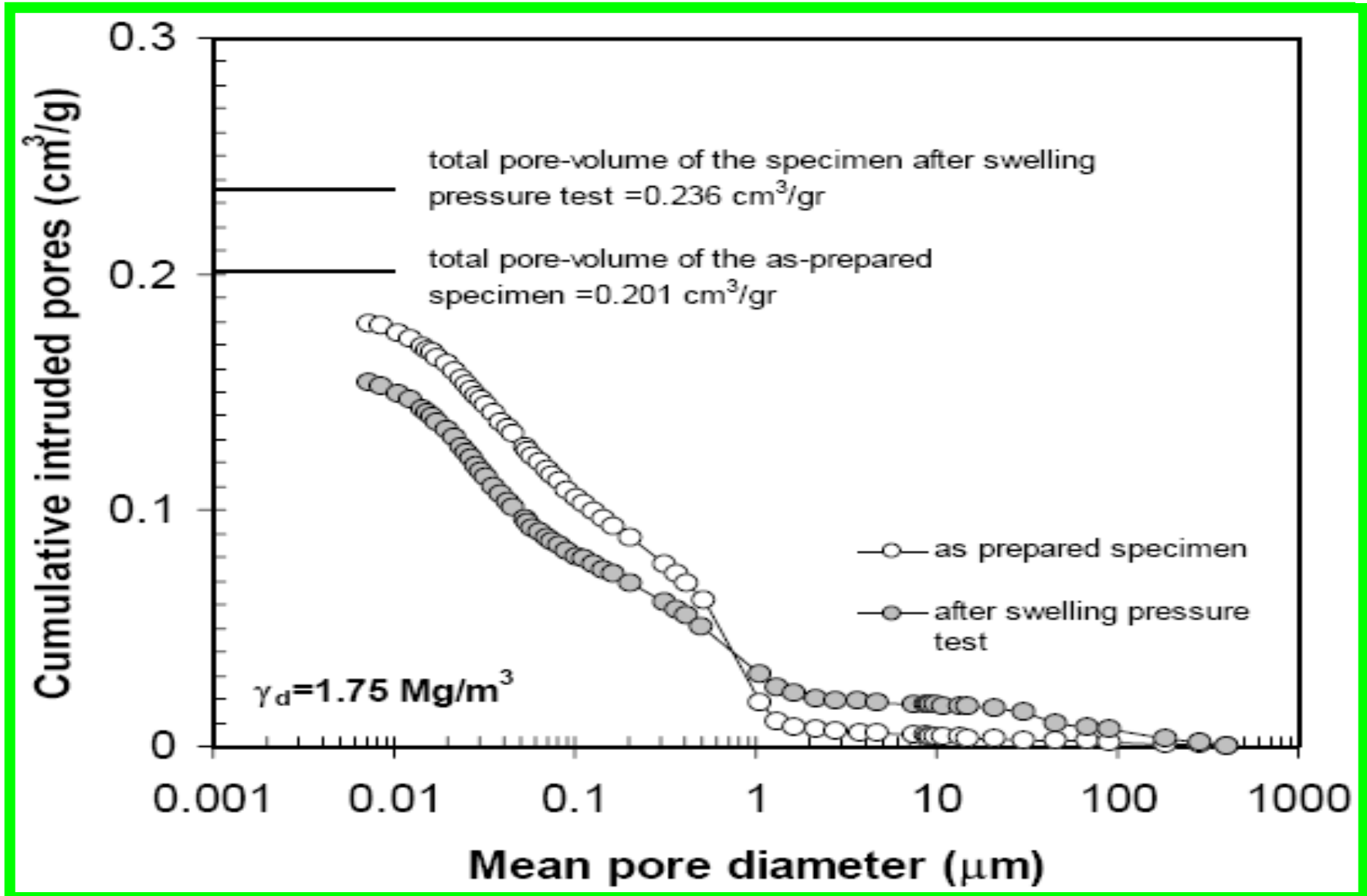
MIP Test

Initial conditions of specimens (dry density 1.75g/cm³)

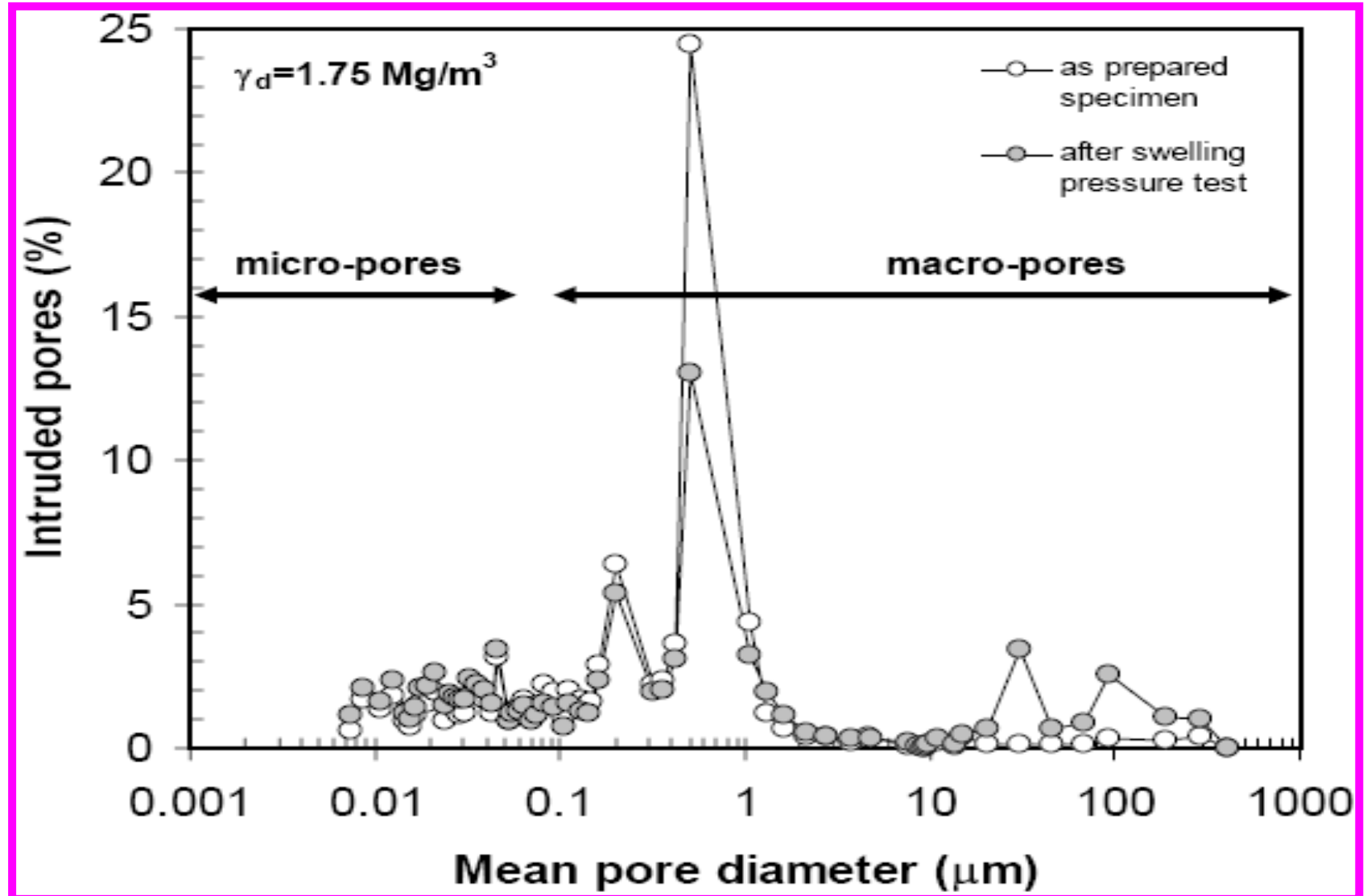
Specimen	Water content (%)	Void Ratio
As-prepared	11.14	0.55
Swollen	24.41	0.64

Pore-size distribution of compacted GMZ bentonite at two different states

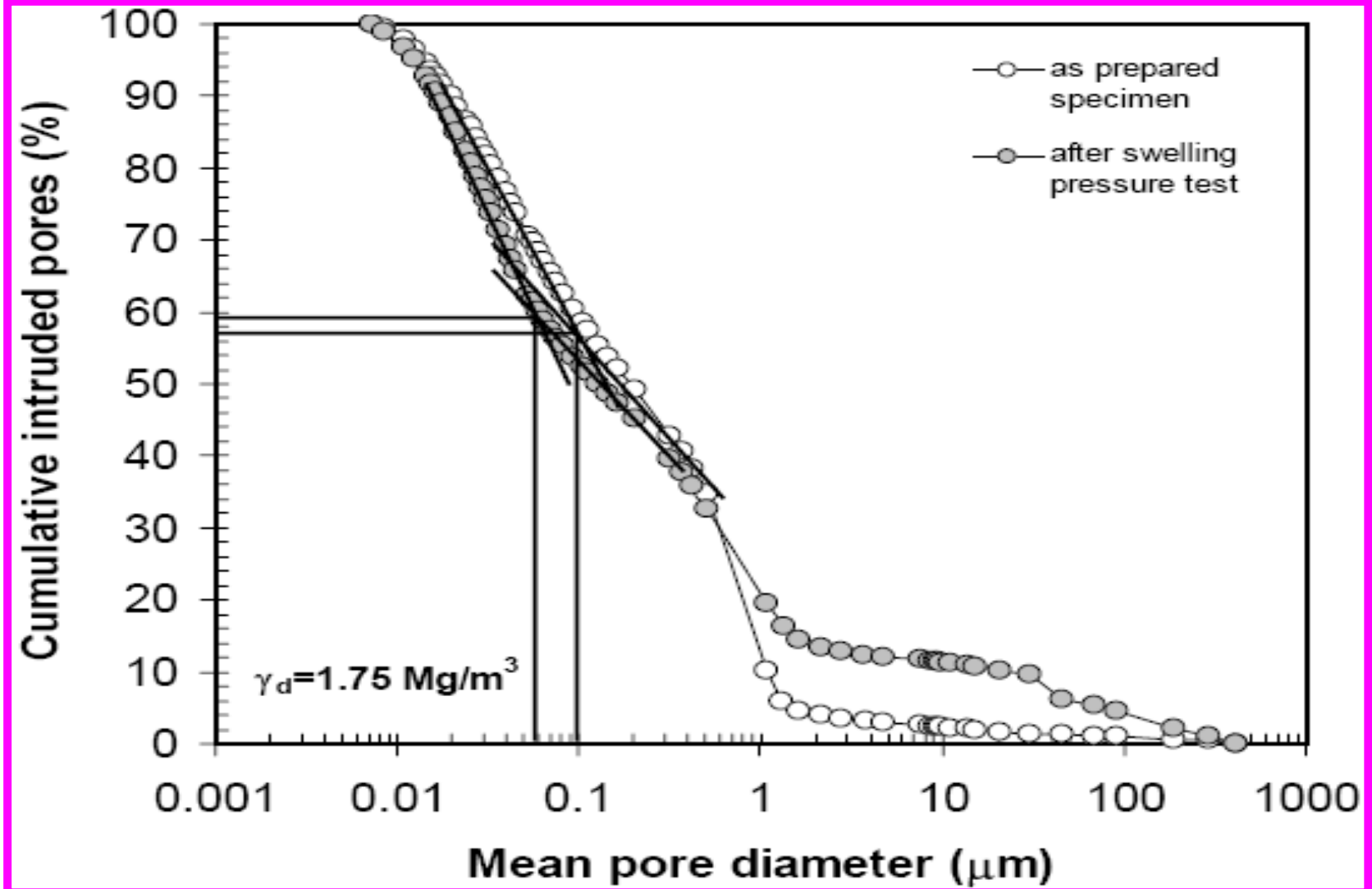
bentonite at two different states



Intruded pore volume vs. mean pore diameter at two different states



Determination of micro- and macropores from the pore size distribution data of the compacted GMZ bentonite



Summary of MIP test



MIP data	As-prepared	Swollen
Total pore volume(cm ³ /g)	0.201	0.236
Total intr. pore volume(cm ³ /g)	0.179	0.154
Percent of total pore volume(%)	89.1	65.3
Average diameter(μ m)	20.5	20.5
Micro-pore: diameter(μ m)	<0.1	<0.06
Average diameter(μ m)	0.037	0.025
volume(cm³/g)	0.096	0.141
Percent of total pore volume(%)	48	60
Macro-pore: diameter(μ m)	0.1-409.22	0.06-409.38
Average diameter(μ m)	37.9	31.3
volume(cm³/g)	0.105	0.095
Percent of total pore volume(%)	52	40

Summary of MIP test



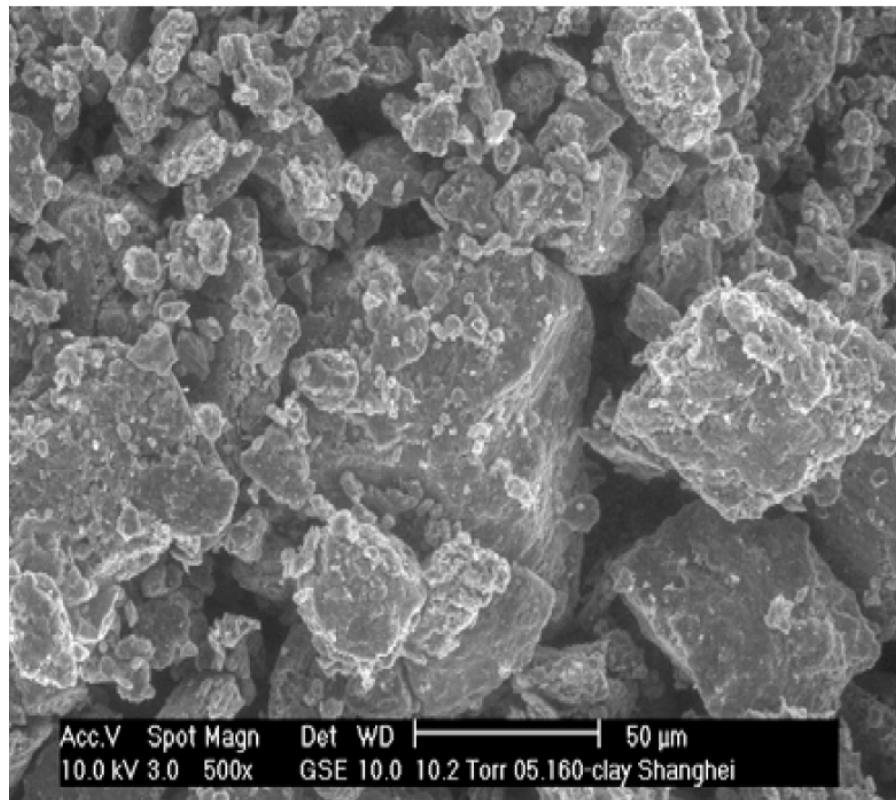
An internal rearrangement of clay clusters may occur when the specimen is wetted under constant volume conditions.

ESEM Test

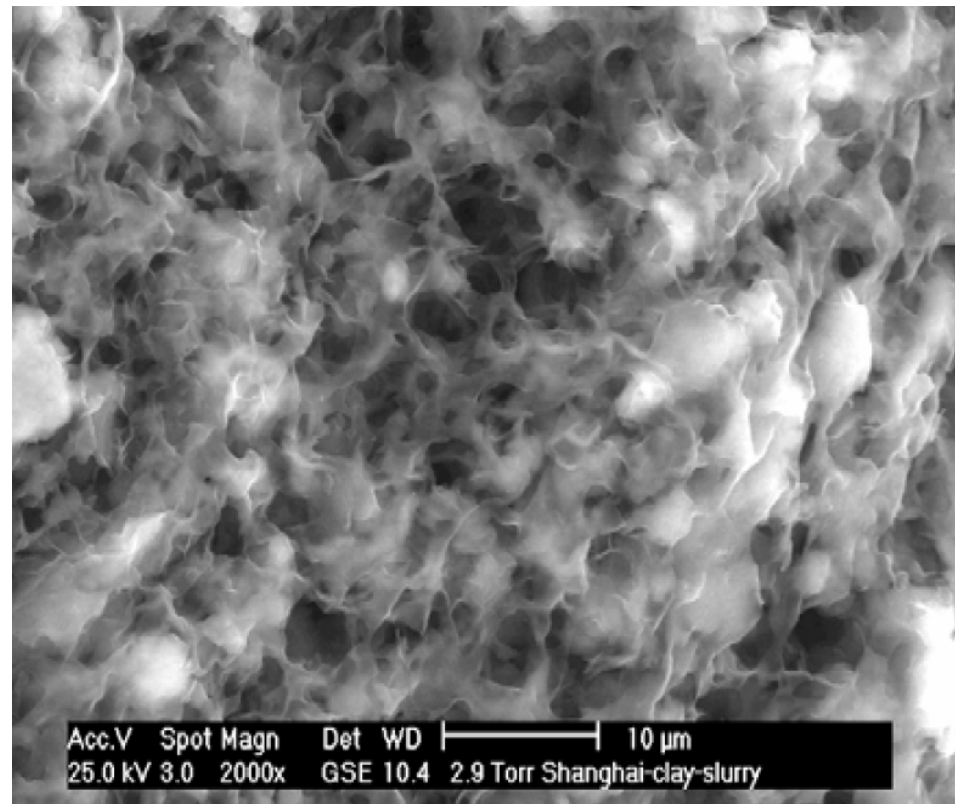
Initial conditions of the specimens tested

Specimen	Water content (%)	Dry density (g/cm ³)	Remarks
1	11.14		Powder
2	>270		Slurry
3	11.14	1.35	As-prepared
4	11.14	1.75	As-prepared
5???	24.41	1.65	Swollen

Effect of **water content** on microstructure of GMZ bentonite

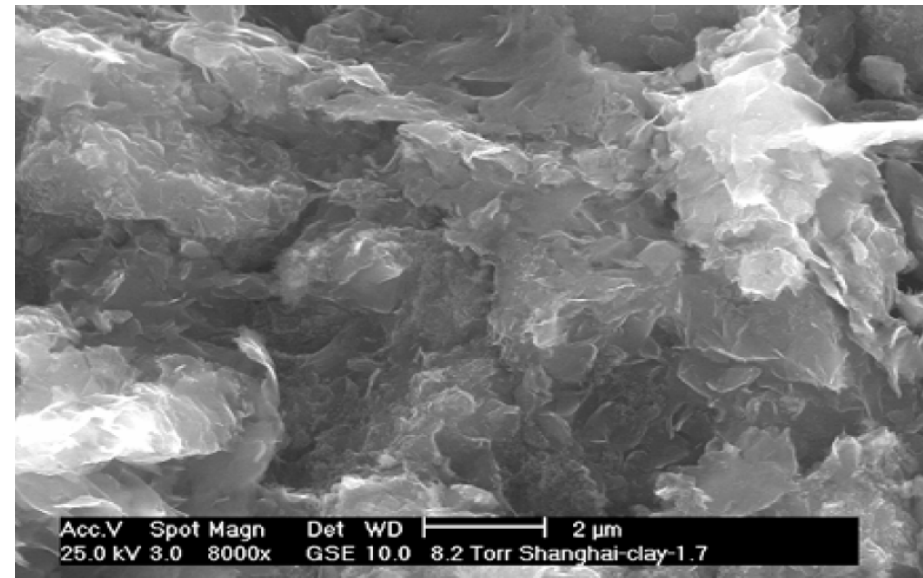
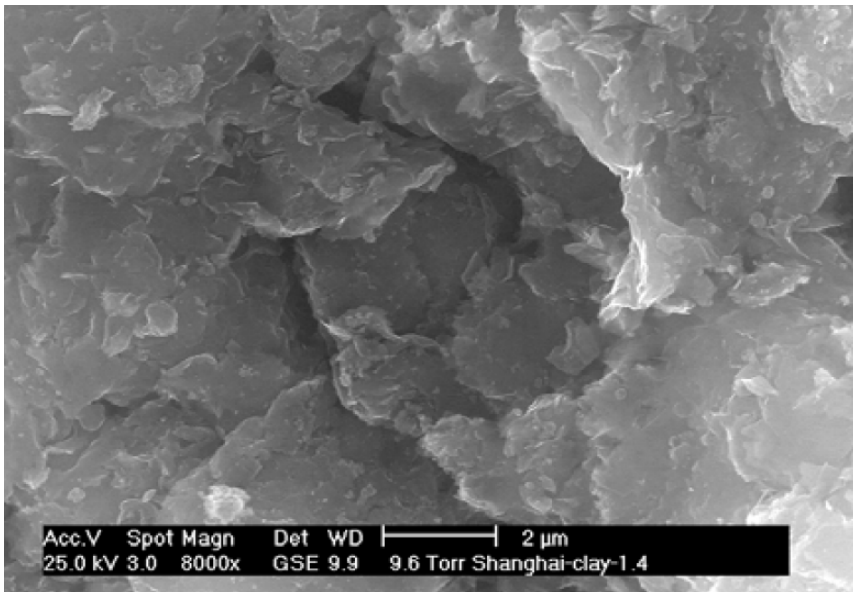
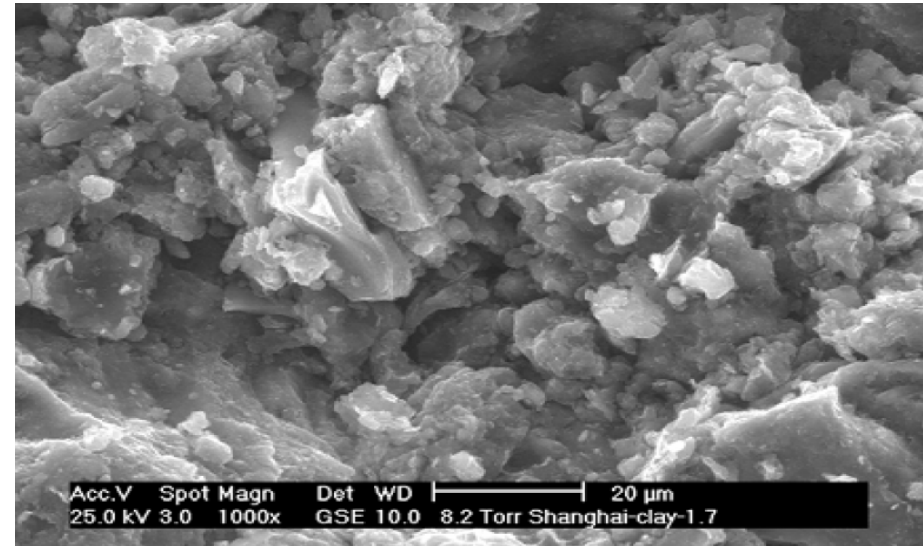
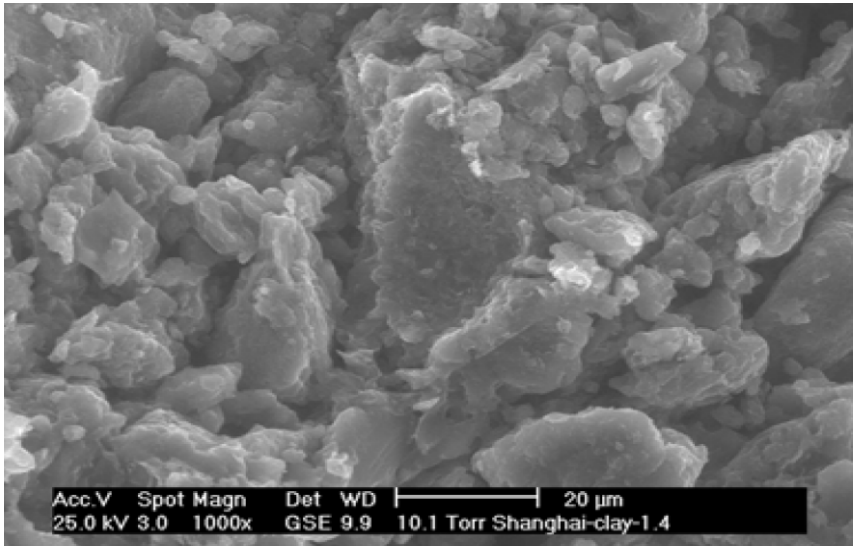


**ESEM photo of GMZ bentonite
(powder form, 500 \times)**



**ESEM photo of GMZ bentonite
(slurry form, 2000 \times)**

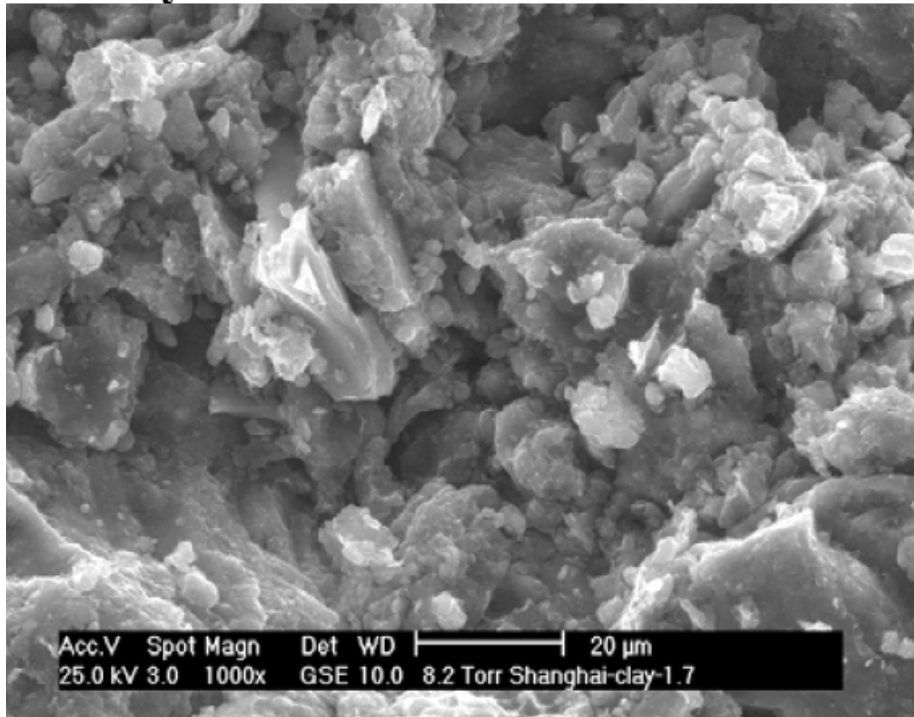
Effect of **density** on microstructure of GMZ bentonite



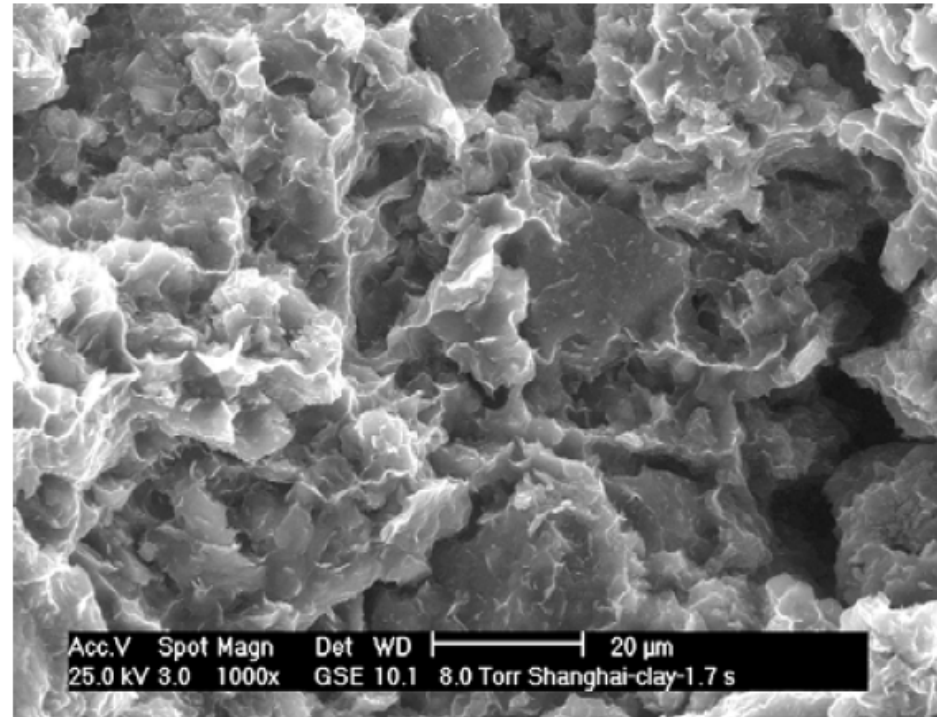
**ESEM photo of GMZ bentonite
(dry density 1.35g/cm³)**

**ESEM photo of GMZ bentonite
(dry density 1.75g/cm³)**

Effect of **swelling** on microstructure of GMZ bentonite



as-prepared



swollen

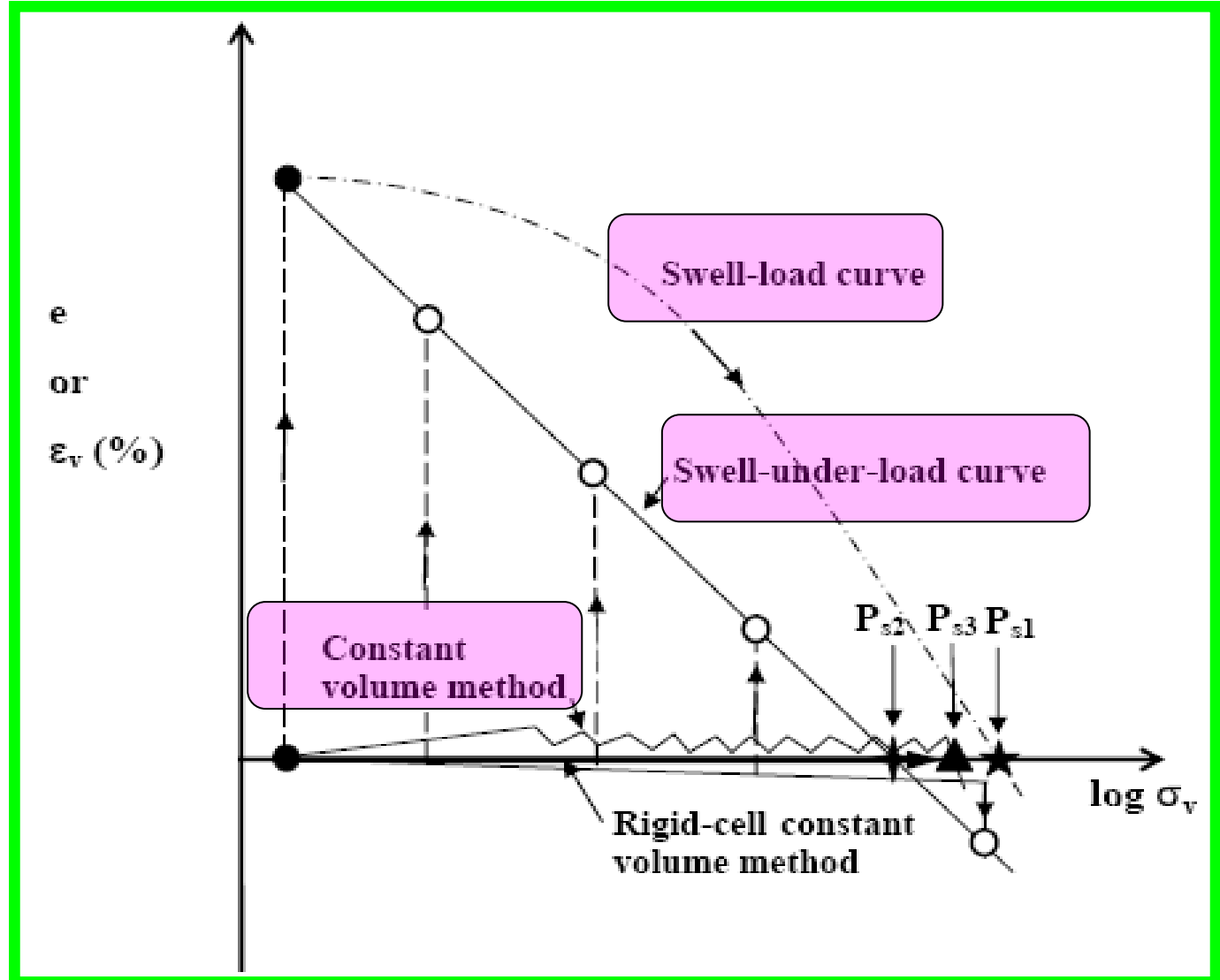
5 Swelling Pressure



Swelling pressure is defined as the pressure needed to maintain constant volume conditions when water is added to an expansive soil.

5 Swelling Pressure

Methods

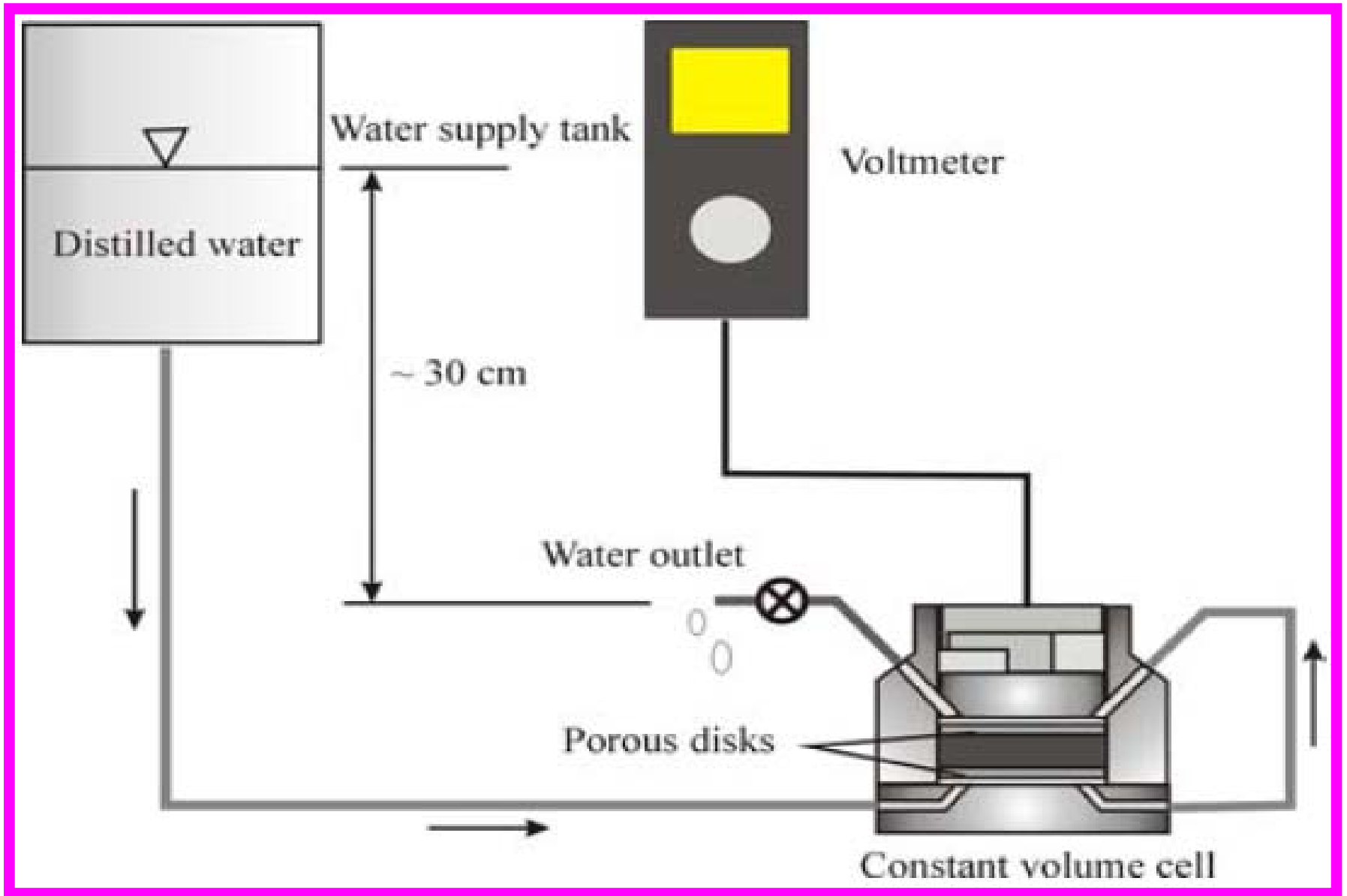


Experimental Techniques

**Constant
Volume**



UPC Barcelona constant volume cell



The scheme of constant volume test (Weimar 2005)

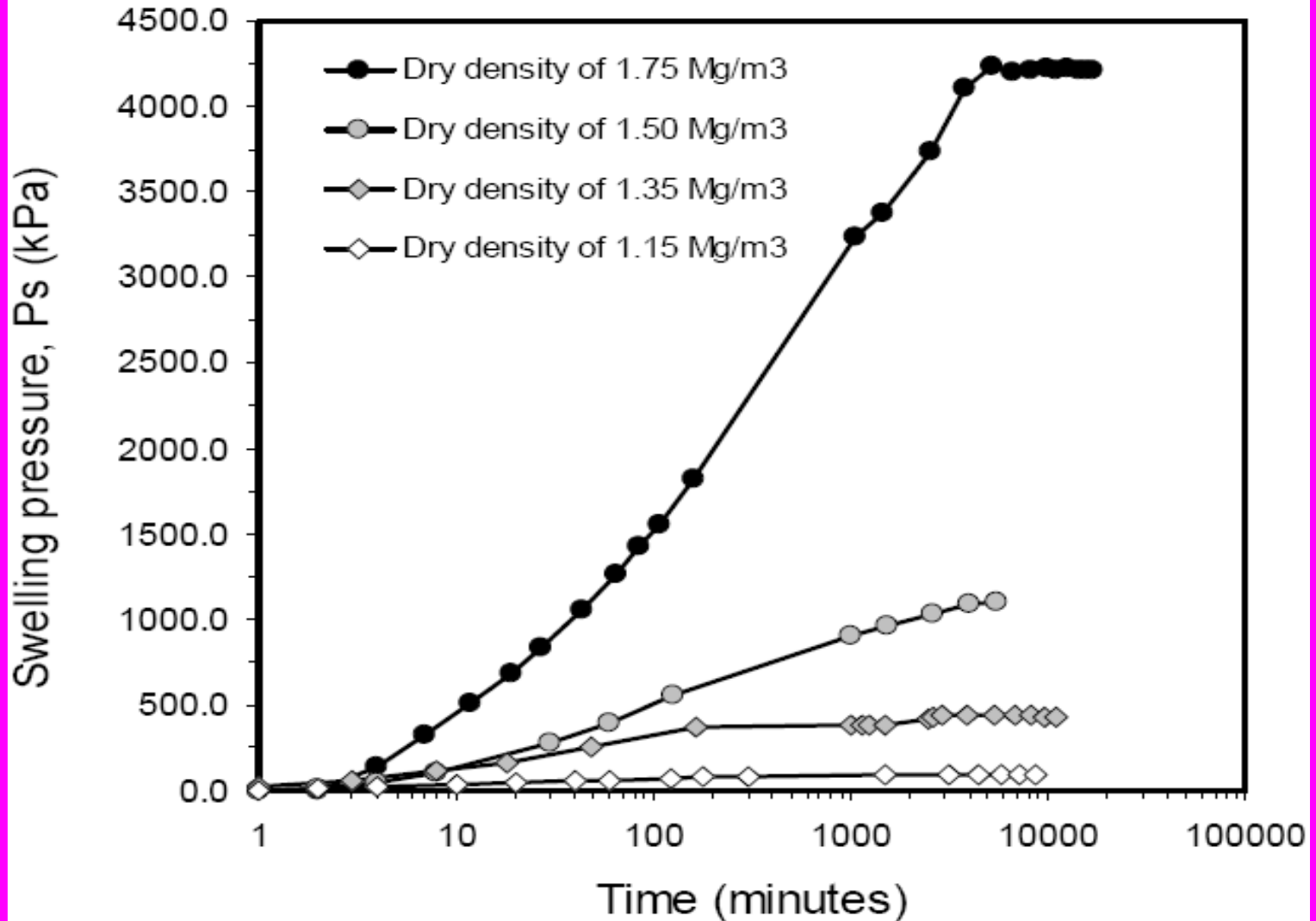
5 Swelling pressure

Initial conditions of the specimens in swelling pressure test

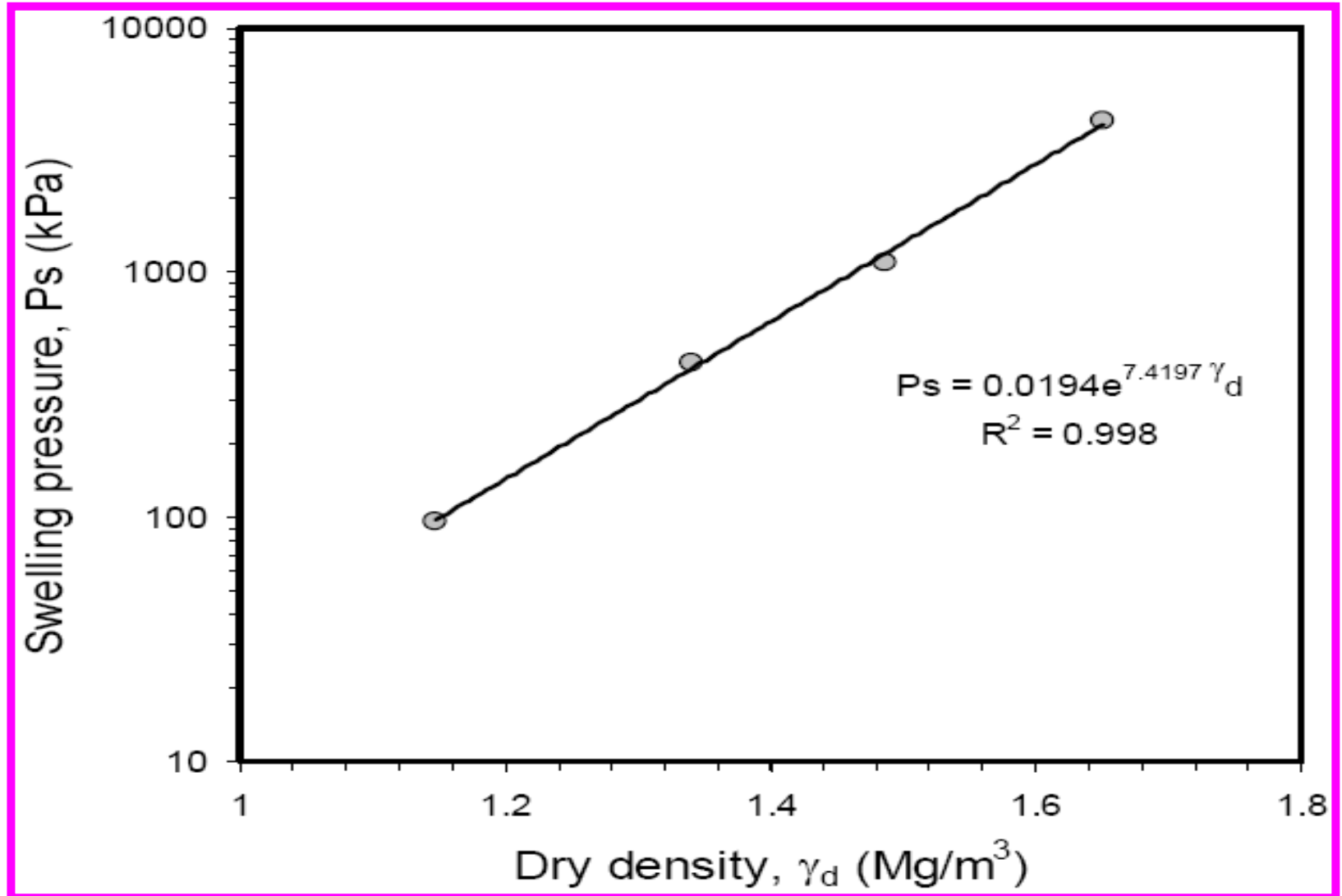
Specimen	Water content (%)	Dry density (g/cm ³)
1	11.14	1.15
2	11.14	1.35
3	11.14	1.50
4	11.14	1.75

Swelling pressure development with time

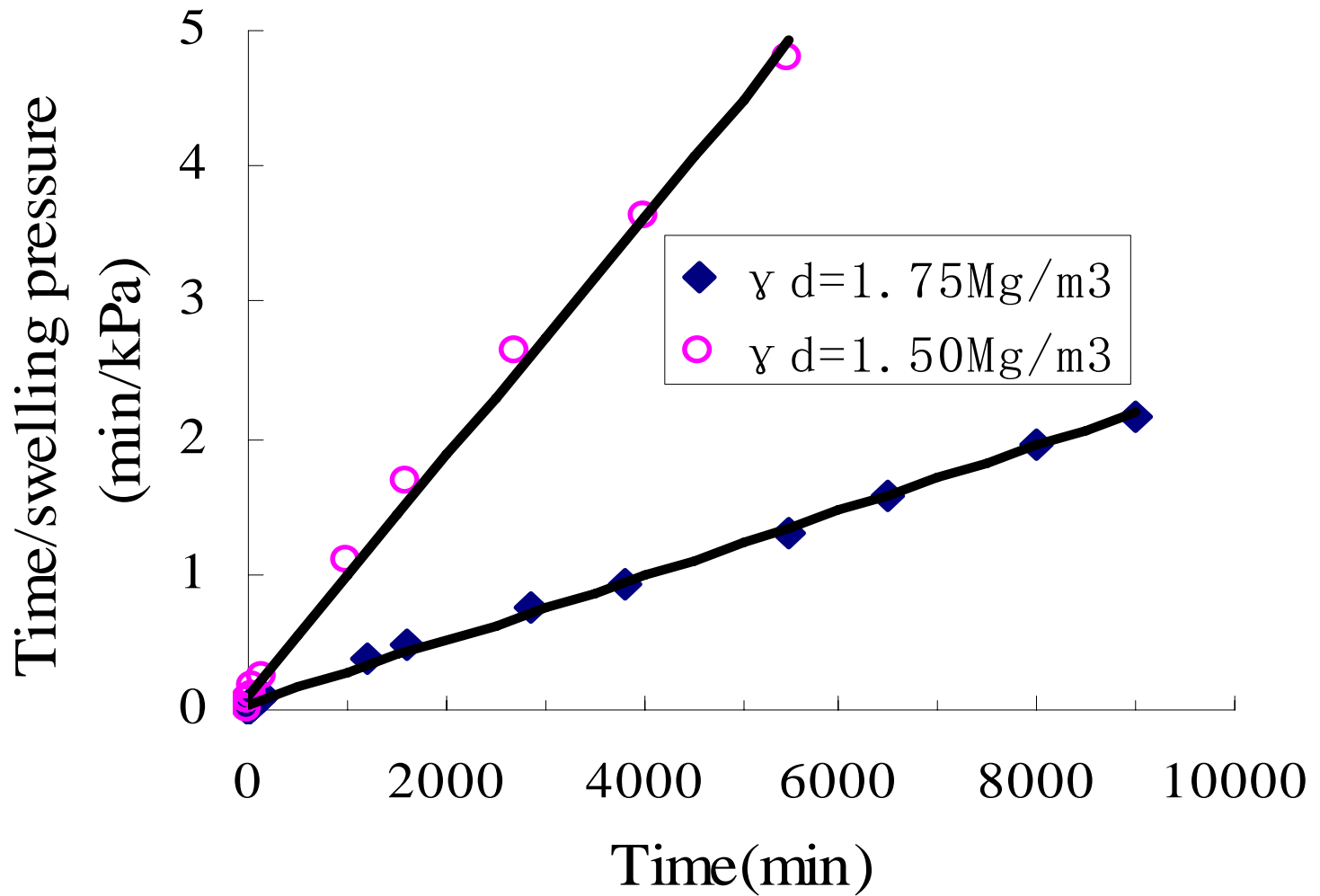
(Weimar 2005)




Swelling pressure vs. bentonite dry density (Weimar, 2005)



Time vs. (time/swelling pressure) relationship




$$\frac{t}{P_s} = a + bt$$

t — time

P_s — swelling pressure

a — intercept

b — slope of the straight line

$1/b$: ultimate swelling pressure

6 Conclusions



Compare to moderately plastic unsaturated soils, compacted bentonites are characterized by a high plasticity index and a high density that confer them a particular behavior.

6 Conclusions



Starting from **the initial suction of 4.2 MPa**, the difference between different confining conditions becomes less significant as the suction increases.

6 Conclusions



The as-prepared compacted specimen exhibits a bimodal pore-size distribution curve indicating the presence of a double porosity structure.

An internal rearrangement of clay clusters may occur when the specimen is wetted under constant volume conditions.

6 Conclusions



The swelling pressure increases with increase in dry density. The time over swelling pressure vs. time bears a good linear relationship.

Acknowledgement



- **National Natural Science Foundation of China**
- **DAAD, Bauhaus University Weimar and Prof T. Schanz**
- **Commission of Science Technology and Industry for National Defense**

Thank you!



Development of a new Closure Concept for the Richard Repository, Czech Republic

An Example for Successful International Cooperation

Disposal of Radioactive Waste - An Area of International Cooperation with Long Tradition

Since the early times of nuclear power production the importance of not only safe operation of the NPPs but also for safe management and disposal of radioactive waste has been recognized.

It also had been recognized that potential dangers are not limited to the borders of the individual nations.

Therefore the first organisations for international cooperation in the field of the peaceful use of nuclear energy were established very early and they also promote international cooperation in finding solutions for the safe disposal of radioactive waste.

Main International Organisations

- IAEA (International Atomic Energy Agency)
Technology Section and Waste Safety Section
- OECD (Organisation for Economic Cooperation and Development)
NEA (Nuclear Energy Agency) – RWMC (Radioactive Waste Management Committee)
- EDRAM (Environmental Safe Disposal of Radioactive Material)
- EURATOM (European Atomic Energy Community)
- European Commission (Research and Transport & Energy)
- Club of Agencies (most Western Waste Management Agencies)
- Large number of multi- and bilateral cooperations

DBE/DBE TECHNOLOGY mbH has

cooperation agreements with a broad range of waste management organisations and institutions working in the same field:

- including most of the radioactive waste management organisation in Western and East Europe, DOE of the USA and engineering companies working in the US in this area, with institutions in Russia, IHI and RWMC of Japan, Organisations in South Africa, Argentina, and BRIUG of the People's Republic of China

is a member of EDRAM, Club of Agencies, ITC (International Training Center for Geological Disposal)

has carried out a wide range of R&D projects in the framework of EC financed projects



European Projects

Chinese German Workshop, Beijing 2007

Phare Project

Solution for the Closure of a Chamber in the Richard Repository

EUROPEAID/113986/D/SV/CZ



**A project funded by the
European Union and the Czech Republic**

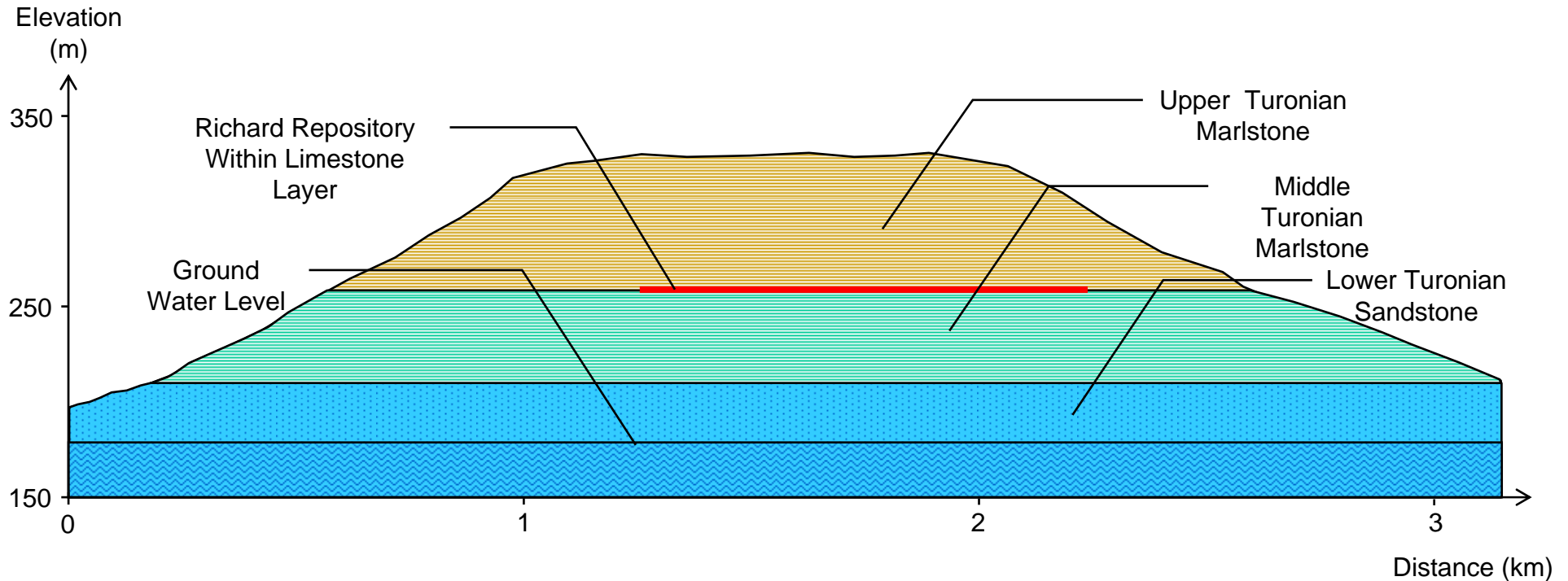


Location of Richard Repository



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Simplified Geological Cross Section



History of Richard Repository

- 1930´s Limestone mine
- 1940´s Military production
- 1960´s Repository
- Inventory ca. 10^{15} Bq
- Approx. 25,000 waste packages disposed of
- 2000 RAWRA takes over RICHARD



Main Tasks of Phare Project on Richard Repository

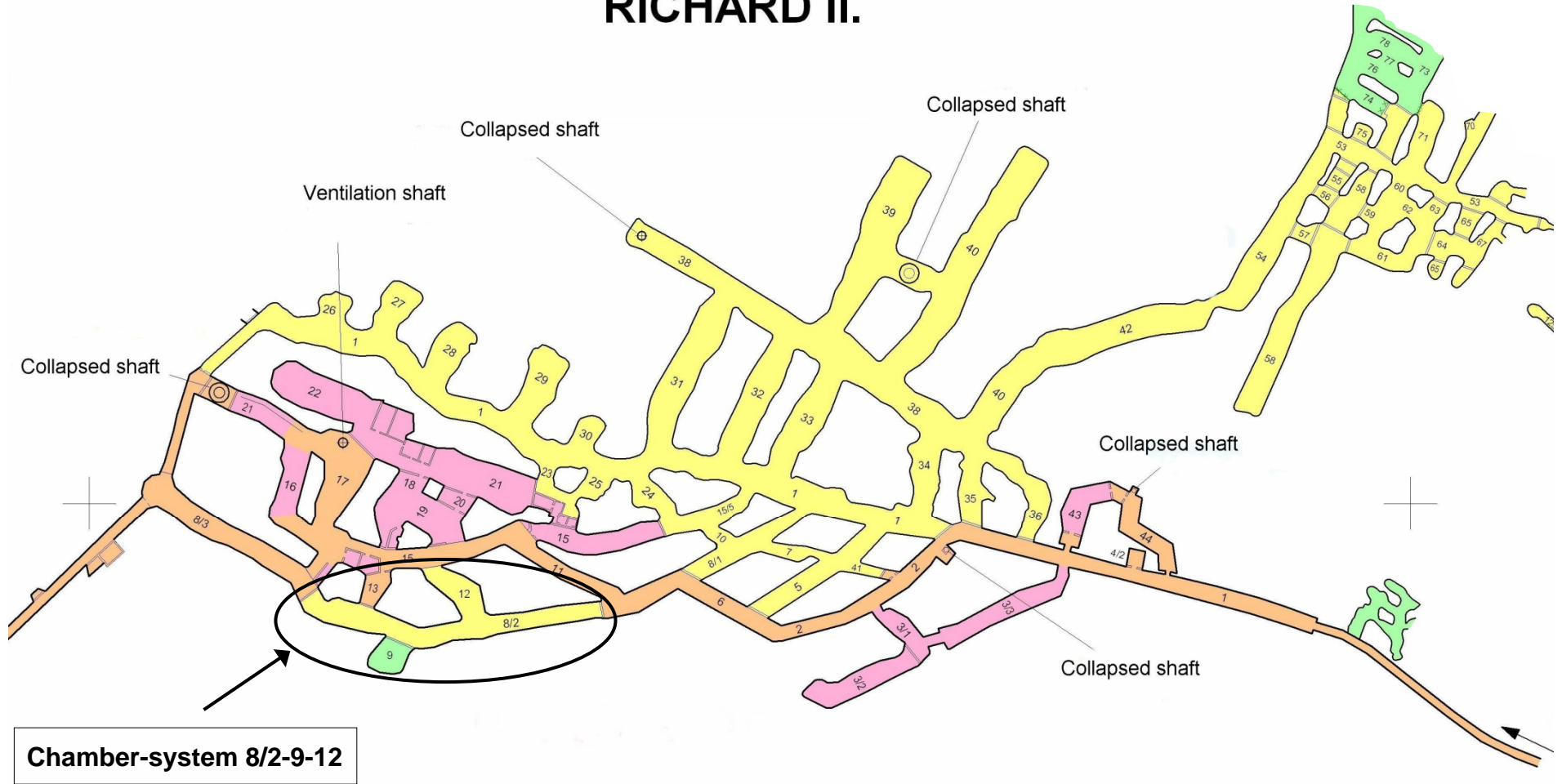
- Review of existing closure plan and safety assessment
- Revision of closure plan (if necessary)
- Update of the safety assessment
- Detailed technical planning for specific chamber-system
 - Preparation of the non operated chamber-system
 - Handling and treatment of waste (incl. historical waste)
 - Backfilling of chamber-system
- Preparation of documents for realization of closure concept
 - licensing
 - tender process

Main Topics of Presentation

- Brief description on the reasons for changing the former closure concept
- Principal description of new closure concept and its impact on the long-term safety
- Description of planned technical implementation and its realisation

Map of Richard Repository

RICHARD II.



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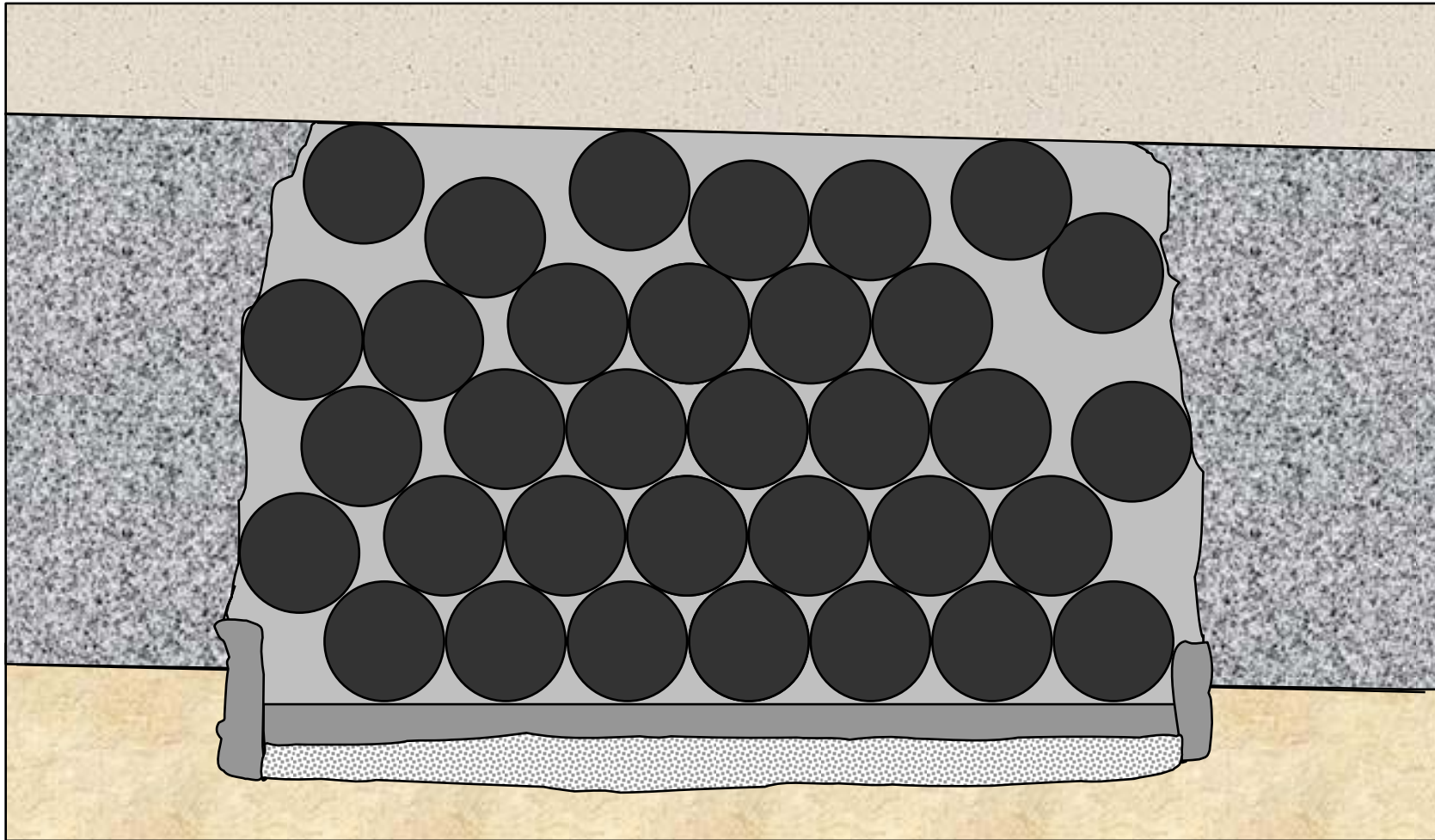
Waste Chamber



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Previous Closure Concept

Simplified Chamber Model

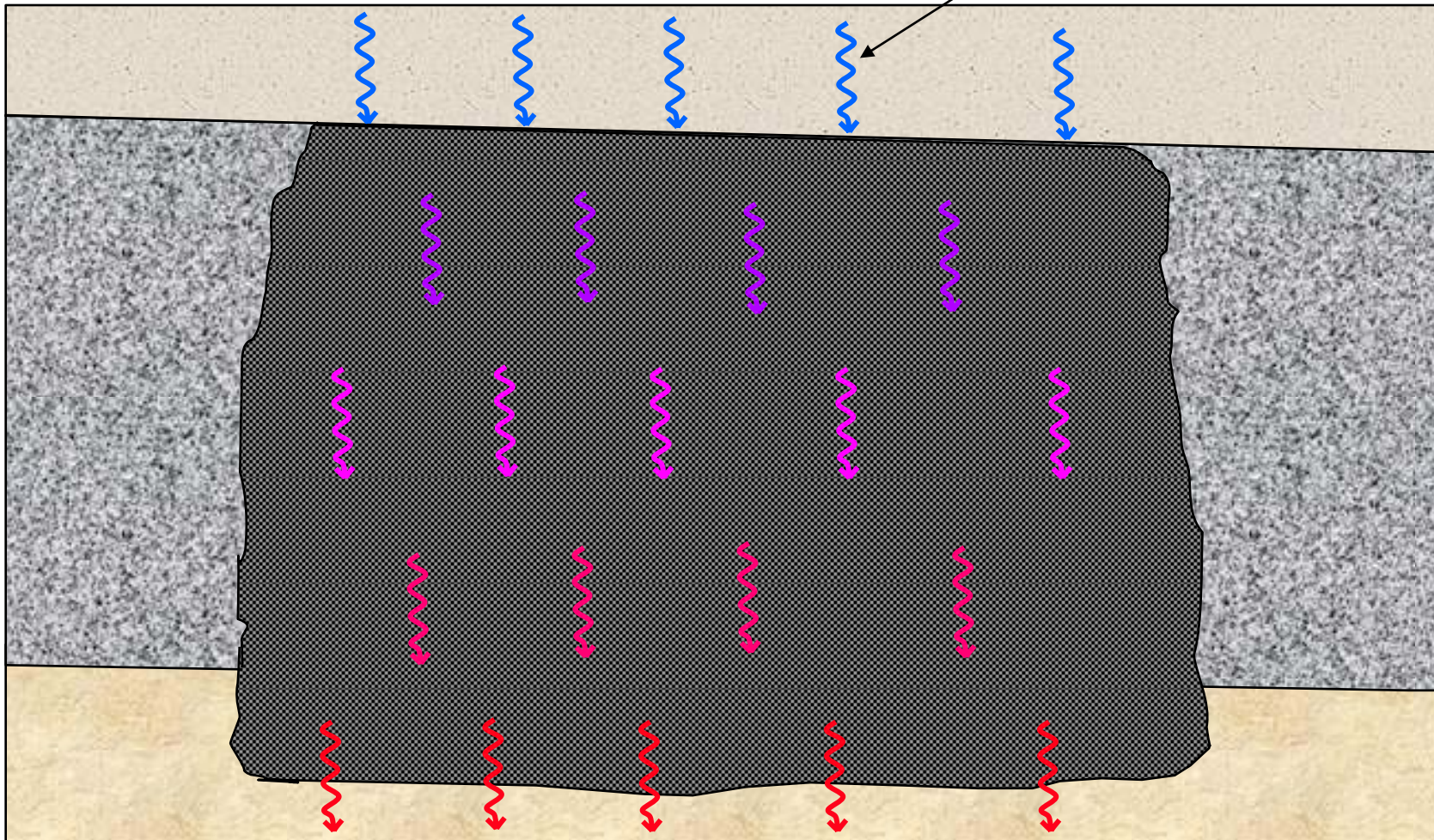


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Previous Closure Concept

Advective Flow through Waste/Concrete

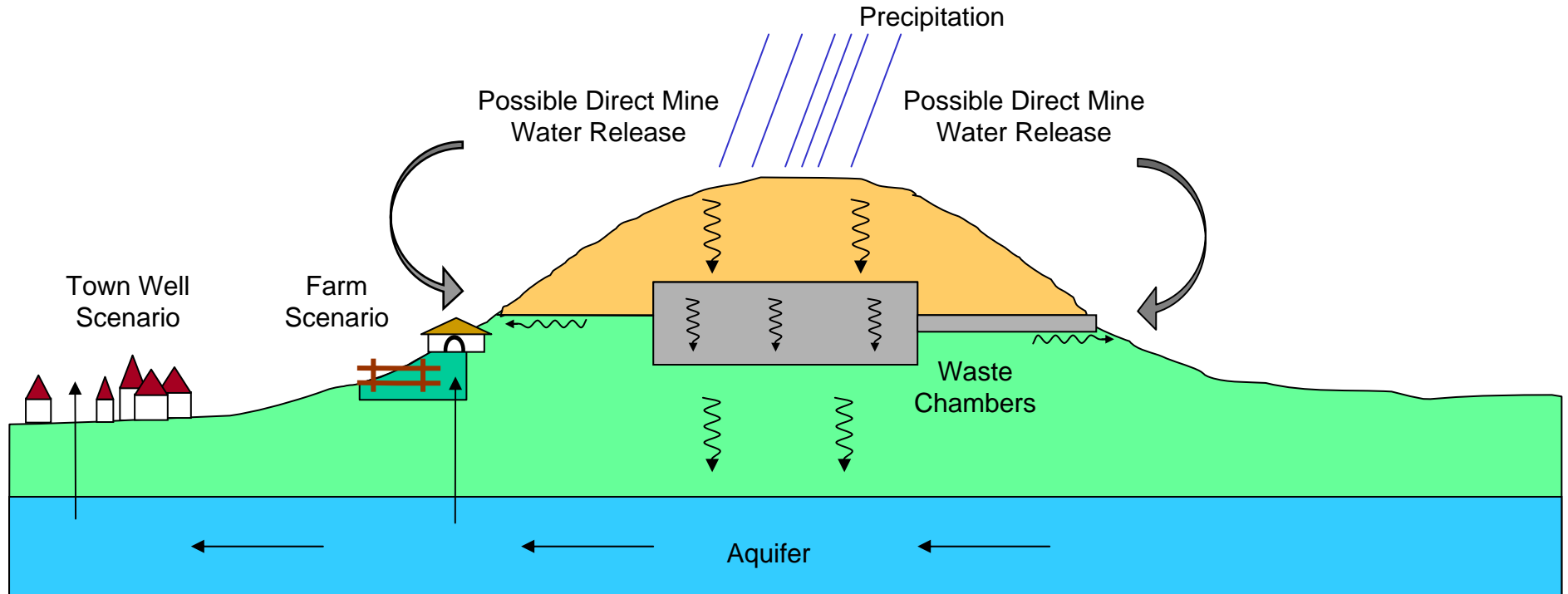
Percolating Water from Surface



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Previous Closure Concept

Simplified Model for Scenarios



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Main Problems of Previous Closure Concept

- Direct contact between water and waste packages not prevented
- Advective transport without delay
- Due to special stratigraphy, scenarios related to direct release of mine water difficult to exclude

Hydraulic Cage Concept

Main Working Principle

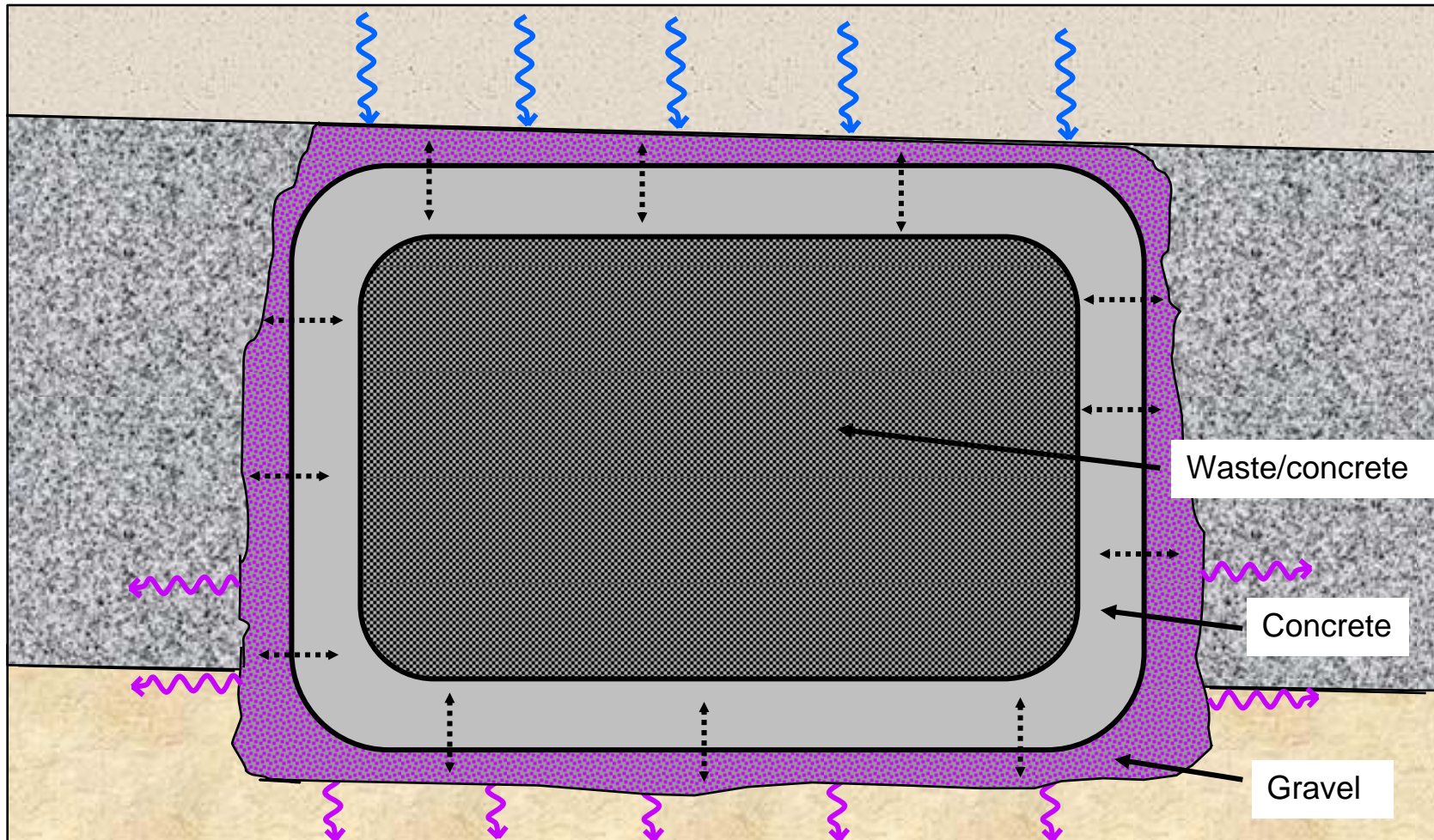
Hydraulic Cage Concept

**Elimination of radionuclide transport mechanism
by transport gradient elimination
through implementation of an HYDRAULIC CAGE**

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Hydraulic Cage Concept

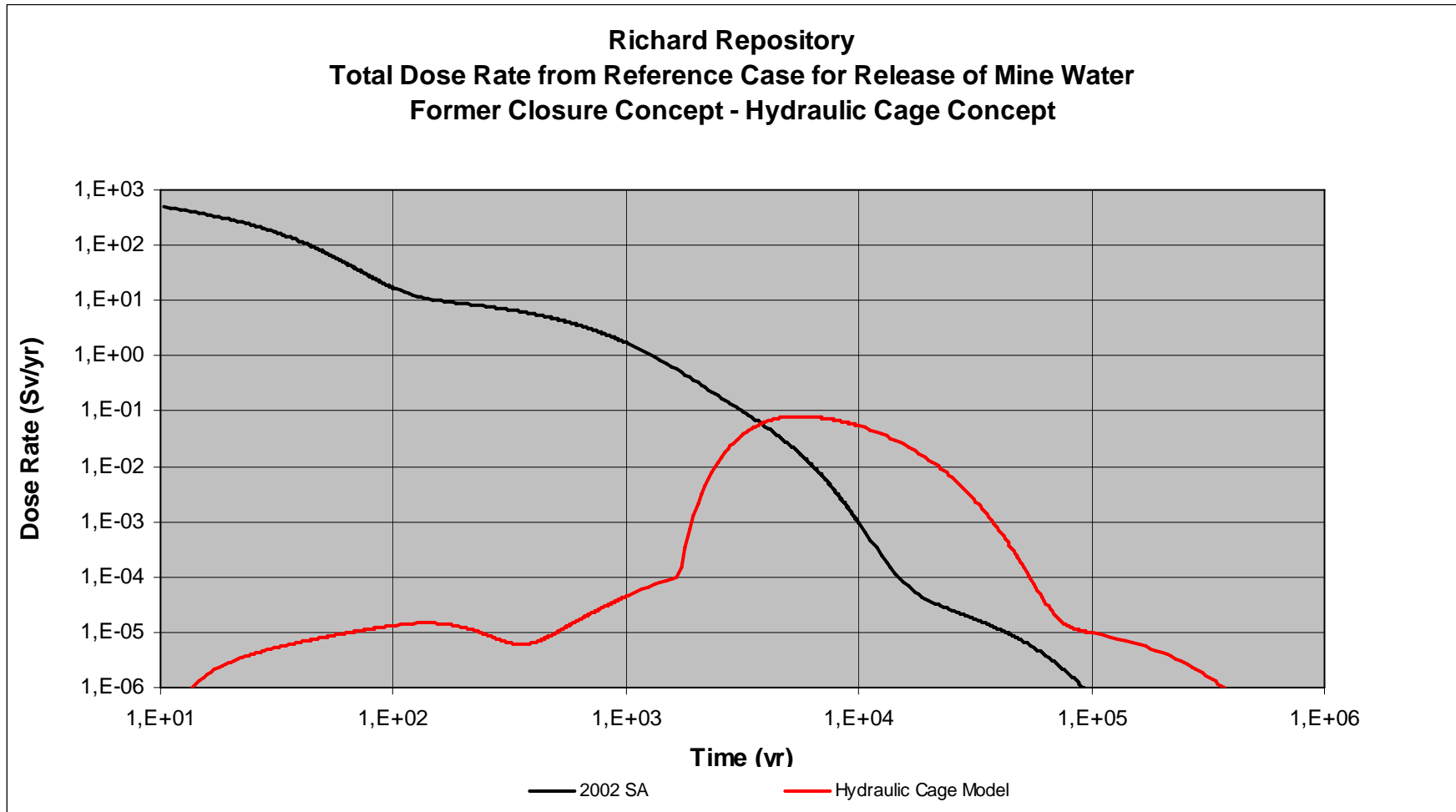
Simplified Radionuclide Transport



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Safety Assessment Richard Repository

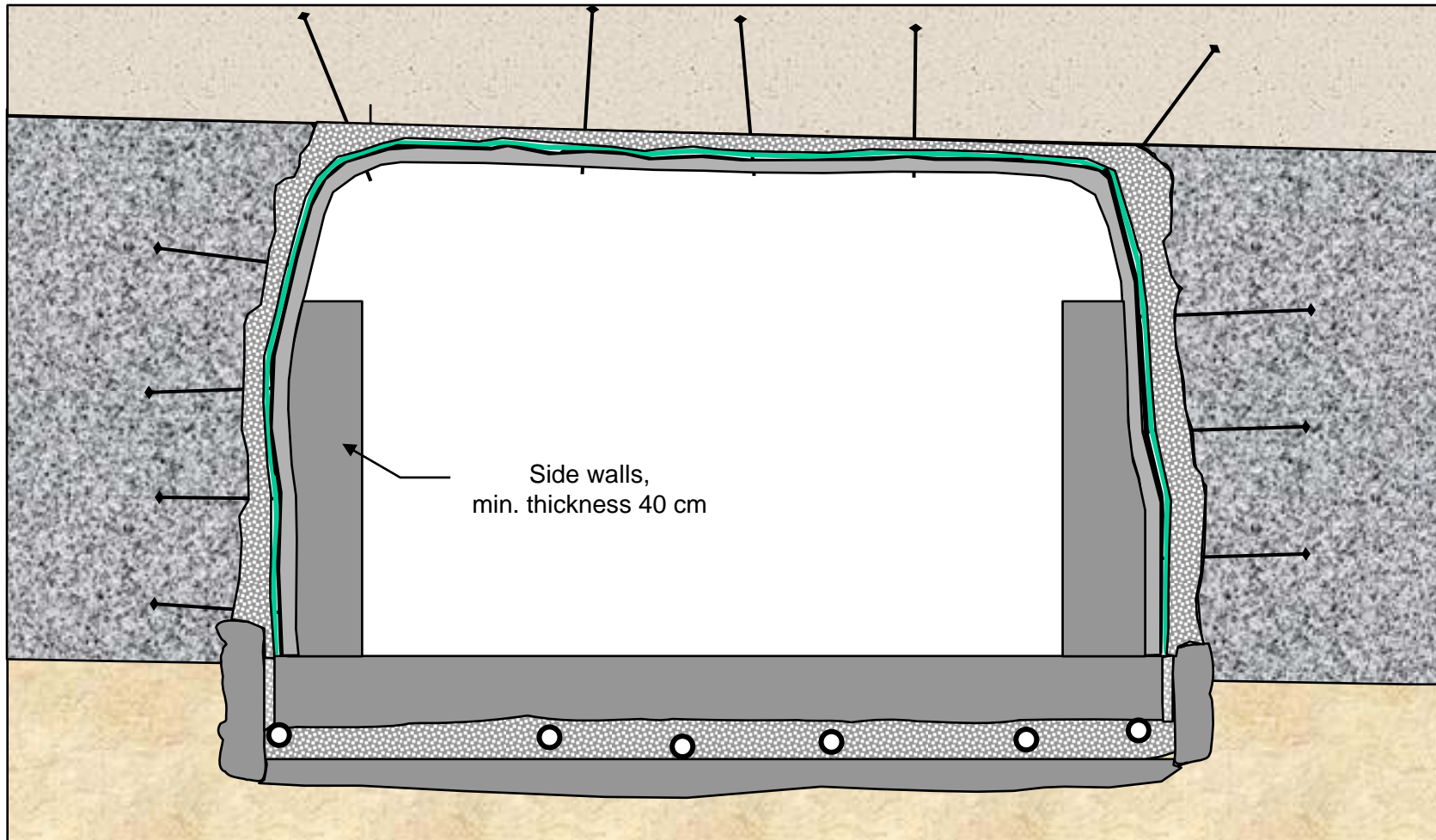
Total Dose Rates from Mine Water Release Scenario



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Chamber Preparation

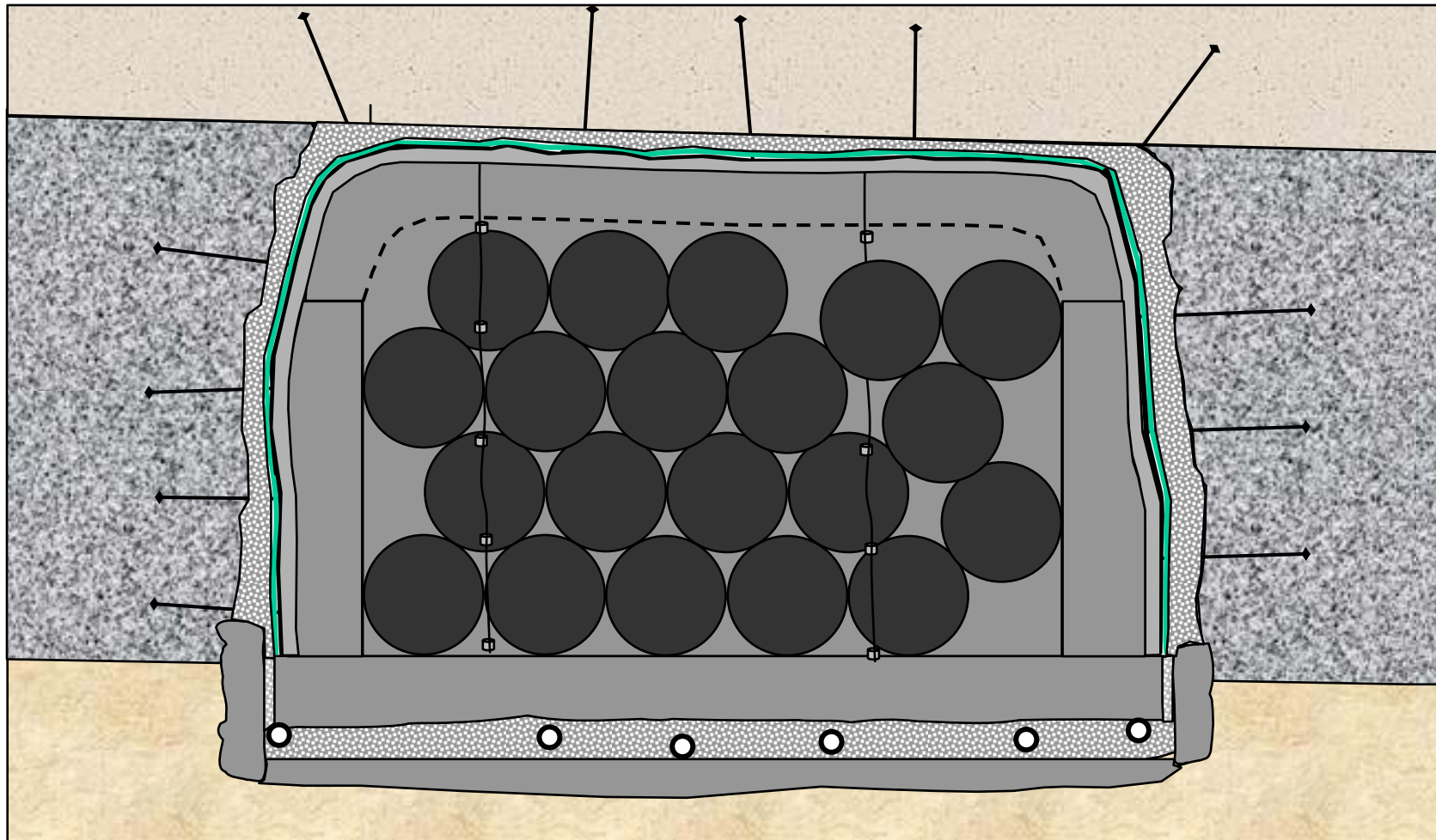
Preparation of Concrete Side Walls



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Closure of Chamber

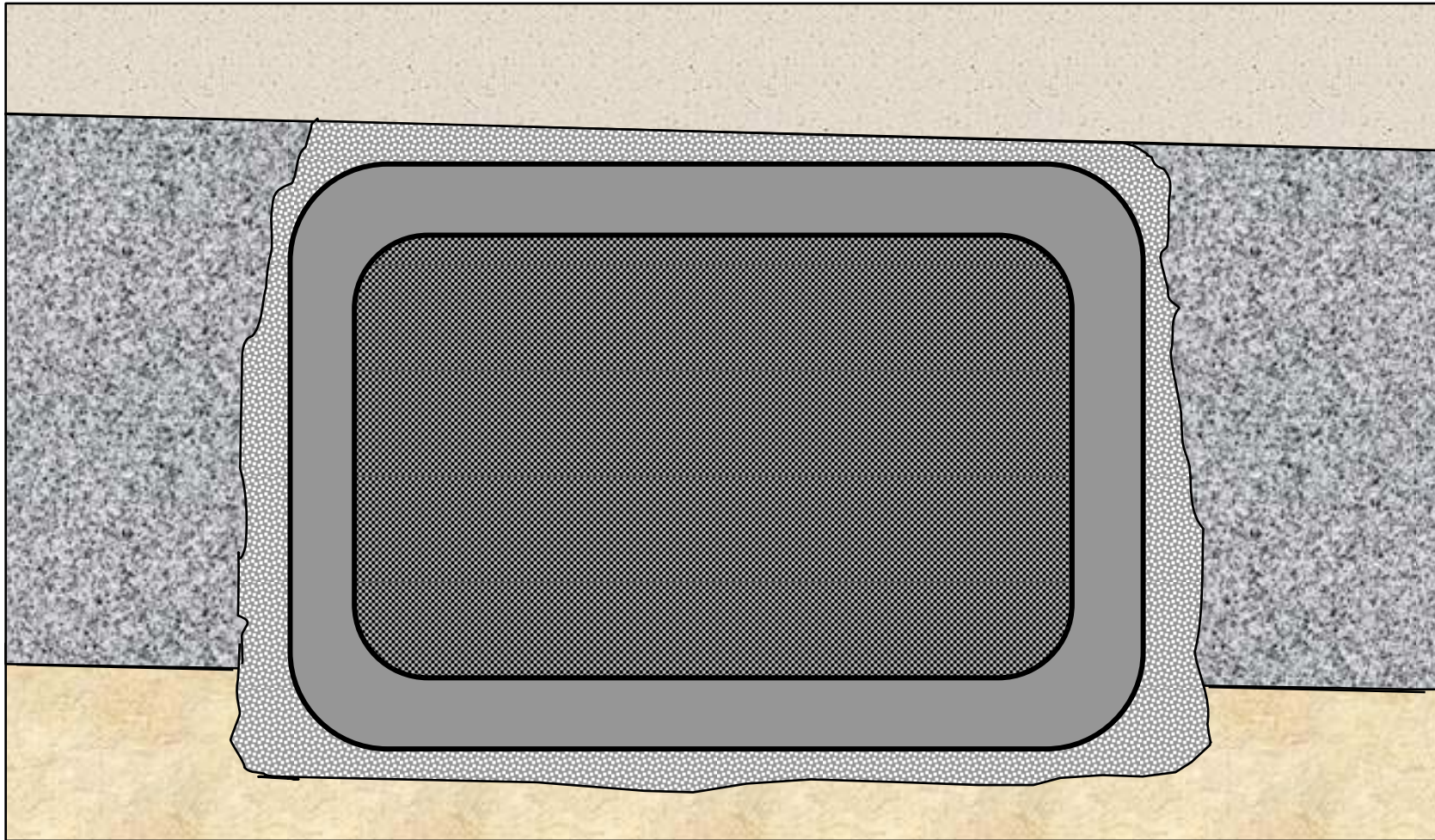
Situation after Backfilling



Chinese German Workshop, Beijing 2007

Closure of Chamber

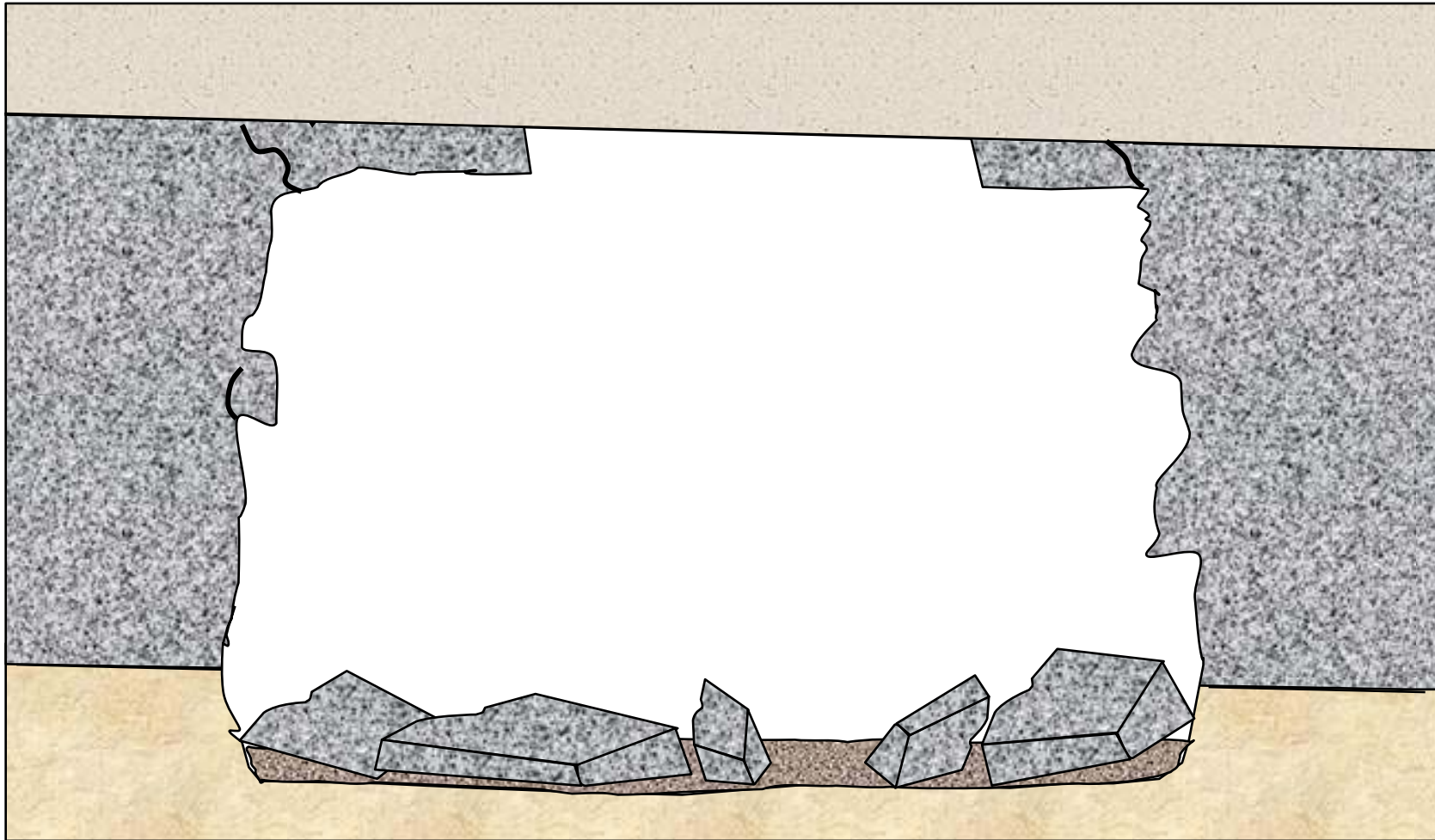
Further Simplified Model of Situation after Backfilling



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Chamber Preparation

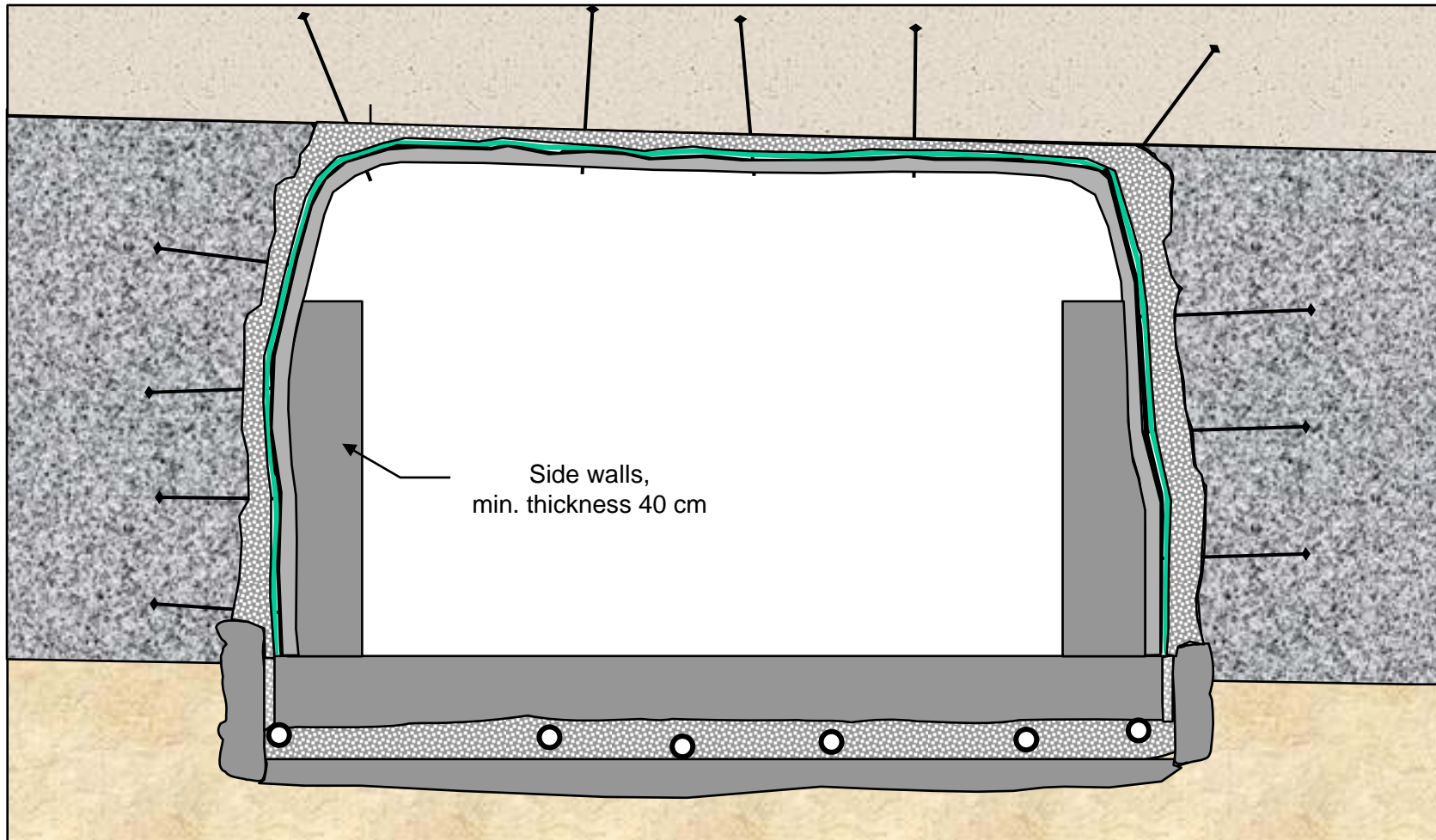
Present Situation



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Chamber Preparation

Preparation of Concrete Side Walls



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Chamber Preparation

Initial Situation



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Presentation TopSeal 2006, Olkiluoto



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Presentation TopSeal 2006, Olkiluoto



Chinese German Workshop, Beijing 2007

Presentation TopSeal 2006, Olkiluoto



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Thank you very much for your attention

Hydraulic Cage Concept

Technical Implementation

Technical Implementation of

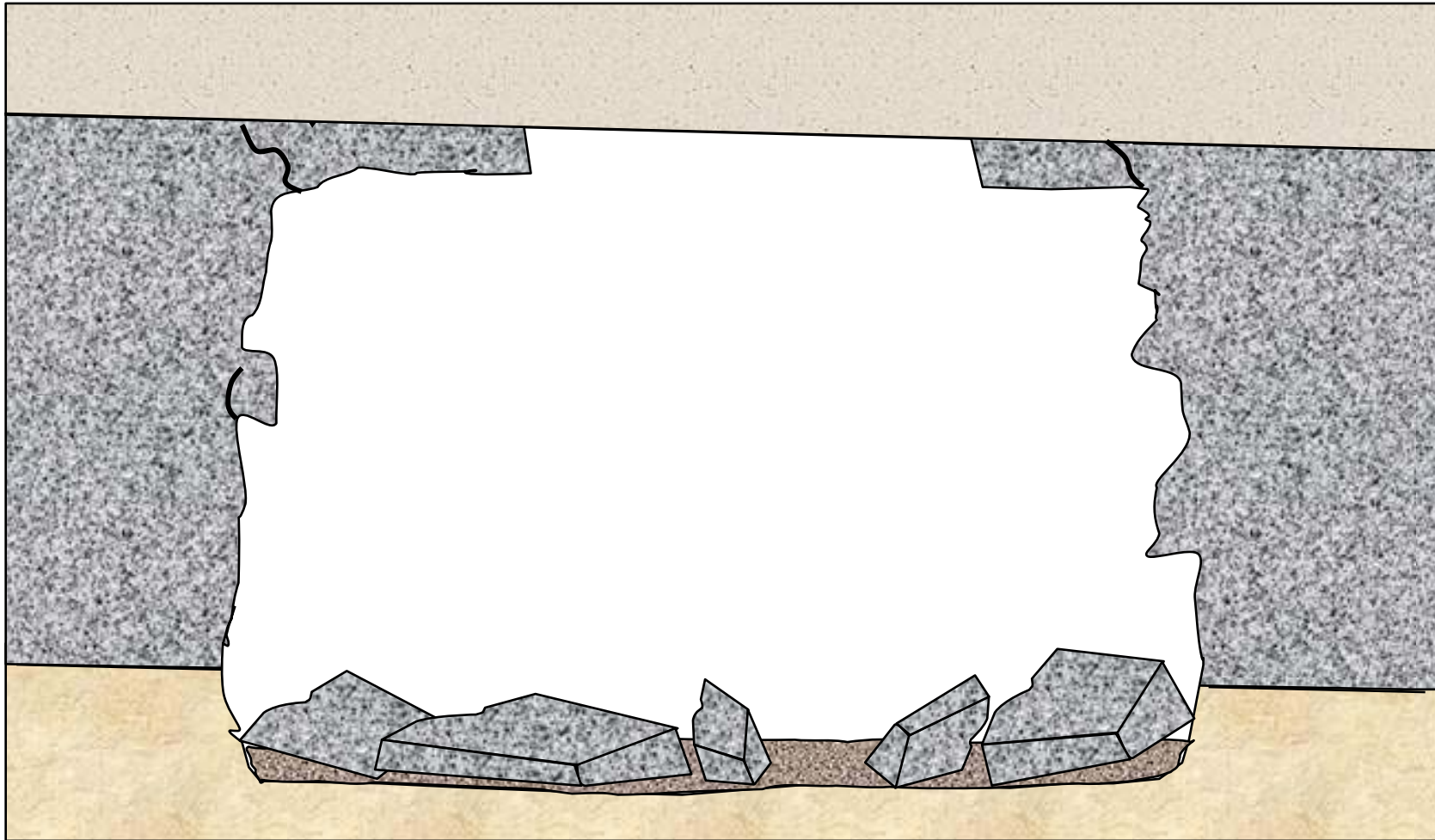
Hydraulic Cage Concept

Main Steps during Technical Implementation of Hydraulic Cage

- Clearing of Chamber
- Construction of Roadway and Hydraulic Cage
- Preparation for Waste Disposal
- Disposal and Backfilling

Chamber Preparation

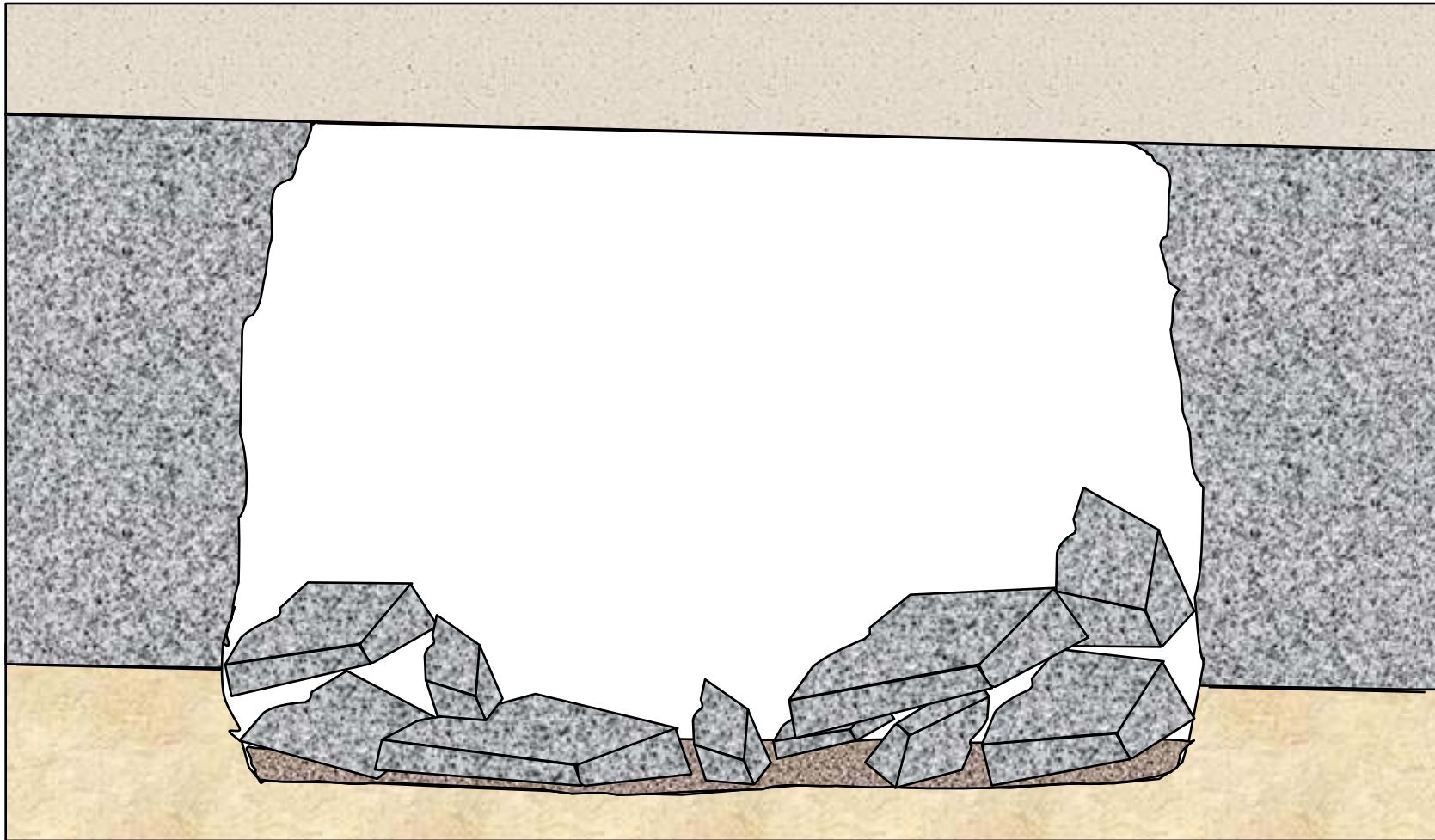
Present Situation



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Chamber Preparation

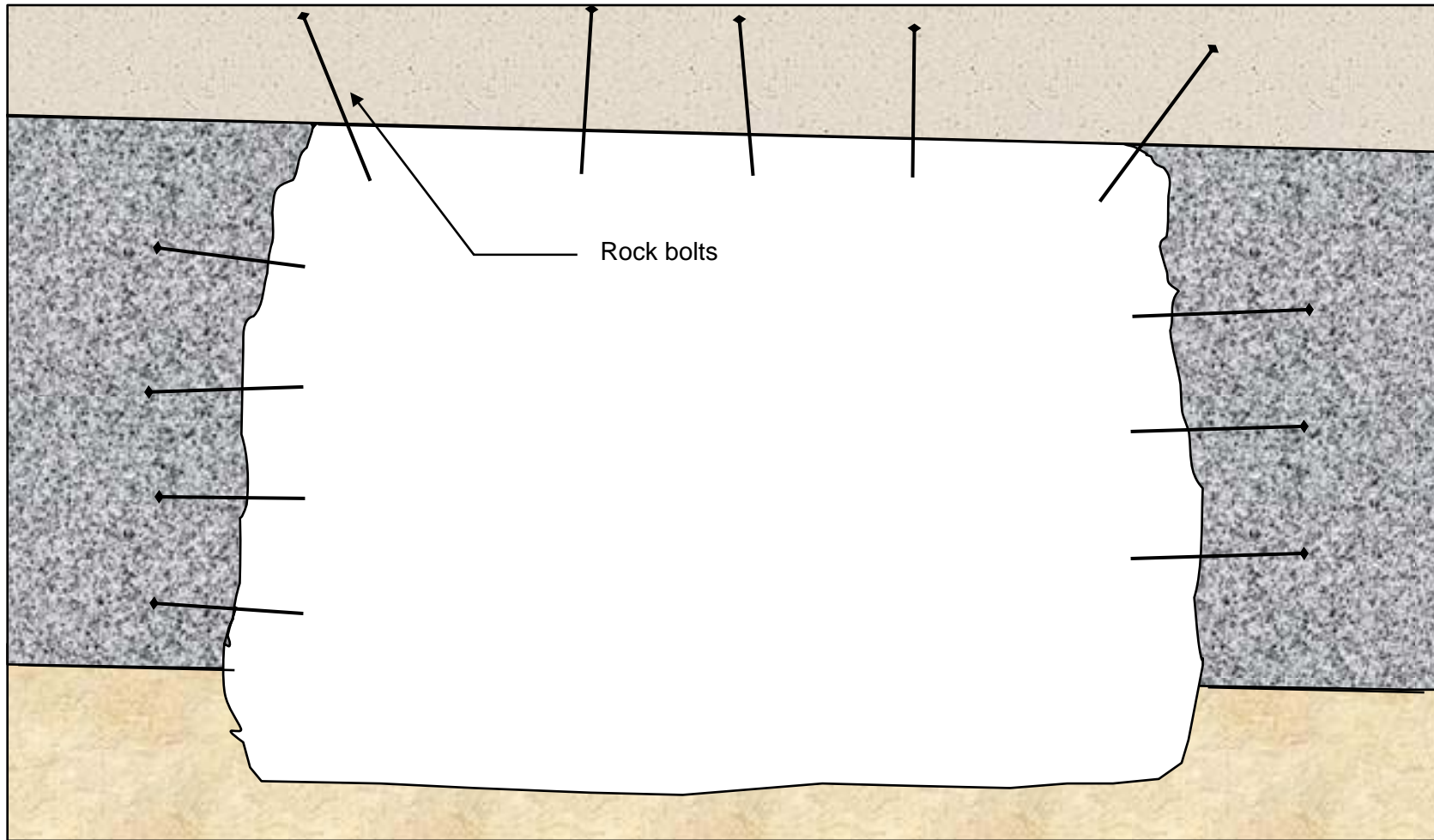
Situation After Clearing of Loosened Rocks



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Chamber Preparation

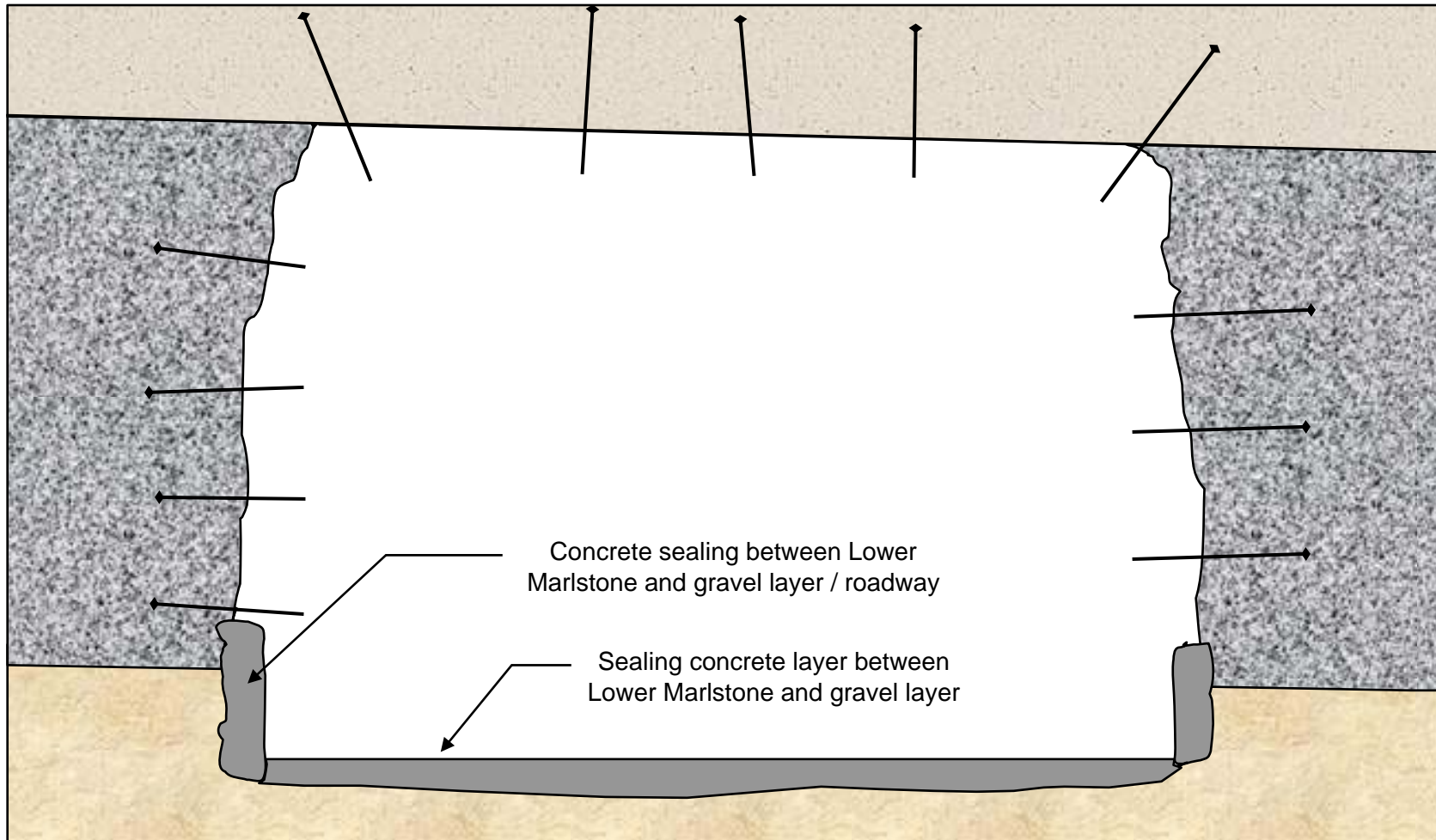
Installation of Rock Bolts



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Chamber Preparation

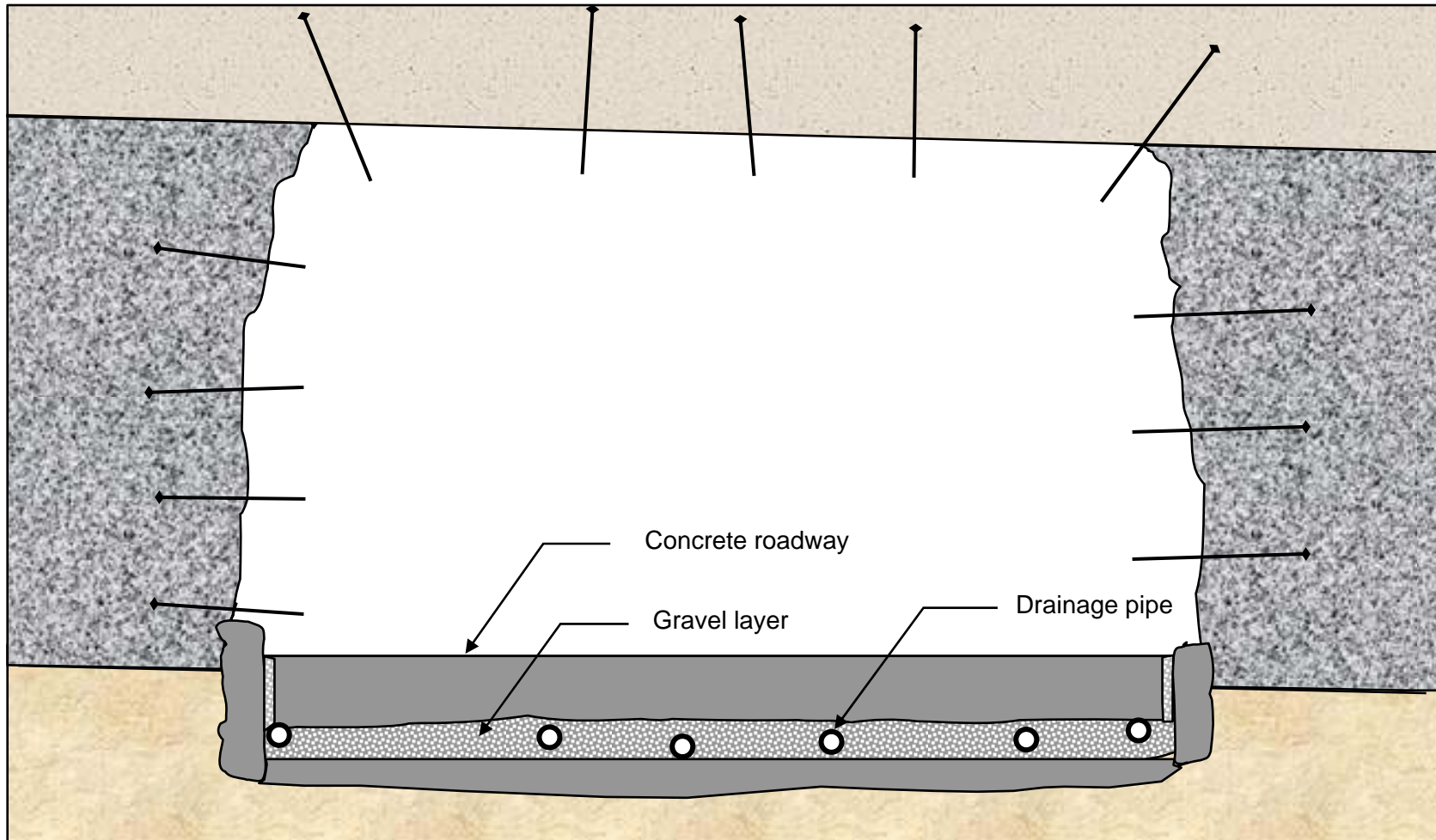
Installation of Separating Layer



Chinese German Workshop, Beijing 2007

Chamber Preparation

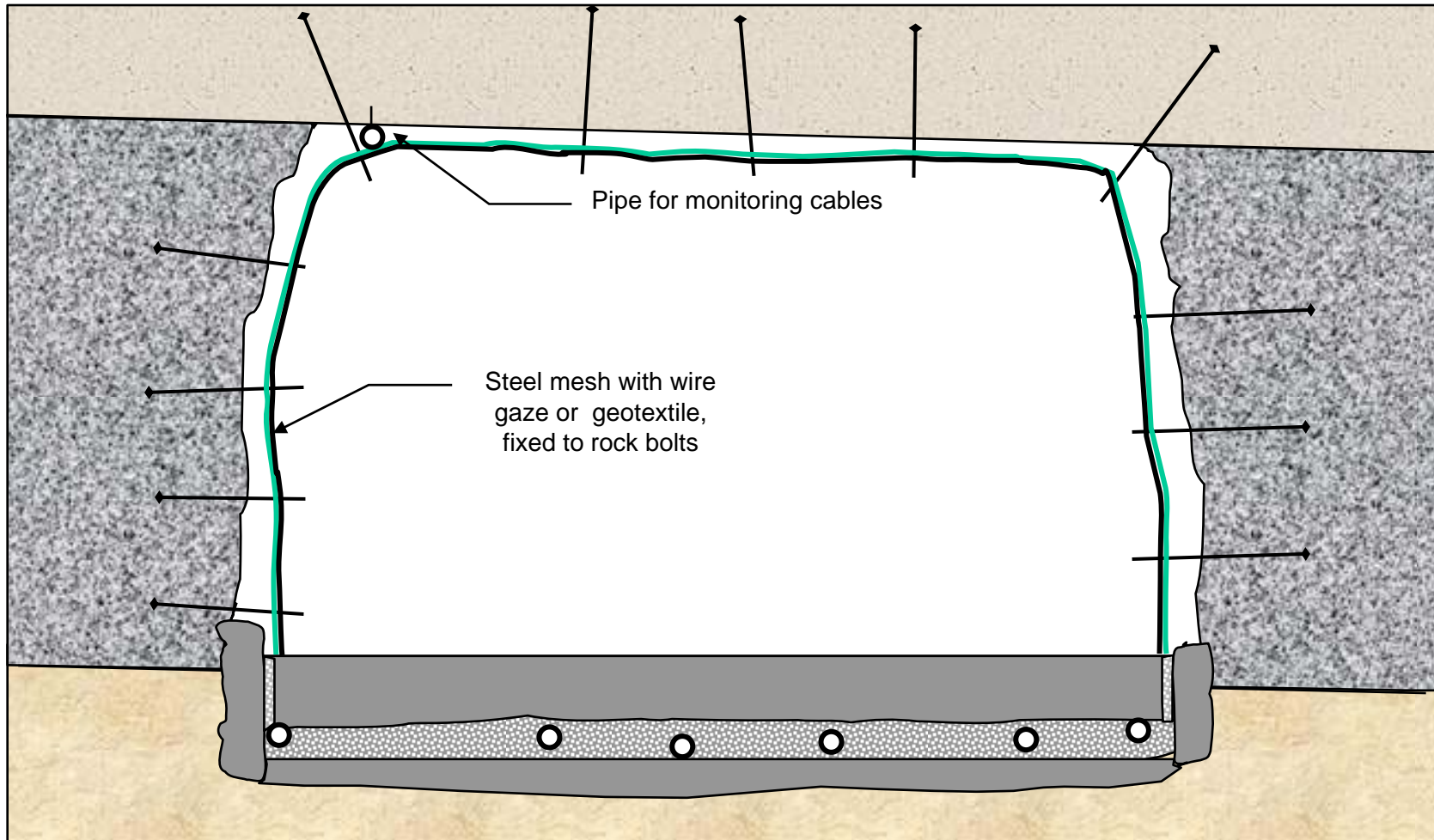
Installation of Concrete Roadway



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Chamber Preparation

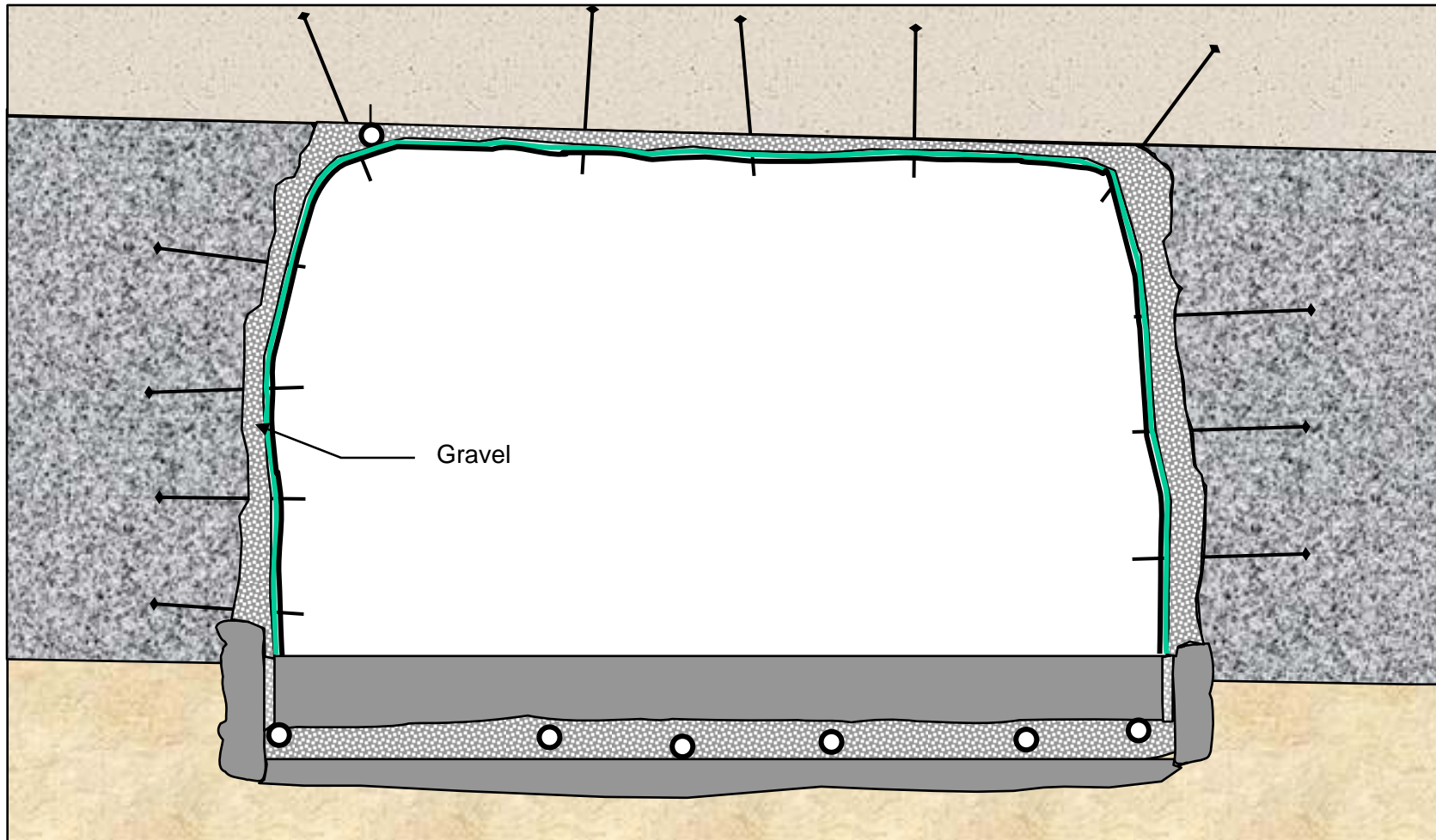
Installation of Hydraulic Cage



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Chamber Preparation

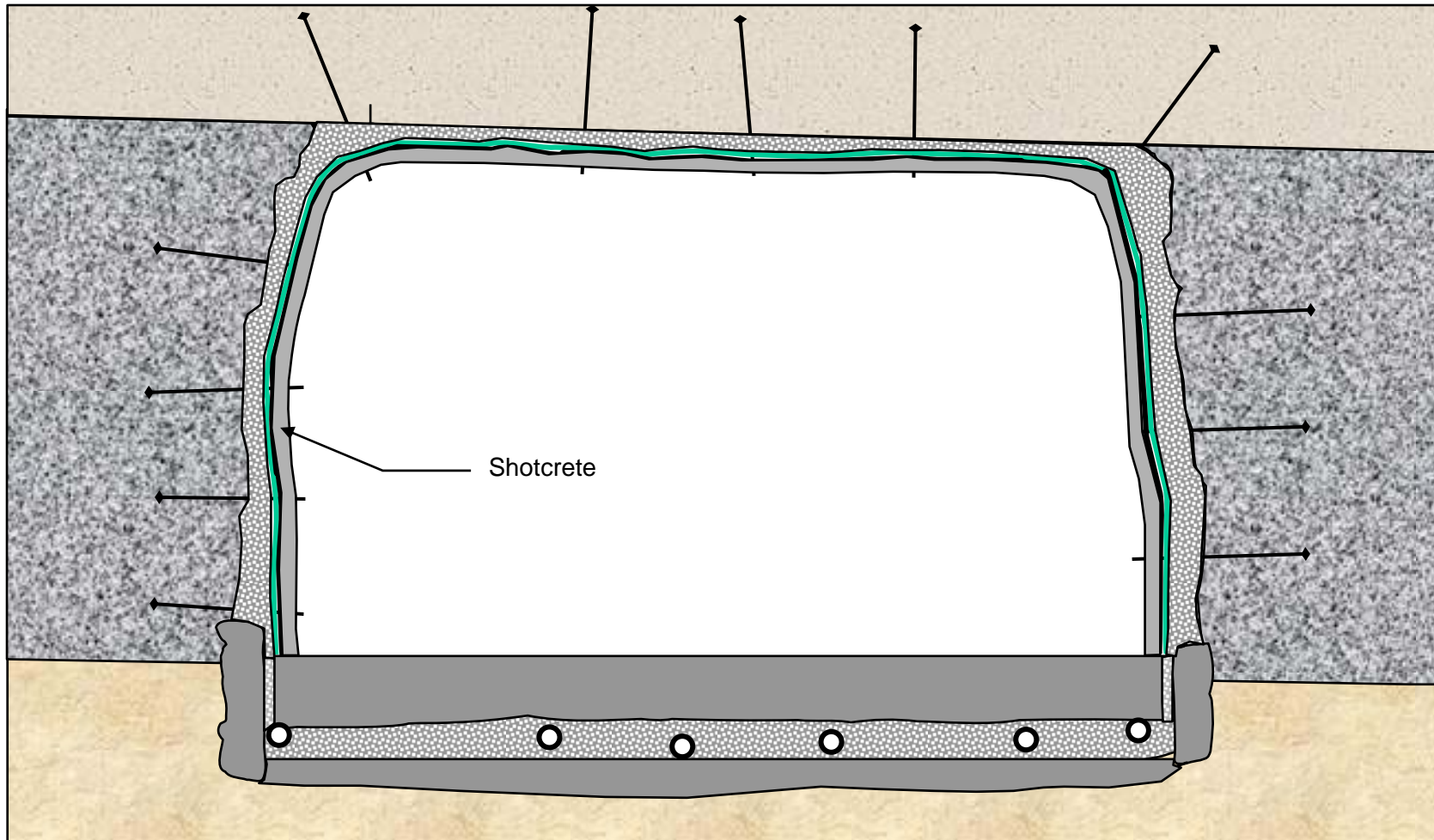
Installation of Gravel Layer



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Chamber Preparation

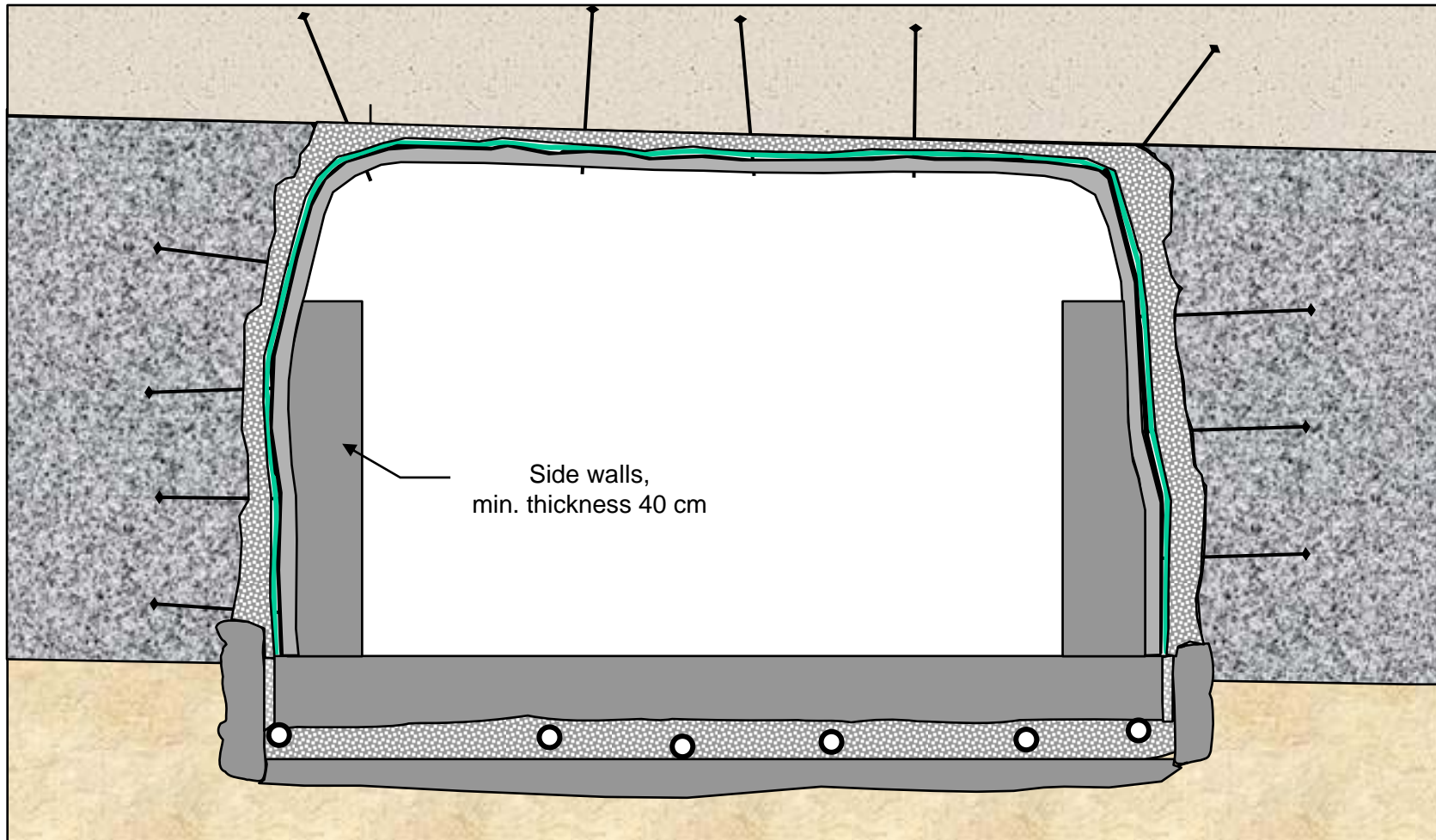
Application of Shotcrete Layer



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Chamber Preparation

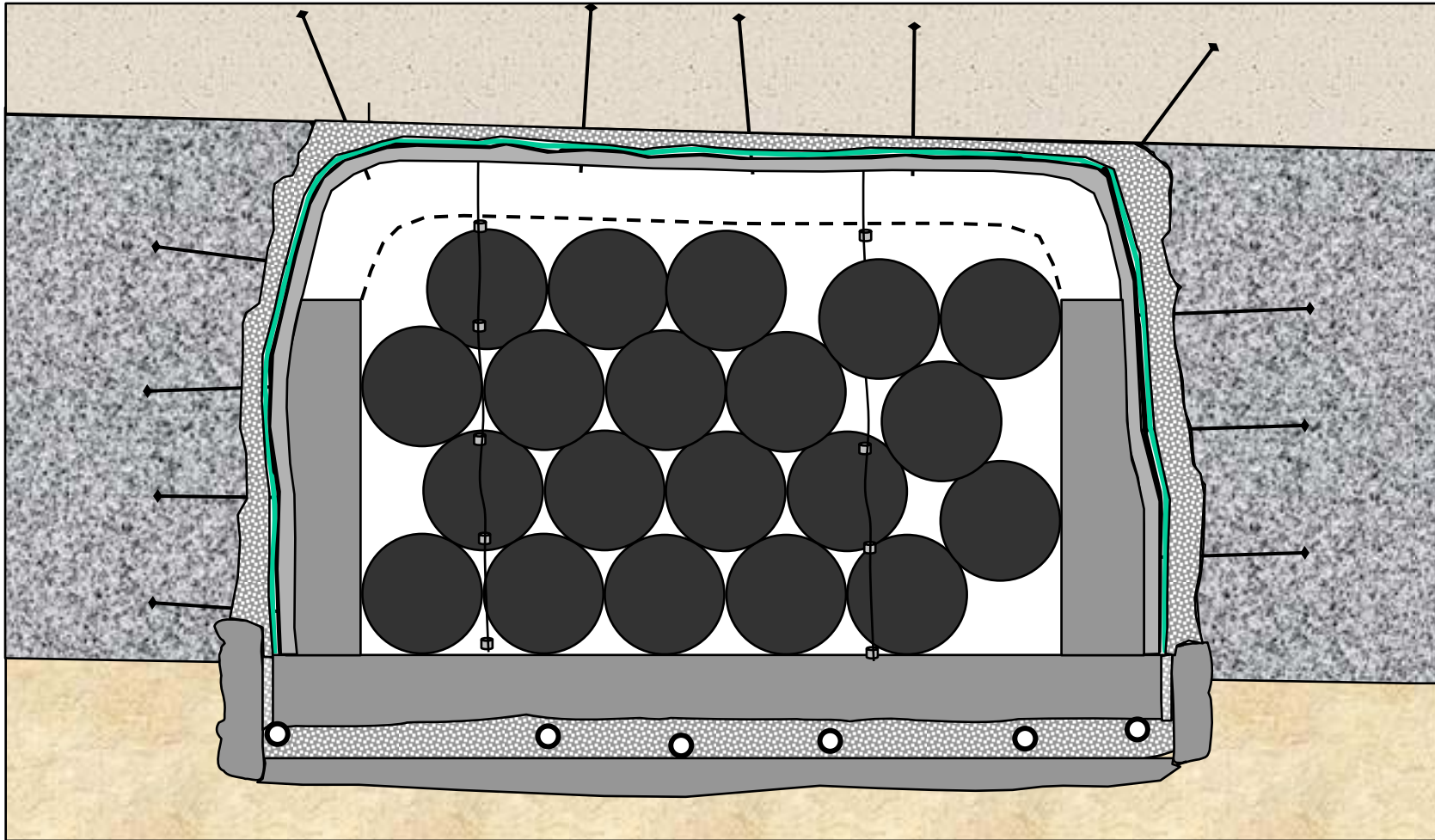
Preparation of Concrete Side Walls



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Disposal of Waste

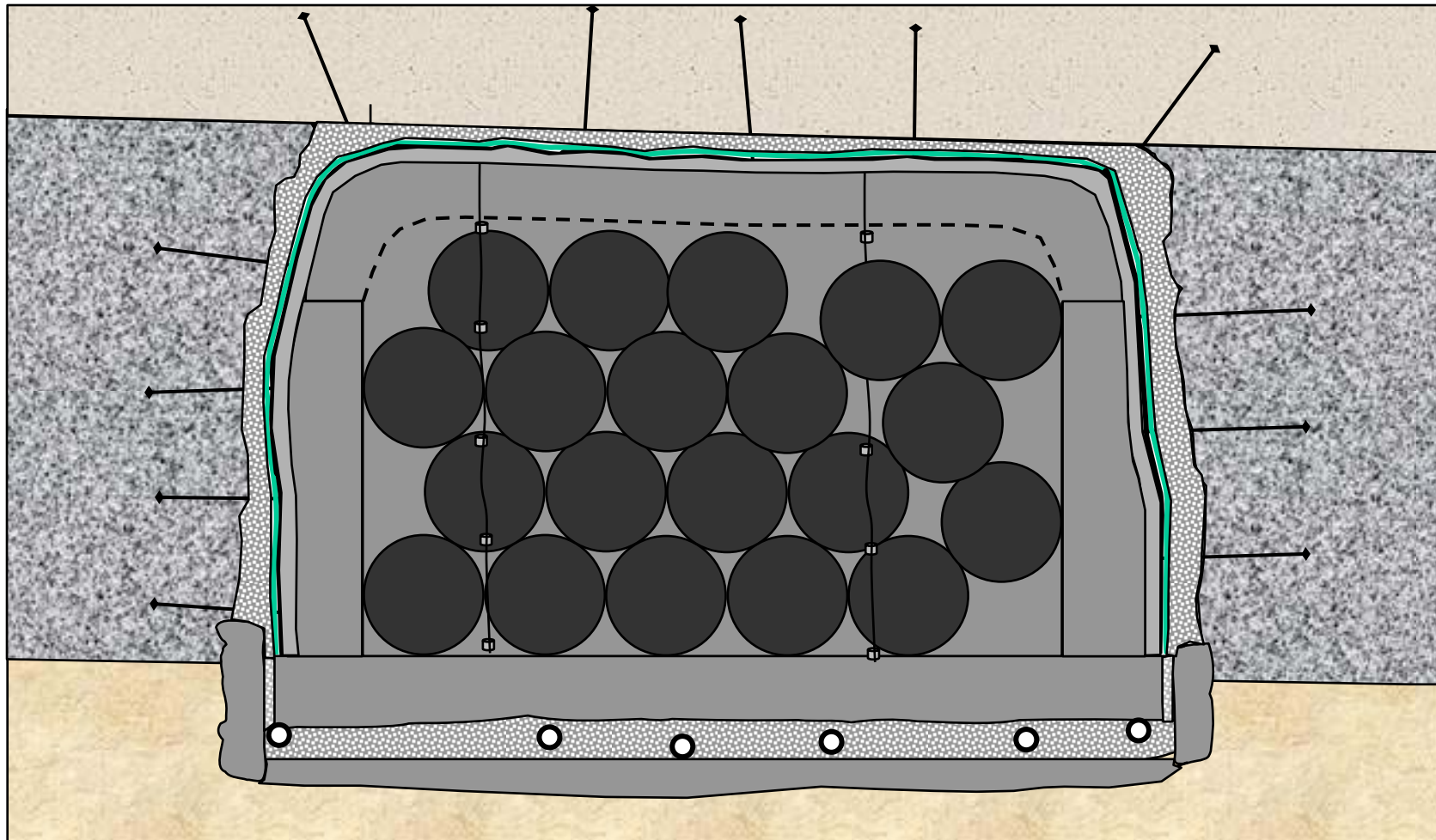
Disposal of Waste Drums



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Closure of Chamber

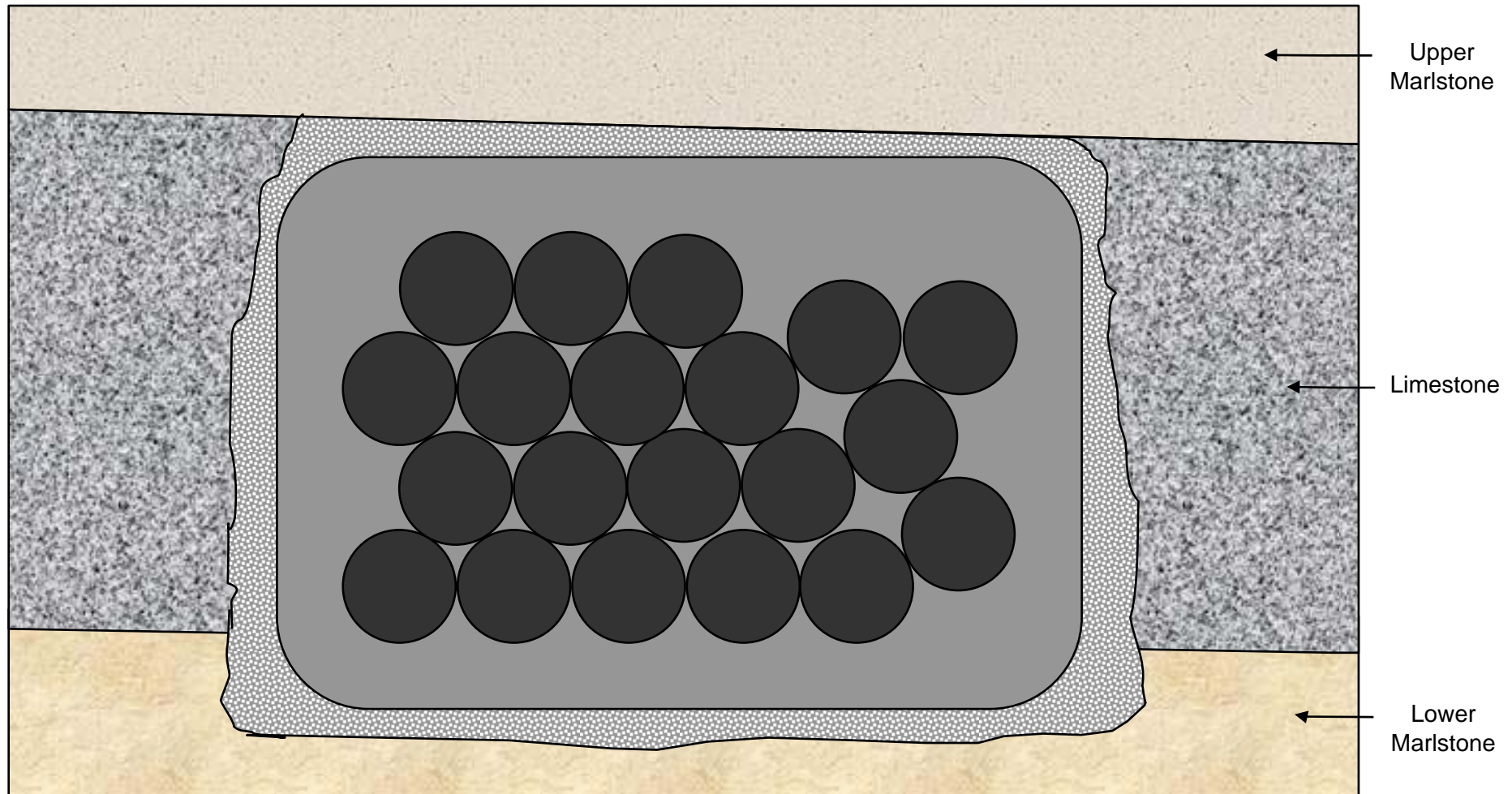
Situation after Backfilling



Chinese German Workshop, Beijing 2007

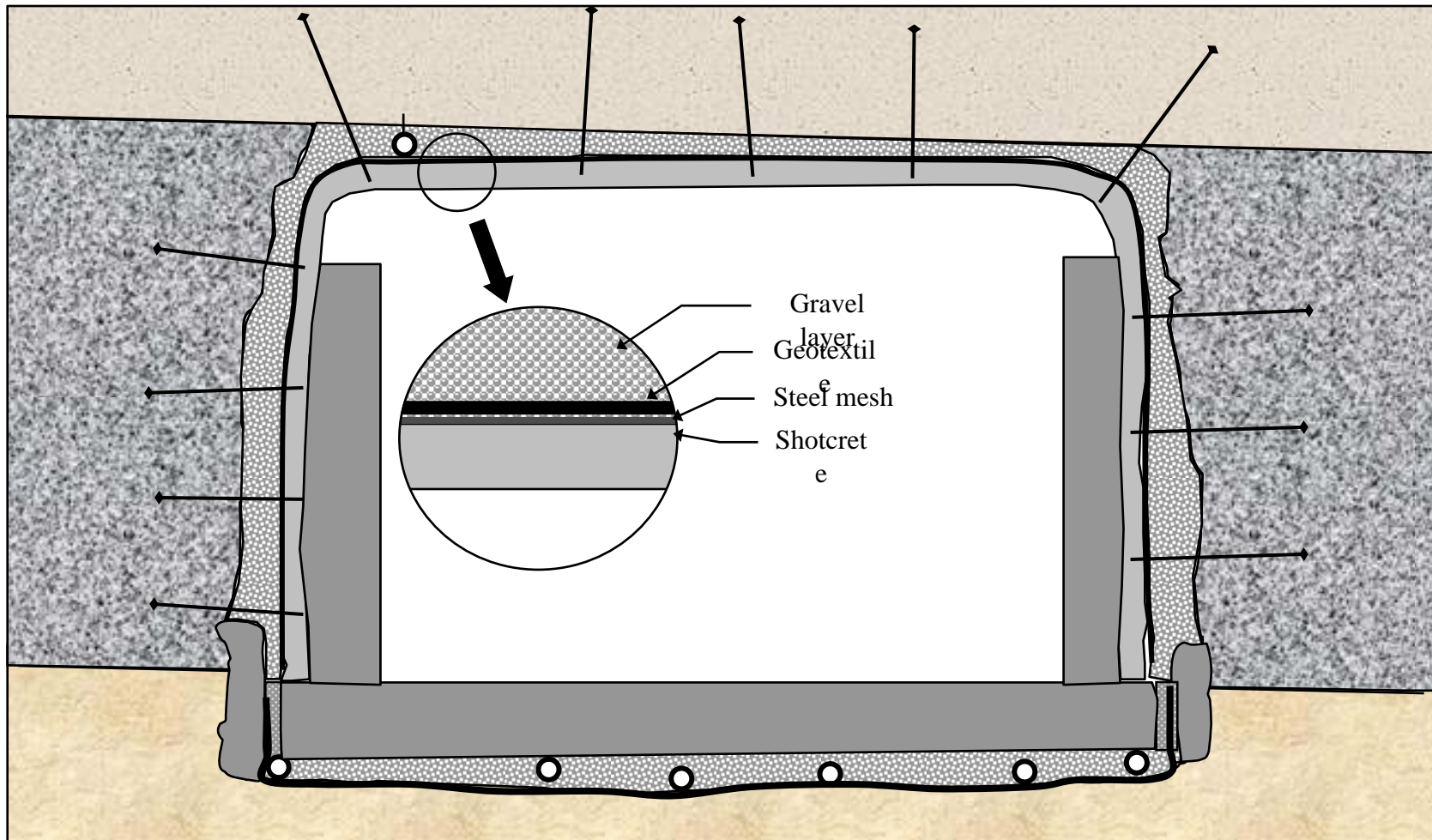
Closure of Chamber

Simplified Model of Situation after Backfilling



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Presentation TopSeal 2006, Olkiluoto



Chinese German Workshop, Beijing 2007

Presentation TopSeal 2006, Olkiluoto



Chinese German Workshop, Beijing 2007

Presentation TopSeal 2006, Olkiluoto



Chinese German Workshop, Beijing 2007

Monitoring and Modelling of Groundwater Parameters as a Basis for Radionuclide Transport Modelling

Wernt Brewitz

GRS – Final Repository Research Division
Technical University of Braunschweig

Sino-German Workshop
Beijing, May 28 – June 1, 2007

The importance of groundwater in radwaste disposal

- Water / groundwater is a source of life
- Water has to be protected in order to ensure an adequate living standard for present and future generations
- Groundwater reacts with the waste and can mobilize radionuclides in the repository
- Groundwater is the medium for transporting contaminants from the deep repository to the biosphere
- Groundwater can disperse contaminants in the entire system
- Groundwater quality has a direct impact on the quality of food and stocks and on the health of mankind

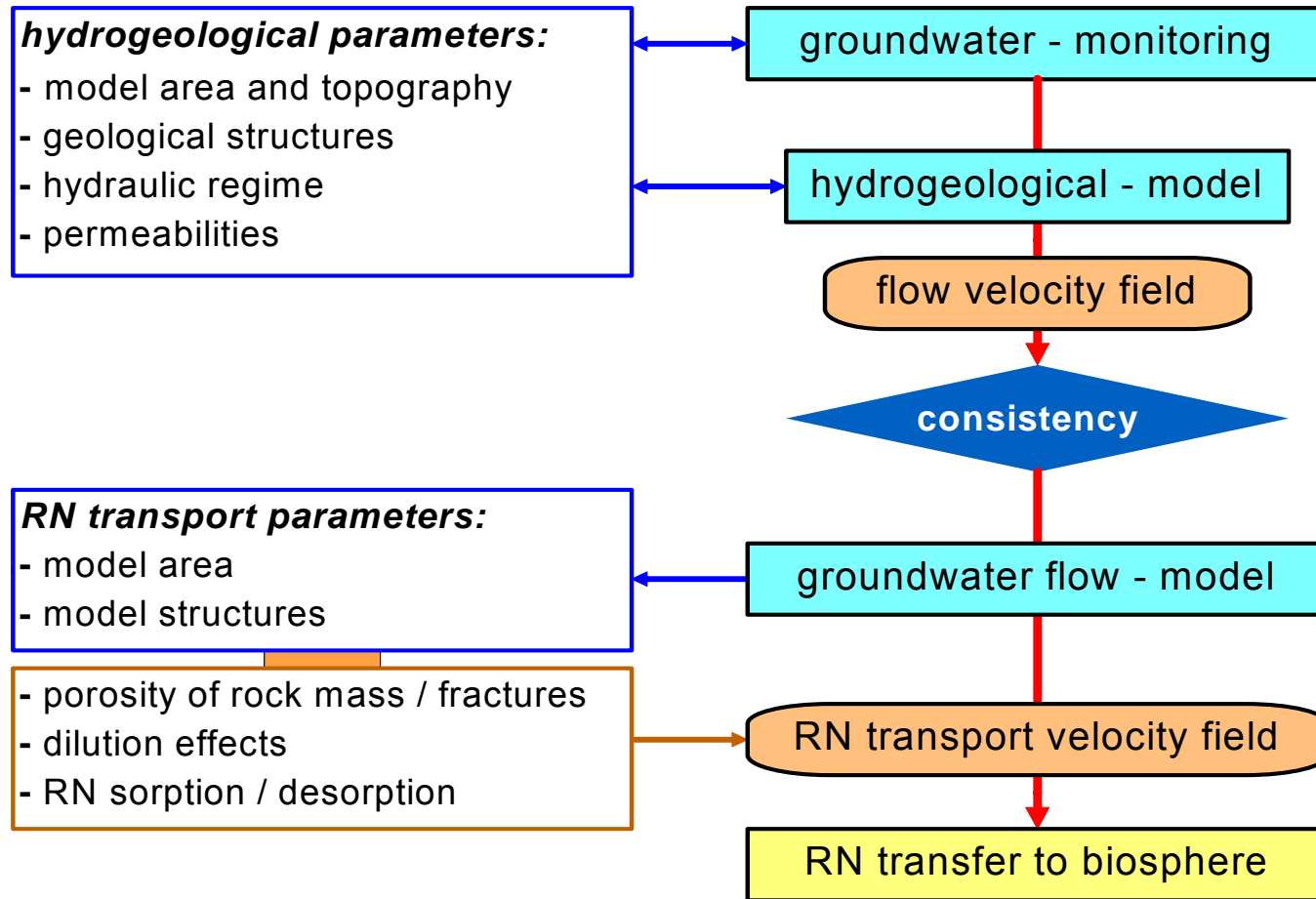
The feasibility of a disposal site depends predominantly on the hydrogeology

- Any disposal site has to be characterised in detail for its hydrogeological system and properties before construction
- Flow velocity and groundwater age of each aquifer are important for the classification of the groundwater regime
- By numerical modelling it has to be demonstrated that all governing parameters and their interactions are well understood
- On the basis of hydrogeological models the radionuclide transport by groundwater has to be simulated for extended periods of time
- The hydraulic regime has to be monitored during construction and operation in order to check the model parameters

Hydrological modelling and understanding of the geological processes are important for the safety case

- For any High Level radioactive waste repository the **normal evolution** has to be assessed for about 10^4 to 10^6 years. **Load cases** as well as **scenarios** have to be taken into account.
- For **tight and dry** rock formations (**rock salt**) the durability of the geological barrier is of utmost importance. Barrier failure and possible consequences are essential for any performance assessment.
- In **tight and slightly moist** rock formations (**clay, indurated claystone**) diffusion is the most relevant transport process. Fracturing might occur, fracture flow is often suppressed by swelling of clay minerals.
- In **hard rock** formations (**granite, basalt, tuff**) fracturing is very common. Advective flow in fracture networks is very site specific and has to be investigated and modelled in detail. Mineral fillings in fractures might contribute substantially to the retardation of radionuclides.

Stylized approach in RN transport modelling



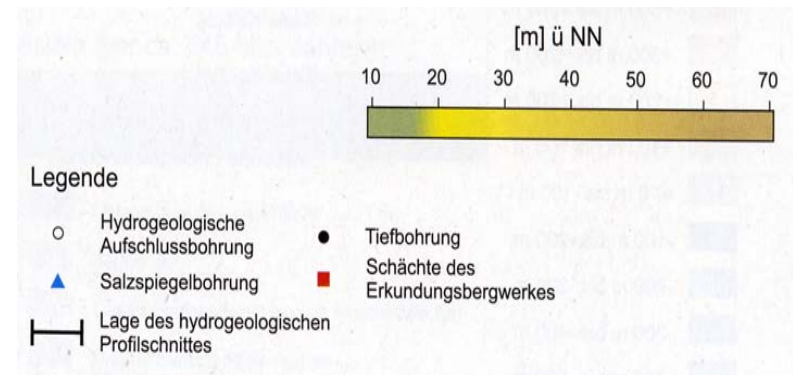
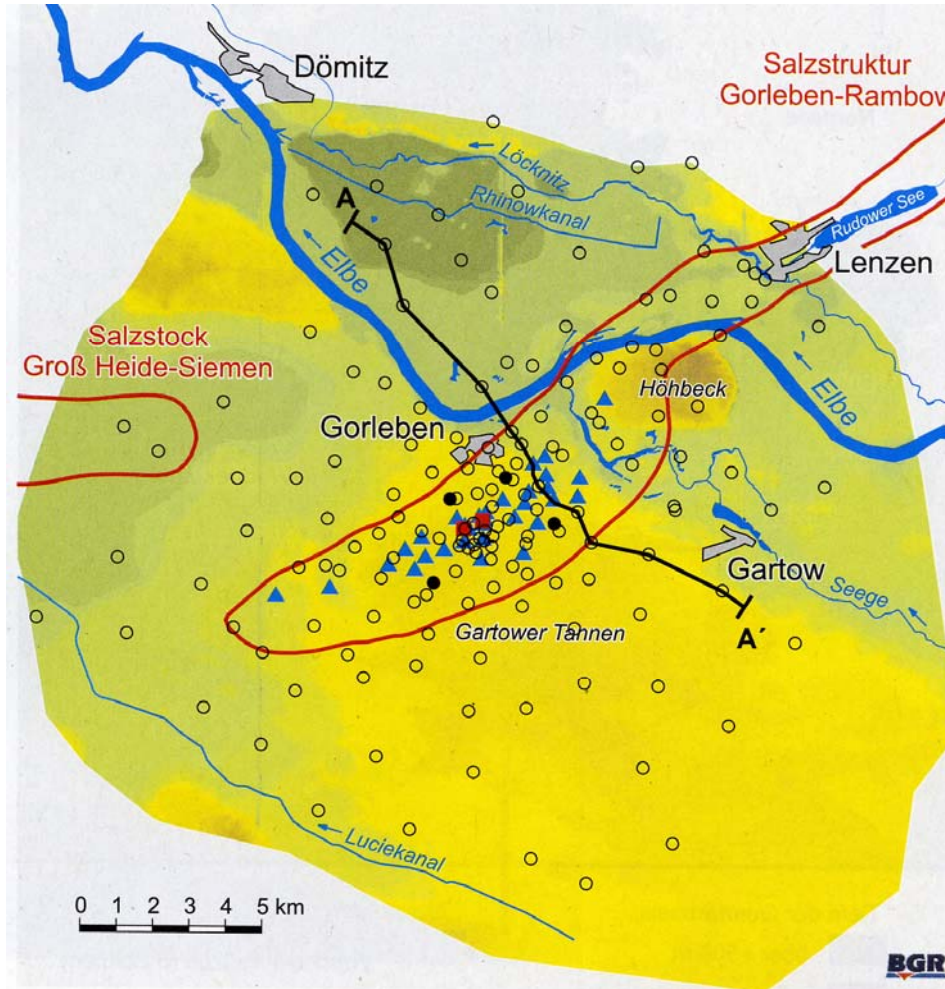
Groundwater monitoring

Groundwater regime in Tertiary and Quaternary Sediments

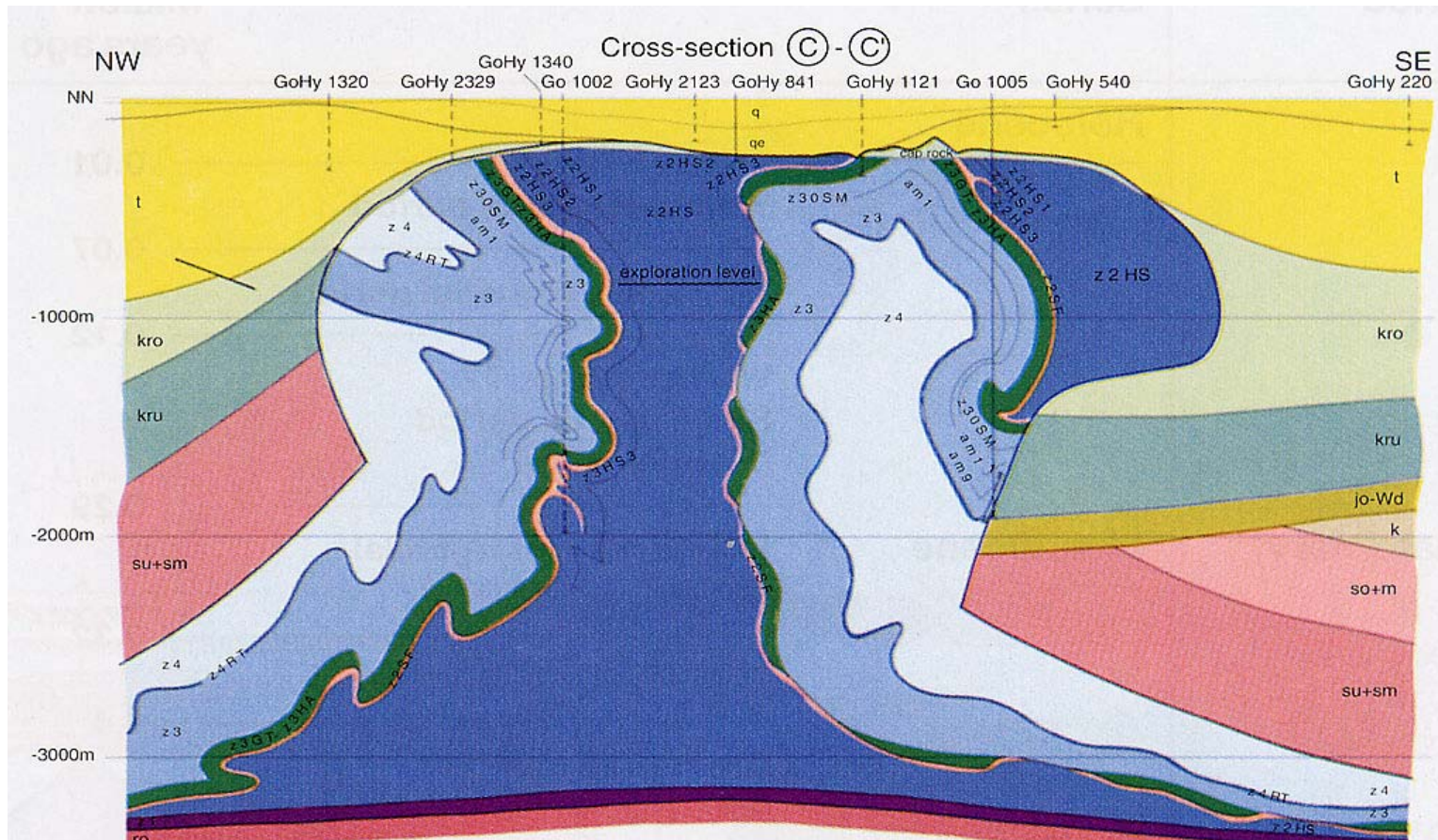
Measurements at the Gorleben site performed by BGR

Modelling and interpretation of flow and age by BGR

Hydrogeological Characterisation of the Gorleben Site (Groundwater Monitoring)

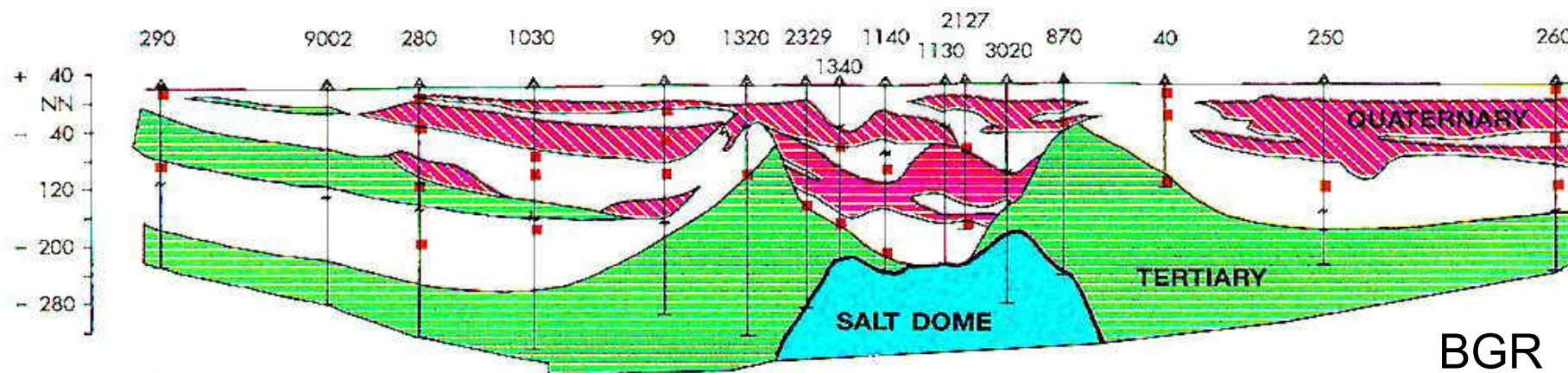
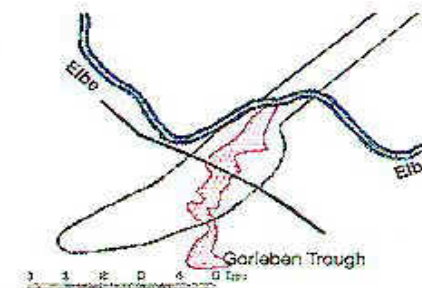
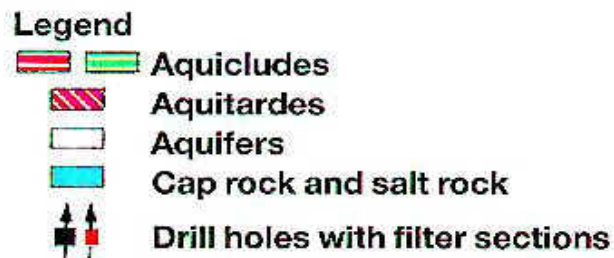


Salt dome Gorleben with overlying Quaternary and Tertiary Sediments



BGR

Aquifers and aquicludes in the covering rock formations



BGR

Groundwater salinity rises with depth

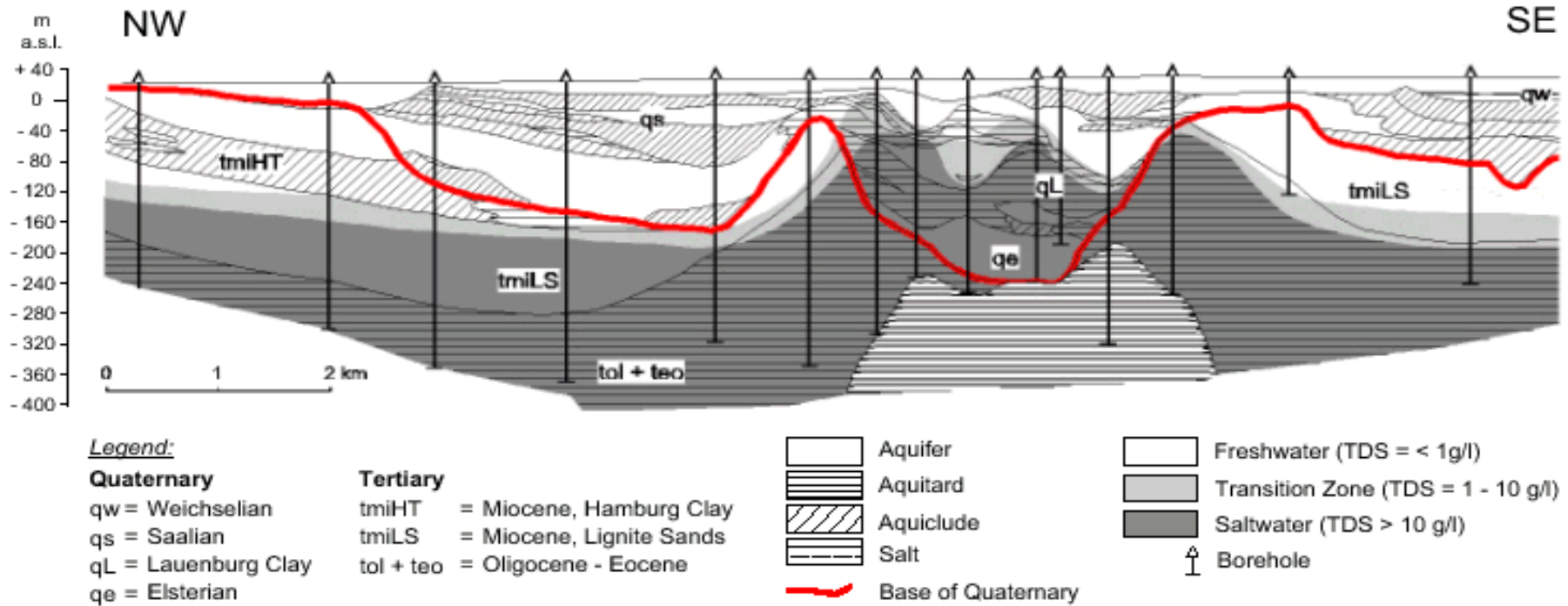
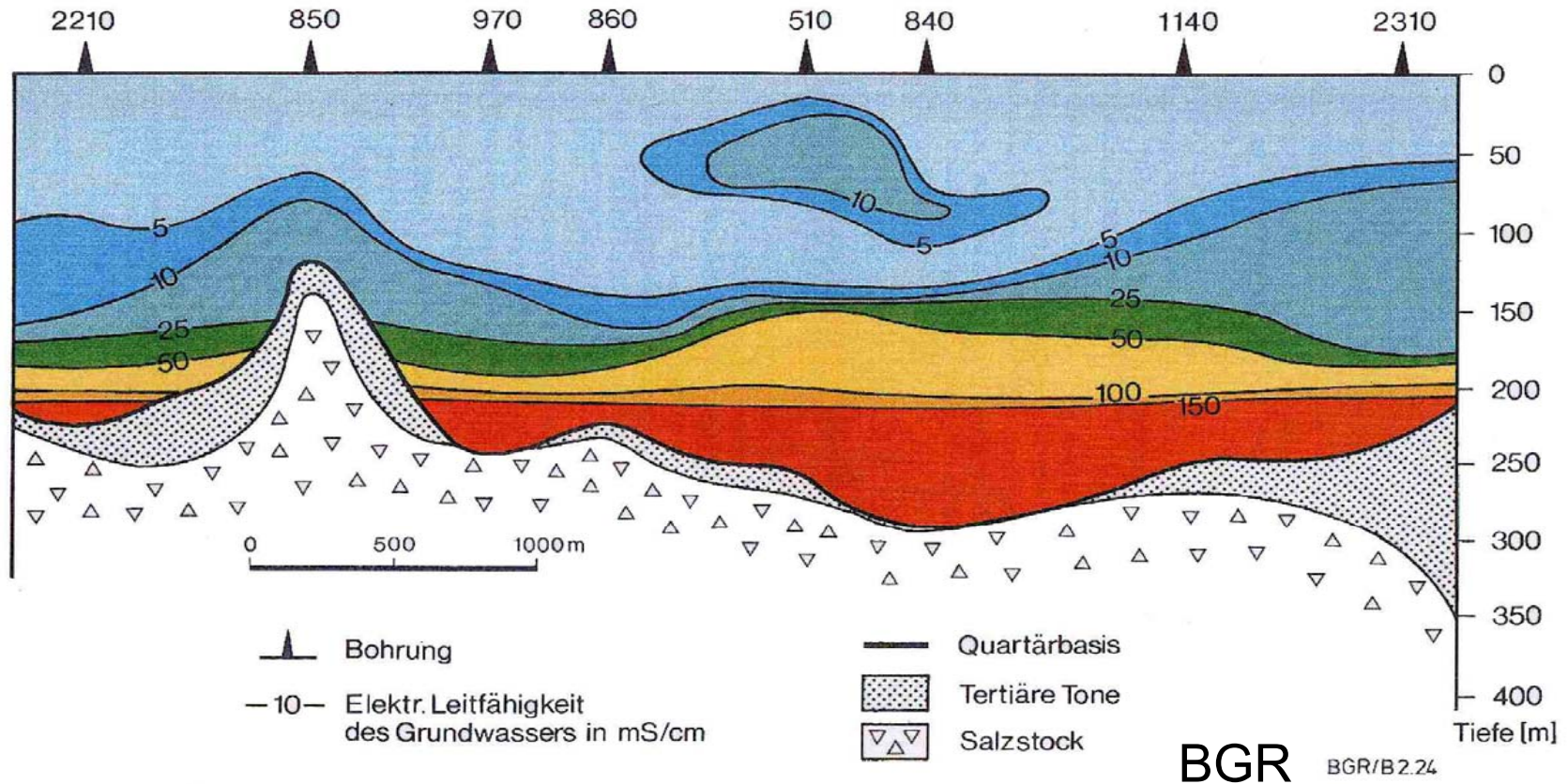
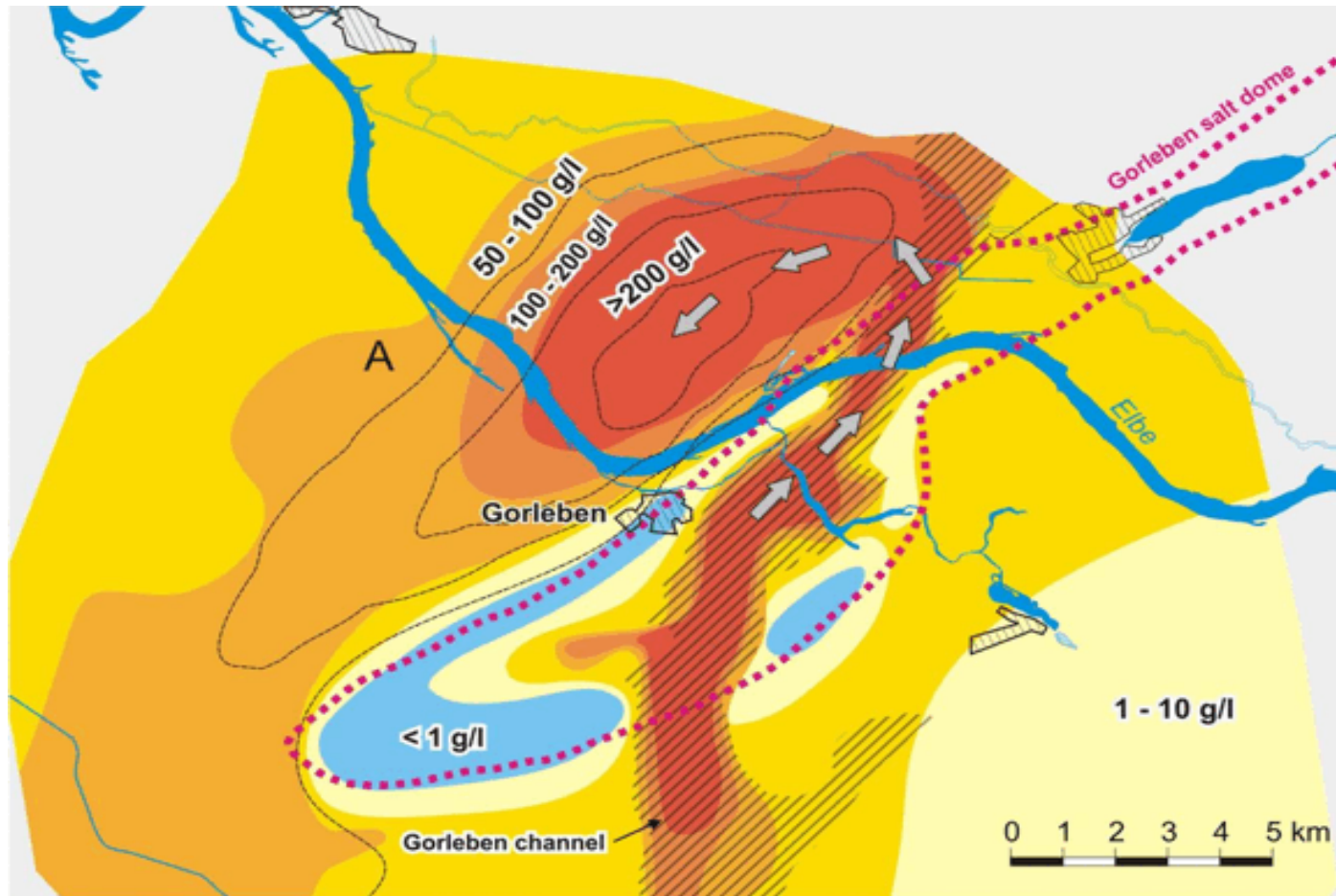


Figure 6: Hydrogeological and hydrochemical cross section along the buried channel at Gorleben (TDS = Total dissolved solids)

Residual groundwater disturbance - imprints of the last ice age



Groundwater regime in the Quaternary channel



BGR

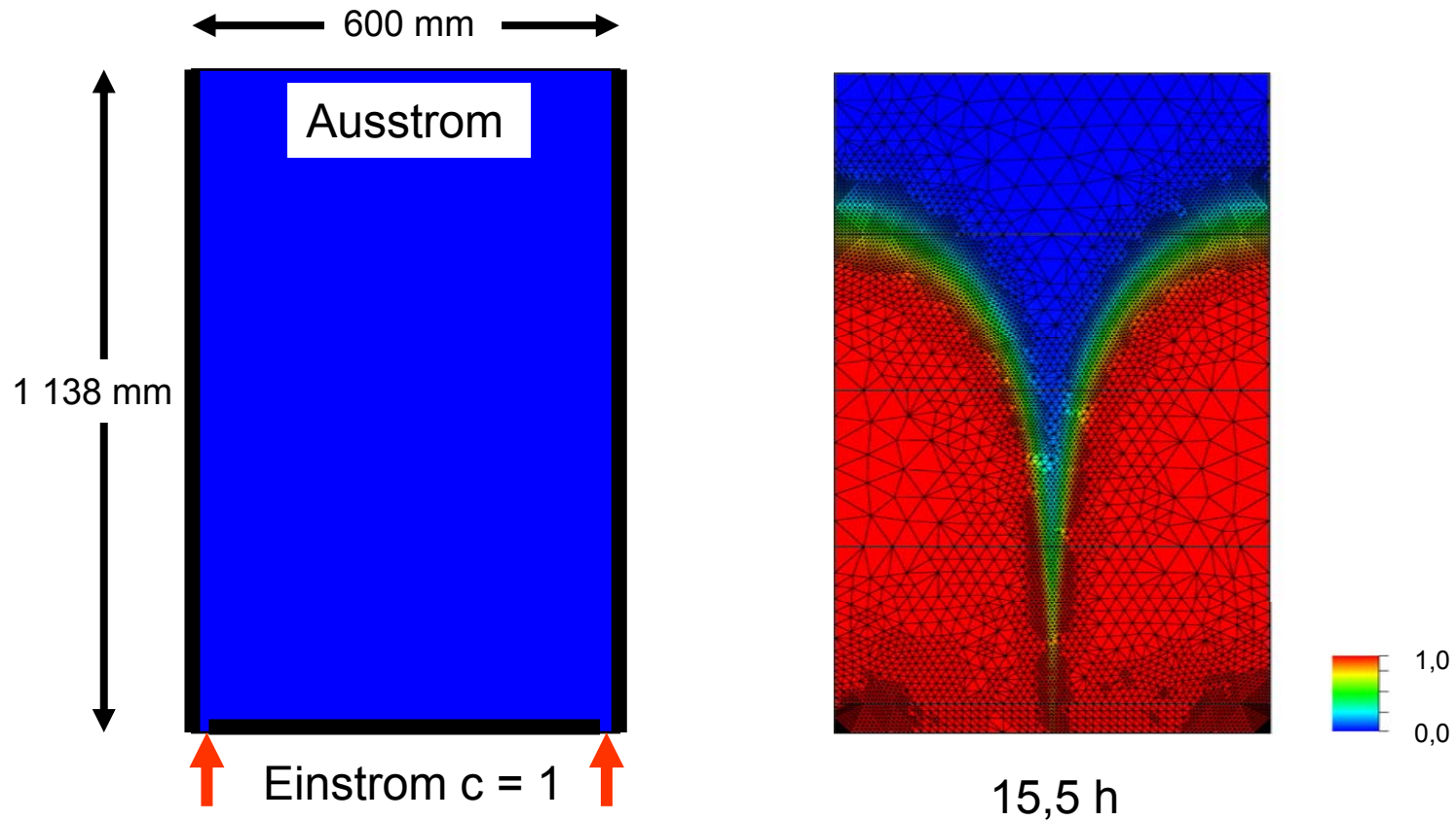
Development of computer programs for 3D simulation of density driven flow and radionuclide transport in complex hydrogeological systems

Basics of program development

Test cases

Simulations

Lab experiment: Fresh water / salt water displacement (RIVM)



PA Codes developed and applied in Germany

- **EMOS group of codes (GRS):**
Near-, Far-Field, Biosphere-Model

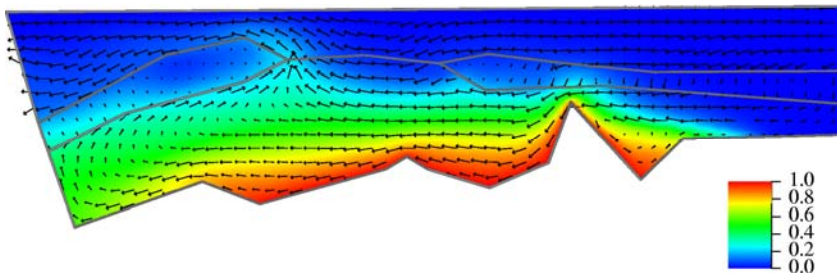
output => breakthrough curves of radionuclides

programs in testing stage
for porous media:

- **d³f**: groundwater flow model
- **r³t**: contaminant transport model

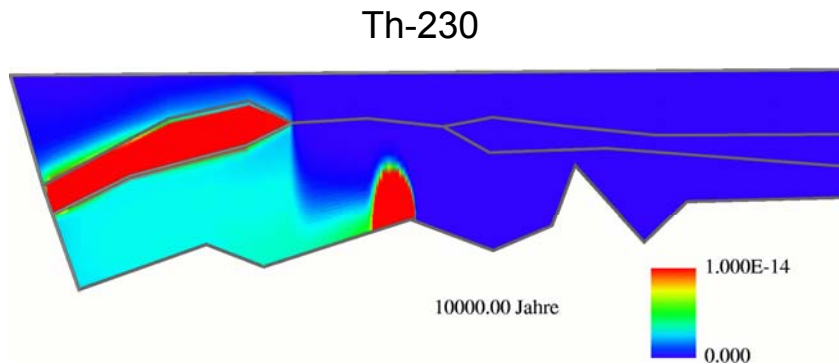
- radionuclide decay
- element dependent sorption
- kinetically controlled sorption
- diffusion in immobile porewater
- precipitation
- complexation
- formation of colloids

Distributed Density-Driven Flow: d^3f



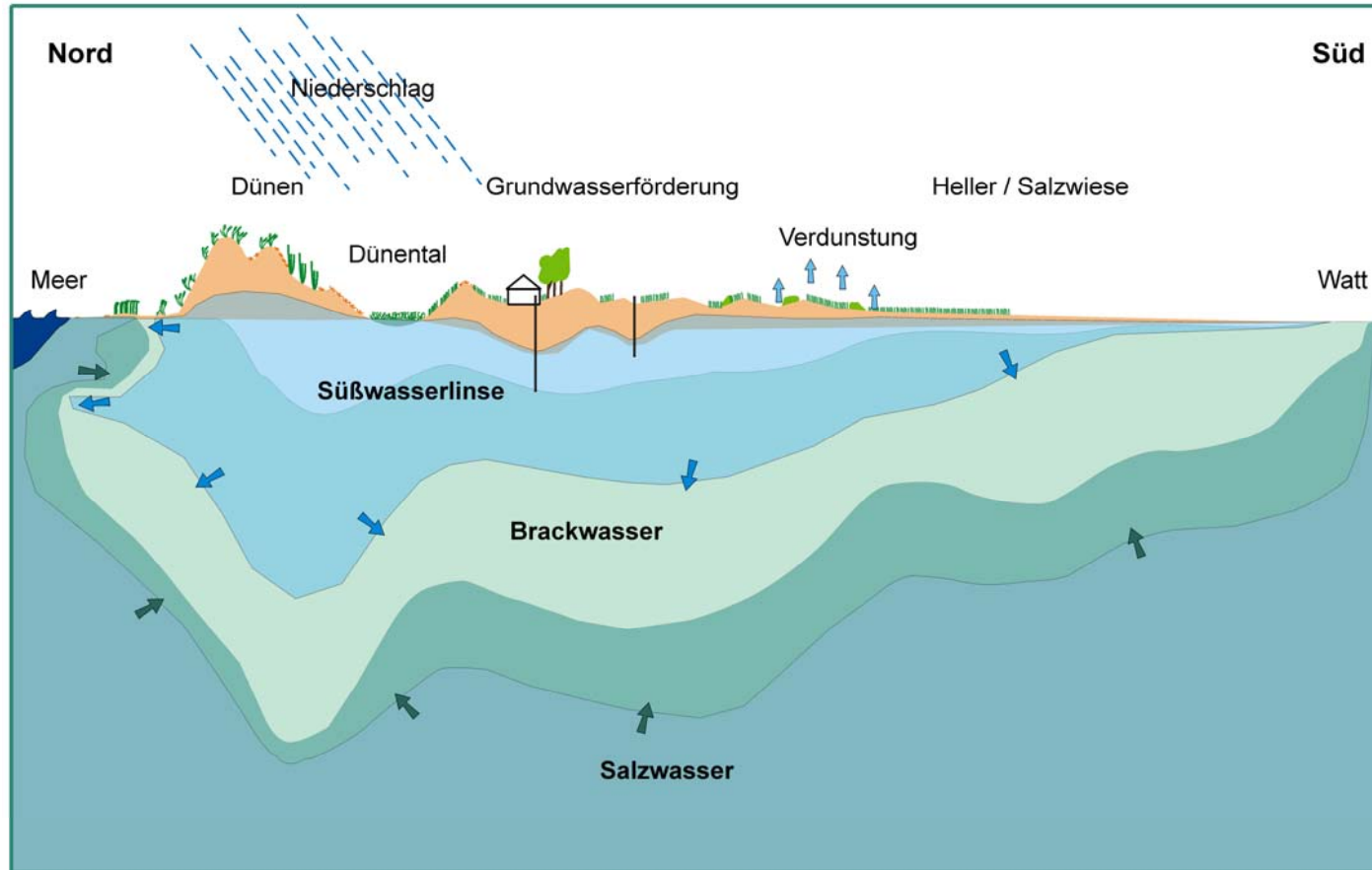
- finite volume discretisation
- spatial and temporal adaptivity controlled by a-posteriori error estimator
- multigrid solver
- completely parallelised
- flow through porous, fluid-saturated, heterogeneous, anisotropic media
- confined aquifer systems
- transient transport of salt (or heat)
- constitutive equation for density and viscosity dependent on concentration (or temperature)
- stochastic modelling

Radionuclide, Reaction, Retardation, and Transport: r^3t

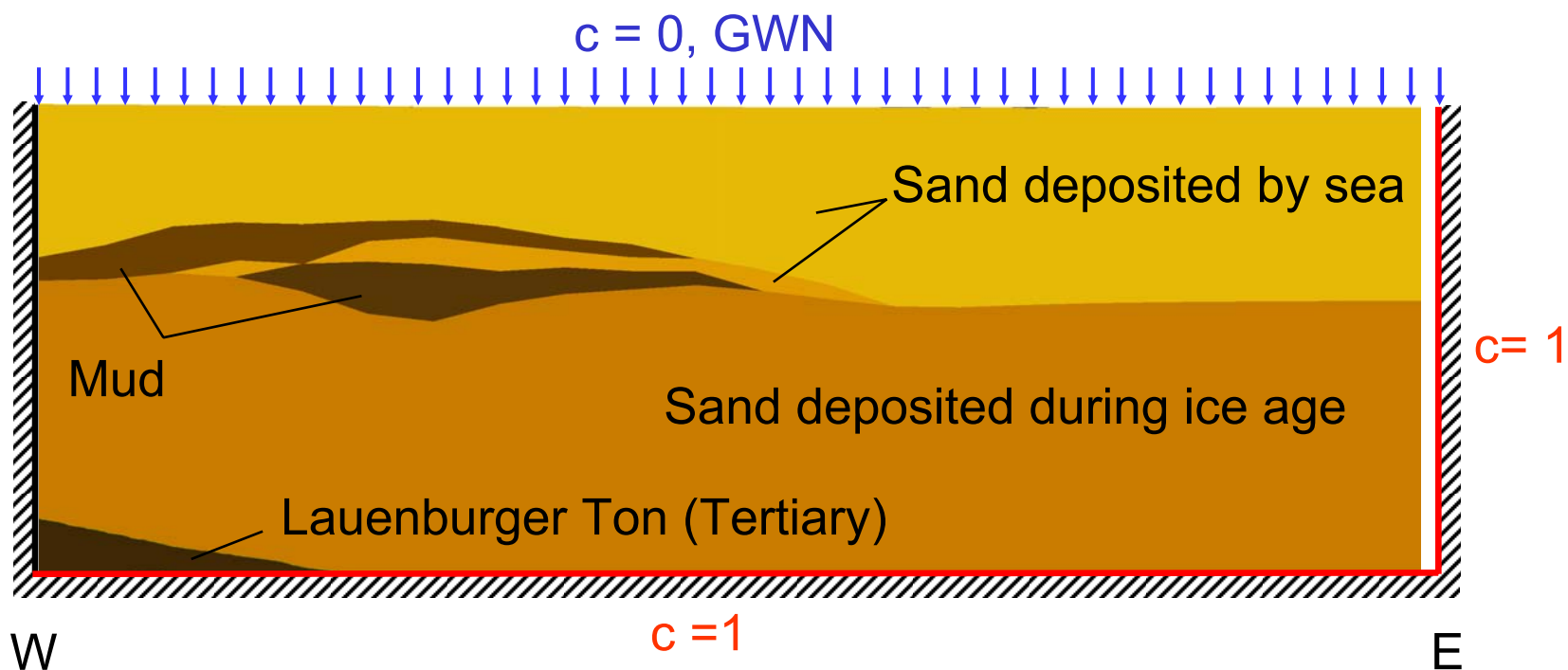


- transport through porous media
 - radioactive decay (chains)
 - linear and nonlinear sorption (equilibrium, kinetically controlled)
 - precipitation / dissolution
 - complexation
 - diffusion into immobile porewater
 - no speciation
- finite volume discretisation
 - spatial and temporal adaptivity controlled by a-posteriori error estimator
 - multigrid solver
 - completely parallelised

Sea water intrusion model into a fresh water aquifer

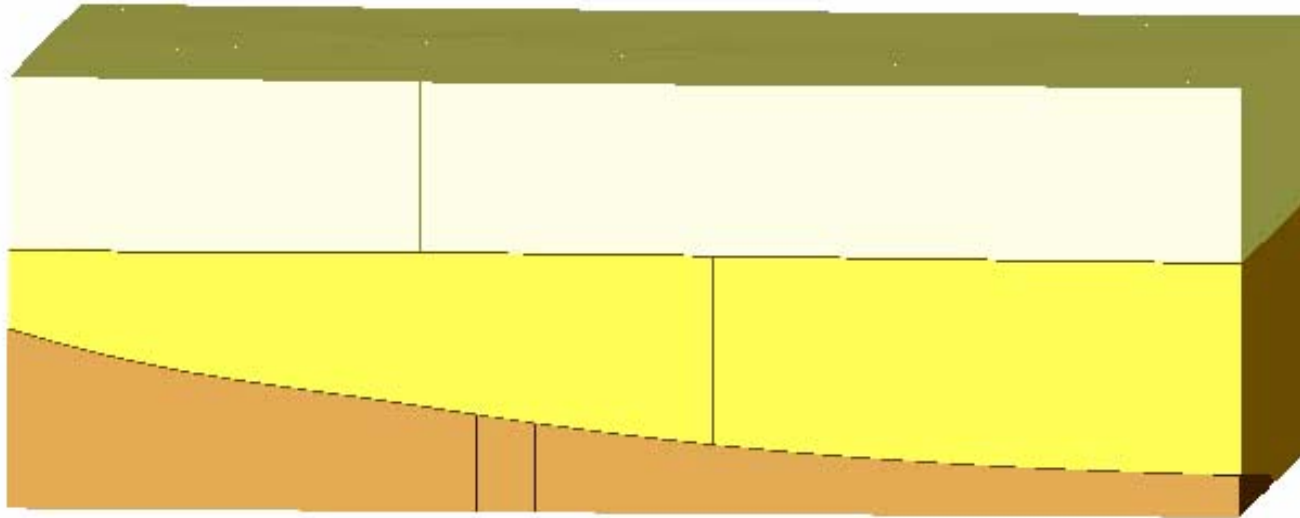


Conceptual hydrogeological model

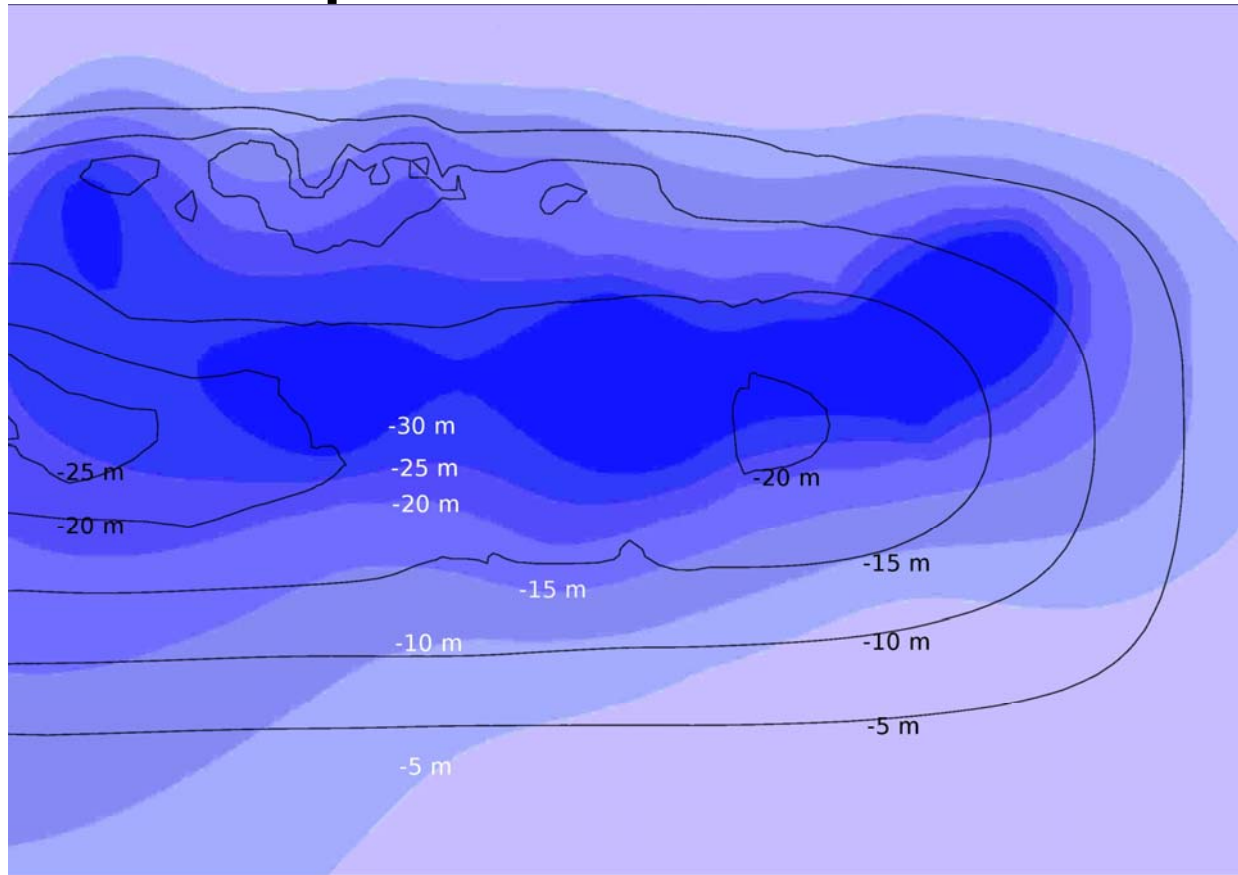


north- und south boundary: $c = 1$ (Seawater), hydrostatic pressure

Drinking water boundary (calculated) $C_{TW} = 1,0 \text{ g TDS / l}$



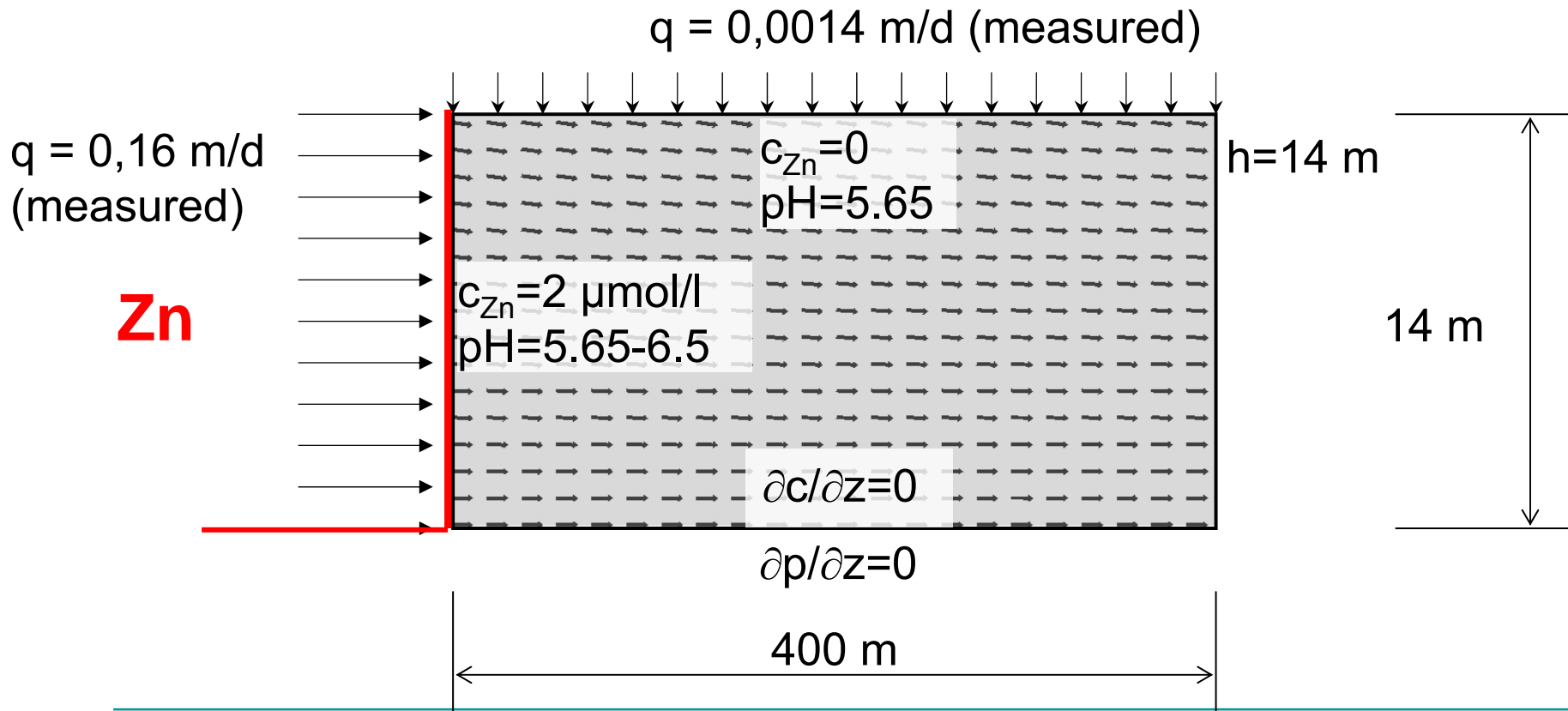
Drinking water boundary development: comparison measurement vs d³f-simulation



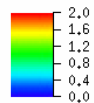
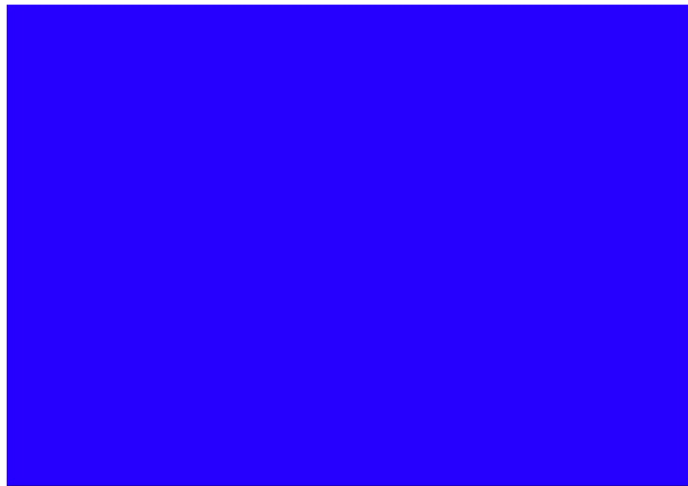
**Geoelectric survey
(blue)**

d³f (black)

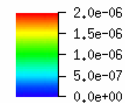
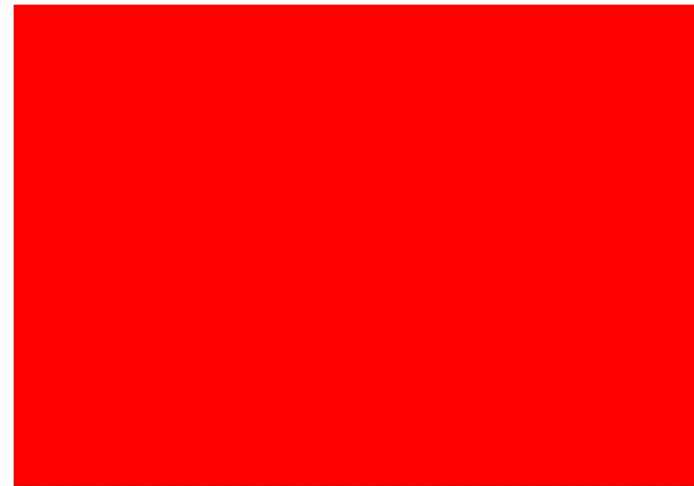
Flow / Transport model Cape Cod (USA)



Changing Zn concentration and pH value with time



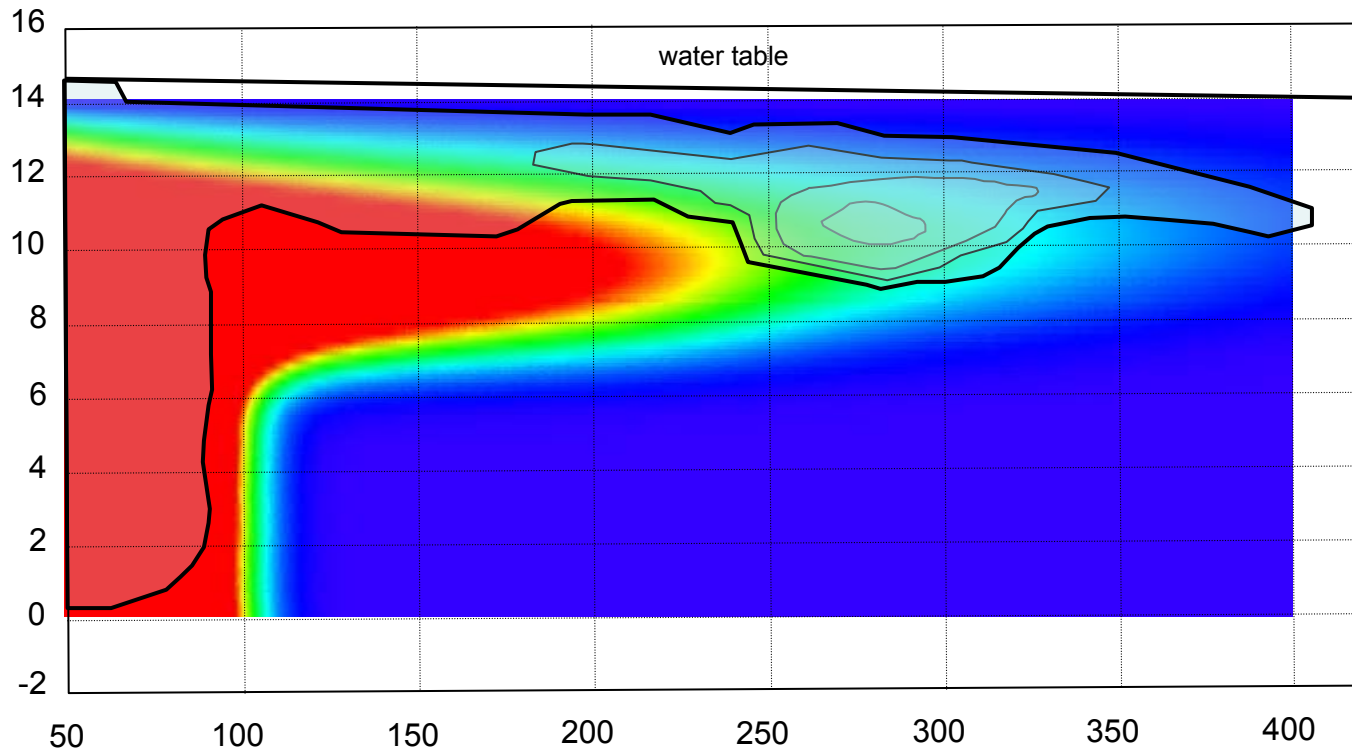
0.0 years



0.0 years

Start Animation

Comparison of results: r³t - simulation / field data

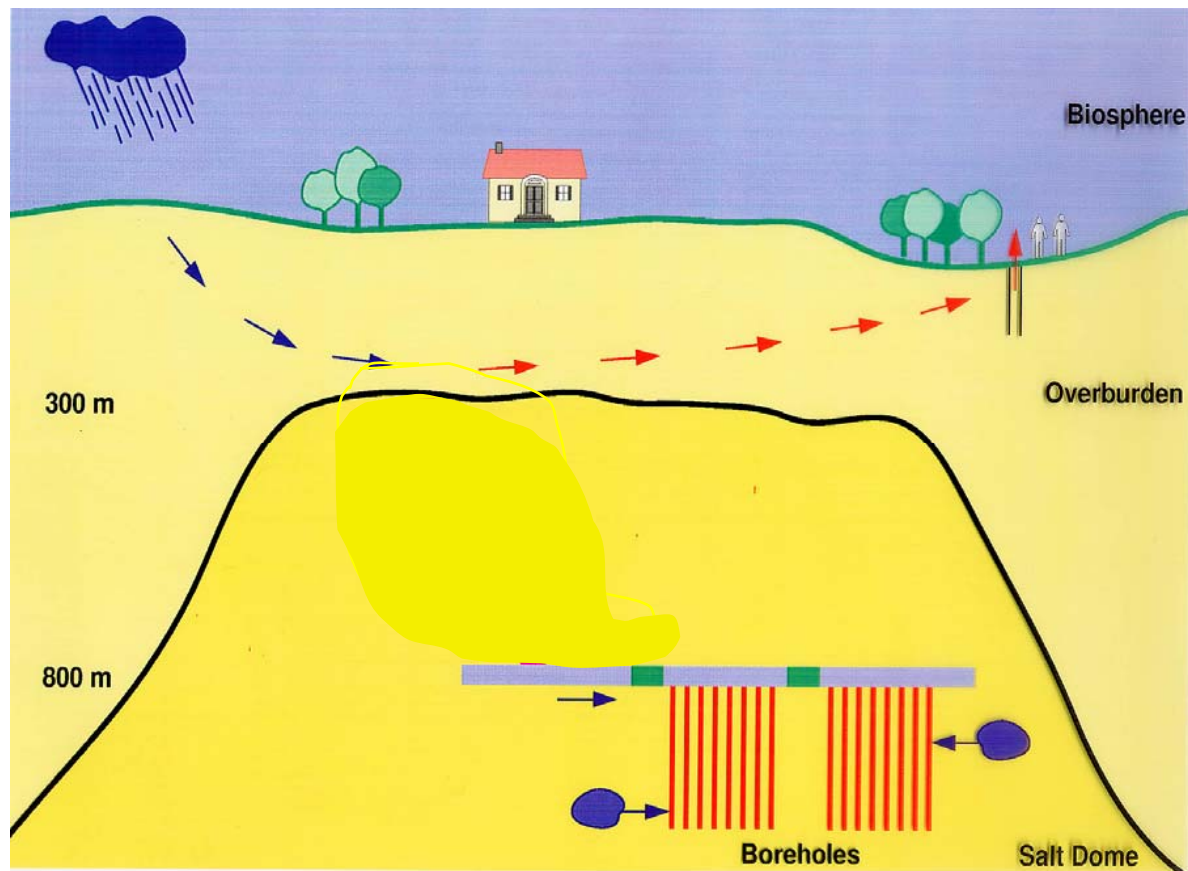


Zn concentration in aquifer after 61 years

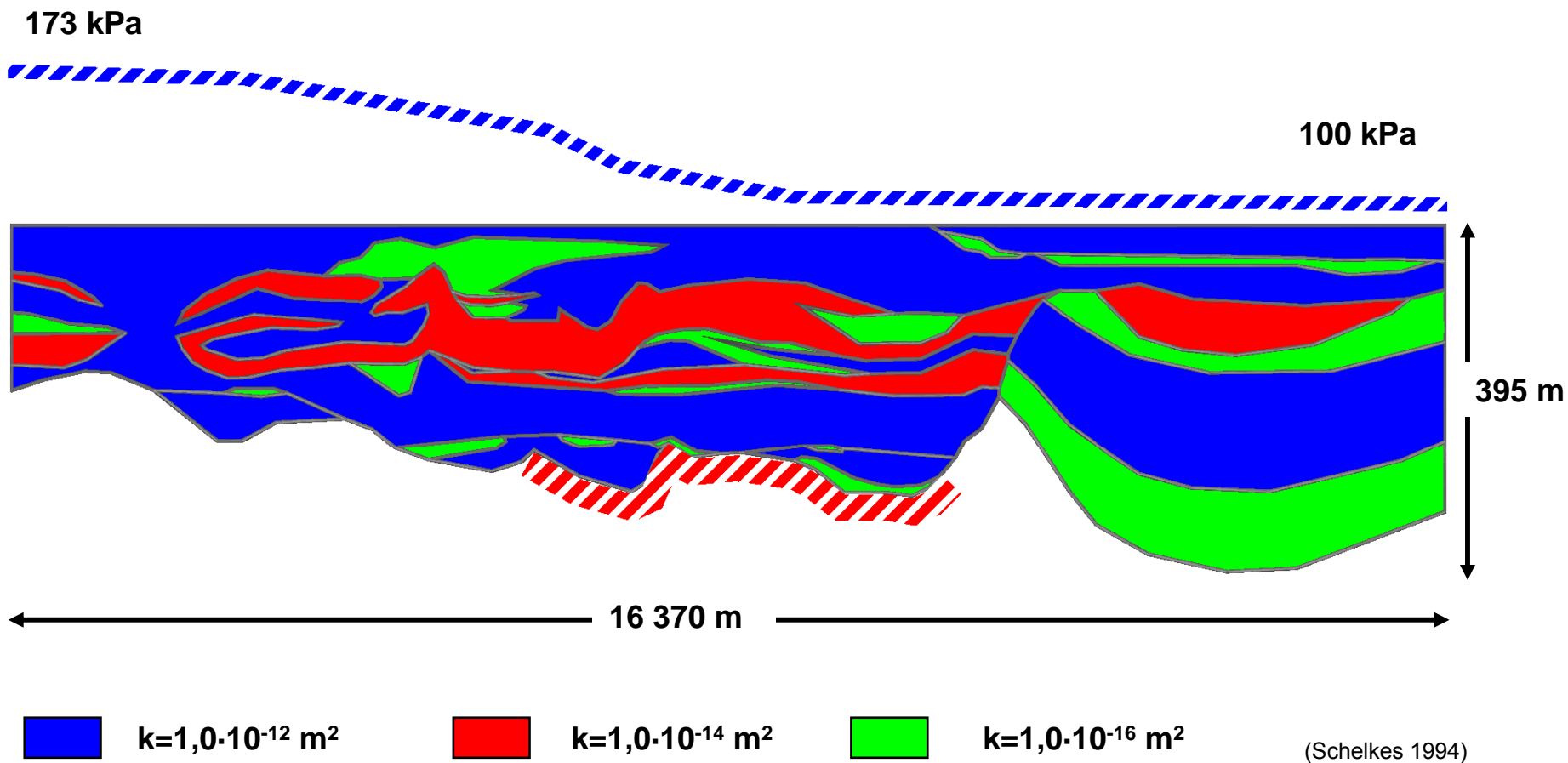
Radionuclide transport in Tertiary and Quaternary sediments

The Gorleben case

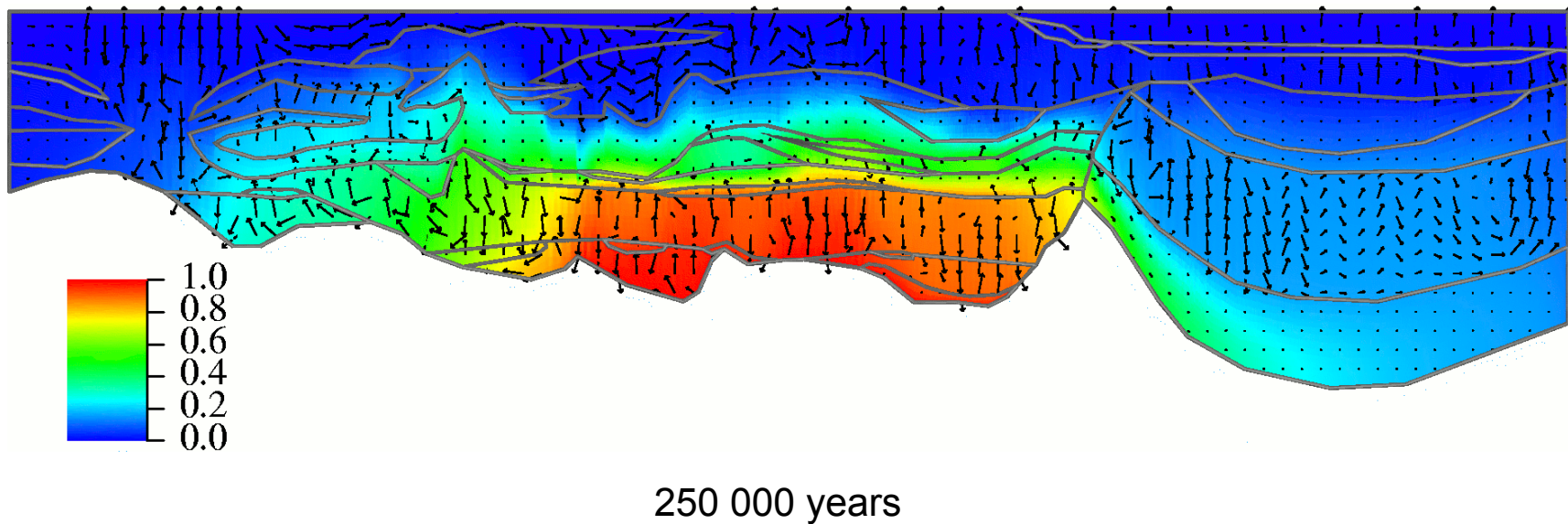
Worst case scenario of brine intrusion into the repository



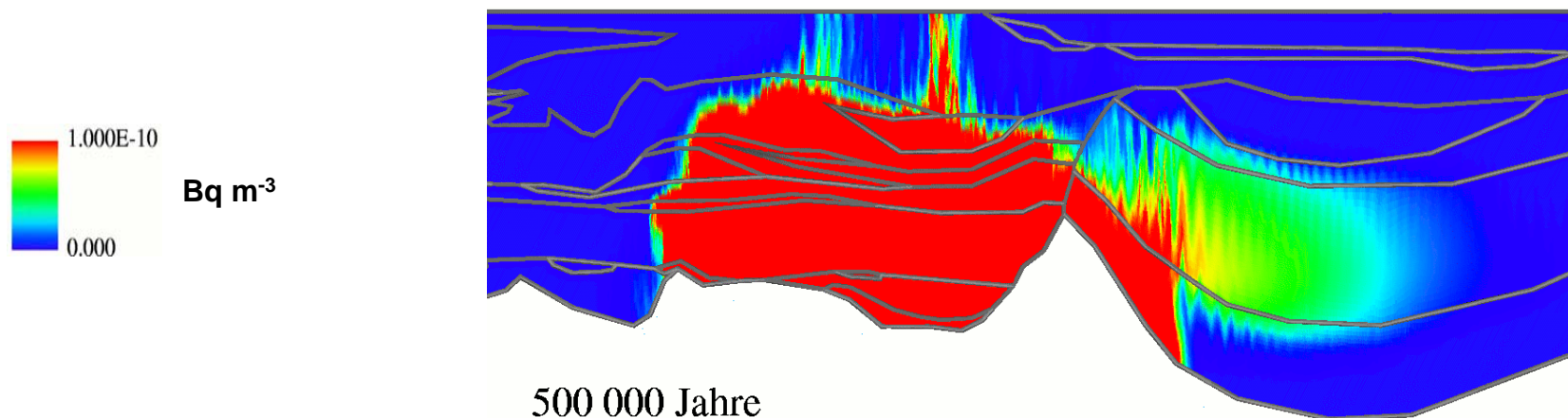
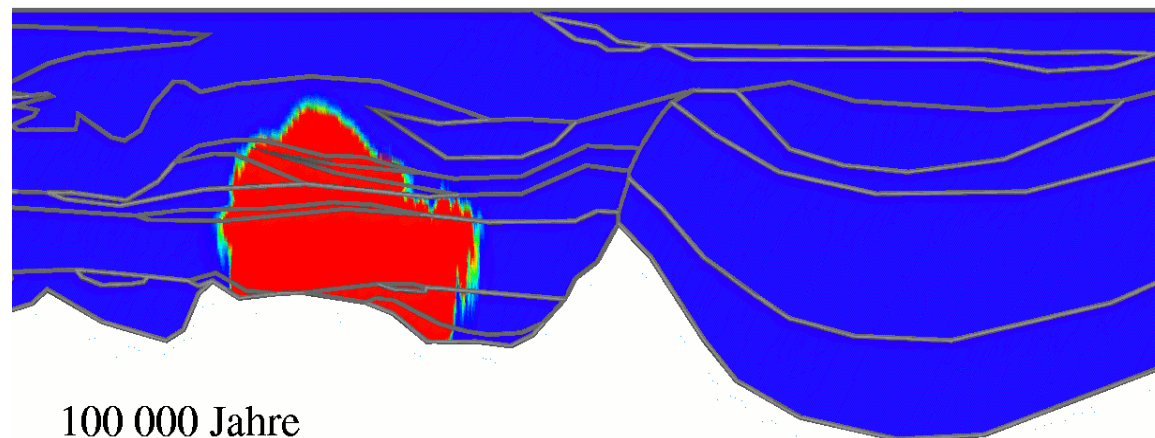
Hydrogeological model Gorleben



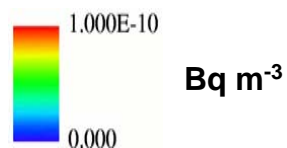
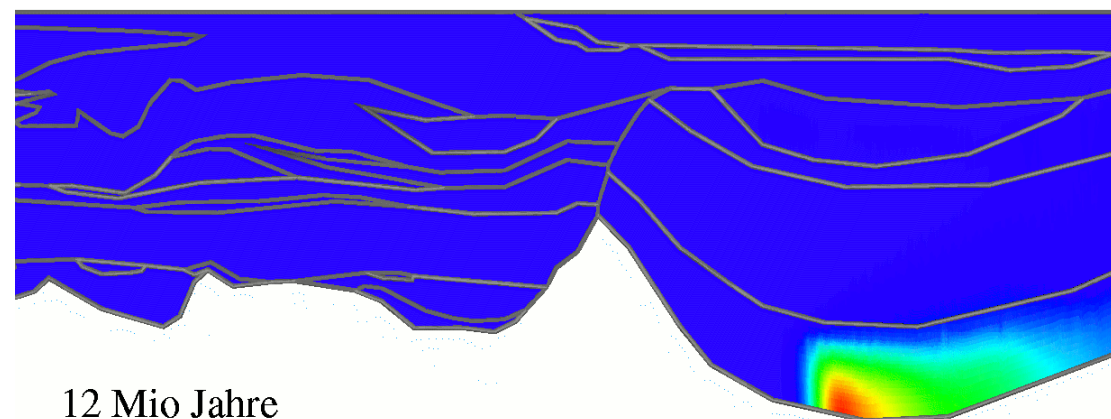
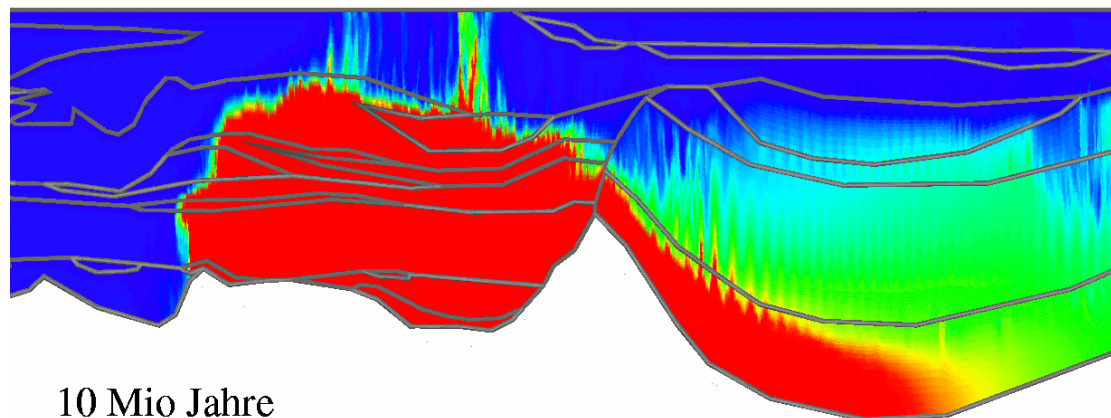
Advective flow and change of density by dissolved salt in the covering formations of the Gorleben salt dome

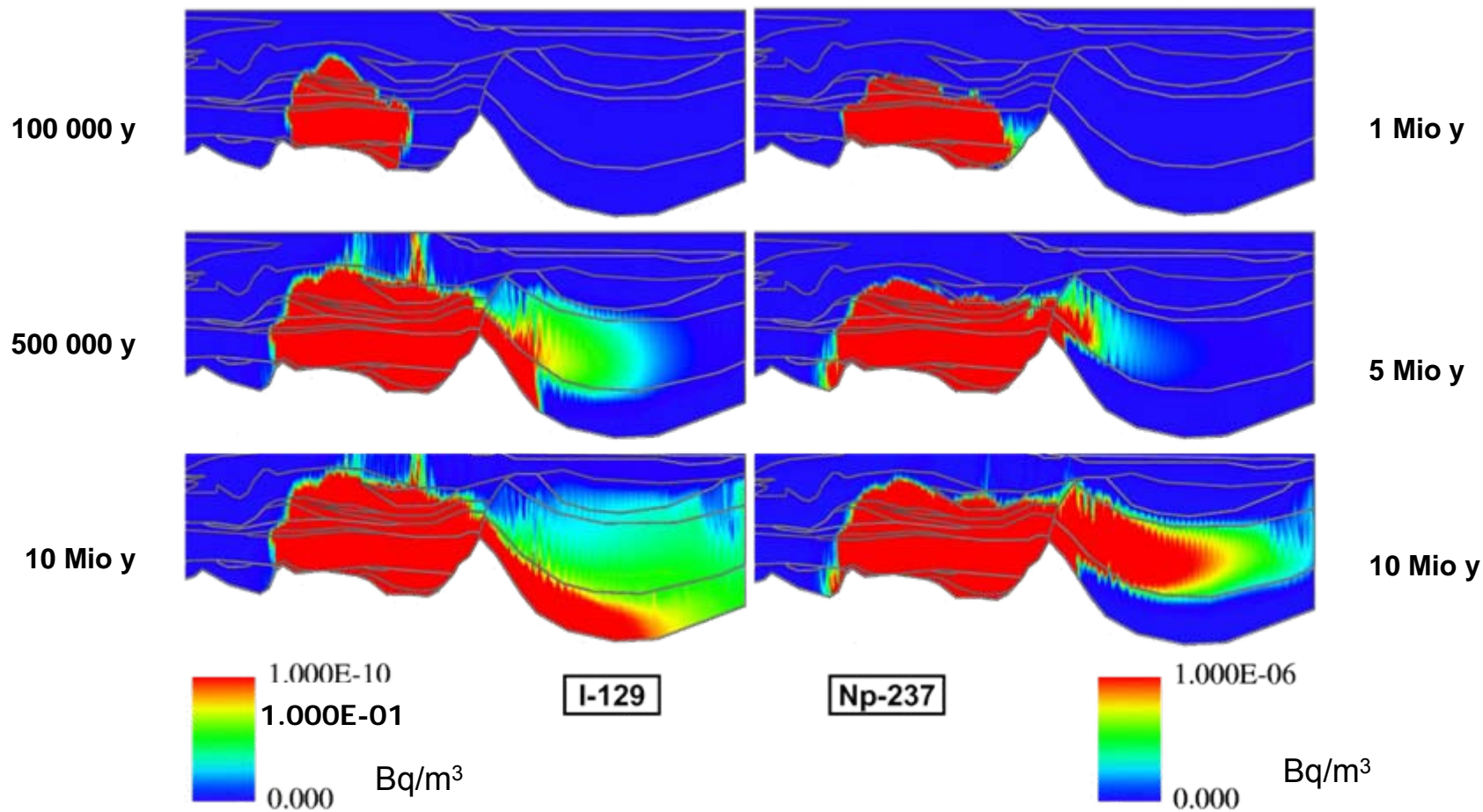


Hypothetical release of I-129 into the covering sediments (I)



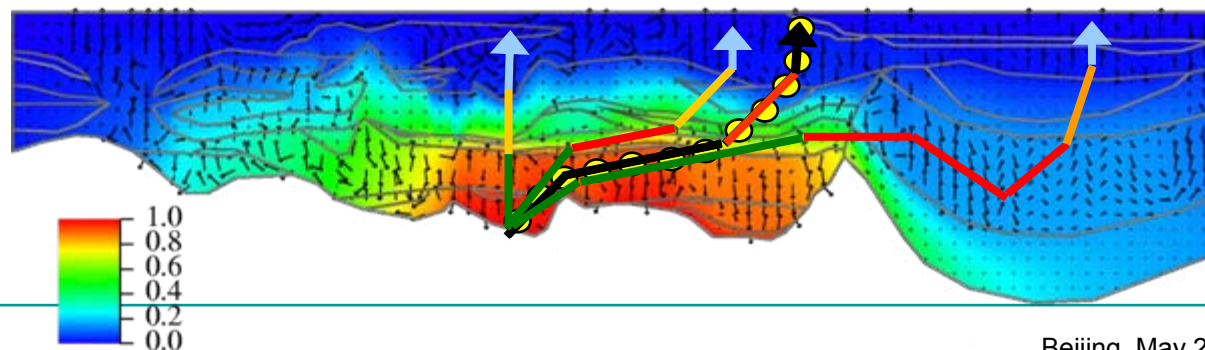
Hypothetical release of I-129 into the covering sediments (II)



Simulation with d^3f/r^3t 

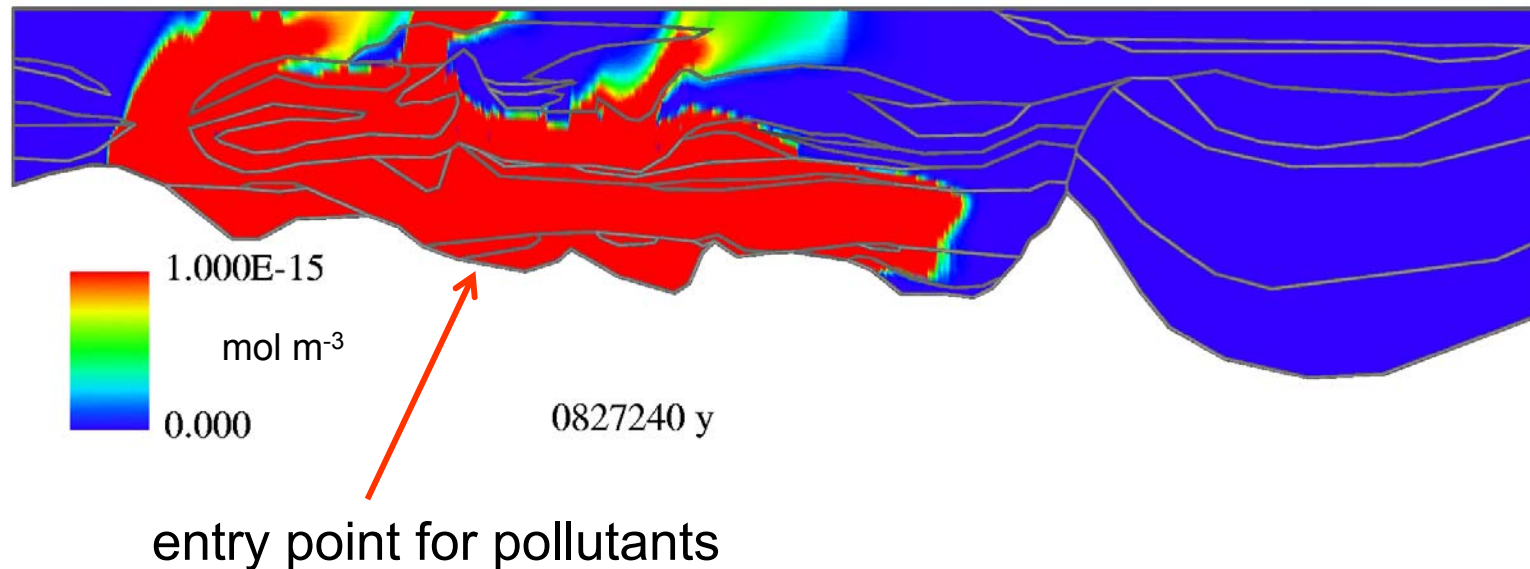
Abstraction to Performance Assessment

- Current approach: particle tracking
 - 1D, few hydrological units
 - Particle tracking
- Alternative approach
 - 1D model
 - = Multi-D model
 - Heterogeneous model



Distribution of U^{238} after 827 240 years

transport calculation with r^3t code
= radionuclide, reaction, retardation, and transport

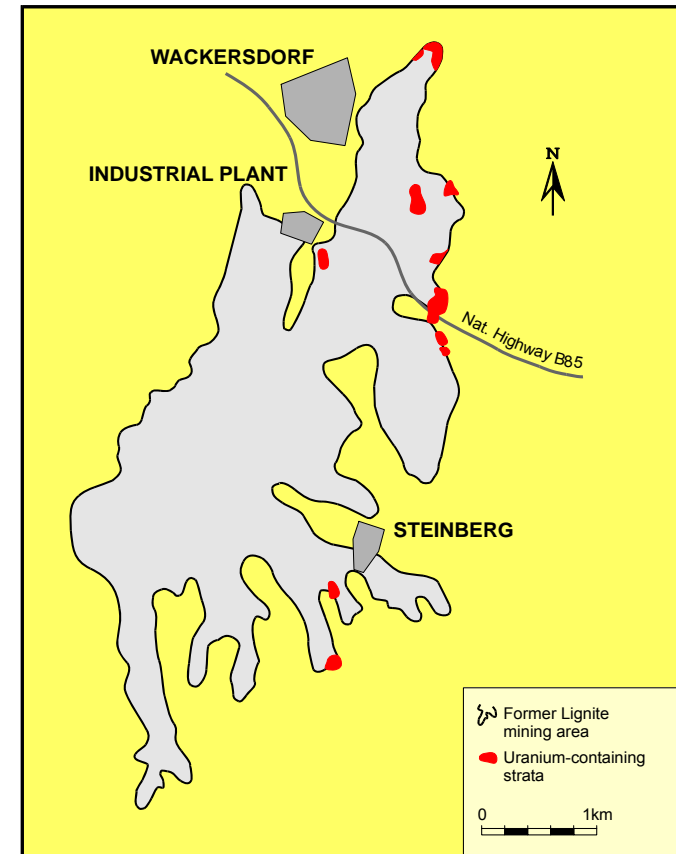


Uranium transport in Tertiary sediments

The Heselbach study area

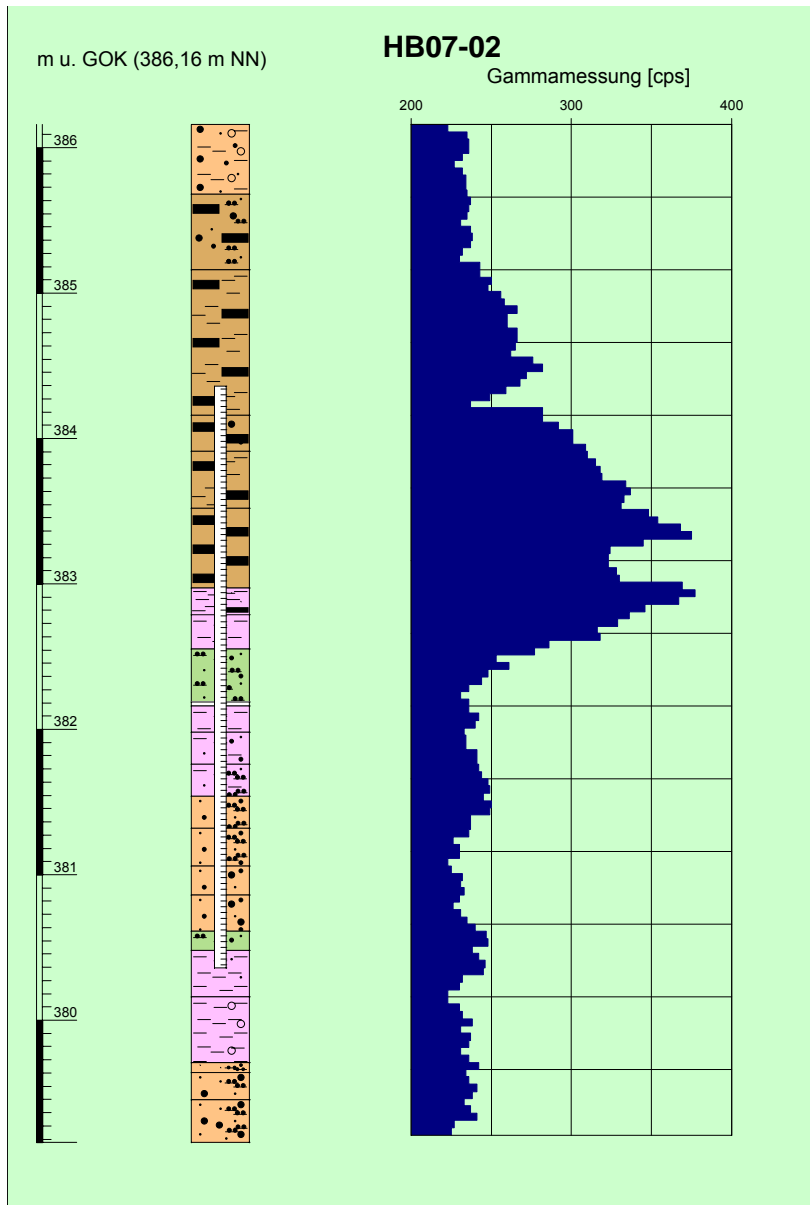
Uranium bearing sediments at Heselbach site

- Uranium rich strata at the outer rim of a lignite mining area
- Investigation as natural analogue for uranium mobilisation and transport in sedimentary rocks under Middle European climatic conditions



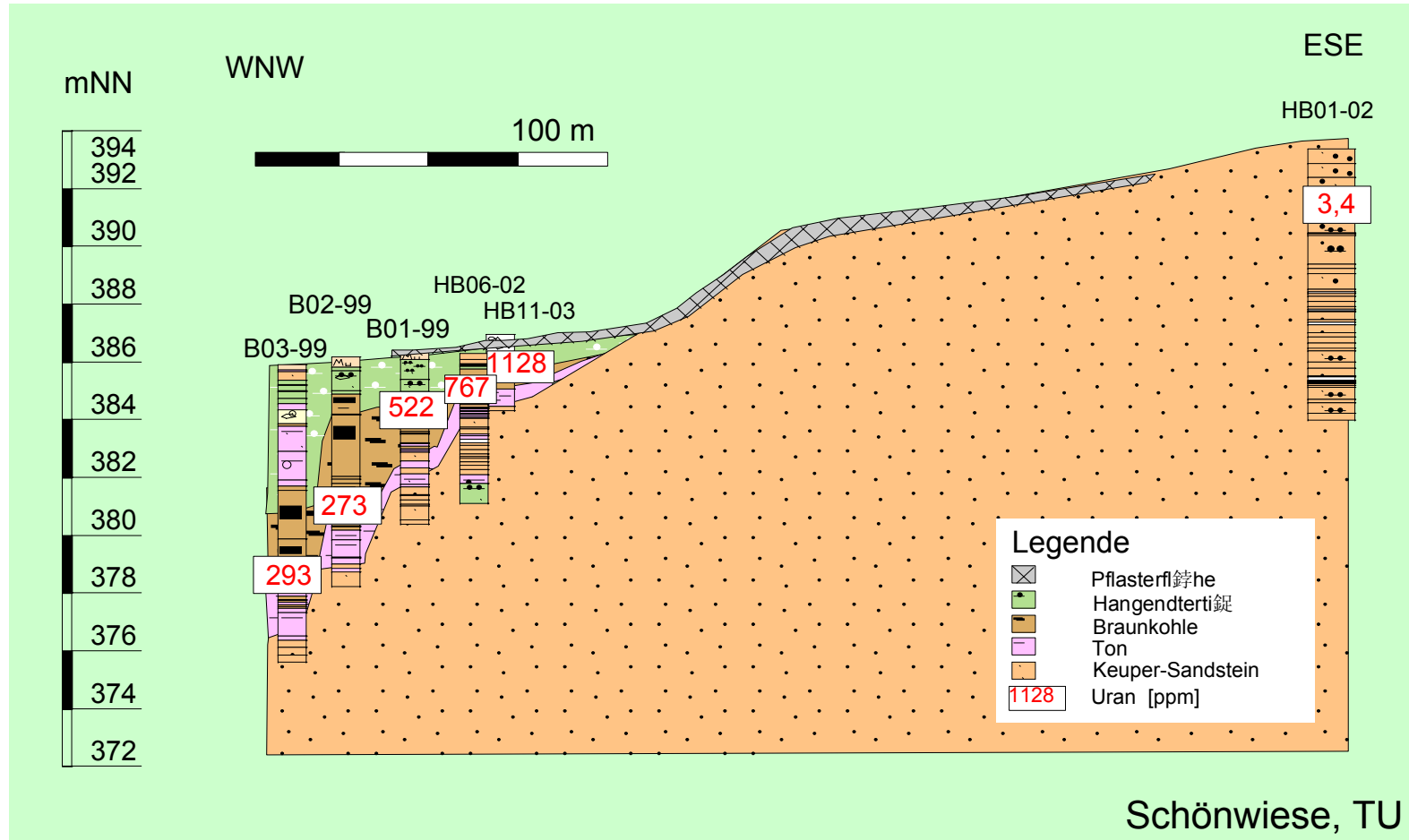
Schönwiese, TU BS

Geological profile with uranium peaks in lignite rich layers

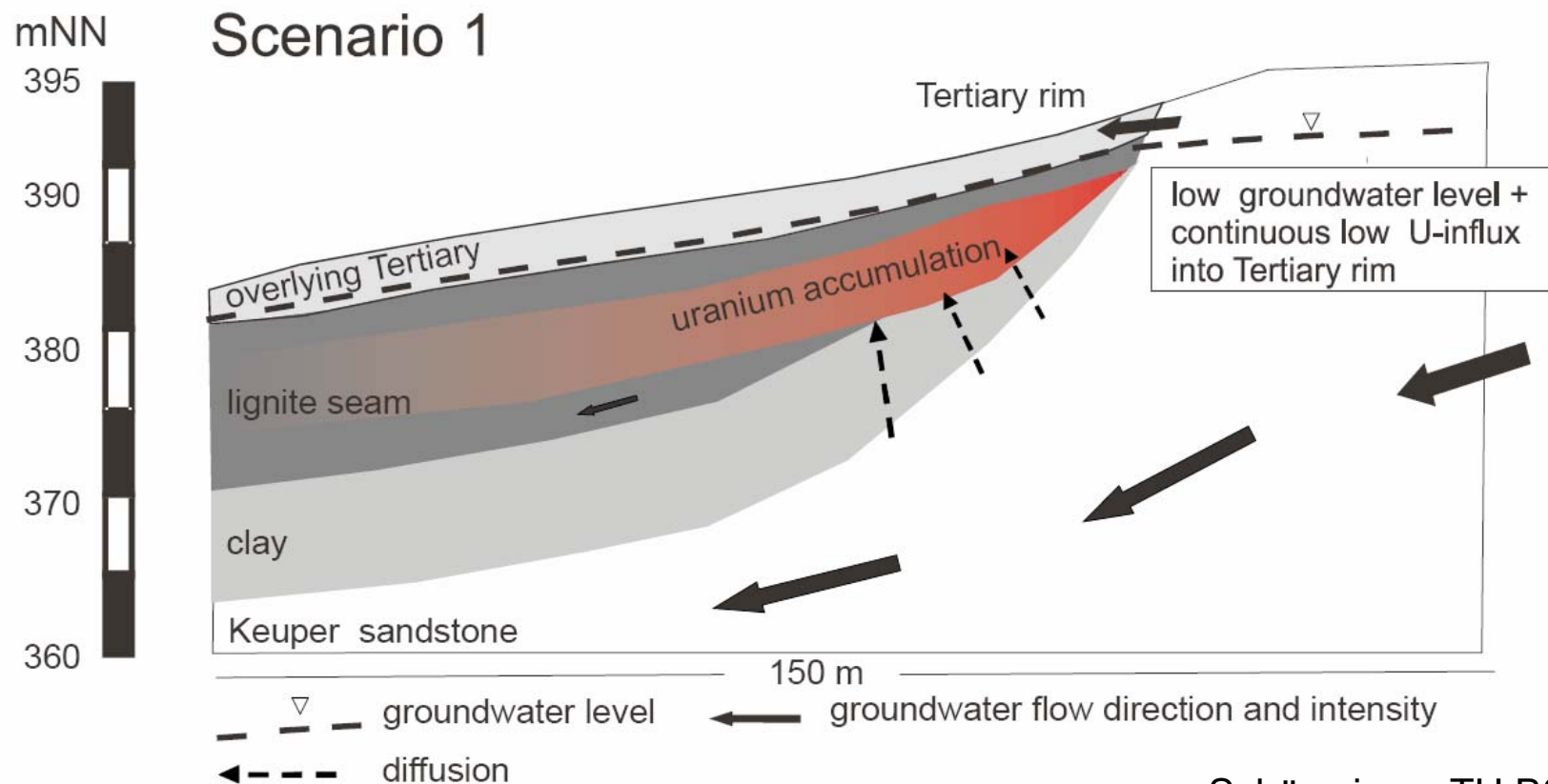


Beijing, May 28 to June 1, 2007

Geological cross section showing uranium contents

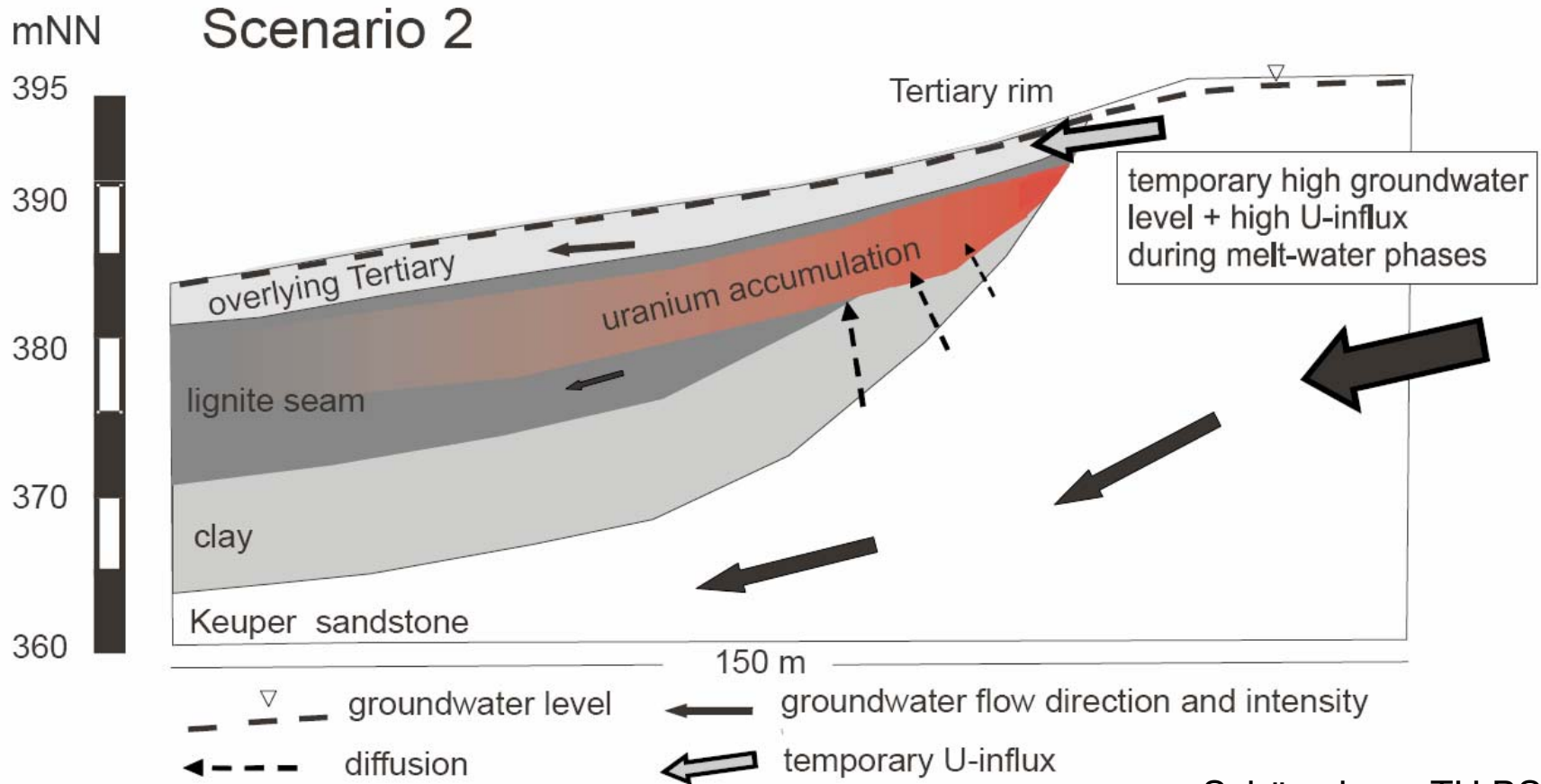


Scenario 1 for uranium enrichment at Heselbach site



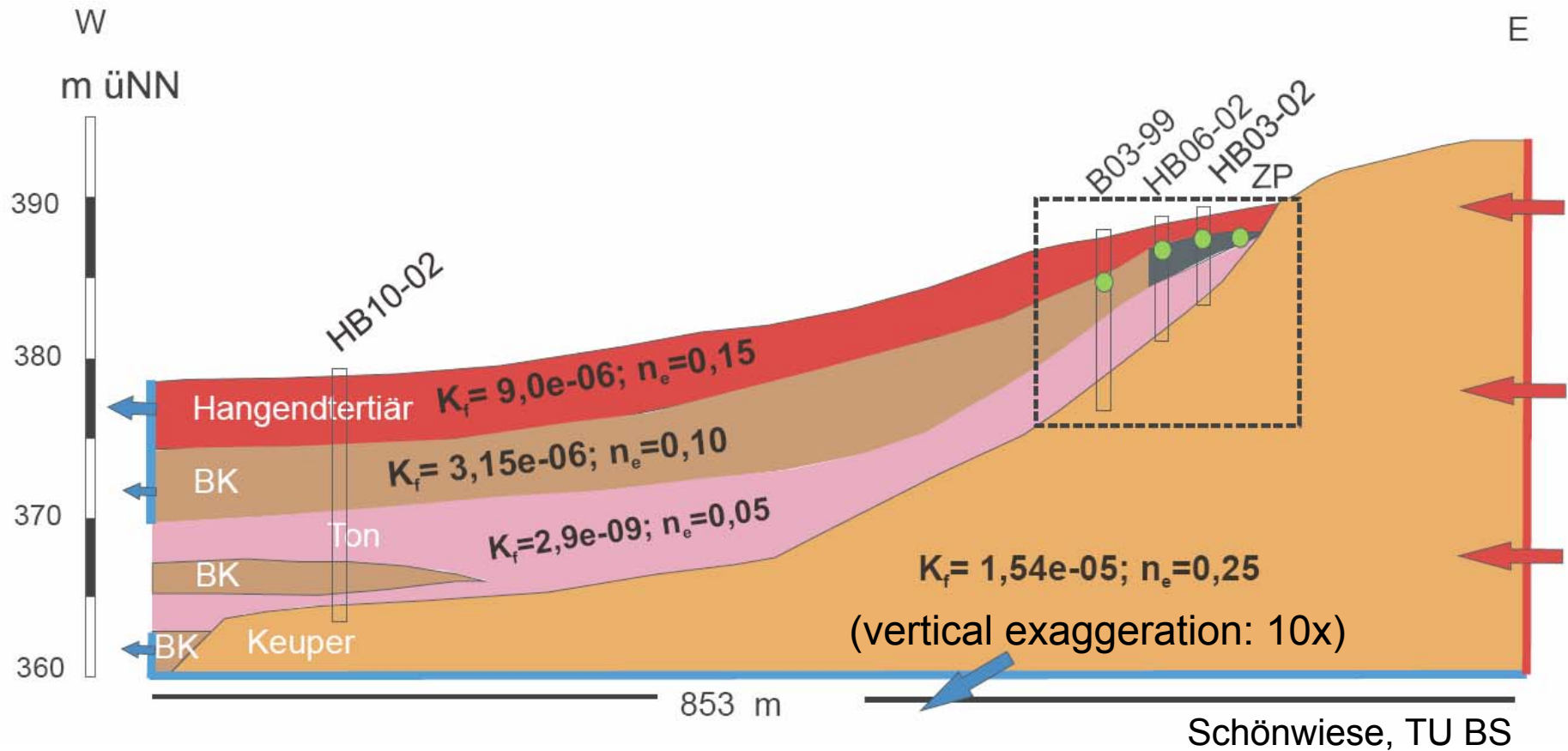
Schönwiese, TU BS

Scenario 2 for uranium enrichment at Heselbach site

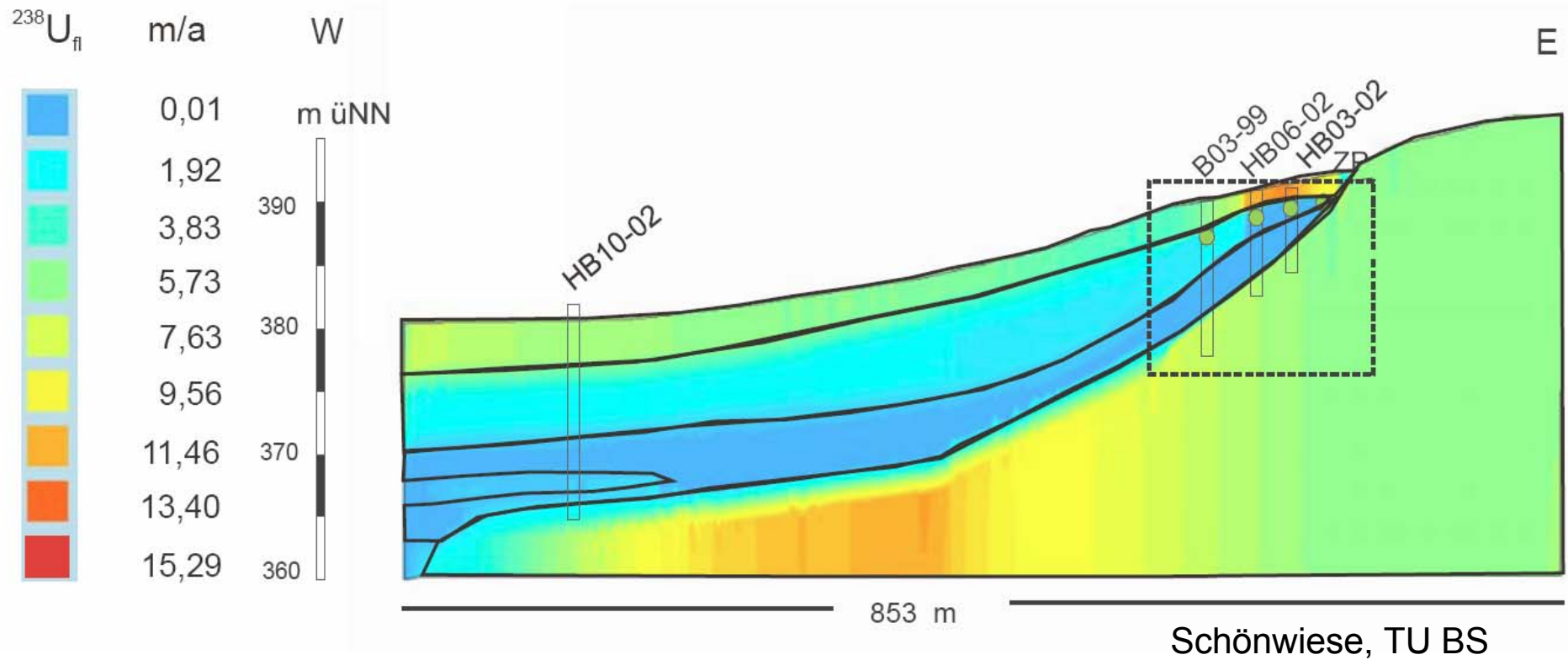


Schönwiese, TU BS

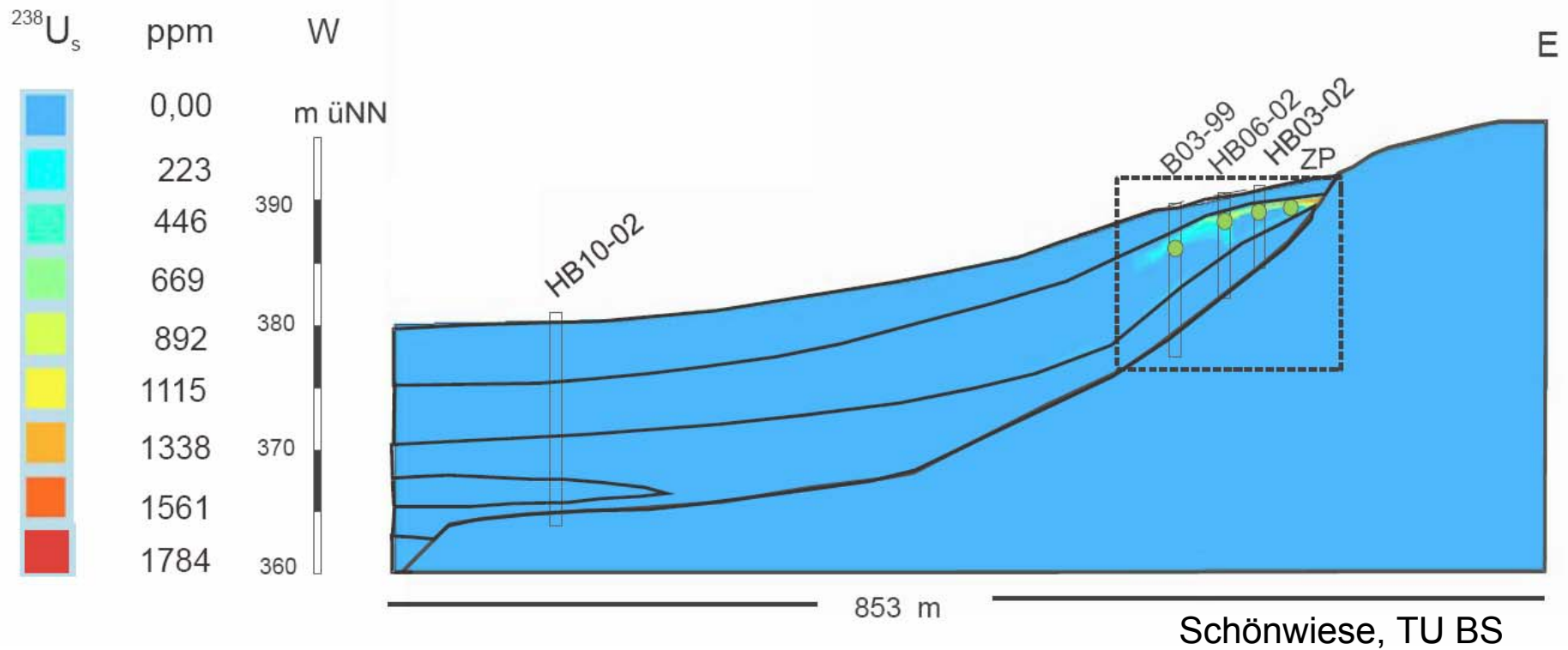
Schematic 2D-Vertical Model of Heselbach site for flow and transport calculations with computer program Feflow



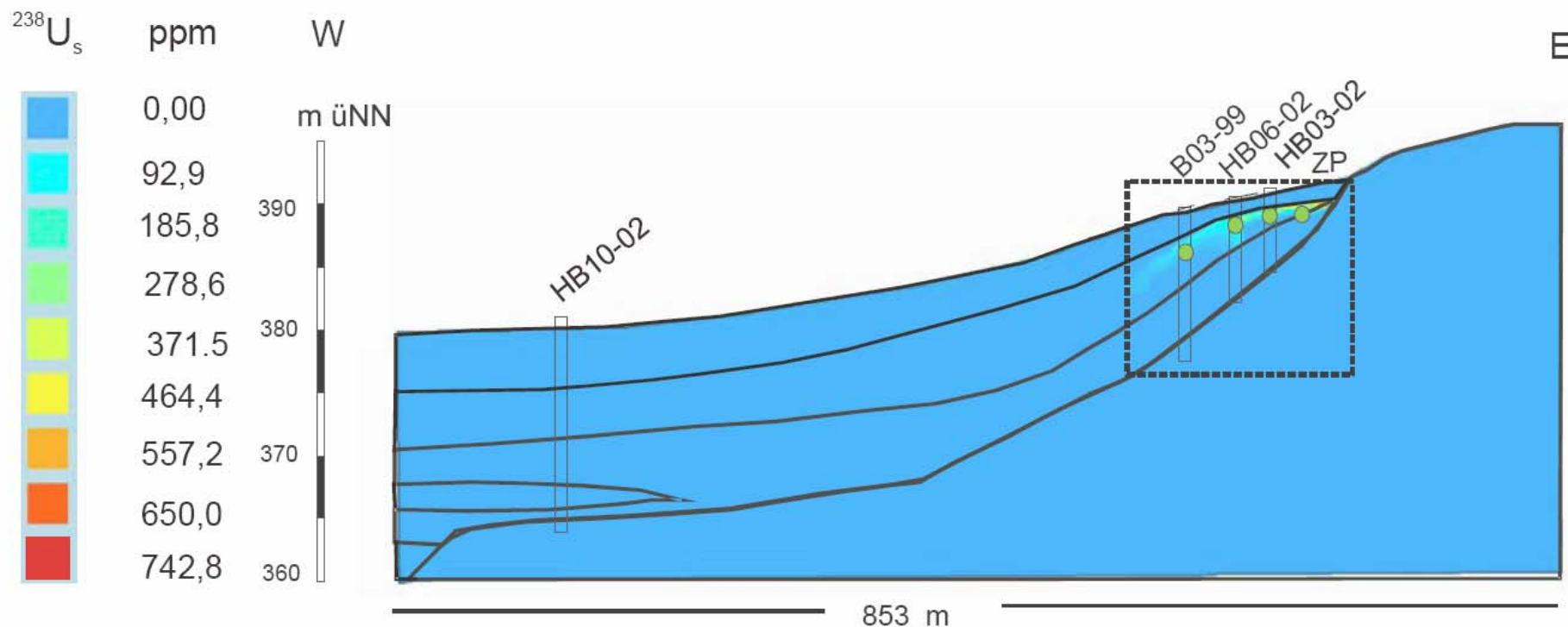
Calculated groundwater velocity under present conditions



Model results (Scenario 1) : Uranium content in the lignite-rich layer after continuous input during 800 000 years



Model results (Scenario 2) : Uranium content in the lignite-rich layer after input during one melt water phase in interglacial of 20 000 years

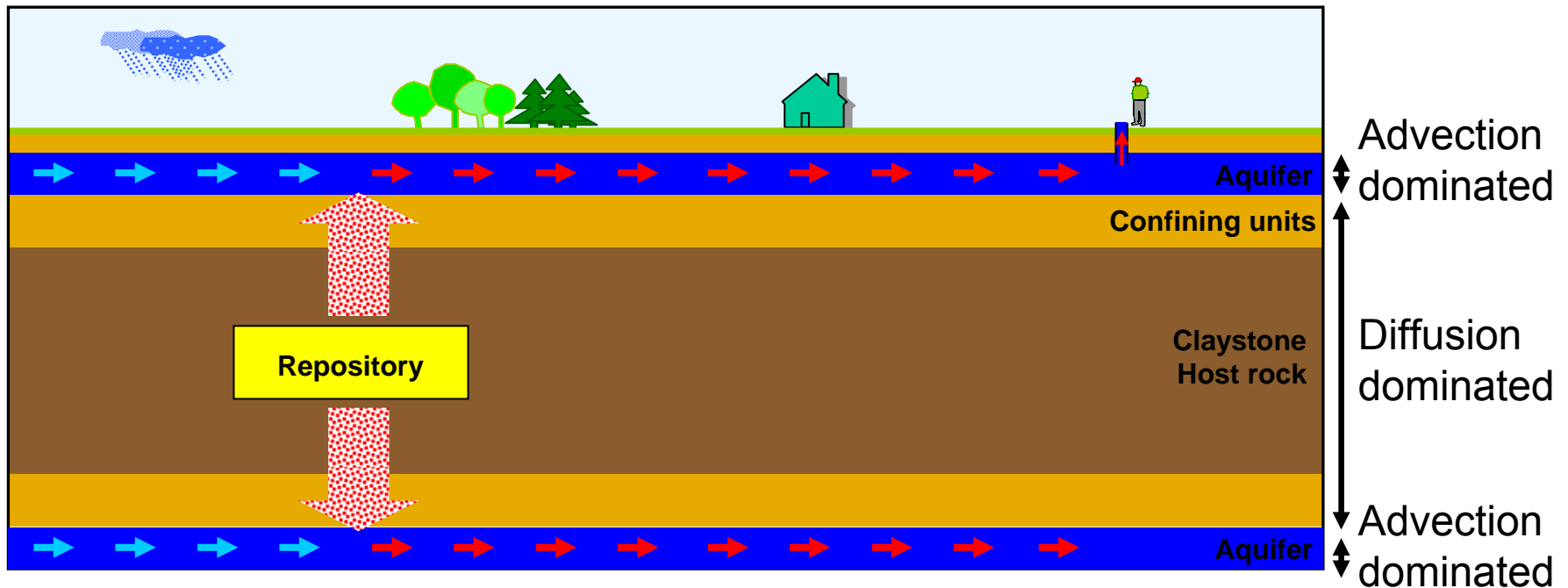


Schönwiese, TU BS

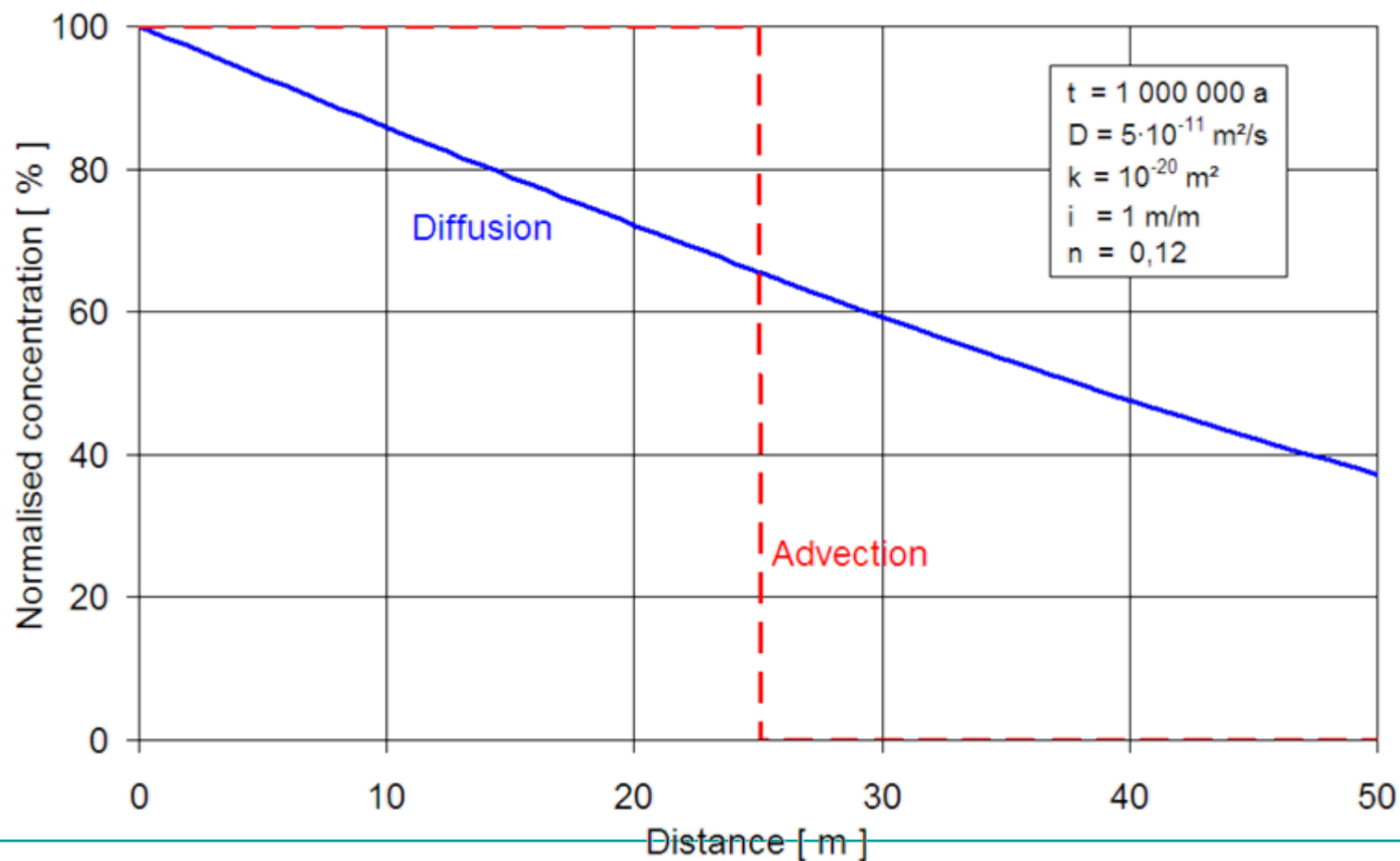
Radionuclide transport in clay formations

Generic concept in accordance
with site studies in Switzerland

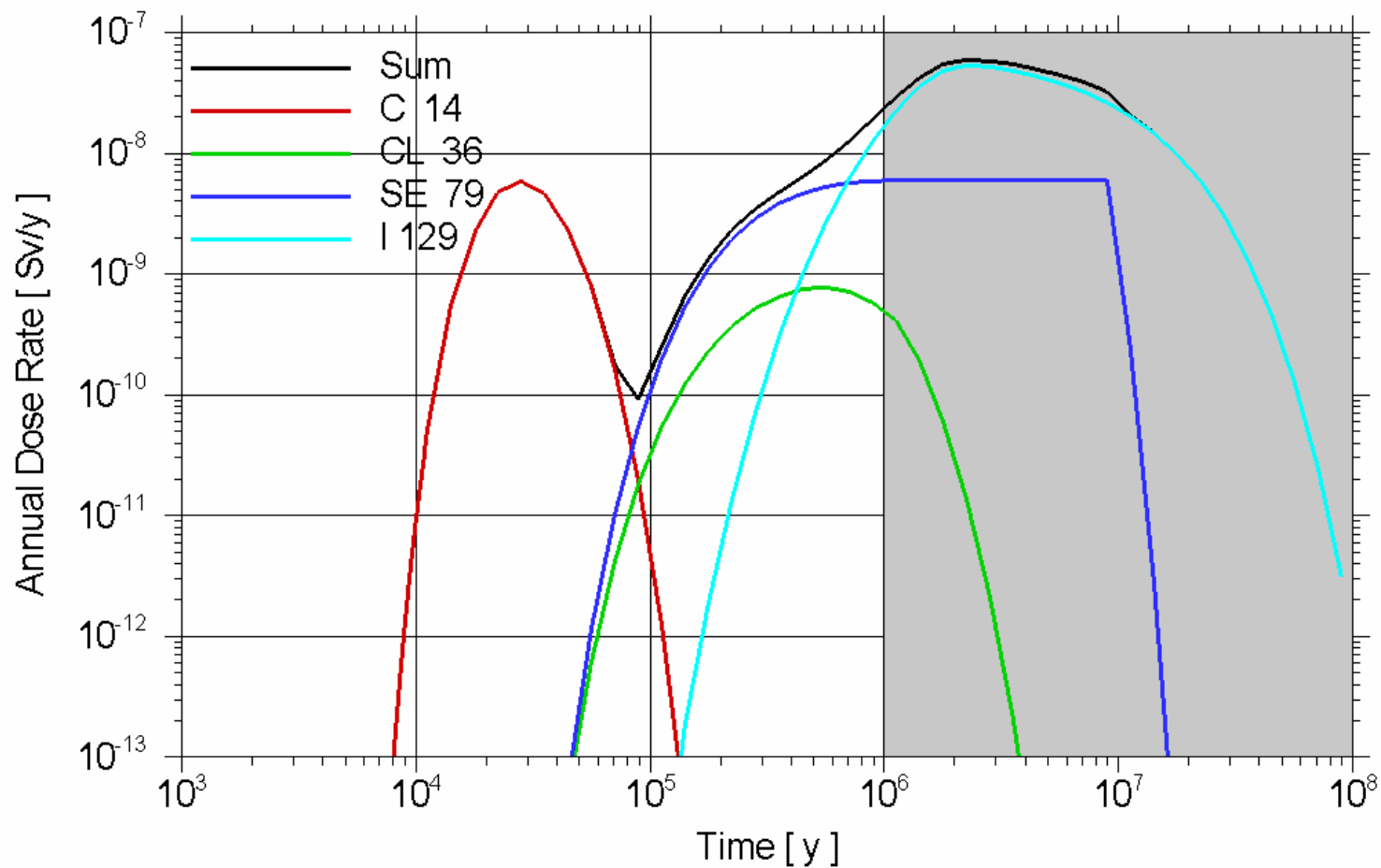
Claystone formations: Transport processes



Claystone formations: Transport processes



Claystone formations: Annual dose rates



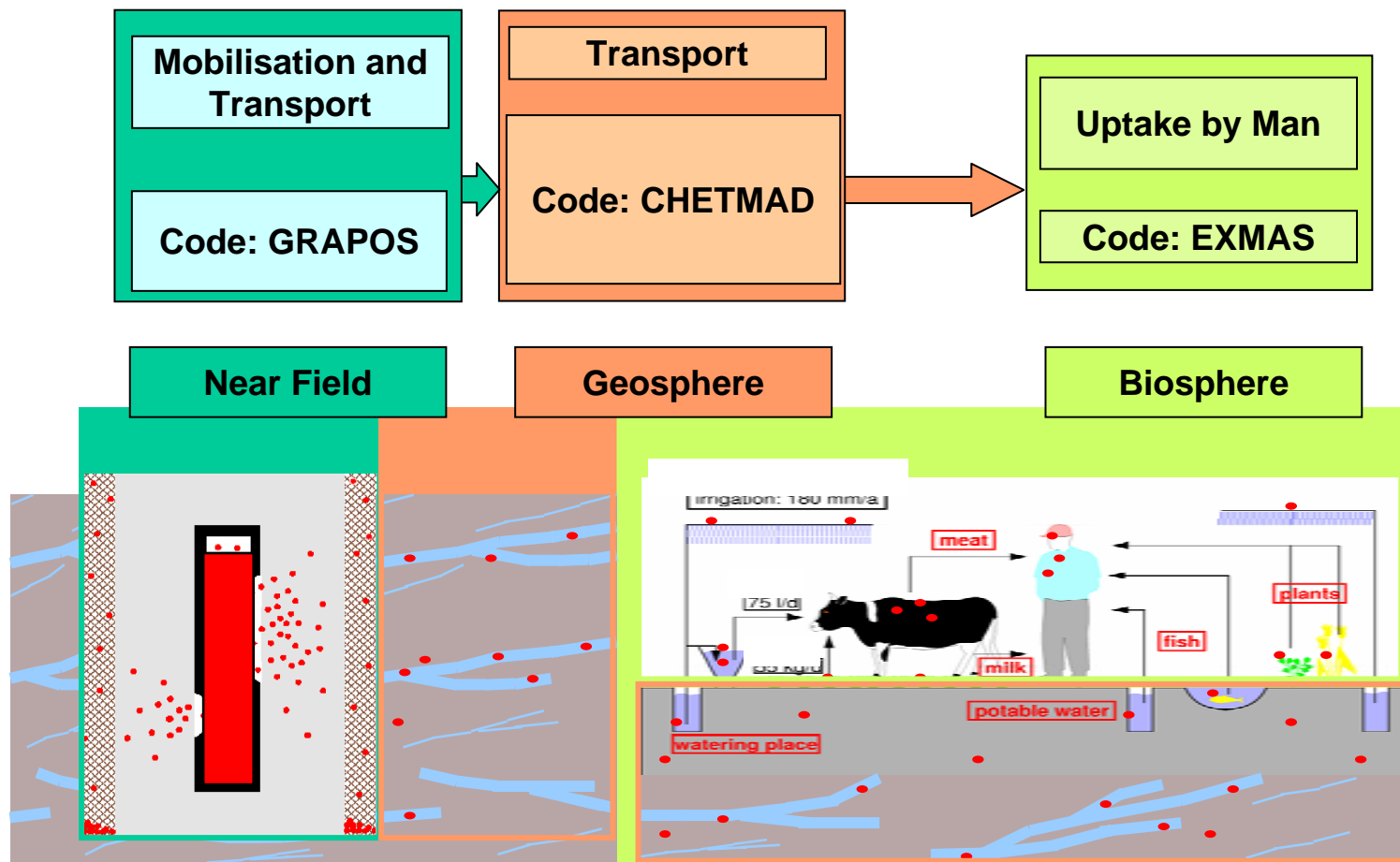
Granite

Hydrogeological modelling studies in order to check the feasibility of a disposal concept in the Siberian Shield

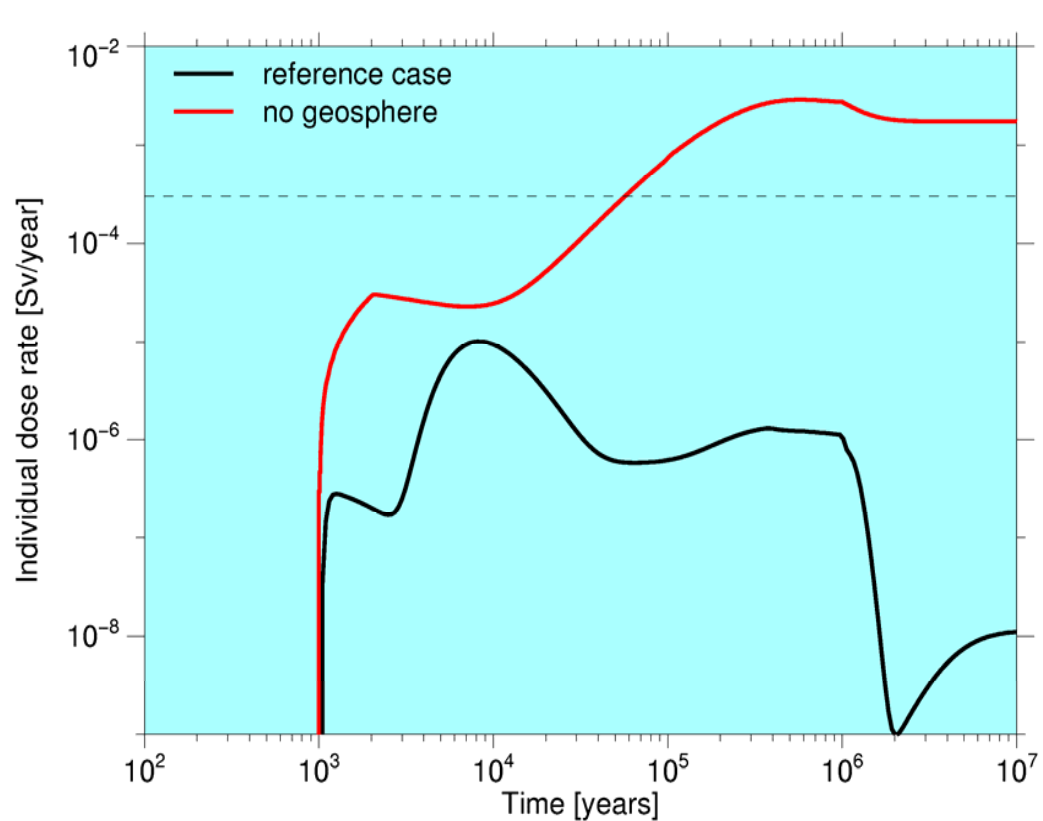
Evaluation of Disposal Concept and Sites by Performance Assessment (PA)

- Development of computer models for the different subsystems of the Russian disposal concept
(waste - container - geobarrier system - biosphere)
- Identification of the safety-relevant parameters and processes of a granite environment
(Inventory - RN mobilisation - transport - exposure of man)
- Stepwise improvement of the system understanding and optimization of the disposal concept *(safety requirements)*
- Integrated performance assessment ISPA for concrete disposal sites and check with *safety criteria and regulations*

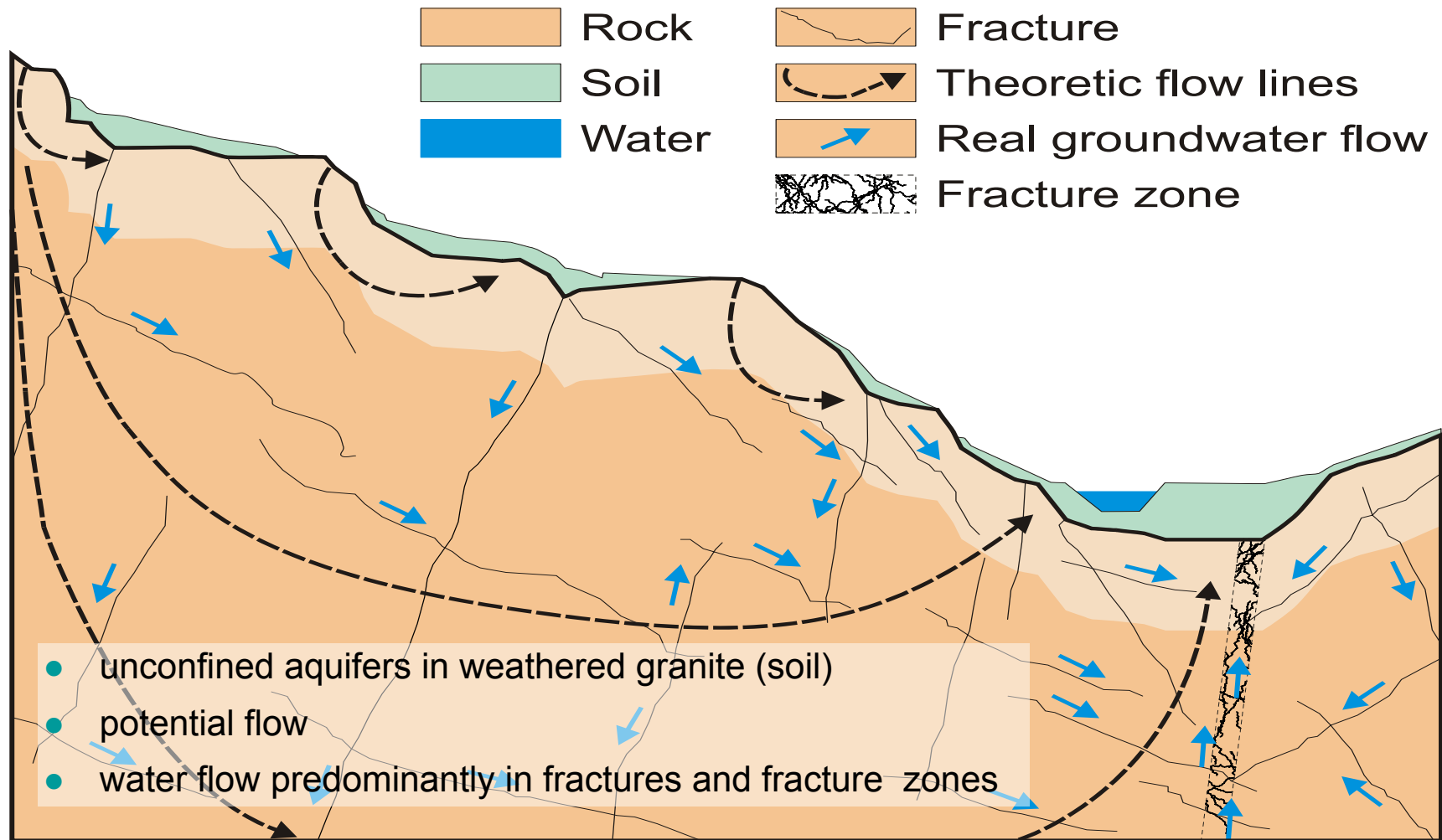
EMOS code for RN Transport & Dose Calculations



Generic studies on the contribution of granitic bedrock to long-term isolation of SF / radioactive waste



Groundwater flow in granitic bedrocks



Russian Taiga: The Problem of Data Acquisition



regional data
data from rock cavities

- climatic data
- fractures and apertures [2d]

- porosity of rock mass
- kf-values [fractures / matrix]
- storage / sorption coefficient

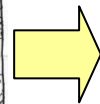
- heat capacity / conductivity [fractures / matrix]

data needs

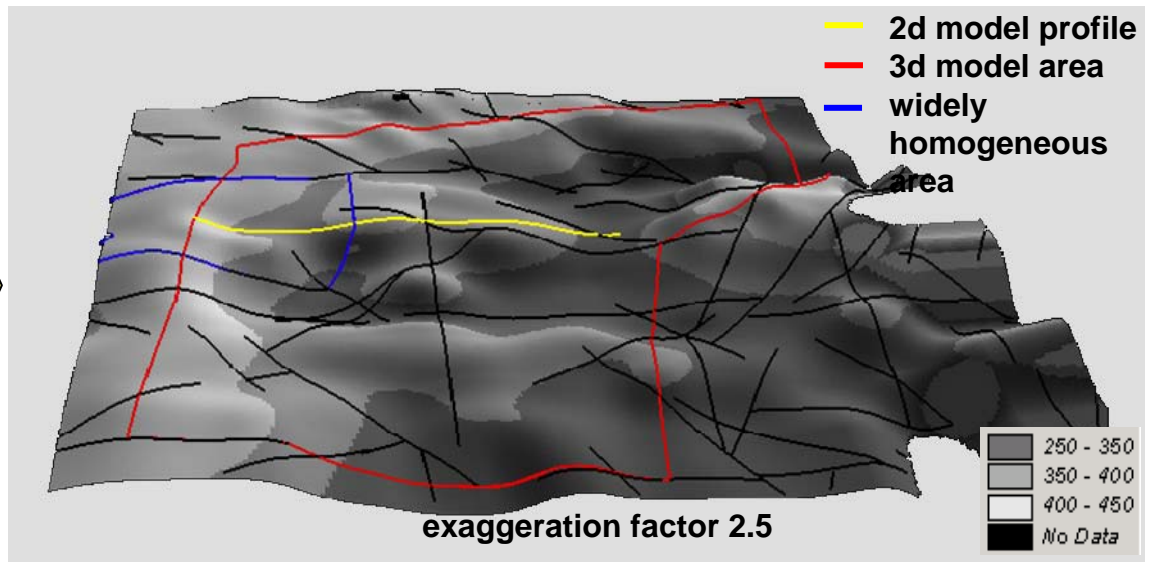
- exact topography
- strike and incline of fractures
- aperture of fractures
- groundwater level
- diffusion coefficient
- permeabilities
- temp. distribution in rock mass

Contour mapping by use of GIS

Map of slopes [Lopatin et al.]



Elevation Model



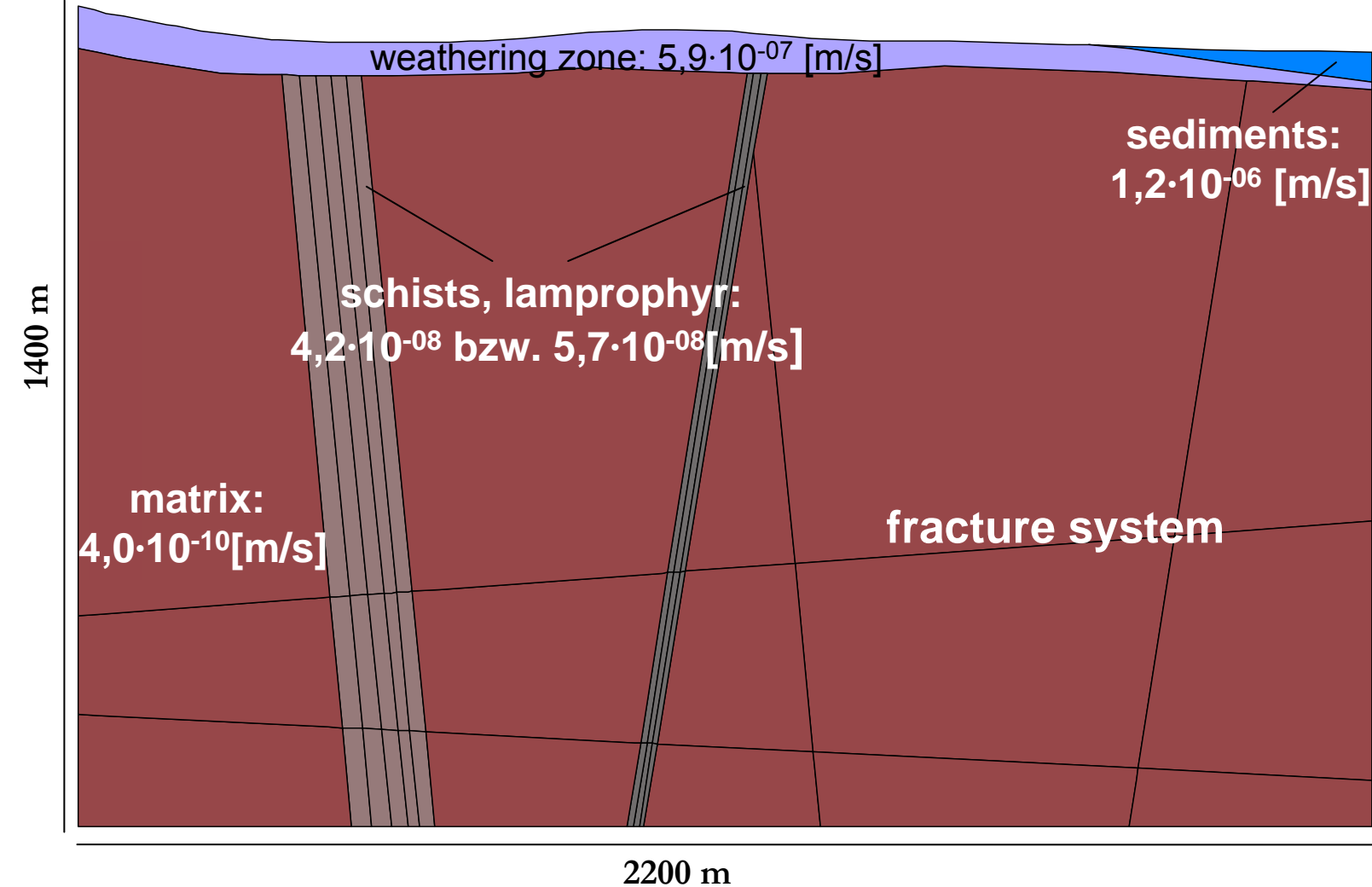
Groundwater flow in granitic bedrock



section	depth [km]	permeability [m/s]			
		matrix		Fractures of III. and IV. order	
		min/max	average	min/max	average
section 1 weathered zone	0 - 0,1	$5,7 \cdot 10^{-8} / 5,8 \cdot 10^{-6}$	$1,2 \cdot 10^{-7}$	$1,2 \cdot 10^{-7} / 1,2 \cdot 10^{-5}$	$5,8 \cdot 10^{-6}$
section 2 stress relaxation	0,1 - 2,5	$1 \cdot 10^{-10} / 1 \cdot 10^{-7}$	$5 \cdot 10^{-8}$	$1 \cdot 10^{-9} / $ $1,2 \cdot 10^{-6}$	$3,4 \cdot 10^{-8}$
section 3 increased regional stress	1 - 5	$1,2 \cdot 10^{-14} / 3,5 \cdot 10^{-12}$	$3,5 \cdot 10^{-13}$	$1,2 \cdot 10^{-12} / 1,2 \cdot 10^{-10}$	$1,2 \cdot 10^{-11}$
section 4 decreased stress	5 - 7	$1,2 \cdot 10^{-13} / 1,2 \cdot 10^{-10}$	$5 \cdot 10^{-11}$	$1,2 \cdot 10^{-14} / $ $5,8 \cdot 10^{-7}$	$1 \cdot 10^{-9}$
section 5 high regional stress	>7	$1,2 \cdot 10^{-15} / 1,2 \cdot 10^{-13}$	$3,5 \cdot 10^{-14}$	$1,2 \cdot 10^{-13} / 1,2 \cdot 10^{-11}$	$1,2 \cdot 10^{-12}$

Parameterisation of soil & fracture permeability with respect to sections of different rock pressure (Anderson et al. 1998)

Geological Structure Model



W. Brewitz **flow direction**

Beijing, May 28 to June 1, 2007

Hydraulic Boundary Conditions

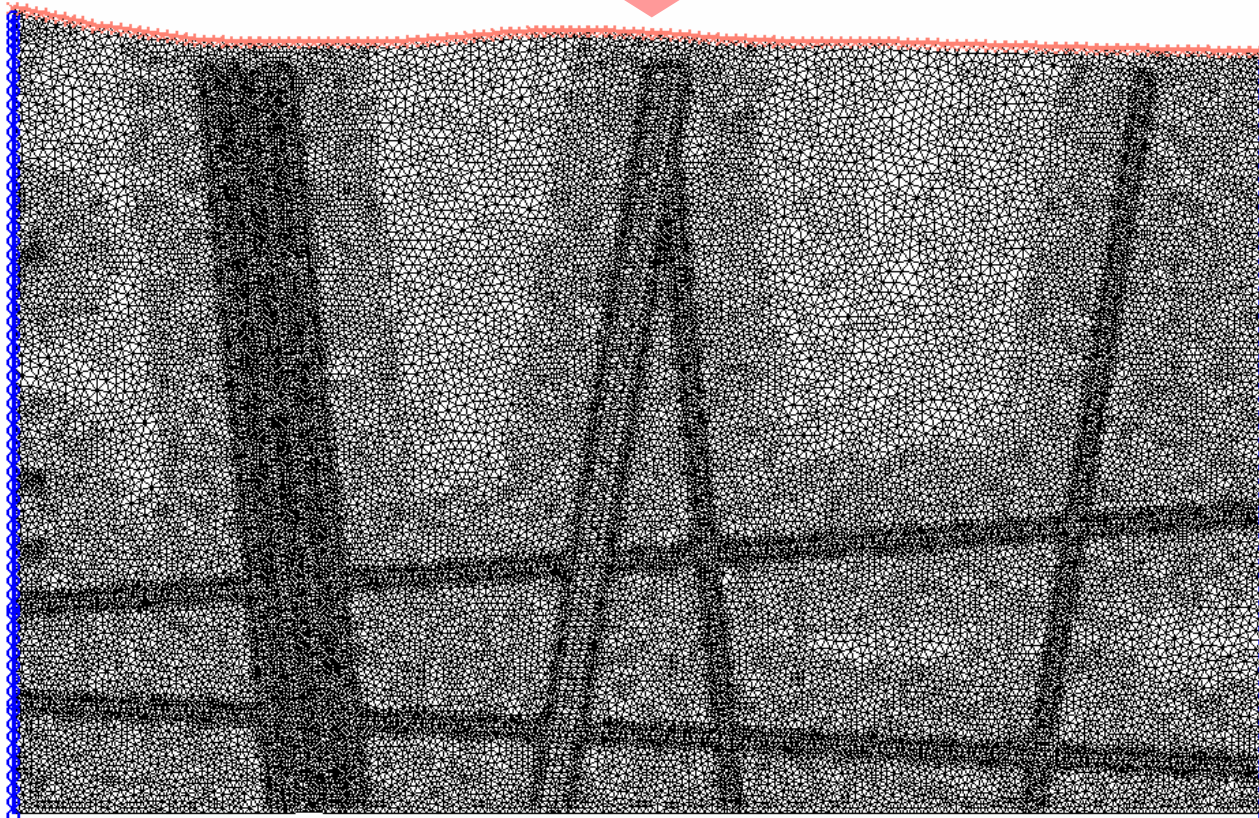


Groundwater Recharge:
 $1,64 \cdot 10^{-04}$ [m/d]



Hydraulic Gradient:
 $3 \cdot 10^{-02}$

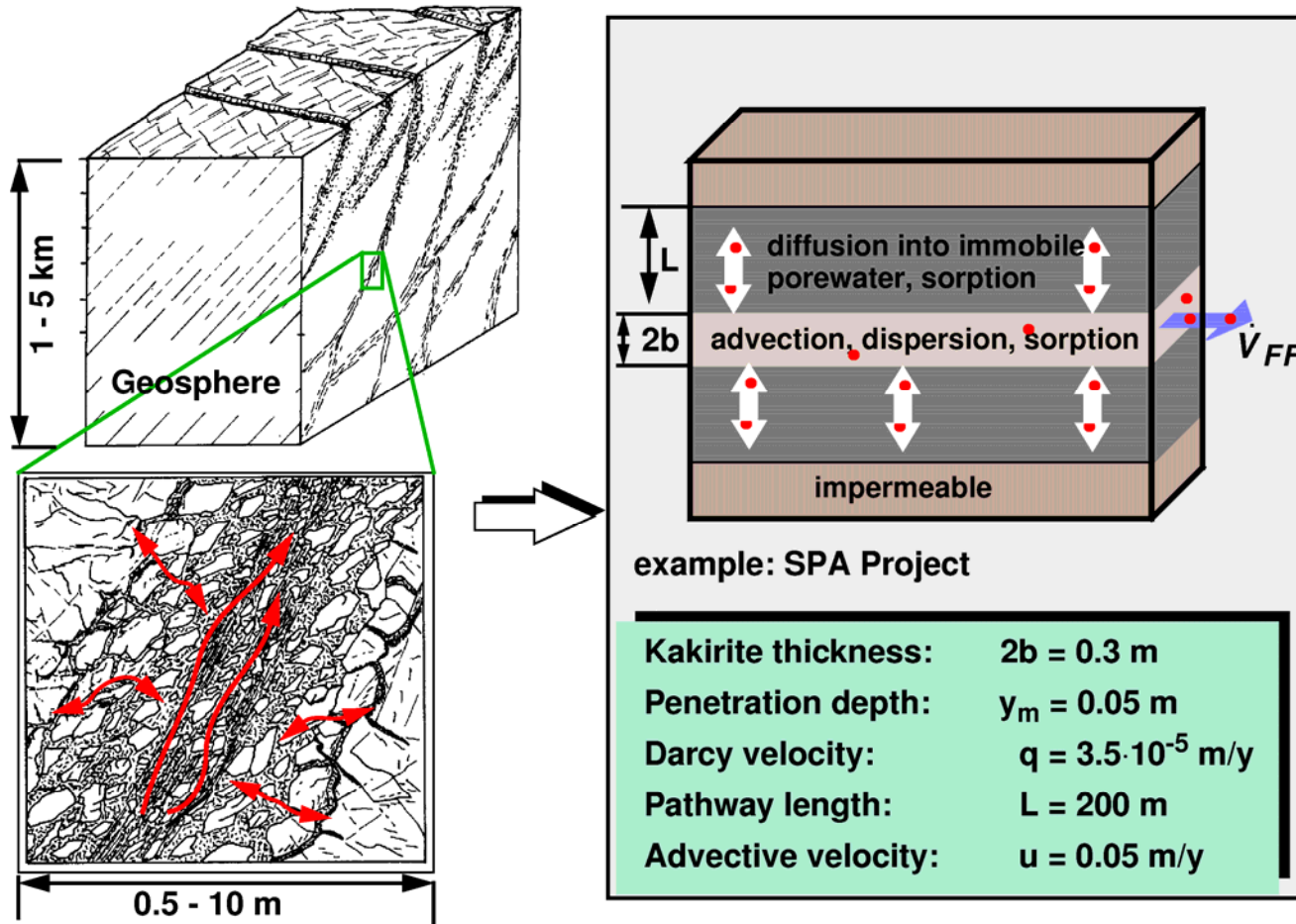
Elements: 61.322
Knotes: 30.936



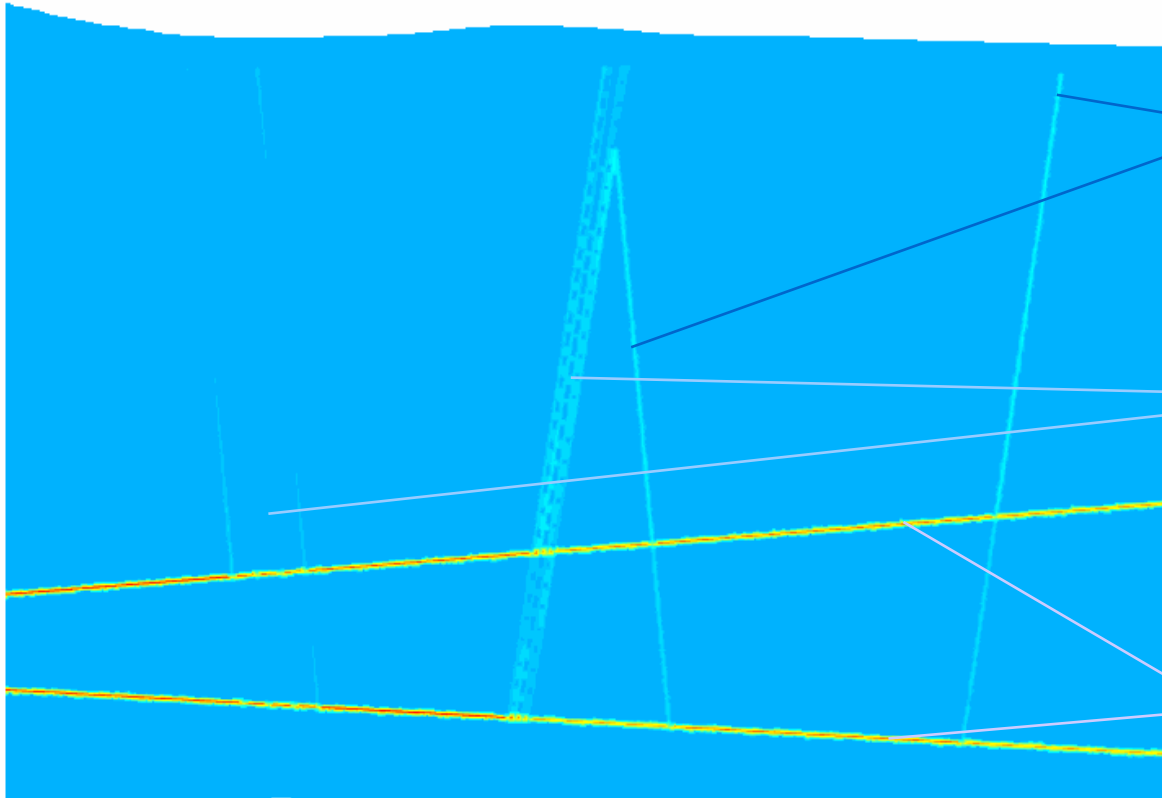
Far field granite – RN transport in Kakirite zone



CHETMAD code



Groundwater Flow Velocity



Fractures perpendicular to groundwater flow

- => lower groundwater flow velocity as in the horizontal fractures.
- => taking the radionuclides to the surface

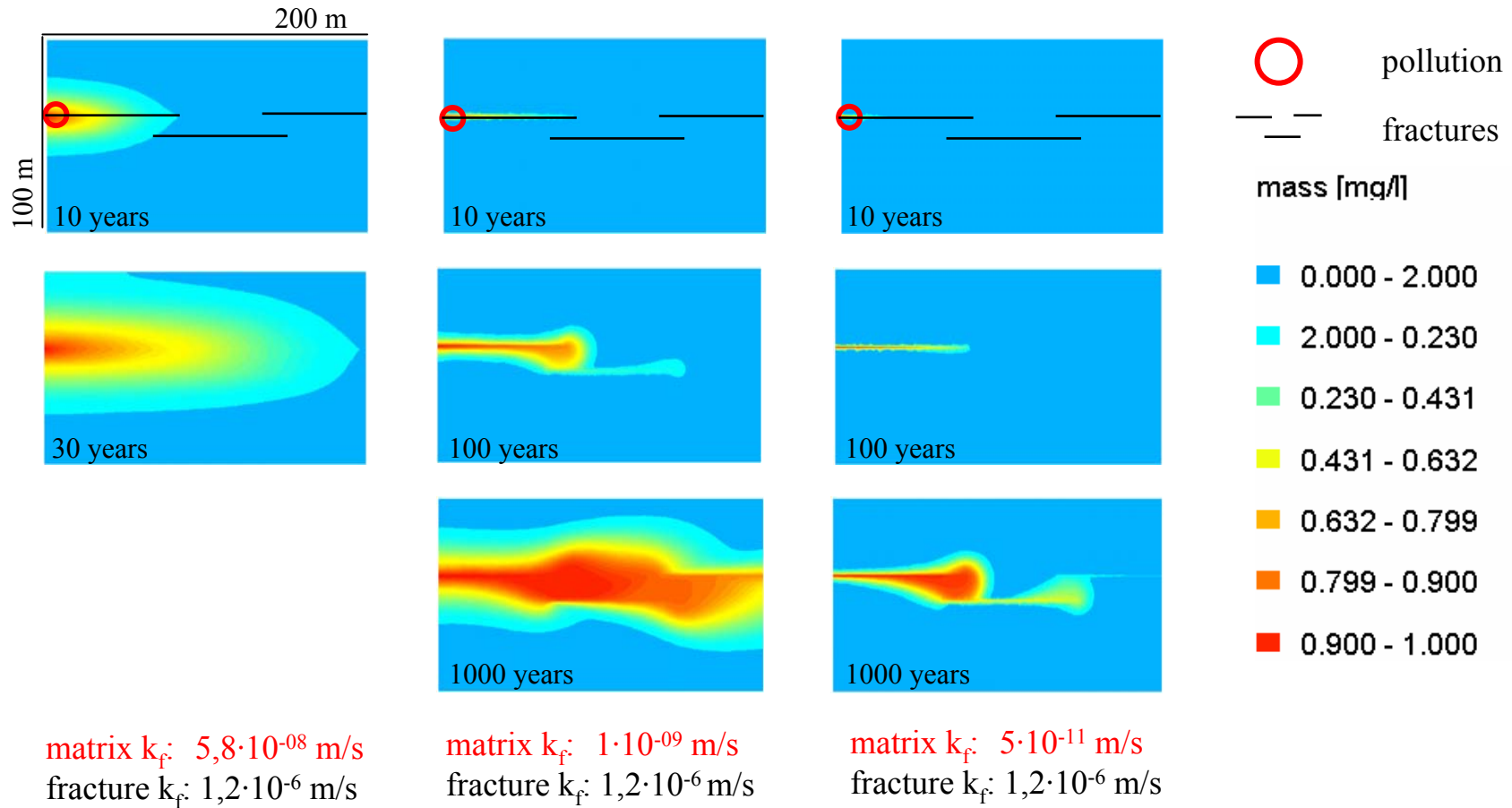
Sections with high fracture density

- => decreasing groundwater flow velocity, increasing diffusion and dispersion.
- => „stand-alone“ fractures are the most effective pathways

Fractures in direction of groundwater flow

- => fast and far radionuclide transport

Schematic 2d Transport Model with FEFLOW

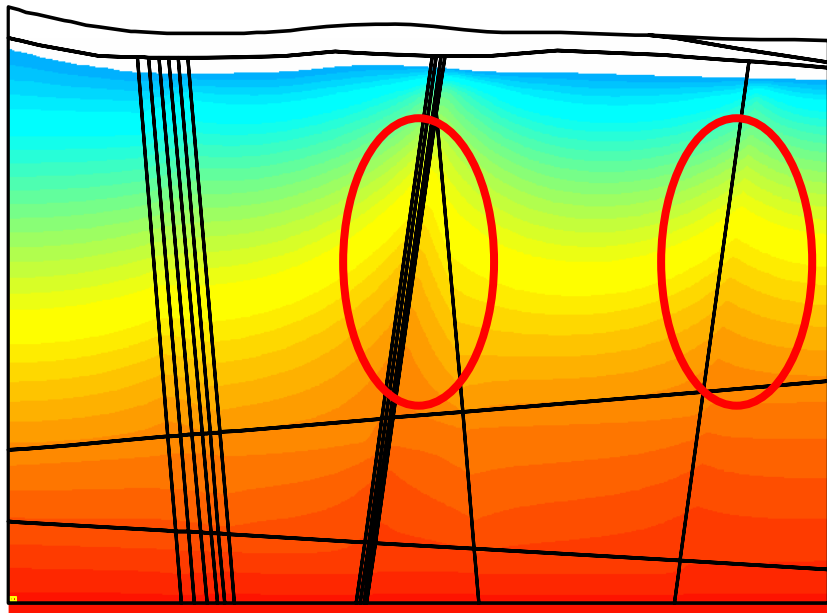


2d Transportmodel with Temperature Gradient



matrix kf: $4 \cdot 10^{-10}$ [m/s]

fracture aperture: 50 [cm]

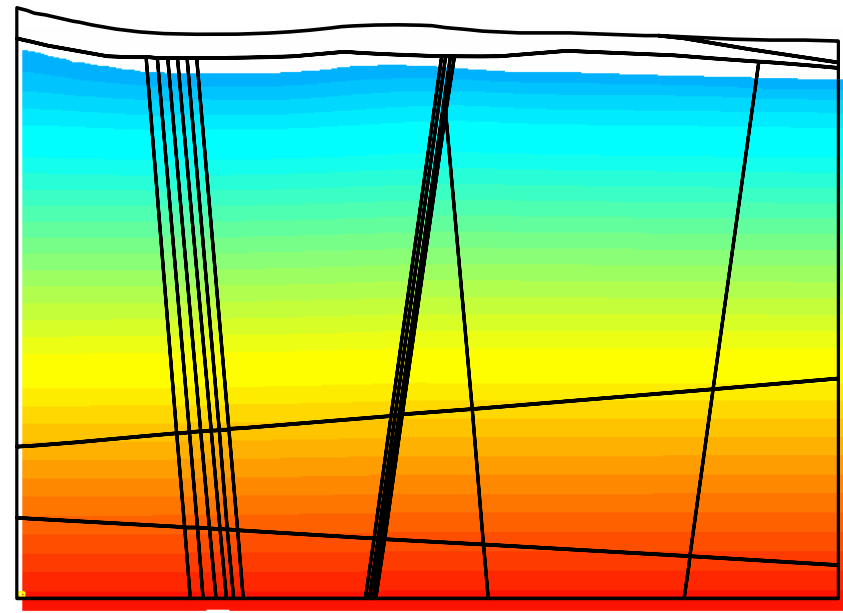


fractures with a fast groundwater flow

fracture kf: $7 \cdot 10^{-05}$ [m/s]

=> inhomogenic natural heat field

=> alteration of the groundwater flow direction



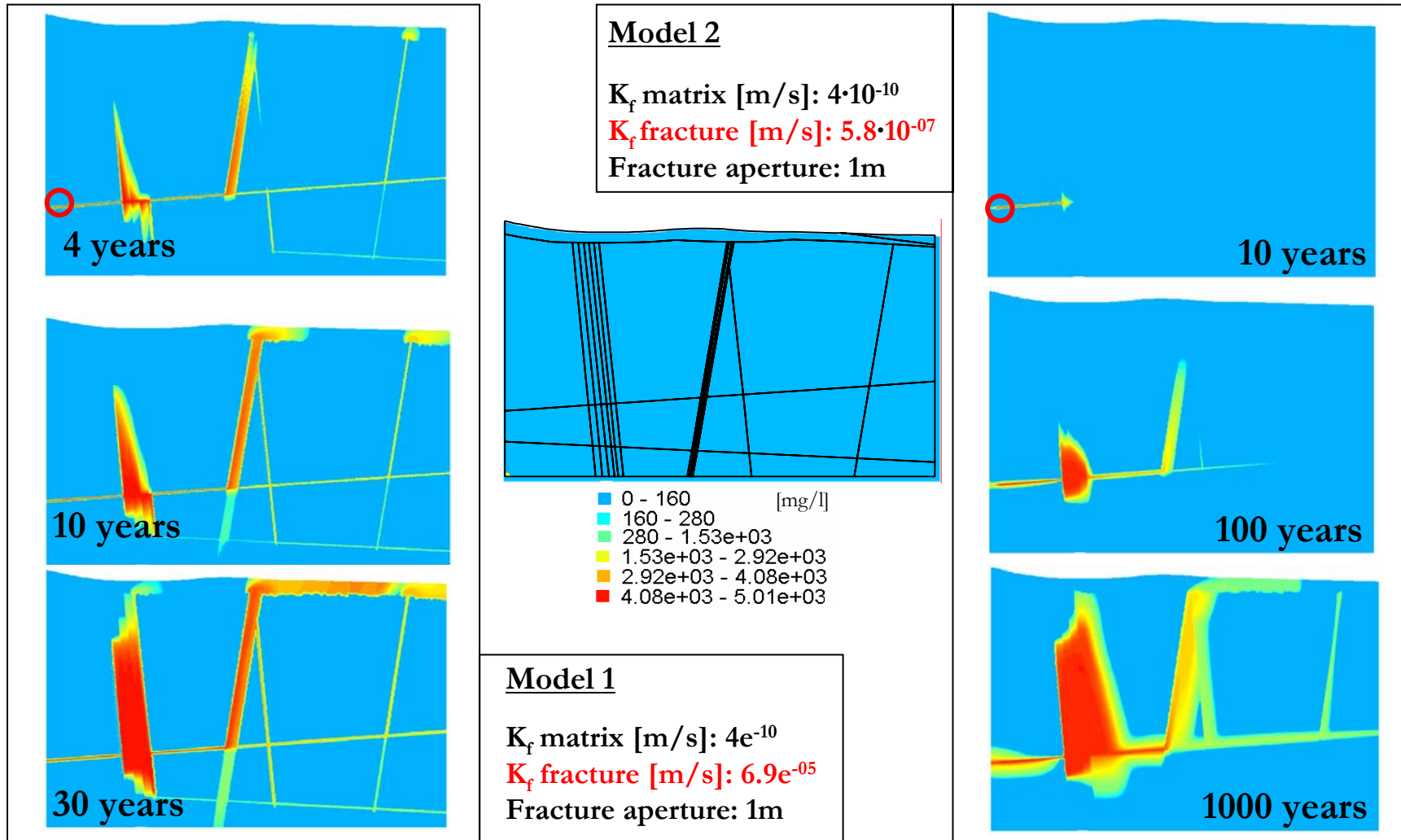
fractures with a low groundwater flow

fracture kf: $6 \cdot 10^{-07}$ [m/s]

=> homogeneous heat field

=> groundwater flow direction to the surface

2d Transportmodel with Temp. Gradient and Tracer



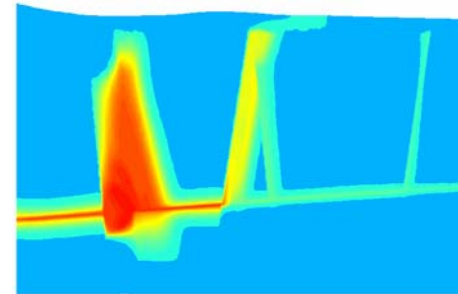
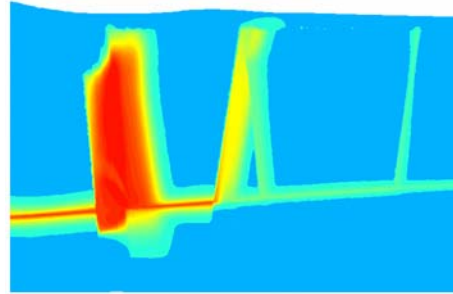
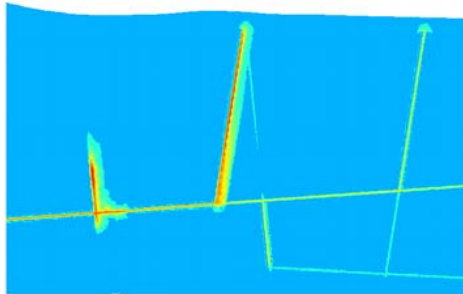
2d Model with Temperature Gradient after 10.000 Years



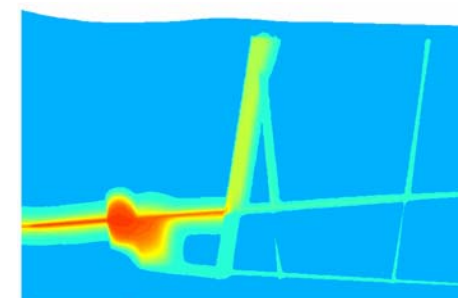
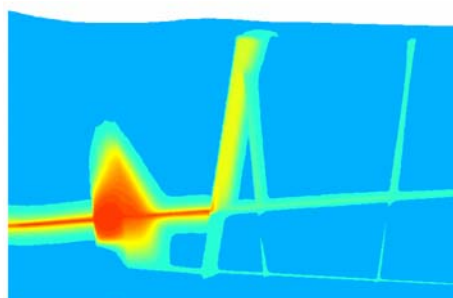
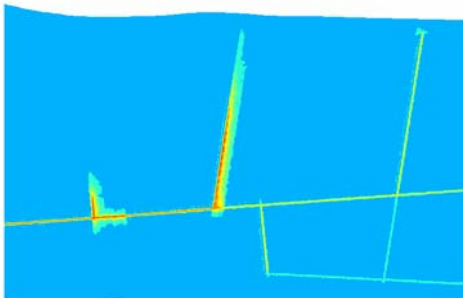
matrix k_f [m/s]: $4e^{-10}$
fracture k_f [m/s]: $6,9e^{-05}$

matrix k_f [m/s]: $4e^{-10}$
fracture k_f [m/s]: $1,2e^{-06}$

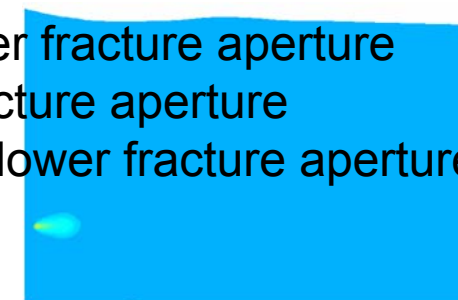
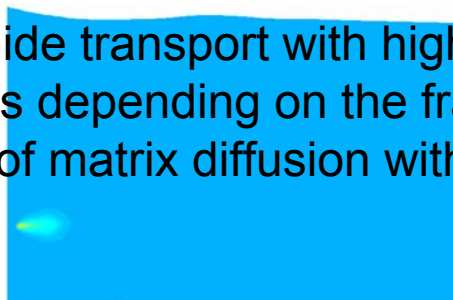
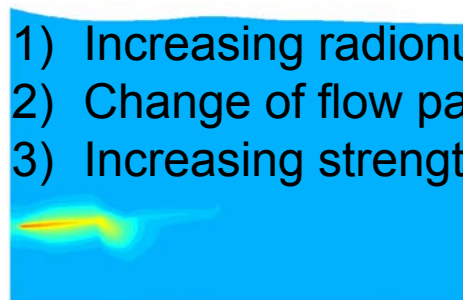
matrix k_f [m/s]: $4e^{-10}$
fracture k_f [m/s]: $5,8e^{-07}$



fracture aperture [m]: 1

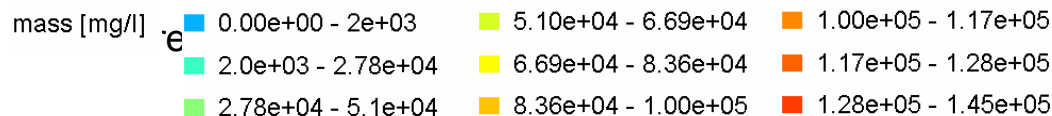


fracture aperture [m]: 0,5



fracture aperture [m]: 0,01

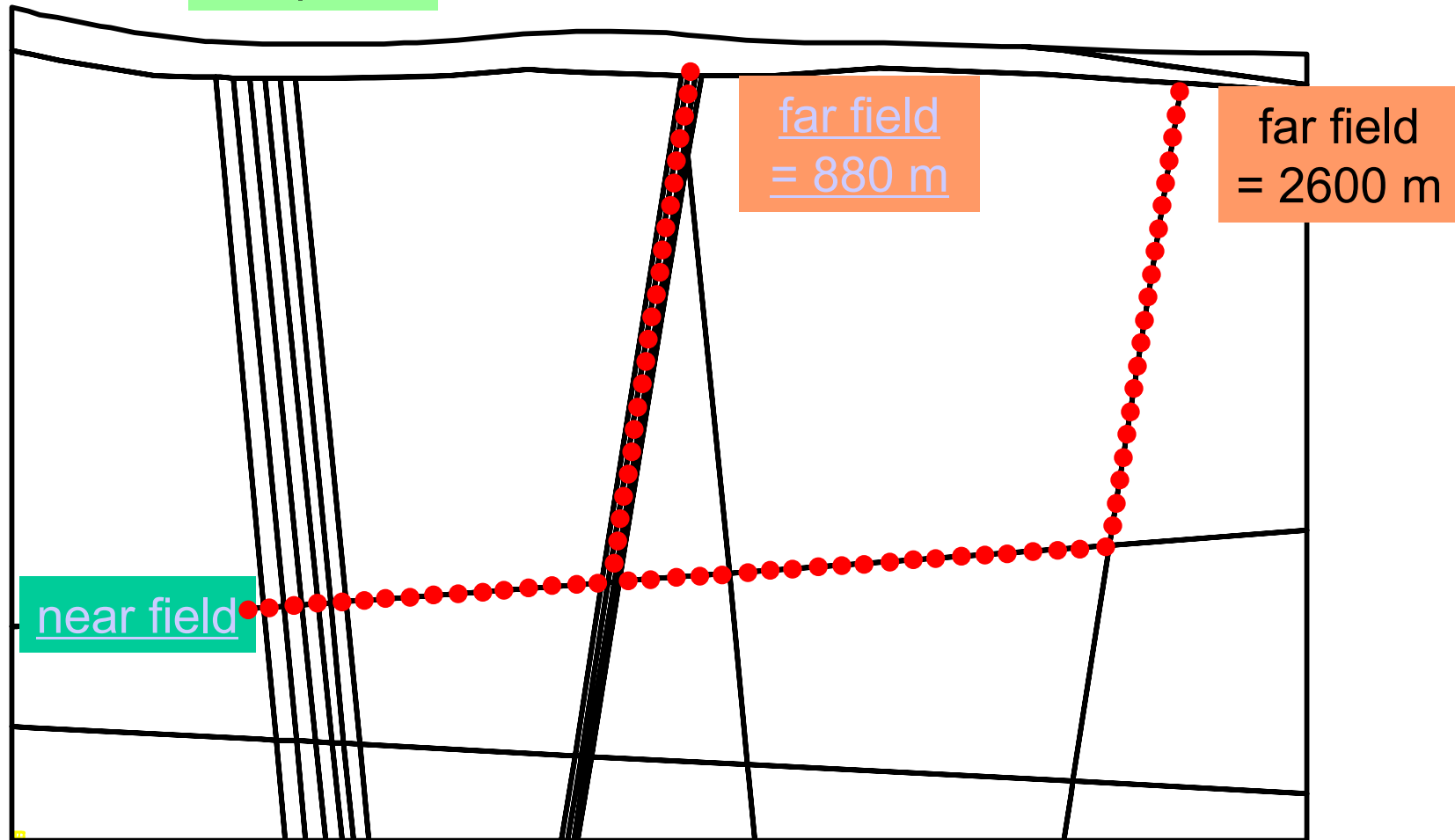
- 1) Increasing radionuclide transport with higher fracture aperture
- 2) Change of flow paths depending on the fracture aperture
- 3) Increasing strength of matrix diffusion with lower fracture aperture



Results of Emos Calculation and Realistic 2d Modelling

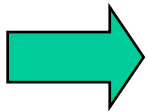
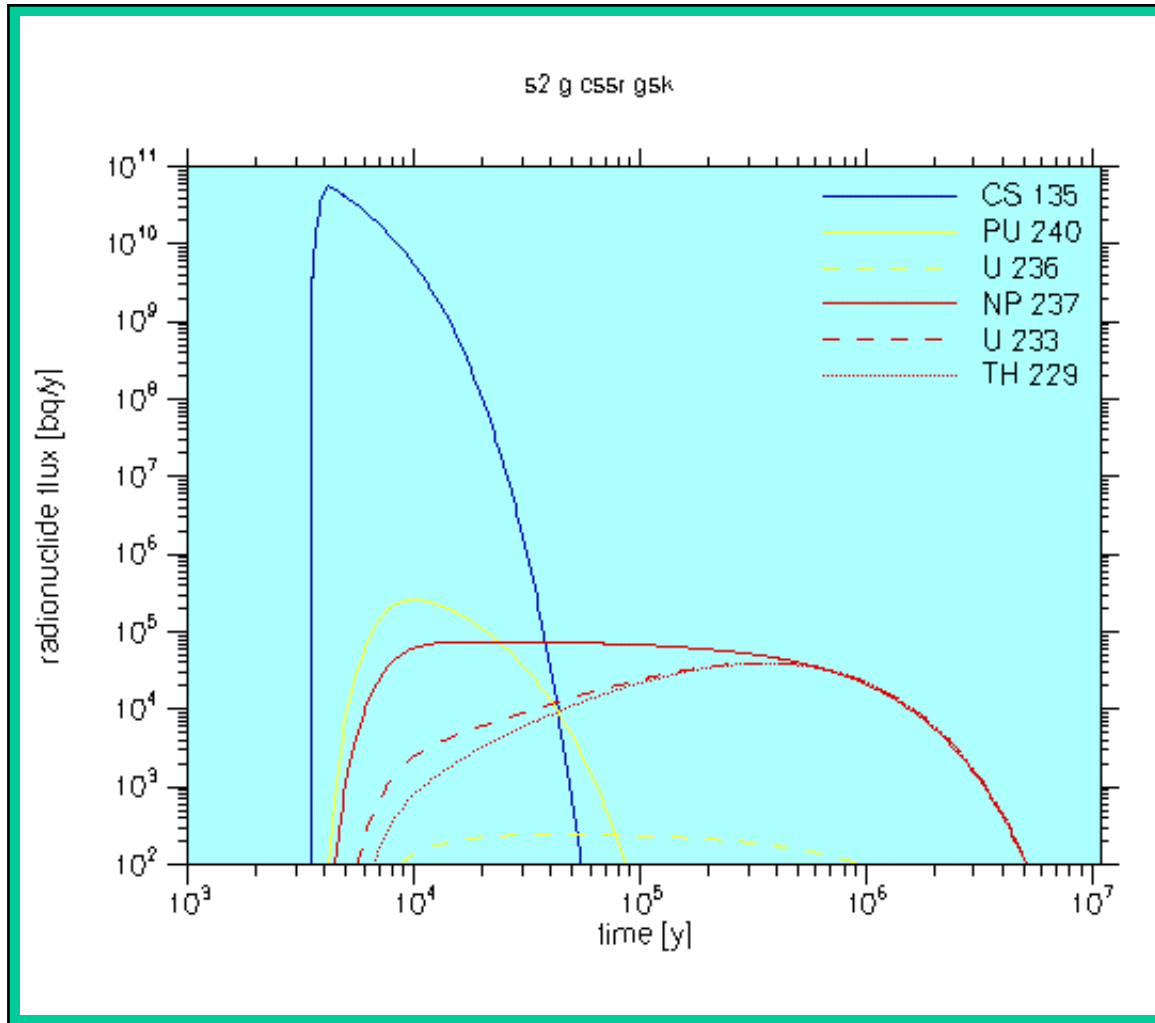


biosphere



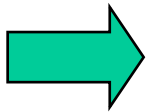
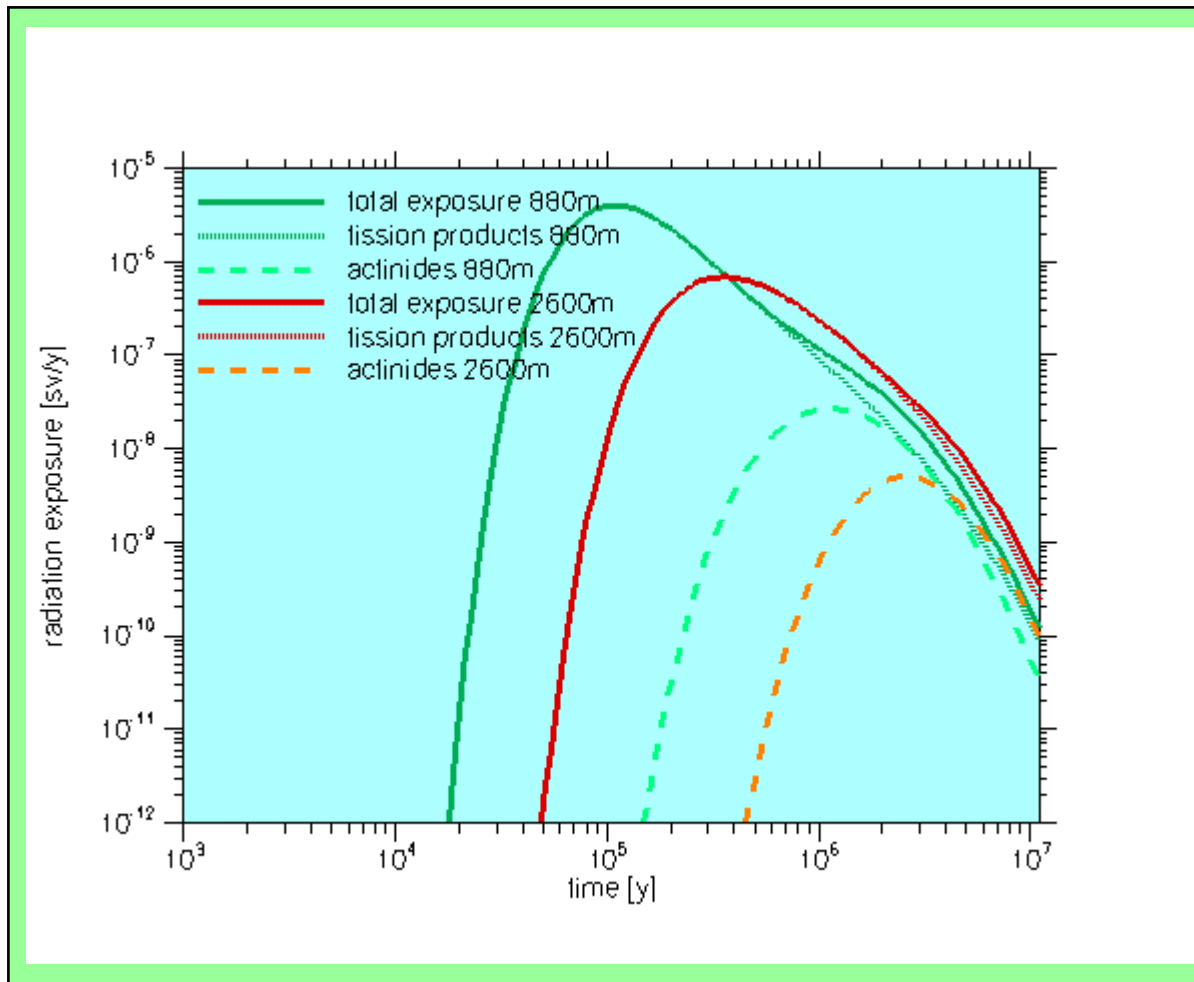
Transport Calculation for the Near Field

Case S2 CsSr



Transport Calculation for the Far Field and Biosphere

Case S2 CsSr



Models Used for Preselection of Potential Areas

Task - 2d and 3d simulation of groundwater regime and contaminant transport in fractured rock

- Geostructural model – *ArcView, FEFLOW*
- Density-driven groundwater flow, induced by heat or / and salt – *d^{3f}, FEFLOW*
- Mobilisation of radionuclides, time-dependent release rate – *EMOS*
- Transport and retention of radionuclides – *EMOS, r^{3t}*

Future Works

- **Improvement of data base**
 - geometrical 3 d model of fractures
 - intersection of fractures
 - mineralisation and filling of fractures
 - retardation parameters in rock mass (far field)
- **Further development of computer models**
 - incorporation of radionuclide decay chains in FEFLOW code
 - application of GRAPOS code to non fractured rock
- **Investigation of the effects the heat generating waste has on the near field of the repository and the ground water flow**



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**Thank you very much
for your hospitality**

ROCK MECHANICS FOR YUCCA MOUNTAIN

An overview of rock mechanics investigations in support of a
proposed high level nuclear waste repository at Yucca Mountain, NV,
USA

Jaak J.K. Daemen
University of Nevada, Reno

Lumin Ma
Vector Engineering, Inc
Grass Valley, CA

5/24/2007

Summary/overview

- Initial Site Selection
- Narrowing down sites considered
- Characterization studies for three sites
- Yucca Mountain
- Initial Yucca Mtn site investigations
- Yucca Mtn site characterization
- Rock Mechanics at Yucca Mountain

A Little Bit of History

- 1957: NAS (National Academy of Sciences) recommends deep geologic disposal, with emphasis on disposal in salt.
Early salt mechanics investigations (Lyons, Kansas)
- 1982: NWPA (Nuclear Waste Policy Act)
→ Nine sites identified as potential candidate sites: 7 in salt, 1 in basalt, 1 in volcanic ash flow (tuff)
- 1984: 3 sites selected for detailed studies (site characterization) (Tuff, basalt, bedded salt)
- 1987: Yucca Mountain designated as only site to be characterized

Initial investigations to select a potential nuclear waste repository site.

- Nationwide review of geological formations that might be acceptable for high level nuclear waste disposal.
- Preliminary selection of 17 (?) sites that might be acceptable.
- Narrowed down to three sites for detailed geological characterization.

Site selection criteria

- Waste isolation
- Geology
- Hydrology
- Geochemistry
- Rock mechanics

Initial Site Screening for the First Repository (starting in 1976) (DOE, 1984, p. 3-A-9)

Twofold approach:

systematic survey of areas underlain by salt
evaluate lands owned by the Department of
energy, and dedicated to nuclear activities
(Hanford, Washington; Nevada Test Site (Yucca
Mountain), Nevada)

GEIS (Generic Environmental Impact Statement) (1978)

Rock Properties, Repository Preconceptual Design Studies, Feasibility and Cost Studies, Thermal and Thermo-mechanical analysis for Salt, Granite, Shale, and Basalt. (Science Applications, Inc., 1978) (23 volumes)

U.S. Nuclear Regulatory Commission (NRC) Site Characterization Information Needs (1985)

(From NRC, 1985)

Rock types: granite, shale, basalt, tuff, bedded salt, dome salt.

Summarizes properties in the literature.

Identifies properties/characteristics that need to be identified/defined.

NRC (1985) Information Needs Geomechanics

Precharacterization

Temperature

Stress field

Thermal conductivity and specific heat

Deformation moduli

Geometry of discontinuities and
inhomogeneities

NRC (1985) Information Needs Geomechanics

Site Characterization

Detailed survey of discontinuities and inhomogeneities

Mechanical behavior of host rock at elevated temperatures

Radiation effects

Structural stability of the repository

Rock types identified for site selection (1986) (DOE, August 1986, p. 19)

Mined Geological Disposal System

Program Components:

Basalt

Tuff

Salt

Crystalline

Civilian Radioactive Waste Management Program (1986)

Mined Geological Disposal System (MGDS) will
investigate: Basalt, Tuff, Salt, and Crystalline
rock. (DOE, 1986, August)

Nine sites selected for early site selection

Basalt, tuff, bedded salt (4), salt domes(3)



From DOE, 1984, May, b, p. 2

Selection of three sites for final site characterization

DOE, 1986: preferred sites for site characterization, in order:

1. Yucca Mountain, NV
2. Deaf Smith County, Texas (bedded salt)
3. Hanford, Washington (basalt flows)

(DOE, 1986, May, b)

Five sites investigated to select these three included two (rejected) salt sites: a dome (Richton), and a bedded site (Davis Canyon).

Sites selected for detailed characterization

- Yucca Mountain: ashflow tuffs/volcanic
 - Unsaturated: above the water table
- BWIP: basalt flows (Hanford, Washington)
- Deaf Smith County (Texas): bedded salt

HLW Salt Mechanics Research Examples

- Dome-Salt Thermomechanical Experiments at Avery Island, Louisiana (Van Sambek, 1981)
- Influence of Specimen Size on the Creep of Rock Salt (Senseny, 1982)

Yucca Mountain designated by U.S. Congress

Decision by congress (December 1987)



Strong opposition by the State of Nevada

Location



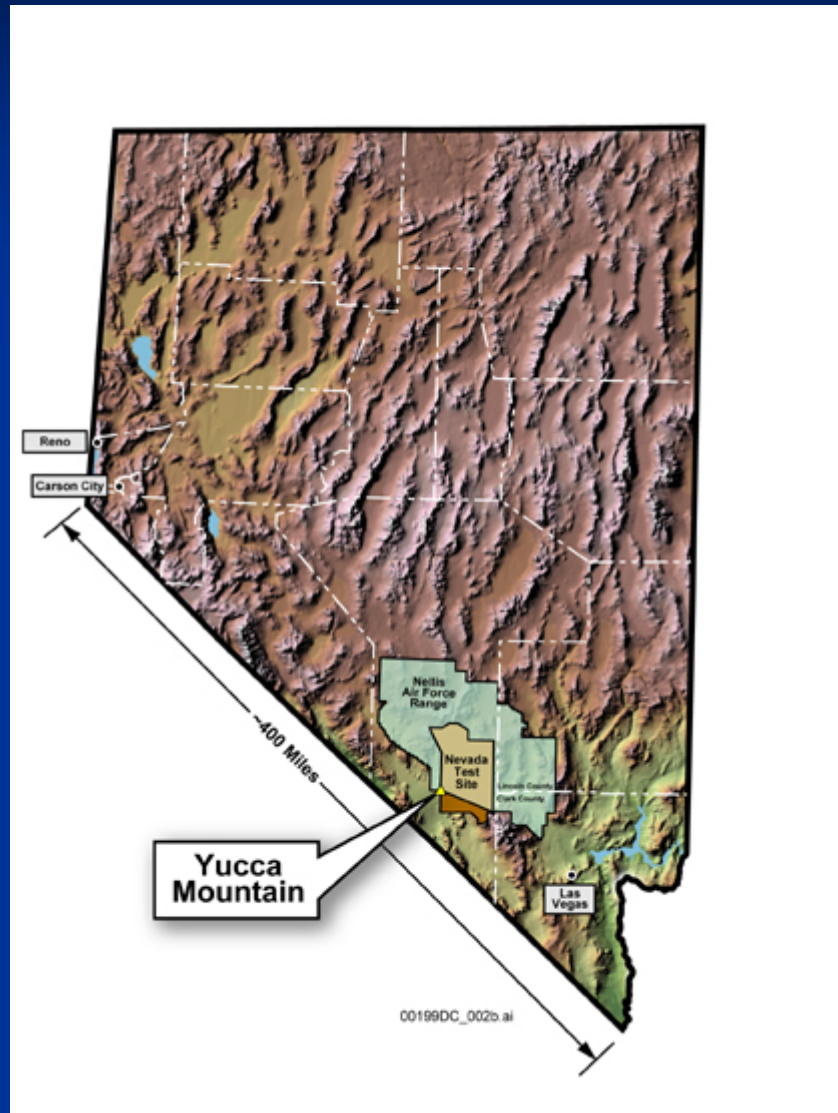
Yucca Mountain location



Yucca Mountain: western edge of (Nevada) Test Site



Location: 100 km SW of Las Vegas



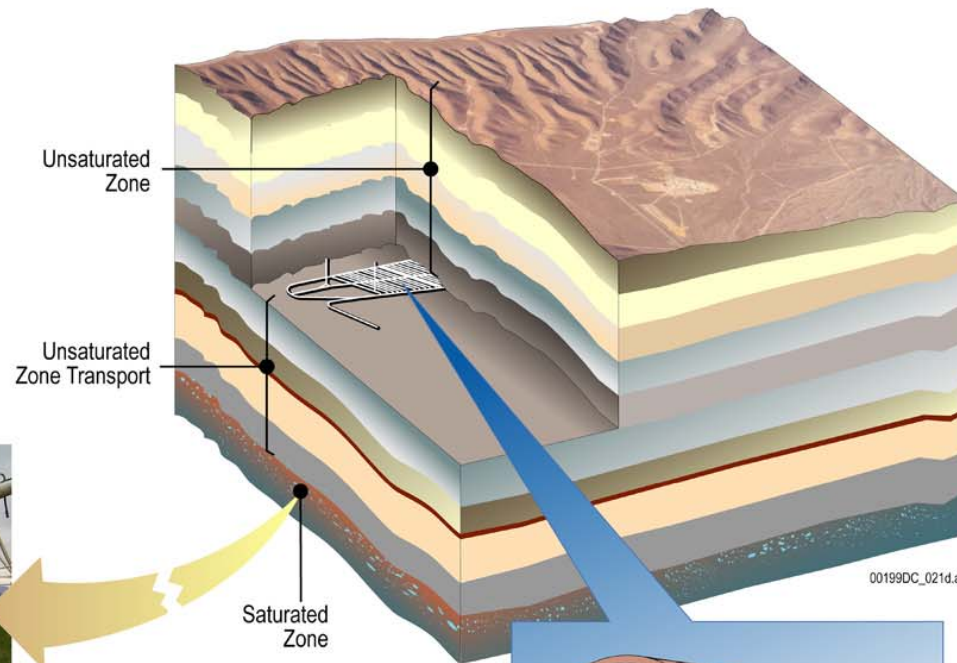


Aerial view of north end of the Yucca Mountain crest



Regulatory/legal context

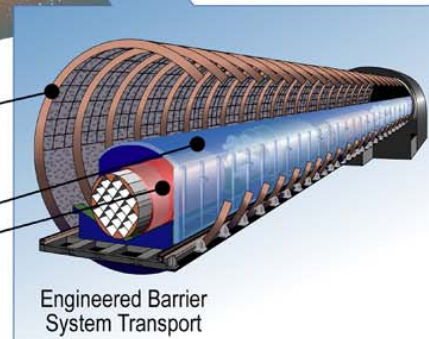
- Operator, designer, builder, owner: DOE (U.S. Department of Energy)
OCRWM (Office of Civilian Radioactive Waste Management)
- Environmental standards set by: EPA (U.S. Environmental Protection Agency)
- Licensed by: NRC (U.S. Nuclear Regulatory Commission)
- Reviewed by NWTRB (Nuclear Waste Technical Review Board)
- Interactions with numerous stakeholders, e.g. state(s), Indian tribes, utilities, environmental groups, etc..



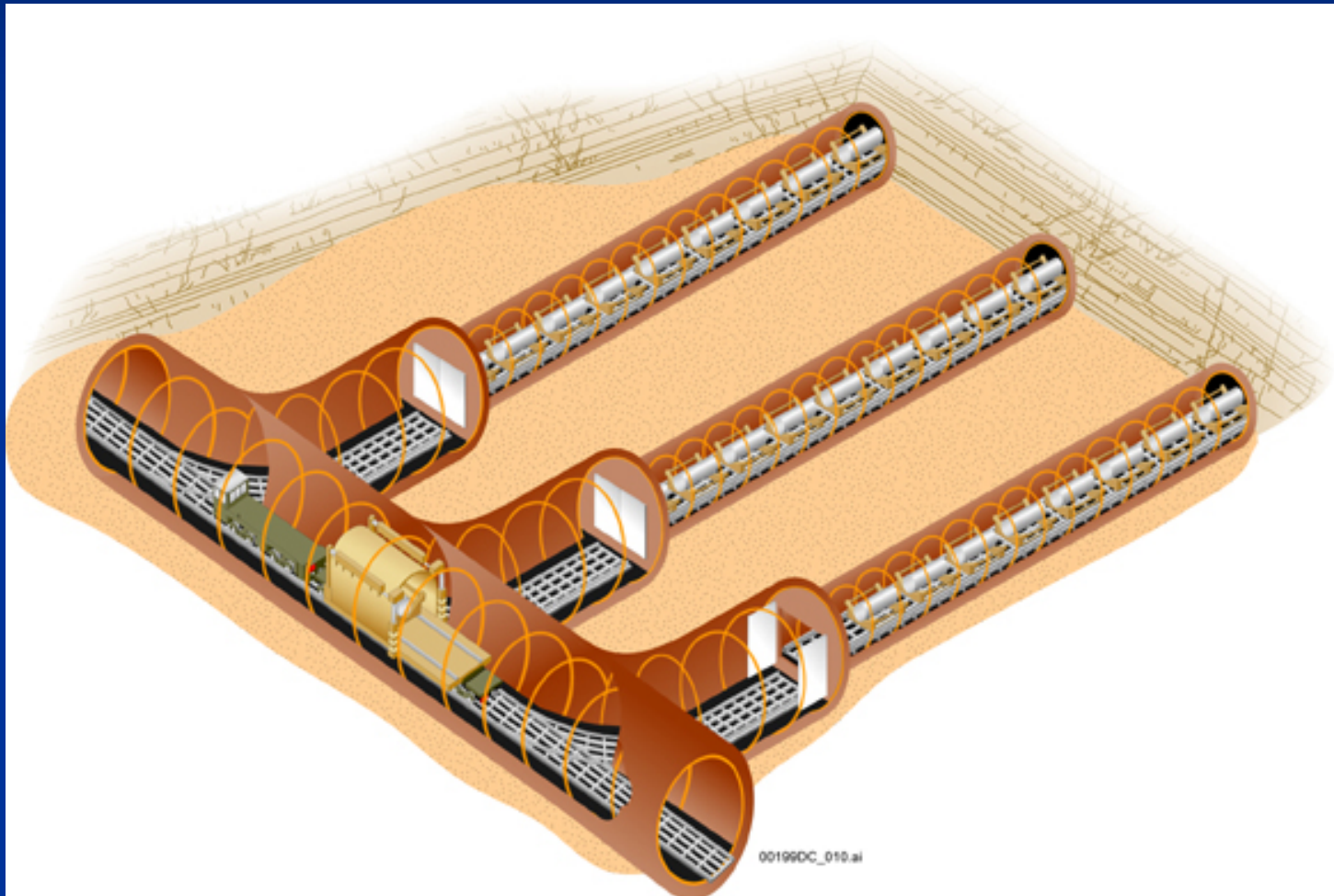
Biosphere

Engineered Barrier System Environments

Drip Shield & Waste Package Degradation



The repository would be a series of emplacement drifts where waste packages would be emplaced and monitored.



Waste emplacement configuration

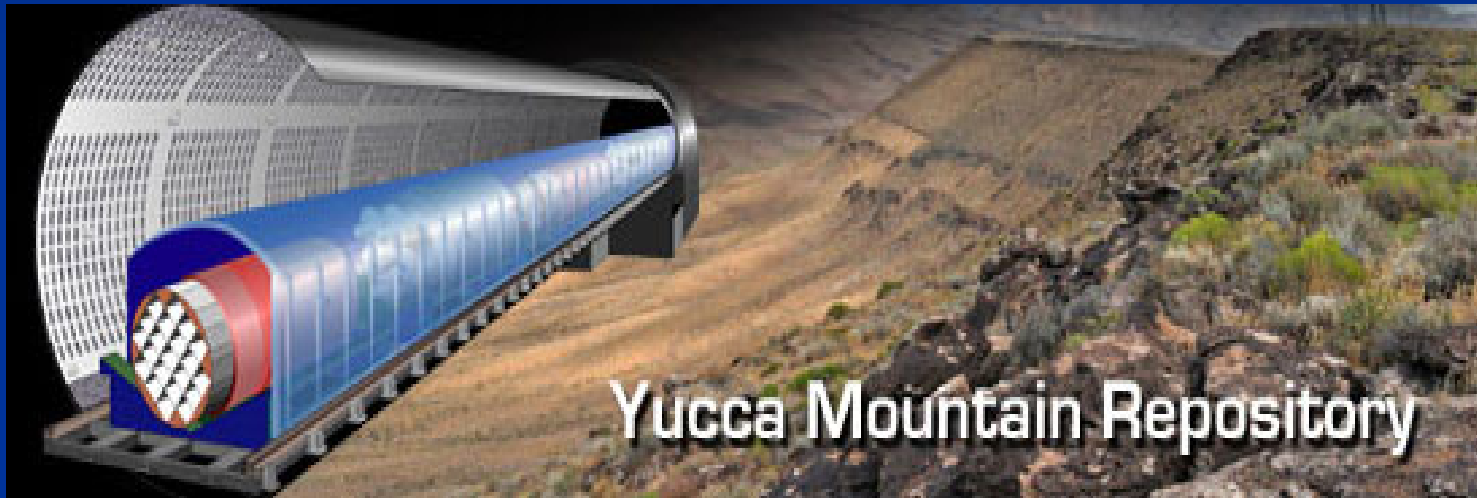
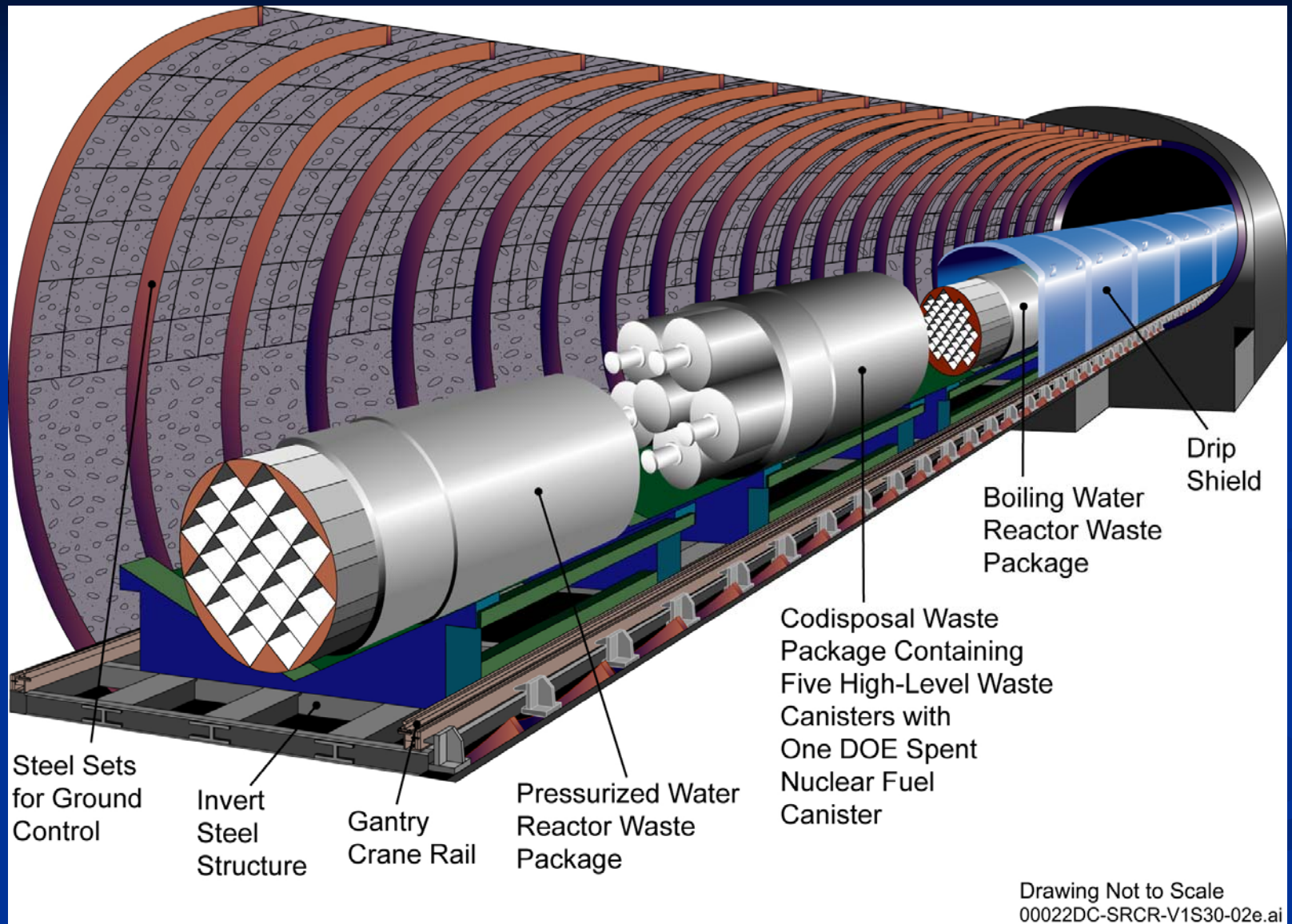
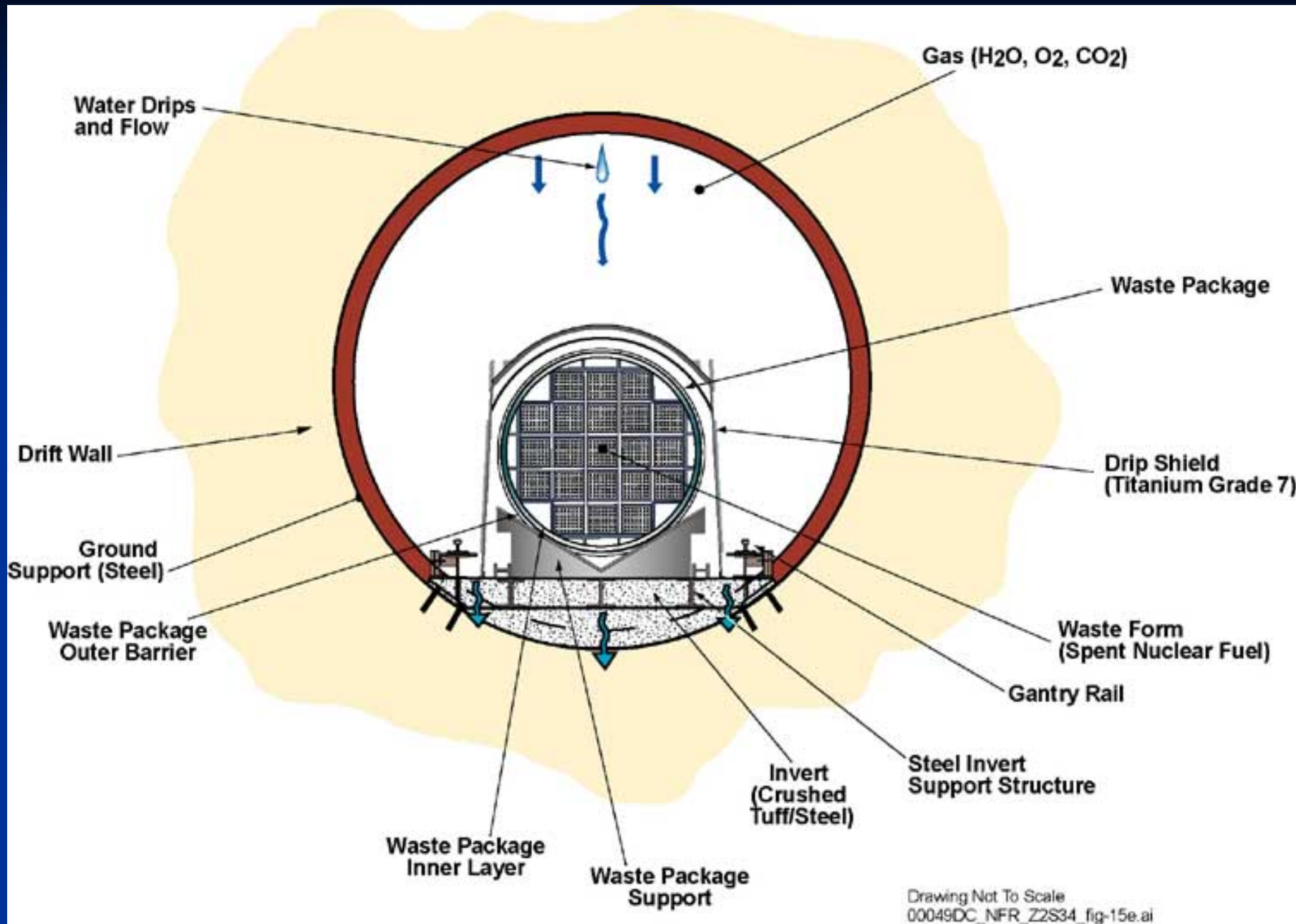


Photo from OCRWM web page





Drawing Not To Scale
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Example of “early” (1980’s) rock mechanics investigations

Summary of Geomechanical Measurements Taken in and Around the G-Tunnel Underground Facility, NTS (Zimmerman and Finley, 1987)

G-Tunnel Tuffs: description:

- Description of Tuff
- Bulk Physical Properties
- Joint Characterization
- Rock Mass Classification
- Stress measurements: overcoring, hydrofracturing
- Strength: uniaxial compression, shear, tensile
- Deformational properties: Young’s modulus and Poisson’s ratio

Laboratory

Field: borehole jacks; slot tests; block tests (with flatjacks)

cross hole geophysics

Further examples of early (1980's) rock mechanics studies

An analysis of the G-Tunnel Heated Block Experiment
Using a Compliant-Joint Rock-Mass Model (Costin and Chen, 1988)

Continuum 2-D finite element model

Near Field Mechanical Calculations Using a Continuum Jointed
Rock Model in the JAC Code (Thomas, 1987)

A Three-Dimensional Model of Reference Thermal/Mechanical
and Hydrological Stratigraphy at Yucca Mountain, Southern
Nevada (Ortiz et al., 1985)

“The reference stratigraphy defines units with distinct
thermal, physical, mechanical, and hydrological properties.”

Example of early “rock mechanics” (Mining engineering?) study

- Repository Drilled Hole Methods Study (The Robbins Company, 1984)

Analysis of technical feasibility and of cost of drilling vertical and horizontal waste canister emplacement holes.
- Feasibility Studies and Conceptual Design for Placing Steel Liner in Long, Horizontal Boreholes for a Prospective Nuclear Waste Repository in Tuff (The Robbins Company, 1985)

Regulatory Review – an example

U.S. Nuclear Regulatory Commission Rock Mechanics Concerns (After NRC, 1989)

- Will site investigations adequately cover the full range of rock characteristics?
- Is there sufficient integration of all site characterization activities (e.g. mapping, drilling, geophysics)?
- Are expected operational conditions addressed in sufficient detail?

Initial site characterization

- Boreholes
- Geological mapping
- Hydrological/geochemical testing
- Rock mechanics: core sample testing
 - Uniaxial compression
 - Density/porosity/water content

Prototype dry-hole drilling operations at Mercury Gold Mine near Salt Lake City, Utah, in May 1989.



Rock mechanics issues

Drift stability

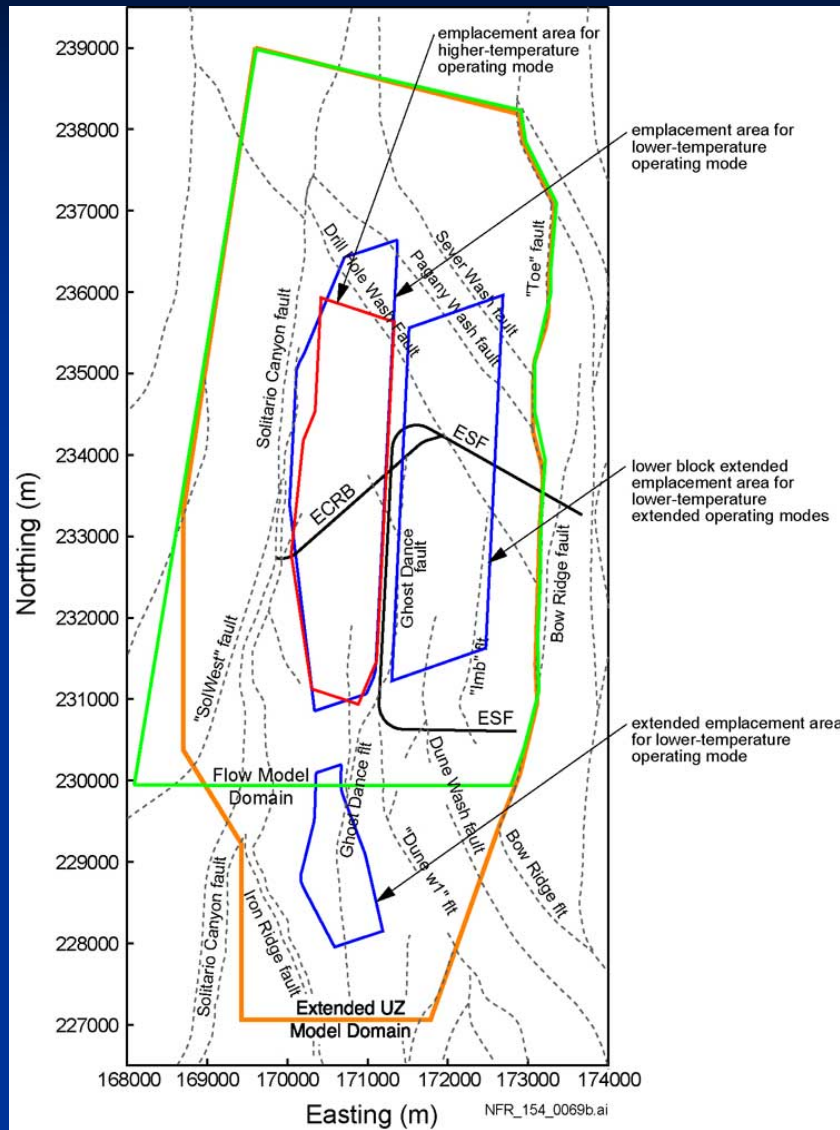
- Retrievability: access needs to be maintained
 - Long term rock strength?
- Waste (drift shield) package loading

Dynamic (earthquake) effects on drift stability

e.g. fault shear?

Technical rock mechanics questions

- Rock strength
 - Effects of heat, moisture content, long term sustained loading
 - Extrapolation from laboratory scale to field scale
- Discontinuity geometry, strength
 - Wedge formation?



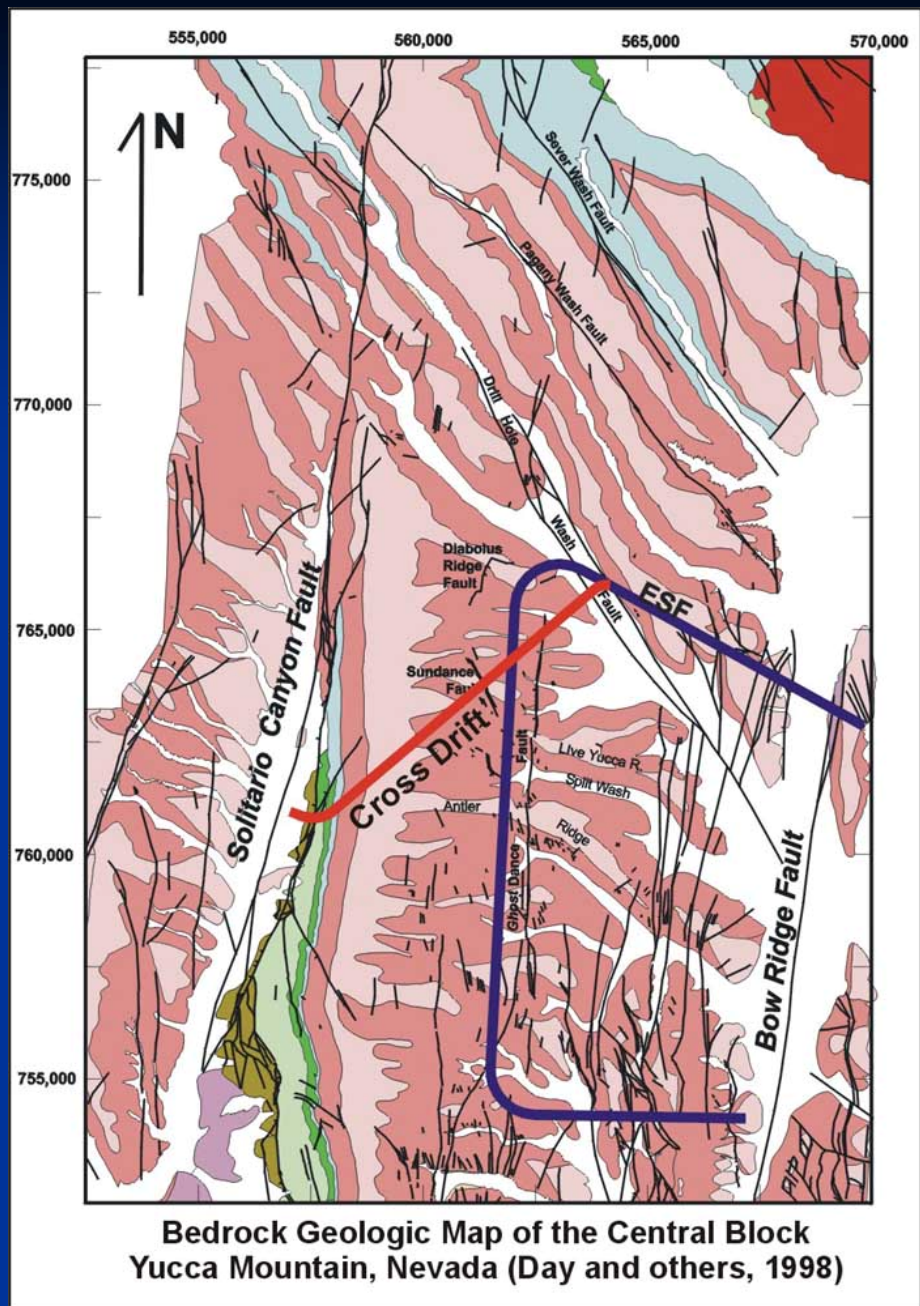


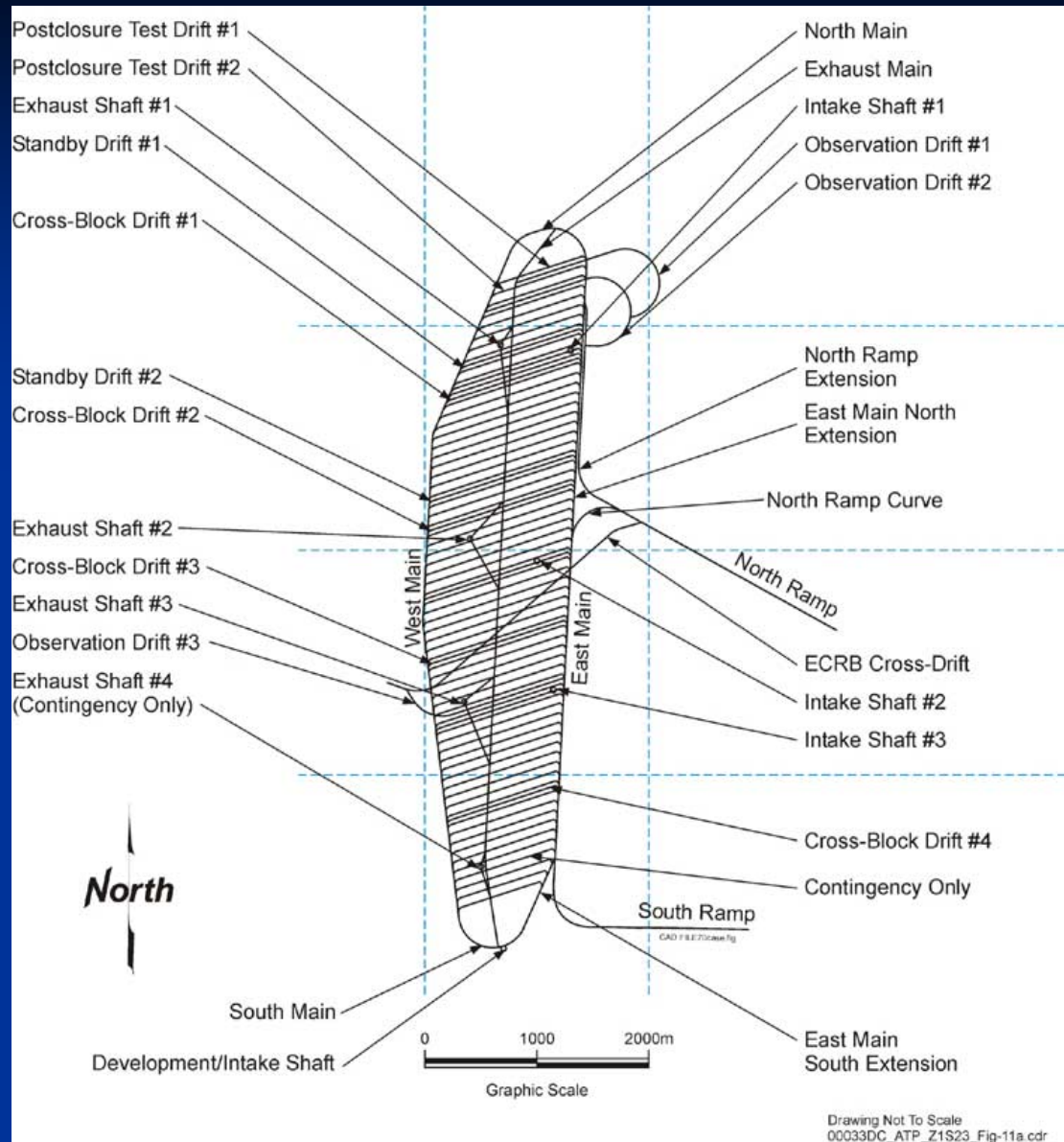
Figure 2. Simplified geologic map of the Yucca Mountain region with plan view of the ESF and the Cross Drift.

From:

**GEOLOGY OF THE ECRB CROSS
DRIFT - EXPLORATORY
STUDIES FACILITY, YUCCA
MOUNTAIN PROJECT, YUCCA
MOUNTAIN, NEVADA**

G.S. Mongano, W.L. Singleton, T.C.

**Moyer, S.C. Beason, G.L.W.
Eatman, A.L. Albin, and R.C.
Lung**



Tunnel boring machine cutter head at the South Portal in April 1997.



Photo from OCRWM web page

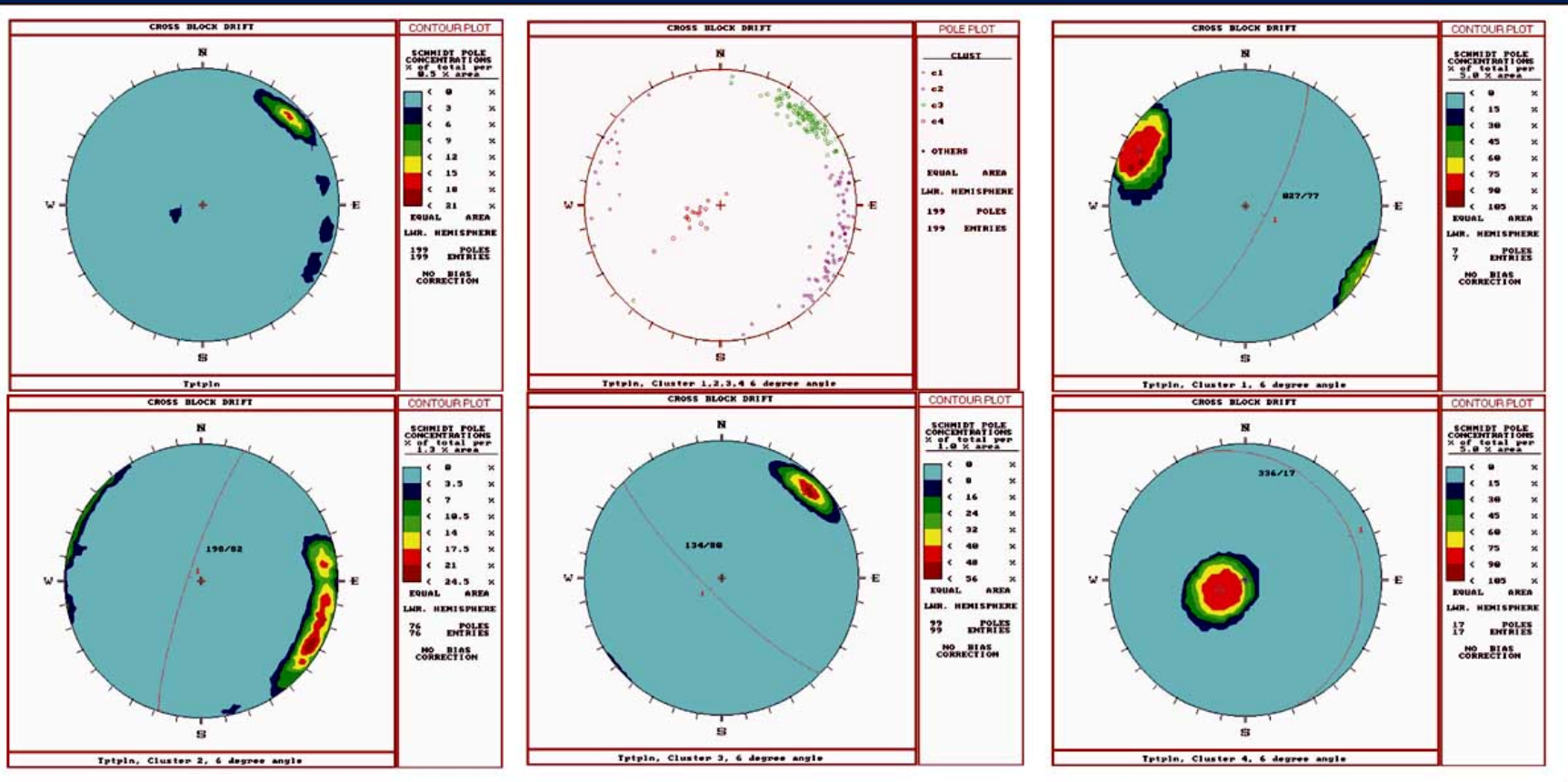


Figure 12. Tptpln contour plot of all fractures compared with pole plot (each cluster with a unique symbol), and contour plots for each cluster.

From:

GEOLOGY OF THE ECRB CROSS DRIFT - EXPLORATORY STUDIES FACILITY, YUCCA MOUNTAIN PROJECT, YUCCA MOUNTAIN, NEVADA
 G.S. Mongano, W.L. Singleton, T.C. Moyer, S.C. Beason, G.L.W. Eatman, A.L. Albin, and R.C. Lung

Cross Drift Rock Quality (Q) Rating

(Kirsten Method)

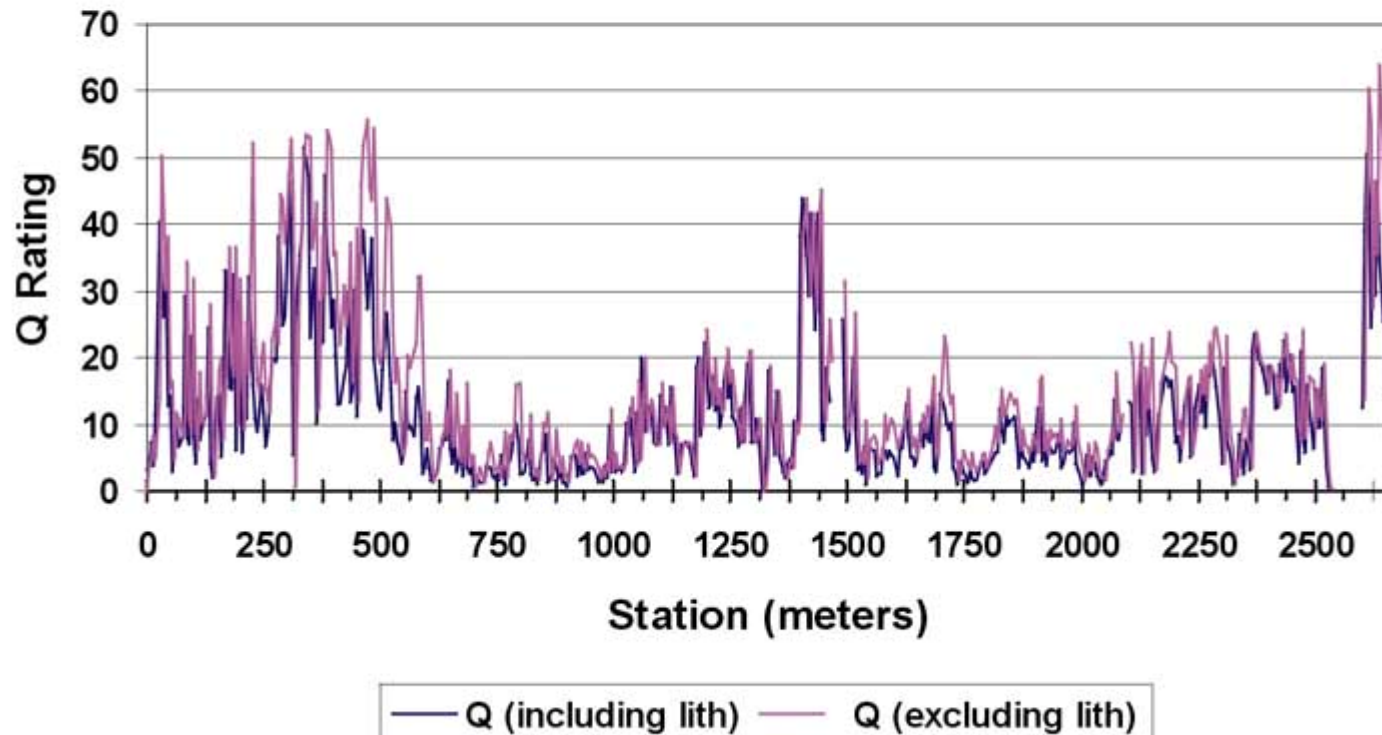


Figure 27. Q ratings, including and excluding, lithophyses for the Cross Drift against stationing.

From:

GEOLOGY OF THE ECRB CROSS DRIFT - EXPLORATORY STUDIES FACILITY, YUCCA MOUNTAIN PROJECT, YUCCA MOUNTAIN, NEVADA

G.S. Mongano, W.L. Singleton, T.C. Moyer, S.C. Beason, G.L.W. Eatman, A.L. Albin, and R.C. Lung

Rock mechanics testing

- Laboratory
- Small scale (in borehole) field tests
- Large scale field tests
 - Block tests
 - Plate bearing tests
 - Heater tests
 - Large scale heated room tests

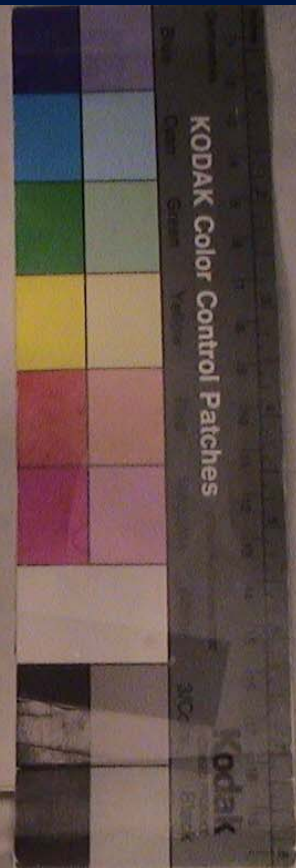
Specimen ID:

01014759-U



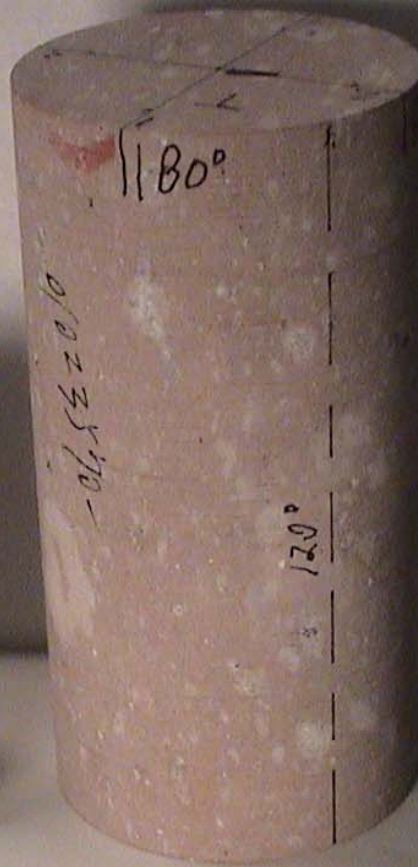
Specimen ID:

01014979-4



Specimen ID:

01023570-U



Tuff samples

Left and right: nonlithophysal, welded

Center: lithophysal



Laboratory heated block test

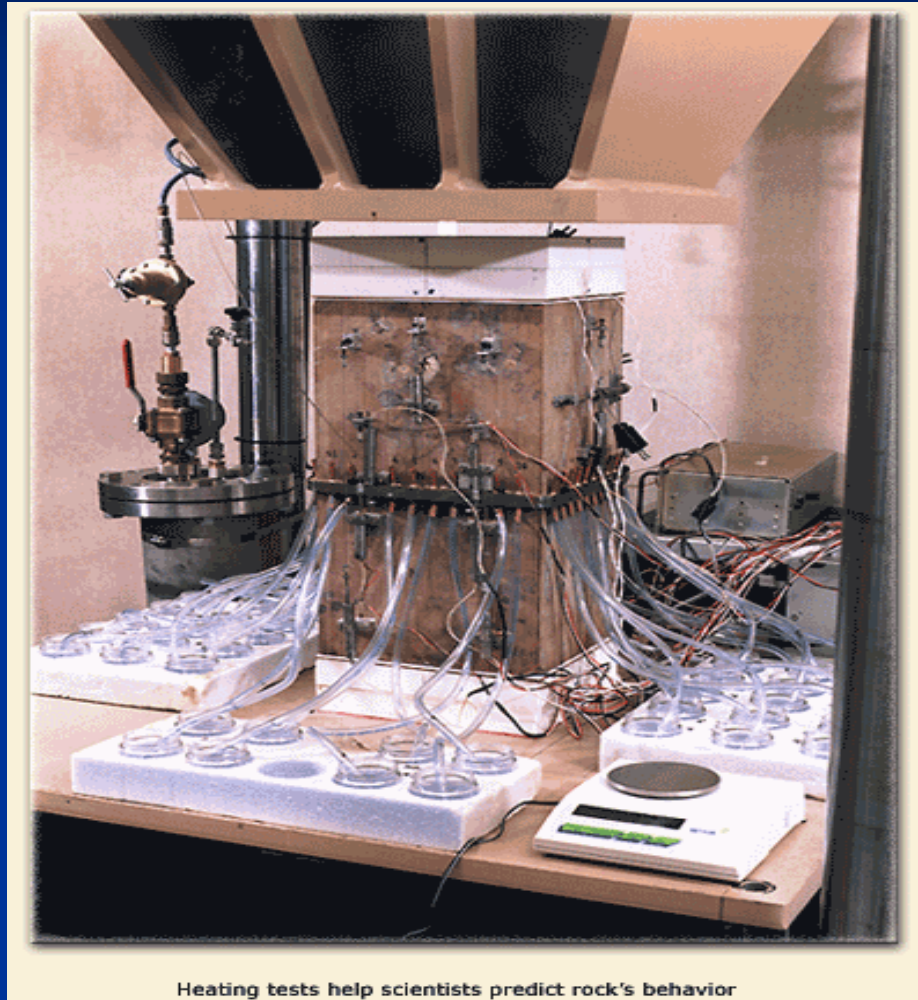


Photo from OCRWM web page

Sawing operation at the large block experiment on Fran Ridge in January 1994



Photo from OCRWM web page; technical description of test: e.g. Lin et al, 1994

Installation of heat exchanger for large block test at Fran Ridge in January 1997.



Photo from OCRWM web page; for test description, e.g. see Lin et al, 1994.

Single heater assembly installation in the single heater test, July 1996.



Photo from OCRWM web page

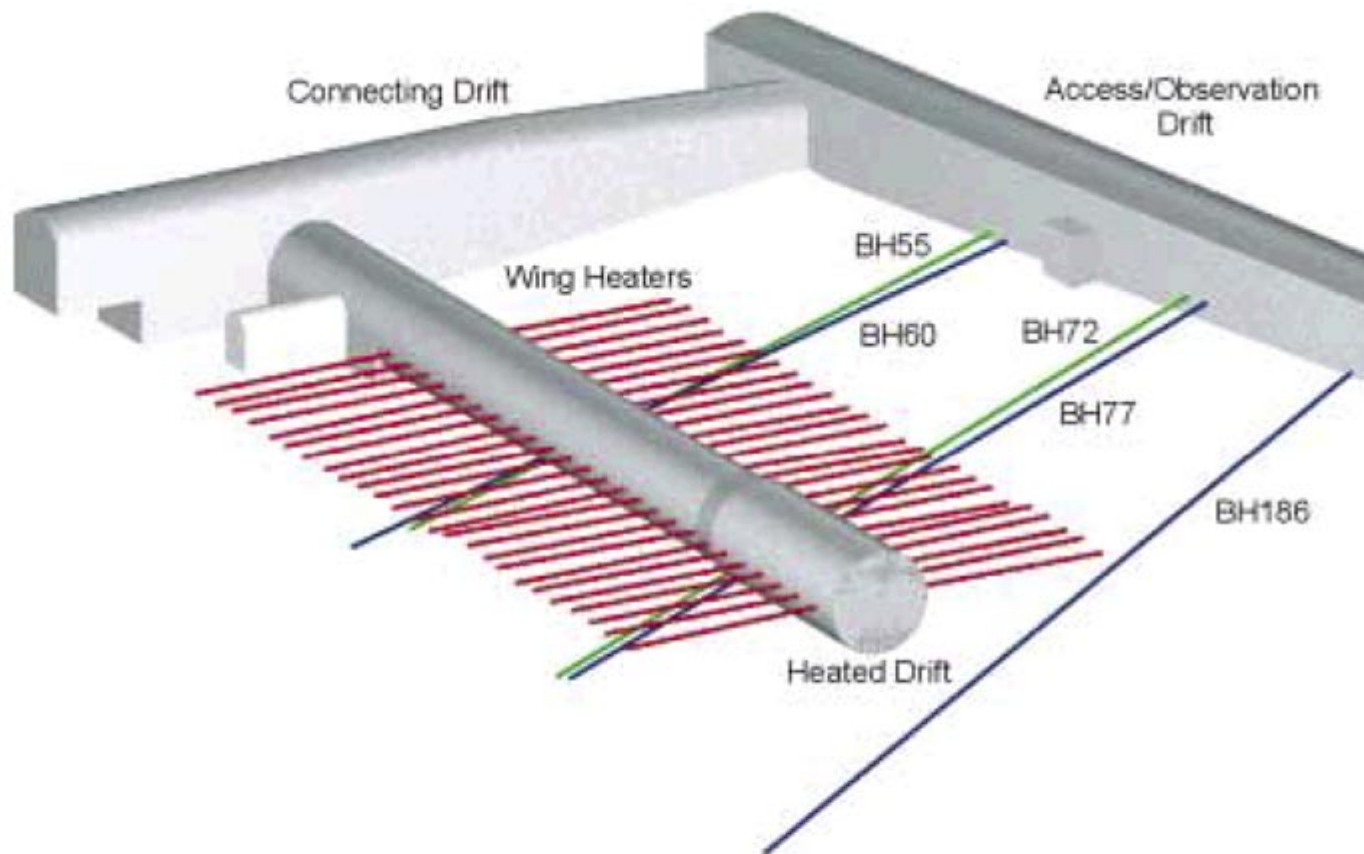


Figure 1. 3-Dimensional view of the Drift Scale Test showing the hydrology boreholes (blue) that contain Viton™ packers, wing heater boreholes (red), and SEAMIST™ holes (green).

Interior view of the drift scale test. This experiment is designed to determine how heat would affect the rock in a potential repository



Ground support / rock reinforcement Longevity/durability/corrosion

Stainless steel rock bolts, steel sets, straps?

(e.g. Shaffer et al, 1994)

Research, e.g. Prof Dhanesh Chandra (University
of Nevada, Reno) (Numerous publications in corrosion research journals,
conferences, etc...)

Seismic Drift Stability

Yucca Mountain: earthquake prone

Seismically active

→ extensive seismic stability investigations

(e.g. Marine et al, 1982; Damjanac et al, 2007)

Yucca Mountain time frame

- License application: 2008
- License granted (or denied?): 2012
- Start receiving waste: 2017 (??)

Site selection Summary

1. Project “Salt Vault”
2. Broader rock type investigations:
granite, basalt, shale, tuff
bedded and domal salt
3. Nine sites
4. Five sites
5. One site: Yucca Mountain

Yucca Mountain Rock Mechanics Summary

- Site characterization: boreholes, geophysics, mapping
- Rock testing: laboratory tests on core
- Stress measurements
- Rock testing: laboratory: large core, blocks
- Field testing: blocks, boreholes, plate
- Drift monitoring
- Drift scale tests

Rock Mechanics for Yucca Mtn Reviews - Summary

- U.S. Nuclear Regulatory Commission (NRC)
CNWRA (Center for Nuclear Waste
Regulatory Analysis)
- NWTRB (Nuclear Waste Technical Review
Board)
- State of Nevada
- EPRI (Electric Power Research Institute)

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*Many of these reports have been summarized in publications that are readily and widely available, e.g. in US rock mechanics symposia, journals, etc...

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Location



